



UNIVERSITÀ
POLITECNICA
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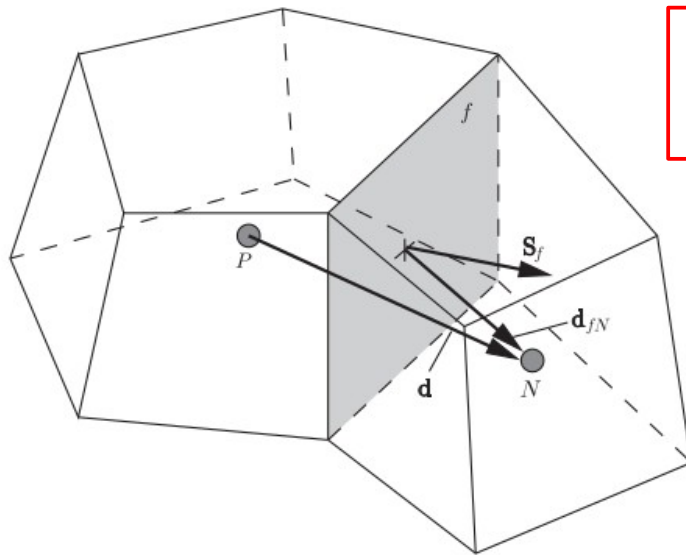
Numerical Heat Transfer
for Applications

**FVM for unsteady state
heat conduction**

Dr Valerio D'Alessandro

Finite volume discretization of Fourier equation

Fourier equation is discretized its integral form over each control volume:



$$\boxed{\frac{\partial T}{\partial t} - \alpha \nabla^2 T = 0} \Rightarrow \int_{V_P} \frac{\partial T}{\partial t} dV - \int_{V_P} \alpha \nabla^2 T dV = 0$$

$$\int_{V_P} \frac{\partial T}{\partial t} dV - \int_{V_P} \alpha \nabla \cdot (\nabla T) dV = 0$$

$$\int_{V_P} \frac{\partial T}{\partial t} dV - \int_{\partial V_P} \alpha \nabla T \cdot d\mathbf{S} = 0$$

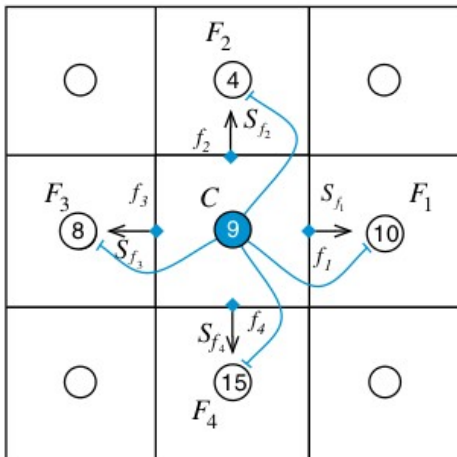


$$\int_{V_P} (\mathbf{x} - \mathbf{x}_P) dV = \mathbf{0}$$

$$\boxed{V_P \frac{dT_P}{dt} - \sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f = 0}$$

Finite volume discretization of Fourier equation

$$\sum_f (\nabla T)_f \cdot \mathbf{S}_f = 0 \quad \longrightarrow \quad a_C T_C + \sum_{nb} a_{nb} T_{nb} = b_C$$



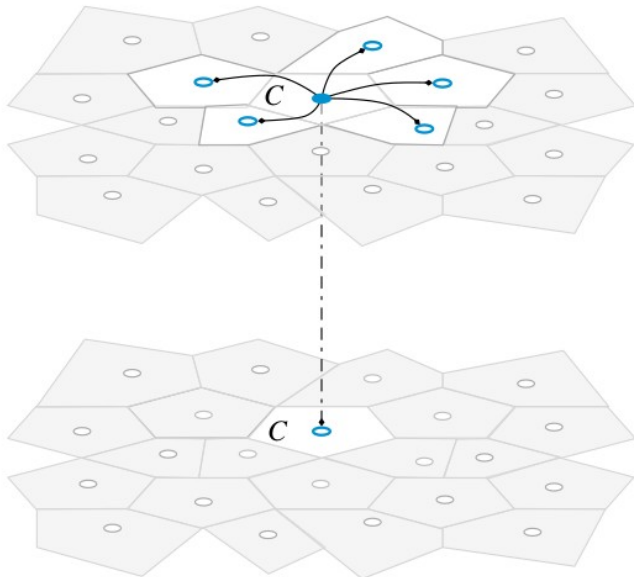
$$a_9 T_9 + a_{10} T_{10} + a_4 T_4 + a_8 T_8 + a_{15} T_{15} = 0$$

$$V_P \frac{dT_C}{dt} - \sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f = 0$$

$$V_P \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t} - \underbrace{\sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f}_{\text{Implicit or explicit ?}} = 0$$

