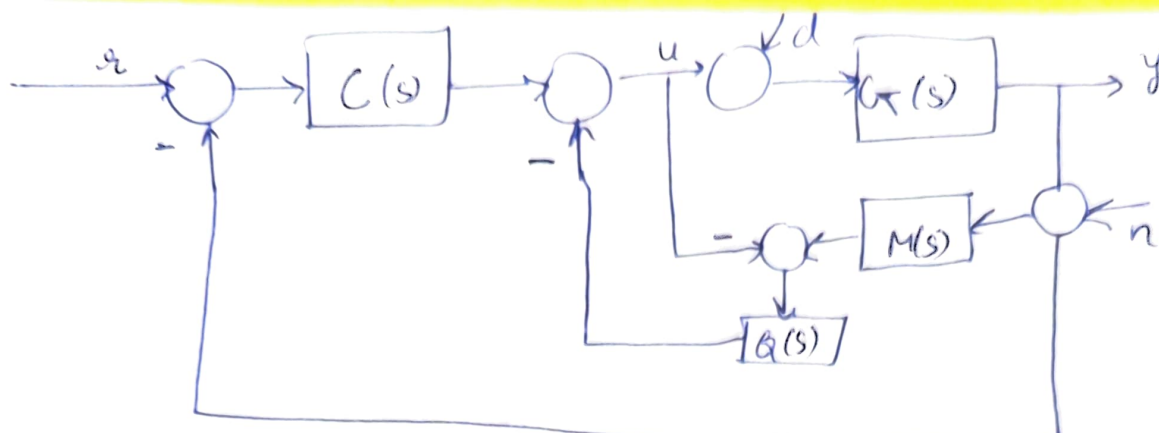


Q1



$$y = G u + G d \Rightarrow u = \frac{y}{G} - d \quad \text{--- (1)}$$

$$C(r - (y+n)) - Q(M(y+n) - u) = u$$

$$C(r - y - n) - Q(My + Mn + d - \frac{y}{G}) = \frac{y}{G} - d$$

$$Cr - Cy - Cn - QMy - QMn - Qd + \frac{Qy}{G} = \frac{y}{G} - d$$

a) To find Transfer function, $T = \frac{y}{R}$

assume $d=0, n=0$

$$Cr - Cy - QMy + \frac{Qy}{G} = \frac{y}{G}$$

$$Cr = y \left(\frac{1}{G} + C + QM - \frac{Q}{G} \right)$$

$$\boxed{\frac{y}{r} = \frac{CG}{1 + GC + QMG - Q}} = T \quad \text{--- (2)}$$

for sensitivity function $S = \frac{E}{R}$

$$\frac{y}{r} - T = \frac{CG}{1 + GC + QMG - Q} - T = \frac{Q - QMG - 1}{1 + GC + QMG - Q} = -\frac{E}{R}$$

$$\Rightarrow \boxed{\frac{E}{R} = \frac{1 + QMG - Q}{1 + GC + QMG - Q}} = S$$

collaborated with
Ruchita Sinha
Aditya Rath

b) Input sensitivity function $\frac{y}{d}$,

assume, $n=0$, $r=0$

$$-Cy - QMy - Qd + \frac{Qy}{u} = \frac{y}{u} - d$$

$$d(I+Q) \quad d(I-Q) = y\left(\frac{1}{u} + C + QM - \frac{Q}{u}\right)$$

~~$$\frac{y}{d} = \frac{u - Qu}{I + Cu + QMu - Q}$$~~

$$\frac{y}{d} = \frac{u - Qu}{I + Cu + QMu - Q}$$

when $Q = I$, $M = u^{-1}$

$$\frac{y}{d} = 0$$

Q acts as a filter to account for the imperfections in the block M (to remove the disturbance).

