

# Reverse engineering of the Xmon qubits

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# Chapter 1

## Theoretical introduction

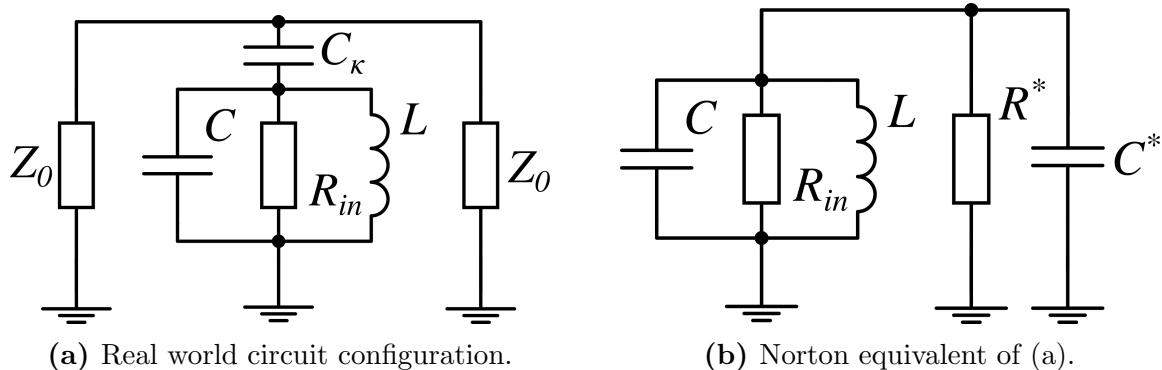
### 1 Superconducting microwave coplanar waveguide resonators

#### 1.1 Equations for quality factors

The total quality factor of a microwave transmission line resonator (TLR)  $Q_l$  (loaded quality factor) can be calculated as a sum of two parts – the internal and external quality factors. The internal quality factor  $Q_i$  describes how excitations leave the resonator in the absence of coupling to any external circuitry, so damping in this case comes from the internal defects (i.e. resonant two-level systems) in the resonator itself. When, however, the resonator is coupled to the external circuitry having some active resistance, the damping is enhanced and the total Q-factor is reduced according to the following expression:

$$Q_l^{-1} = Q_i^{-1} + Q_e^{-1}, \quad (1.1)$$

where  $Q_e$  is determined by the value of the externally connected resistance and the way of its connection.



**Figure 1.1:** Equivalent circuit for a  $\lambda/4$  TLR, capacitively coupled to the transmission line near resonance.

A common way of measuring a resonator is to couple it capacitively to an external transmission line. The coupling on the equivalent scheme of the circuit is represented as  $C_\kappa$ , as depicted in Fig. 1.1 (a). An infinite/properly terminated transmission line can be represented as a single resistance of  $Z_0$  Ohms, where  $Z_0$  is the line's wave impedance; thus, two such resistances are added to the both sides of the resonator circuit. The resonators are of  $\lambda/4$  type, so the equivalent for each of them is a parallel RLC oscillator (see below), where  $C$  and  $L$  are, respectively, its equivalent capacitance and inductance and  $R = R_{in}$  characterises the internal dissipation. Its  $Q_i = \omega_0 C R_{in}$  where  $\omega_0 = \sqrt{1/LC}$  can be calculated from the definition when no external impedance is connected.

The external Q-factor can be derived in a bit more complicated way.<sup>1</sup> We can transform the circuit from the Fig. 1.1 (a) to explicitly include the external parameters into the internal ones. To do so one needs to convert the series connection of the coupling capacitor and the characteristic impedances into parallel, as done on the Fig. 1.1 (b). The  $R^*$  and  $C^*$  impedances should be chosen in such a way that total impedance of the external circuit is the same as before the transformation:

$$R^* = \frac{1 + \omega^2 C_\kappa^2 (Z_0/2)^2}{\omega^2 C_\kappa^2 (Z_0/2)}, \quad (1.2)$$

$$C^* = \frac{C_\kappa}{1 + \omega^2 C_\kappa^2 (Z_0/2)^2} \approx C_\kappa \text{ (in our case).} \quad (1.3)$$