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

Finite volume discretization of Fourier equation – implicit method



$$V_P \frac{dT_C}{dt} - \sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f = 0$$

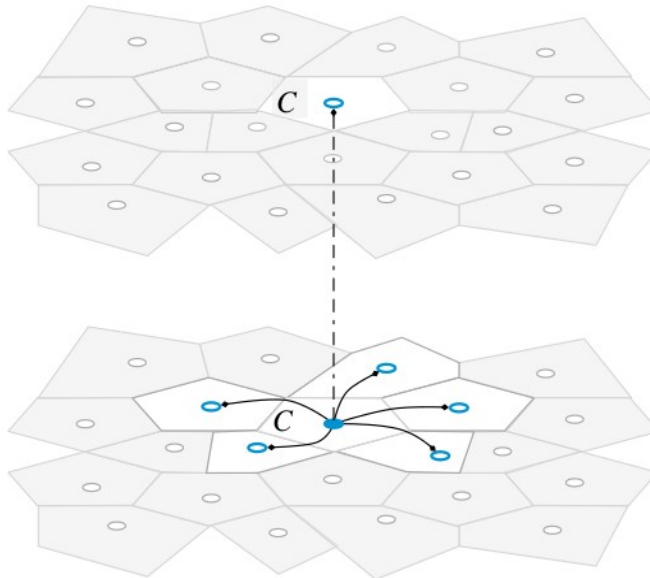
$$\frac{dT_C}{dt} = \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t}$$

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

It is possible to use also different time integration schemes rather than backward Euler. A possible alternative is the following one:

$$\frac{dT_C}{dt} = \frac{3T_C^{(n+1)} - 4T_C^{(n)} + T_C^{(n-1)}}{2\Delta t} + O(\Delta t^2)$$

Finite volume discretization of Fourier equation – explicit method



$$V_P \frac{dT_C}{dt} - \sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f = 0$$

$$\frac{dT_C}{dt} = \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t}$$

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)}$$



$$T_C^{(n+1)} = T_C^{(n)} + \frac{\Delta t}{V_P} \left(a_C T_C^{(n)} + \sum_{nb} a_{nb} T_{nb}^{(n)} + b_C \right)$$

Ex3_FVM – Unsteady state heat conduction

Matlab code

```
format long e

alpha= 1e-2;
dt    = 0.01;
Time = 50;
caseName='cube';
%-----
m=mesh_data(caseName);
Nc=m.numberofElements;
Ni=m.numberofInteriorFaces;
Nb=m.numberofBElements;
A=zeros(Nc,Nc);
b=zeros(Nc,1);

. . .

T0    = ones(Nc,1);
Tc    = zeros(Nc,1);

A     = -alpha*A;
b     = -alpha*b;

for i=1:Nc
    Vc    = m.elements(i).volC;
    A(i,i) = A(i,i) + Vc/dt;
end
```

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

A matrix implementation, as well as B.C. for laplacian term discretization, is exactly the same of the steady state case.

However, it is mandatory to switch **A** and **b** entries sign deriving from spatial terms discretization.