Q2

$$\ddot{\theta} + \frac{g}{l} \sin \theta = \frac{\tau}{ml^2}$$

Assume states $\{x_1, x_2\}$ to be $\{\theta, \dot{\theta}\}$

$$\Rightarrow x_1 = \theta$$

$$x_2 = \dot{\theta} = \dot{x}_1$$

$$\Rightarrow \dot{x}_2 + \frac{g}{l} \sin x_1 = \frac{\tau}{ml^2}$$

$$\Rightarrow \dot{x}_2 = \frac{\tau}{ml^2} - \frac{g}{l} \sin x_1$$

$$\dot{X} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ \frac{\tau}{ml^2} - \frac{g}{l} \sin x_1 \end{bmatrix}$$

$$A = \frac{\partial f}{\partial x} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{l} \cos x_1 & 0 \end{bmatrix}_{n \times n = 2 \times 2}; B = \frac{\partial f}{\partial \tau} = \begin{bmatrix} 0 \\ \frac{1}{ml^2} \end{bmatrix}$$

Assume $C = [1 \ 0]$ [Output as encoder angle]

$$\text{At } x_1 = \frac{\pi}{2}, A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}$$

To check system stability, check eigen values of A

$$\Rightarrow \lambda_1 = \lambda_2 = 0$$

To check whether A is defective, $m = n - \text{rank}(\lambda I - A)$
geometric multiplicity

$$= 2 - \text{rank} \left(\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \right) = 2 - \text{rank} \left(\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \right)$$

$$m = 2 - 1 = 1$$

$$= 2 - \text{rank} \begin{bmatrix} 0 & -1 \\ 0 & 0 \end{bmatrix}$$

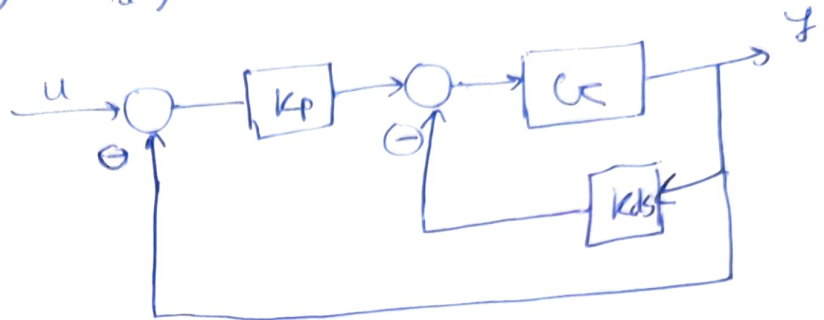
$\therefore A$ is defective \Rightarrow The system is unstable

Linearized form,

$$\begin{bmatrix} \delta \dot{x} \\ \delta y \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \delta x + \begin{bmatrix} 0 \\ \frac{1}{ml^2} \end{bmatrix} \delta \tau$$
$$\delta y = [1 \ 0] \delta x$$

$$\begin{aligned}
 G_c &= C(sI - A)^{-1}B + D \\
 &= [1 \ 0] \left(\begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \right)^{-1} \begin{bmatrix} 0 \\ \frac{1}{md^2} \end{bmatrix} + 0 \\
 &= [1 \ 0] \begin{bmatrix} 1/s & 1/s^2 \\ 0 & 1/s \end{bmatrix} \begin{bmatrix} 0 \\ \frac{1}{md^2} \end{bmatrix}
 \end{aligned}$$

$$G_c = \frac{1}{s^2 md^2}$$



New transfer function, G_c''

$$G_c' = \frac{G_c}{1 + G_c k_d s}$$

$$\begin{aligned}
 G_c'' &= \frac{k_p G_c / (1 + G_c k_d s)}{1 + \frac{k_p G_c}{1 + G_c k_d s}} = \frac{k_p G_c}{1 + k_p G_c + G_c k_d s} = \frac{\frac{k_p}{s^2 md^2}}{1 + \frac{k_p}{s^2 md^2} + \frac{k_d s}{s^2 md^2}} \\
 \Rightarrow G_c'' &= \frac{k_p}{s^2 md^2 + k_p + k_d s} \Rightarrow G_c'' = \frac{k_p}{16s^2 + k_d s + k_p}
 \end{aligned}$$

Characteristic eqn. $\Rightarrow 16s^2 + k_d s + k_p = 0$

Overshoot, $M_p = \exp\left(\frac{-\pi \zeta}{\sqrt{1 - \zeta^2}}\right) = 0.25 \Rightarrow \zeta = 0.403$

Settling time, $t_s = \frac{-\ln 0.02}{\zeta \omega_n} = 2 \Rightarrow \omega_n = 4.85$

$$\frac{k_d}{16} = 2 \zeta \omega_n = 2 \times 0.403 \times 4.85 \Rightarrow k_d = 62.54$$

$$\frac{k_p}{16} = \omega_n^2 \Rightarrow k_p = (4.85)^2 \times 16 = 376.36$$

(c) The system is stable for all initial conditions from $[-\pi, \pi]$. The system is able to achieve steady state for all possible configurations.