From this and Fig. 1.1 (b) it is simple to write down the expression for the internal, external and loaded quality factors:

$$Q_i = \omega(C + C^*)R_{in}, \quad (1.4)$$

$$Q_e = \omega(C + C^*)R^*, \quad (1.5)$$

$$Q_l = \omega(C + C^*) \frac{1}{1/R^* + 1/R_{in}}. \quad (1.6)$$

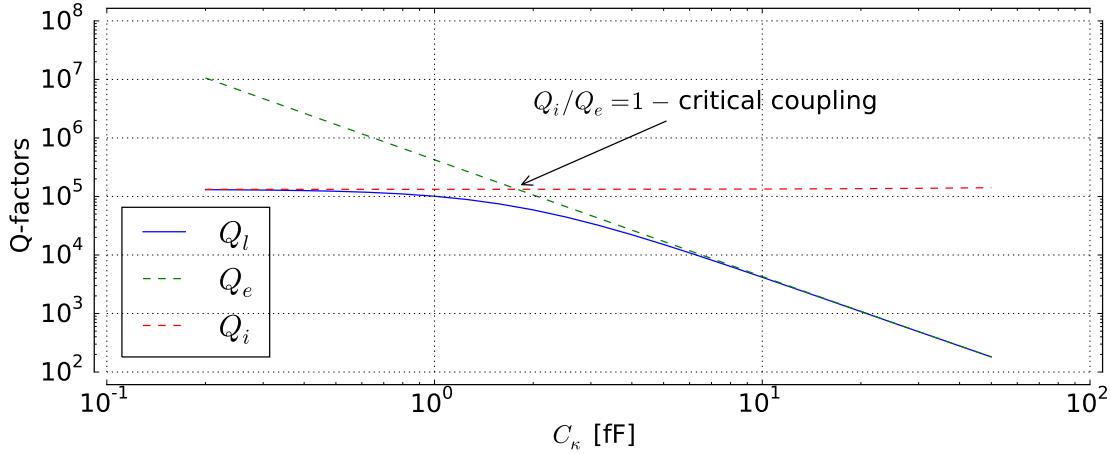
The above expressions readily justify (1.1). The values been used in the simulations are:  $C = 350$  fF,  $L = 2$  nH,  $R_{in} = 10^7$  Ohm,  $Z_0 = 50$  Ohm.

### The lumped-element model of a coplanar waveguide resonator

A  $\lambda/4$  coplanar waveguide (CPW) resonator near a resonance is equivalent to a lumped-element parallel resonance circuit, as in Fig. 1.1.  $L$  and  $C$  for the lumped-element models of CPW resonators are bound not only by the resonance frequency condition  $\omega_0 = 1/\sqrt{LC}$  but also by the geometry of the waveguide or, in other words,  $C'$  and  $L'$  – the transmission line capacitance and inductance per unit length. To show this, one would write down the impedance of the CPW resonator near its resonance frequency  $\omega_0$  and compare it to the lumped-element one's.<sup>2</sup> Such comparison leads to the following expressions:

$$R_{in} = \frac{Z_0}{\alpha l}, \quad C = \frac{\pi}{4\omega_0 Z_0},$$

where  $l$  is the resonator length,  $Z_0 = \sqrt{L'/C'}$  is the wave resistance and  $\alpha$  is the decay constant of the line. Then the resonance condition for the wavelength ( $\lambda = 4l$ ) is used along



**Figure 1.2:** Q-factors dependence on  $C_\kappa$  according to (1.6).

with the phase velocity expression  $v_{ph} = 1/\sqrt{L'C'}$ :

$$\omega_0 = \frac{2\pi}{\lambda v_{ph}} = \frac{\pi}{2l v_{ph}} \Rightarrow C = \frac{C'l}{2}.$$

For the inductance one can use  $L = 1/\omega_0^2 C = 8l L'/\pi^2$ . Finally, the expressions for  $C'$  and  $L'$ :

$$C' = 4\varepsilon_0 \varepsilon_{eff} \frac{K(k_0)}{K(k'_0)}, \quad L' = \frac{\mu_0}{4} \frac{K(k'_0)}{K(k_0)},$$

where  $K(x)$  is the complete elliptic integral of the first kind,  $\varepsilon_{eff} = \frac{1+\varepsilon_{substrate}}{2}$ ,  $k_0 = \frac{W}{W+2G}$ , where  $W$  is the width of the hotwire and  $G$  is the width of the gaps and finally  $k'_0 = \sqrt{1 - k_0^2}$ .