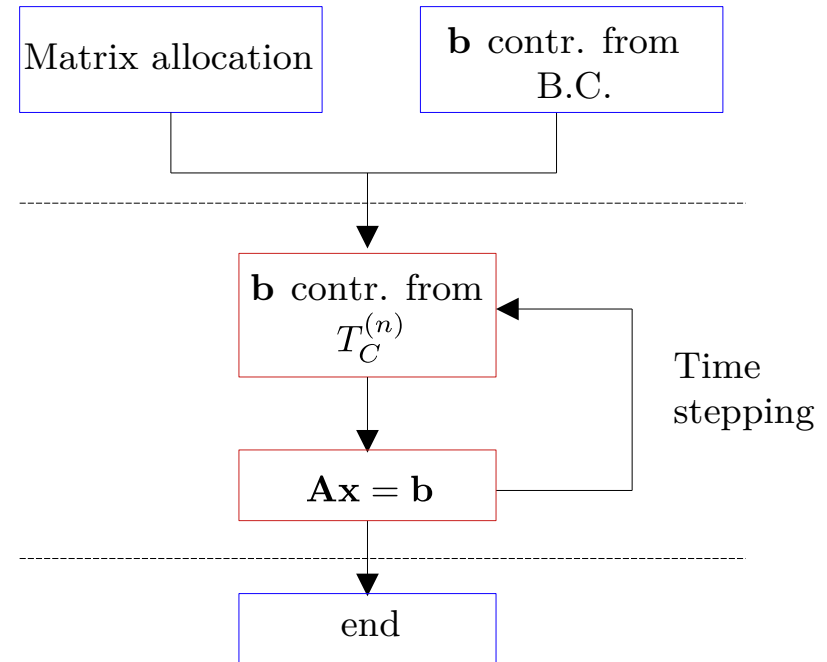
$\left. \begin{array}{l} \text{for } i=1:Nc \\ Vc = m.elements(i).volC; \\ A(i,i) = A(i,i) + Vc/dt; \end{array} \right\} \frac{V_P}{\Delta t} \rightarrow$ **A** matrix diagonal terms contributions deriving from unsteady term discretization.

Ex3_FVM - Unsteady state heat conduction

Matlab code

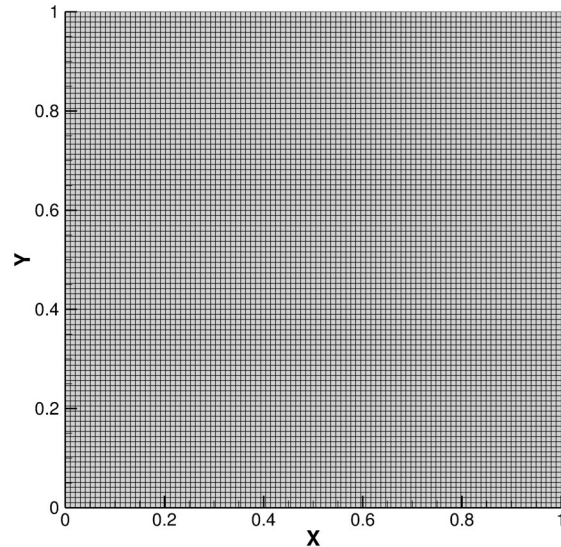
```
bn = zeros(Nc,1);
flow_time = 0;

for i= 1: (Time/dt)
    for j=1:Nc
        Vc = m.elements(j).volC;
        bn(j) = b(j) + (Vc/dt)*T0(j);
    end
    %
    Tc = bicg(A,b,1e-12,1000);
    Tc = pcg(A,b,1e-12,1000,L, U);
    T0 = Tc;
    bn = zeros(Nc,1);
    %
    flow_time = flow_time + dt;
    if ( mod(i,500) == 0)
        wrtfld(flow_time, m , Tc, 'Tc', caseName)
    end
end
```