Q3

$$\dot{x} = \begin{bmatrix} -0.75 & -0.25 \\ -0.5 & -0.5 \end{bmatrix} x + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u$$
$$y = \begin{bmatrix} 4 & 2 \end{bmatrix} x$$

To check observability, $Q = \begin{bmatrix} C \\ CA \end{bmatrix} = \begin{bmatrix} [4 \ 2] \\ [4 \ 2] \begin{bmatrix} -0.75 & -0.25 \\ -0.5 & -0.5 \end{bmatrix} \end{bmatrix}$

$$= \begin{bmatrix} 4 & 2 \\ -4 & -2 \end{bmatrix} \Rightarrow \text{Rank}(Q) = 1 < 2$$

\therefore The system is not observable

To check controllability, $P = \begin{bmatrix} B & AB \end{bmatrix}$

$$= \begin{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} & \begin{bmatrix} -0.75 & -0.25 \\ -0.5 & -0.5 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \end{bmatrix}$$
$$= \begin{bmatrix} 1 & -1 \\ 1 & -1 \end{bmatrix} \Rightarrow \text{Rank}(P) = 1 < 2$$

\therefore The system is not controllable

For minimal realization, first perform controllable decomposition,

$$M = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix} \Rightarrow \hat{A} = M^{-1} A M, \hat{B} = M^{-1} B, \hat{C} = C M$$

\downarrow
To arbitrary vector

$$\Rightarrow \hat{A} = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} -0.75 & -0.25 \\ -0.5 & -0.5 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} -1 & -0.5 \\ 0 & -0.25 \end{bmatrix}$$

$$\hat{B} = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\hat{C} = \begin{bmatrix} 4 & 2 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} 6 & 4 \end{bmatrix}$$

The controllable modes are,

$$\dot{x}_c = A_c x_c + B_c u_c = -1 x_c + 1 u_c$$

$$y_c = C_c x_c = 6 x_c$$

Check observability of (\star) , $Q = \begin{bmatrix} 6 \\ 6 \times (-1) \end{bmatrix} \Rightarrow \text{Rank}(Q) = 1 \Rightarrow \text{Observable}$

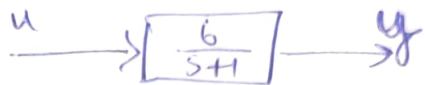
$\therefore (\star)$ is the minimal decomposition as it is both controllable and observable

We know that

$$G = C(SI - A)^{-1}B + D$$

$$= 6(s - (-1))^{-1}1 + 0$$

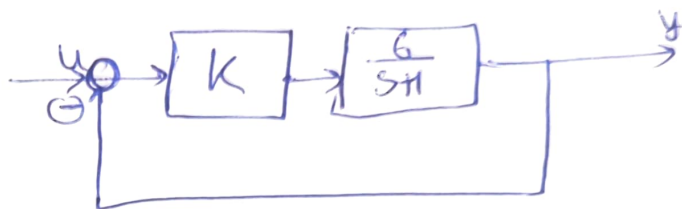
$$G = \frac{6}{s+1}$$



To design a controller, the loop will look like the following diagram,

for the TF, $G' = \frac{b}{Ts+1}$

Time constant = τ



Compare it with, $G'' = \frac{\frac{6k}{s+1}}{1 + \frac{6k}{s+1}} = \frac{6k}{s+1+6k}$

$$\frac{1}{\tau} = 1+6k \Rightarrow \frac{1}{1000} = 1+6k = 1000$$

$$\Rightarrow 1 = 1000 + 6000k$$

$$\Rightarrow k = \frac{999}{6} = \frac{333}{2} = 166.5$$

\therefore A proportional gain $k = 166.5$ will give us a time constant $\tau = 0.001s$.