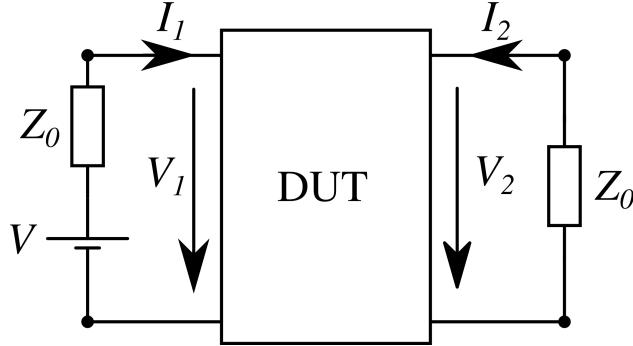
## 1.2 S-parameters for lines with resonators

Typically, a microwave device under test (DUT) is tested with a vector network analyser, which measures the scattering matrix (S-matrix) of the DUT. So below we will discuss the S-matrix for two different coupling configurations. Generally, a two-port DUT can be drawn like in Fig. 1.3. For such system it is possible to calculate different 2 by 2 matrices, which bind together voltages and currents on the ports 1 and 2. S-matrix also has 4 values, named S-parameters.

To calculate S-parameters one needs to treat voltages and currents, which can be calculated from Kirchhoff's laws, as a sum of the incident and reflected components ("+" corresponds to the incident wave and "-" to the reflected wave):

$$V_{1,2} = V_{1,2}^+ + V_{1,2}^-, \\ I_{1,2} = I_{1,2}^+ + I_{1,2}^- = \frac{V_{1,2}^+ - V_{1,2}^-}{Z_0},$$

where the difference in the second expression arises from telegrapher's equations. Solving



**Figure 1.3:** A scheme for the two-port network.

these with respect to incident and reflected components, one can get

$$V_{1,2}^{\pm} = \frac{1}{2}(V_{1,2} \pm Z_0 I_{1,2}).$$

From this, finally, S-parameters are defined:

$$\begin{pmatrix} V_1^- \\ V_2^- \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} V_1^+ \\ V_2^+ \end{pmatrix}. \quad (1.7)$$

However, it's often more convenient to use indirect methods of calculating S-parameters, for example, to extract them from  $ABCD$ -matrix.

### 1.3 Coupled (shunting) design

For a coupled design one can treat the resonator as a shunt in the transmission line as in Fig. 1.4. Except than by the definition (1.7) there are two other ways to calculate the S-matrix. First one is intuitive but is not valid for every configuration. Transmission and reflection parameters are defined<sup>3</sup> below (the second formula is valid only for the “shunt” configuration, no series elements are allowed in the line):

$$\Gamma = \frac{Z_{eff} - Z_0}{Z_{eff} + Z_0} = S_{11} = S_{22}, \quad (1.8)$$

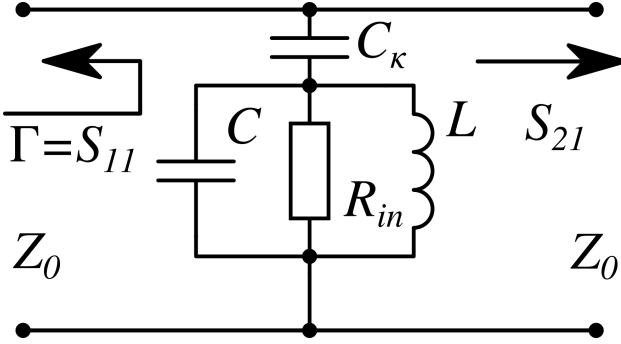
$$T = \frac{2Z_{eff}}{Z_{eff} + Z_0} \stackrel{!}{=} S_{21} = S_{12}, \quad (1.9)$$

where  $Z_{eff} = Z_0 || Z_{shunt}$ ,  $Z_{shunt} = \frac{1}{i\omega C_\kappa} + 1/i\omega C || R_{in} || i\omega L$  and the equalities between S-parameters hold due to the symmetry.