$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

Ex3_FVM - Unsteady state heat conduction in 1-D configuration



$$\frac{\partial T}{\partial t} - \alpha \nabla^2 T = 0$$

$$T(x = 0, t) = 1$$

$$T(x = 1, t) = 0$$

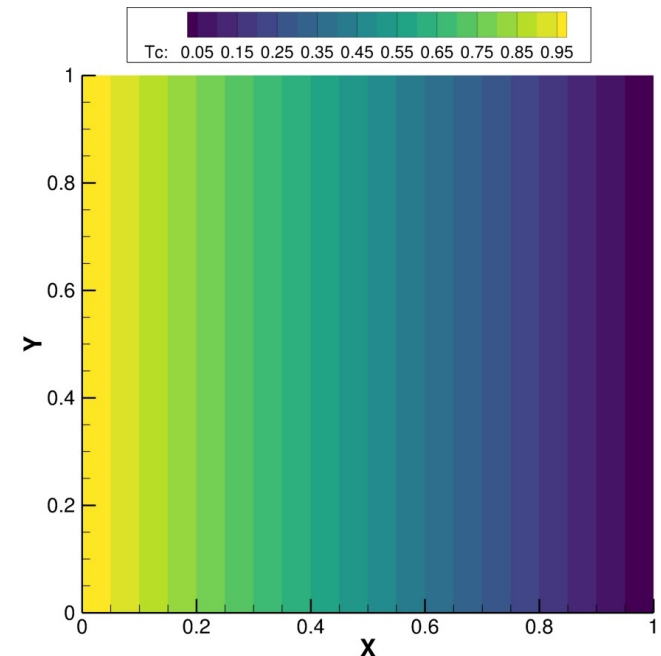
$$\partial_n T(y = 0, t) = 0$$

$$\partial_n T(y = 1, t) = 0$$

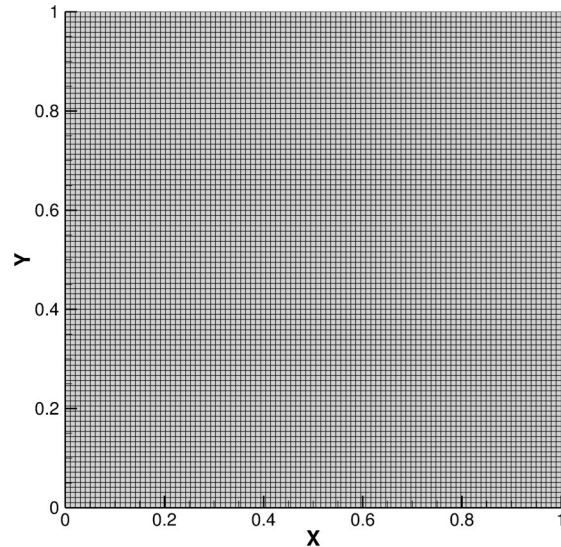
$$T(x, t = 0) = 1$$



$$T(x, t \gg 1) = 1 - \frac{x}{L}$$



Ex3_FVM – Unsteady state heat conduction in 1-D configuration



$$\frac{\partial T}{\partial t} - \alpha \nabla^2 T = 0$$

$$T(x = 0, t) = 1$$

$$T(x = 1, t) = 0$$

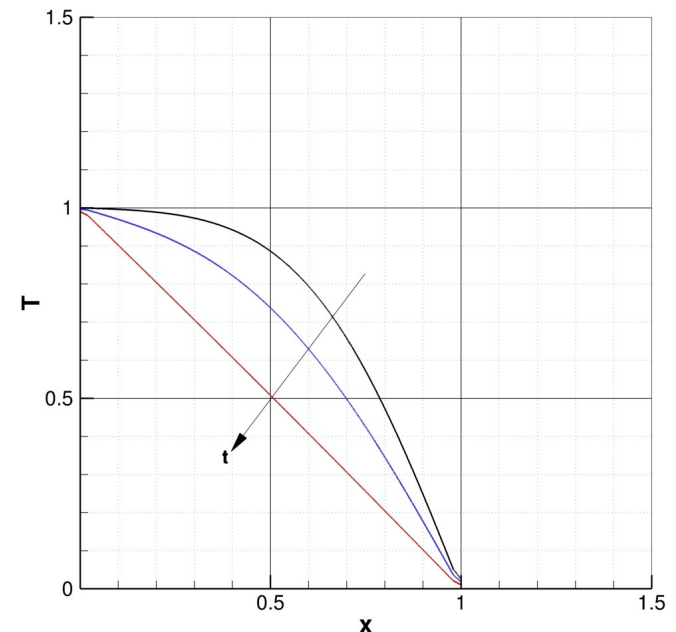
$$\partial_n T(y = 0, t) = 0$$

$$\partial_n T(y = 1, t) = 0$$

$$T(x, t = 0) = 1$$

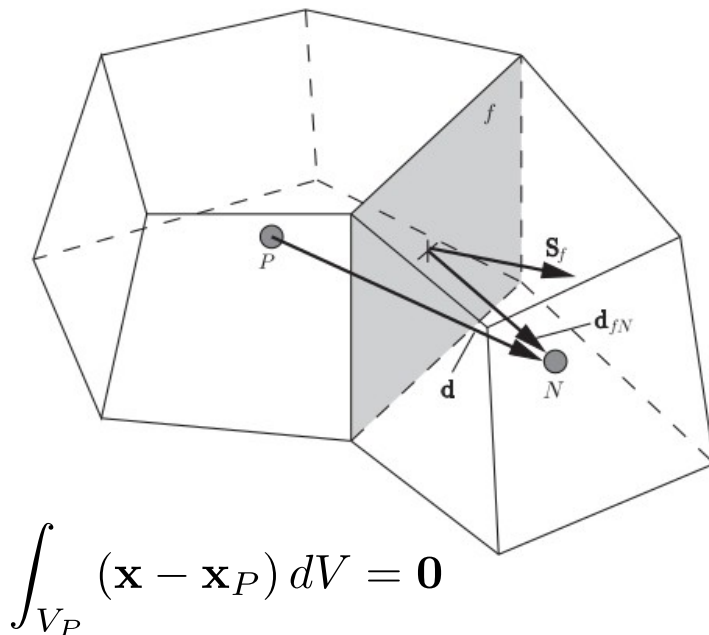


$$T(x, t \gg 1) = 1 - \frac{x}{L}$$



Finite volume discretization of general heat conduction equation

General heat conduction equation is discretized its integral form over each control volume:



$$\rho c \frac{\partial T}{\partial t} - \lambda \nabla^2 T = \rho_b c_{p,b} \omega_b (T_{a,0} - T) + G_L$$

$$G_L = \alpha I(x) \quad I(x) = I_0 e^{-\alpha x} \quad g_p = \frac{\rho_b c_{p,b} \omega_b}{\rho c}$$



$$\frac{\partial T}{\partial t} - \alpha \nabla^2 T + g_p T = g_p T_{a,0} + \frac{1}{\rho c} G_L$$



$$\int_{V_P} \left(\frac{\partial T}{\partial t} - \alpha \nabla^2 T + g_p T \right) dV = \int_{V_P} \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right) dV$$

Finite volume discretization of general heat conduction equation

The FVM discretization of general heat conduction equation differs from the previous case only for the source terms.

$$\int_{V_P} \left(\frac{\partial T}{\partial t} - \alpha \nabla^2 T + g_p T \right) dV = \int_{V_P} \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right) dV$$



$$V_P \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t} - \sum_f \alpha (\nabla T)_f \cdot \mathbf{S}_f + V_P g_P T_C = V_P \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right)$$

Backward Euler and an implicit time integration strategy is adopted:

$$V_P \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} + V_P g_P T_C^{(n+1)} = V_P \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right)$$

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)} \quad \text{Fourier equation}$$

Finite volume discretization of general heat conduction equation

$$V_P \frac{T_C^{(n+1)} - T_C^{(n)}}{\Delta t} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} + V_P g_P T_C^{(n+1)} = V_P \left(g_P T_{a,0} + \frac{1}{\rho c} G_L \right)$$

$$\frac{V_P}{\Delta t} T_C^{(n+1)} - a_C T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = -b_C + \frac{V_P}{\Delta t} T_C^{(n)} \quad \text{Fourier equation}$$

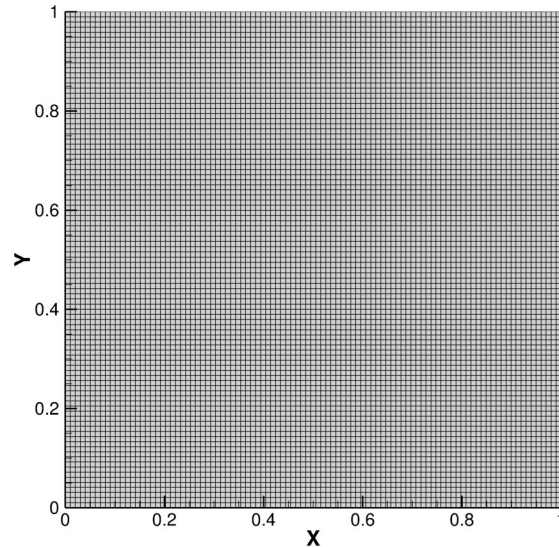


$$\frac{V_P}{\Delta t} T_C^{(n+1)} + \tilde{a}_c T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = \tilde{b}_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

$$\tilde{a}_c = -a_c + V_P g_P$$

$$\tilde{b}_C = -b_C + V_P \left(g_P T_{a,0} + \frac{1}{\rho c} G_L \right)$$

Ex4_FVM - Heat conduction in a biological tissue under laser heating



$$\rho c \frac{\partial T}{\partial t} - \lambda \nabla^2 T = c_{p,b} w_b (T_{a,0} - T) + G_L$$