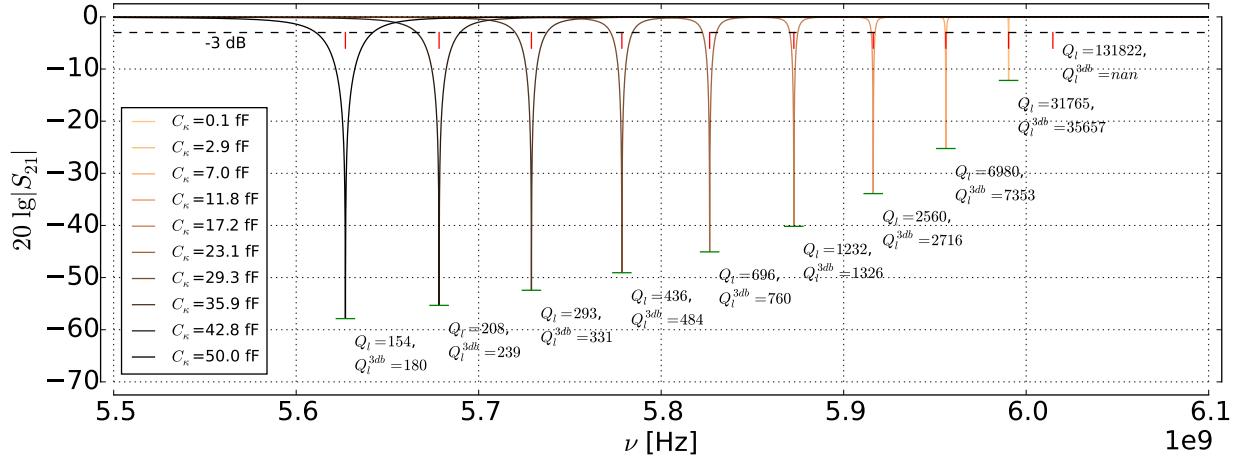
Another way is to calculate  $ABCD$  matrix or impedance matrix and convert it to the S-matrix with corresponding formulae.<sup>2</sup> In the “shunted” case from both this approaches the simplified expressions for the S-parameters follow:

$$S_{11} = -\frac{Z_0}{1 + 2Z_{shunt}/Z_0} = S_{22}, \quad (1.10)$$

$$S_{21} = \frac{1}{1 + Z_0/2Z_{shunt}} = S_{12}. \quad (1.11)$$



**Figure 1.4:** The shunted transmission line. This is Fig. 1.1 (a) from the observer's point of view.



**Figure 1.5:**  $S_{21}$  parameters from (1.11) for different coupling strengths. The loaded quality factors are calculated with (1.6) and with the “3db”-method. The red dashes show the values of expression  $\sqrt{1/L(C + C_k)}$  according to Fig. 1.1 (b), the green ones show the theoretically predicted depths.

The second expression is plotted in Fig. 1.5 along with the loaded quality factors calculated with (1.6) and with the “3db”-method ( $Q_L \approx \omega_0 / \Delta\omega_{3db}$ ). It can be seen that with increase of capacitance resonance frequency and  $Q_l$  decrease, which is expected according to Fig. 1.1 (b) and (1.3).

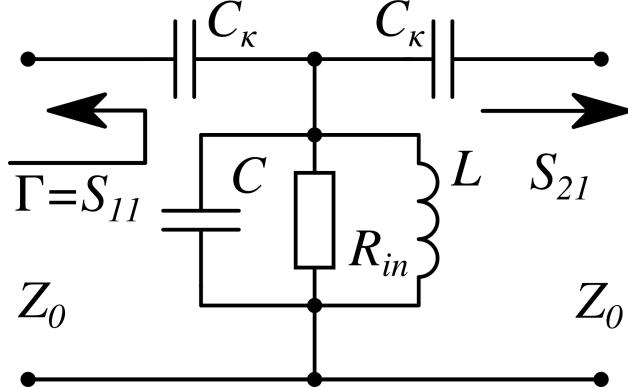
In Fig. 1.5 the resonance frequencies calculated from the equivalent circuit in Fig. 1.1 (b) are shown along with the analytically calculated depths of the peaks:

$$\min_f S_{21} = \frac{2L(C + C_k)}{\sqrt{C_k^2 LZ_0^2 (C + C_k) + (2(C + C_k)L + C_k^2 R_{in} Z_0)^2}}. \quad (1.12)$$