$$T(x = 0, t) = 37$$

$$\partial_n T(x = 1, t) = 0$$

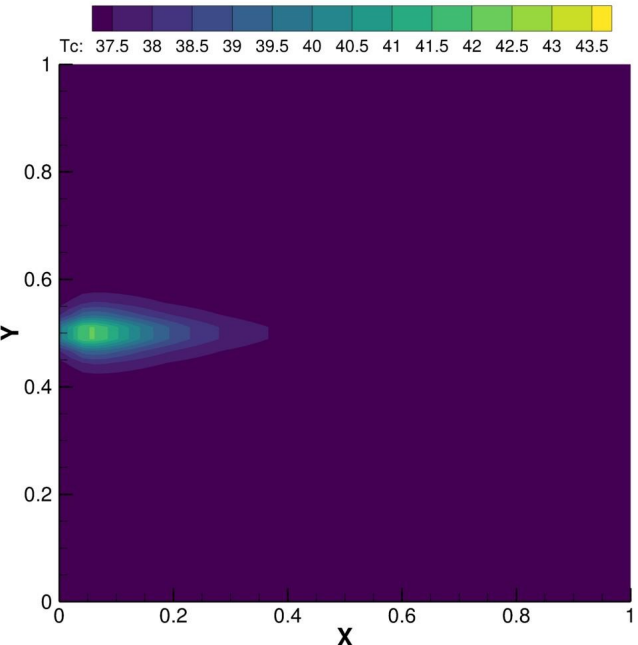
$$\partial_n T(y = 0, t) = 0$$

$$\partial_n T(y = 1, t) = 0$$

$$T(\mathbf{x}, t = 0) = 37$$

- LASER source is active only for 10 s. It is applied at $(x,y)=(0,0.5)$. the spot diameter is 1cm, while LASER intensity is 15 MW/m².
- Tissue properties are standard. (Take a look to the code on gitHub to obtain their values.)

**LASER
source**



Ex4_FVM - Heat conduction in a biological tissue under laser heating

Matlab code

```
alpha = 1.26e-3;
rhot = 1050;
cpb = 3770;
%
cpt = 3340;
wb = 0.5;
Ta0 = 37;
Tini = 37;
om = 0.05;
caseName='cube';
%-----
dt = 0.01;
Time = 1;
writeInt = 100;
%
%-----
%
m=mesh_data(caseName);
Nc=m.numberofElements;
Ni=m.numberofInteriorFaces;
Nb=m.numberofBElements;
A=zeros(Nc,Nc);
b=zeros(Nc,1);
```

$$\frac{V_P}{\Delta t} T_C^{(n+1)} + \tilde{a}_c T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = \tilde{b}_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

$$\tilde{a}_c = -a_c + V_P g_P \quad \tilde{b}_C = -b_C + V_P \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right)$$

- **A** matrix implementation, as well as **b** vector one, for laplacian and unsteady terms are exactly the same of the Fourier equation case.
- Pennes and Beer law terms can be implemented summing their contribution on **b** and **A** diagonal terms deriving from the Fourier equation discretization.

Ex4_FVM – Heat conduction in a biological tissue under laser heating

Matlab code

```
%-----
% Initial condition
%
T0 = zeros(Nc,1);
for i = 1:Nc
    T0(i) = T0(i) + Tini;
end
wrtfld(0, m , T0, 'Tc', caseName);

%-----
% A and b allocation
%
Tc = zeros(Nc,1);
%
A = -alpha*A;
b = -alpha*b;
for i=1:Nc
    Vc = m.elements(i).volC;
    A(i,i) = A(i,i) + Vc/dt;
end

%-----
```

$$\frac{V_P}{\Delta t} T_C^{(n+1)} + \tilde{a}_c T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = \tilde{b}_C + \frac{V_P}{\Delta t} T_C^{(n)}$$

$$\tilde{a}_c = -a_c + V_P g_P \quad \tilde{b}_C = -b_C + V_P \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right)$$

- **A** matrix implementation, as well as **b** vector one, for laplacian and unsteady terms are exactly the same of the Fourier equation case.
- **Pennes** and Beer law terms can be implemented summing their contribution on **b** and **A** diagonal terms deriving from the Fourier equation discretization.

Ex4_FVM - Heat conduction in a biological tissue under laser heating

Matlab code

```
%-----
% Initial condition
%
T0 = zeros(Nc,1);
for i = 1:Nc
    T0(i) = T0(i) + Tini;
end
wrtfld(0, m , T0, 'Tc', caseName);

. . .

%-----
% Beer law term
%
yL = 0.5;
gamma = 8;
I0 = 1.5e7;
bl = zeros(Nc,1);
for i=1:Nc
    Vc = m.elements(i).volC;
    if ( abs( m.elements(i).Cc(2) - yL ) < 0.01 )
        bl(i) = gamma*I0*exp(-
            gamma*m.elements(i).Cc(1))/(rho*cpt);
        bl(i) = bl(i)*Vc;
    end
end
%-----
```

$$\tilde{a}_c = -a_c + V_P g_P$$

$$\tilde{b}_C = -b_C + V_P \left(g_p T_{a,0} + \frac{1}{\rho c} G_L \right)$$

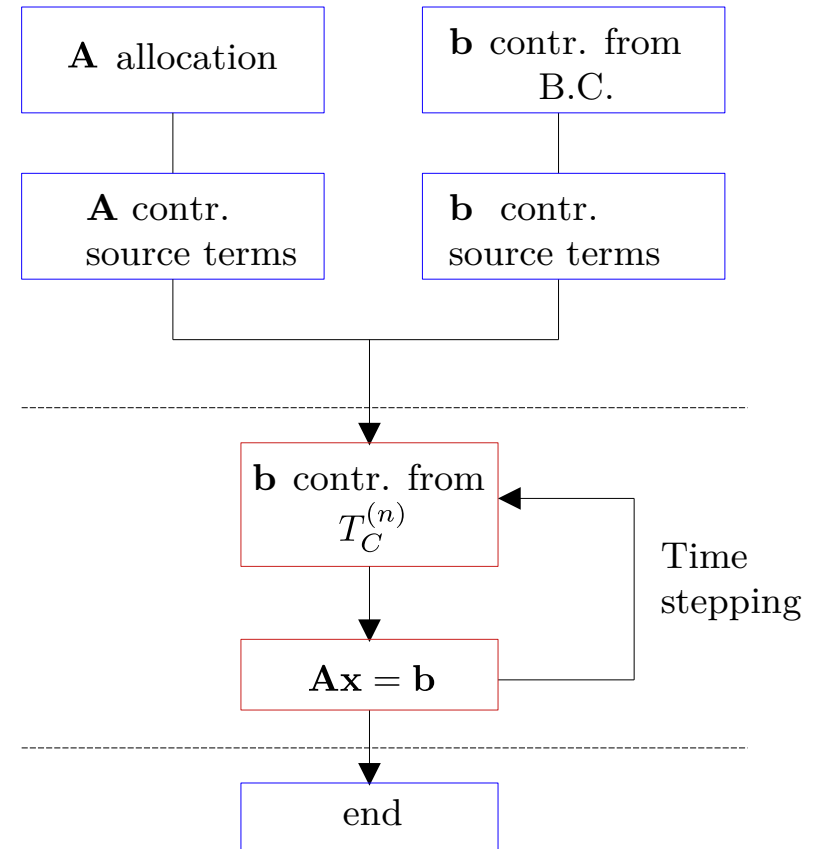
$$G_L = \alpha I(x) \quad I(x) = I_0 e^{-\alpha x}$$

- **A** matrix implementation, as well as **b** vector one, for laplacian and unsteady terms are exactly the same of the Fourier equation case.
- Pennes and **Beer law** terms can be implemented summing their contribution on **b** and **A** diagonal terms deriving from the Fourier equation discretization.

Ex4_FVM - Heat conduction in a biological tissue under laser heating

Matlab code

```
bn = zeros(Nc,1);
flow_time = 0;
for i= 1: (Time/dt)
    for j=1:Nc
        Vc = m.elements(j).volC;
        bn(j) = b(j) -
                bl(j)*min( sign(flow_time-10),0)
                + (Vc/dt)*T0(j);
    end
    %
    Tc = bicg(A,bn,1e-12,1000);
    %Tc = pcg(A,bn,1e-12,1000,L, U);
    T0 = Tc;
    bn = zeros(Nc,1);
    %
    flow_time = flow_time + dt;
    if ( mod(i,writeInt) == 0)
        wrtfld(flow_time, m , Tc , 'Tc', caseName)
    end
end
```



$$\frac{V_P}{\Delta t} T_C^{(n+1)} + \tilde{a}_c T_C^{(n+1)} - \sum_{nb} a_{nb} T_{nb}^{(n+1)} = \tilde{b}_C + \frac{V_P}{\Delta t} T_C^{(n)}$$