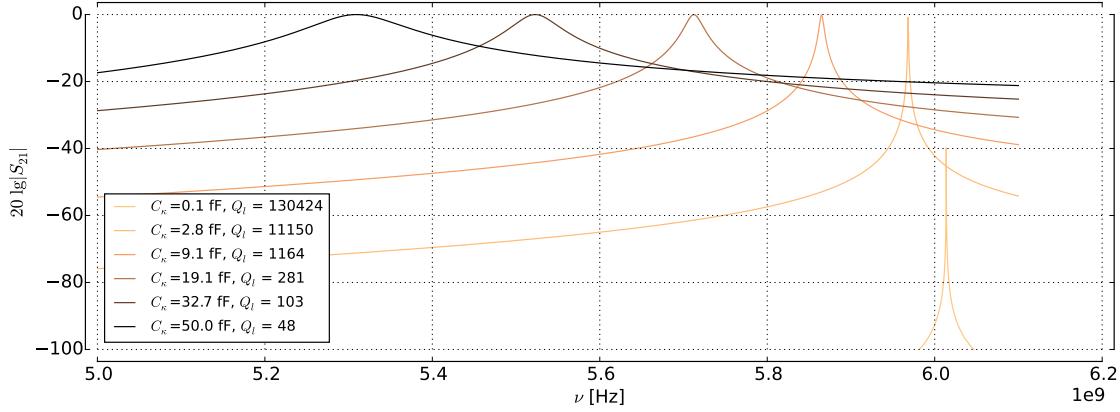
## 1.4 Embedded (series) design

For the embedded resonator it's possible to draw a similar equivalent circuit as for the “shunt” design.<sup>1</sup> It is depicted in Fig. 1.6.

For this kind of connection of the resonator to the transmission line (1.9) is now not valid (however, (1.8) still holds). To calculate transmission in this case one may find the



**Figure 1.6:** The equivalent circuit for the embedded resonator.



**Figure 1.7:**  $S_{21}$  for the series configuration. Loaded Q-factors were calculated via analytic expression similar to (1.6).

transmission matrix and then convert it to the S-matrix or use Kirchhoff's laws and (1.7). For studied case one can get the following  $ABCD$ -matrix<sup>2</sup>

$$\hat{T} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} = \begin{pmatrix} 1 + \frac{1/i\omega C_\kappa}{Z_{res}} & 2/i\omega C_\kappa - \frac{\omega^2 C_\kappa^2}{Z_{res}} \\ 1/Z_{res} & 1 + \frac{1/i\omega C_\kappa}{Z_{res}} \end{pmatrix}, \quad (1.13)$$

where  $Z_{res} = R_{in} || i\omega L || 1/i\omega C$ . The corresponding  $S_{21}$  is plotted in Fig. 1.7, calculated as<sup>2</sup>

$$S_{21} = \frac{2}{A + B/Z_0 + CZ_0 + D}. \quad (1.14)$$

## 2 Circuit QED with transmons

### 2.1 Hamiltonian for the compound system

Here we will use the results acquired by Bader<sup>4</sup> and Koch.<sup>5</sup> Using Fig. 1.8 it is possible to obtain the quantized Hamiltonian for the compound circuit:

$$\begin{aligned} \hat{\mathcal{H}} = & \underbrace{\frac{\hat{\phi}_r^2}{2L_r} + \frac{(C_q + C_g)\hat{Q}_r^2}{2C_*^2}}_{\text{resonator}} + \underbrace{\frac{(C_g + C_\kappa + C_r)\hat{Q}_q^2}{2C_*^2} - E_J(\Phi_{ext}) \cos \frac{2e}{\hbar} \hat{\phi}_q}_{\text{qubit}} + \underbrace{\frac{C_g \hat{Q}_r \hat{Q}_q}{C_*^2}}_{\text{coupling}} = \\ & = \hbar \omega_r \hat{a}^\dagger \hat{a} \otimes \hat{\mathbb{1}}_q \quad (\hat{\mathcal{H}}_r) \\ & + 4E_C \hat{\mathbb{1}}_r \otimes \hat{n}^2 - \frac{E_J(\Phi_{ext})}{2} \hat{\mathbb{1}}_r \otimes \sum_{n=-\infty}^{+\infty} |n+1\rangle\langle n| + |n\rangle\langle n+1| \quad (\hat{\mathcal{H}}_q) \\ & - 2e \frac{C_g}{C_*} \sqrt{\frac{\hbar \omega_r}{2(C_q + C_g)}} i(\hat{a}^\dagger - \hat{a}) \otimes \hat{n}, \quad (\hat{\mathcal{H}}_i) \end{aligned} \quad (2.1)$$

where

$$\begin{aligned} C_*^2 &= C_q C_g + C_q C_\kappa + C_g C_\kappa + C_q C_r + C_g C_r, \\ \omega_r &= 1/\sqrt{L_r C_*^2 / (C_q + C_g)}, \\ E_C &= \frac{(C_g + C_\kappa + C_r)e^2}{C_*^2}, \\ E_J(\Phi_{ext}) &= E_{J,\Sigma} \cos(\Phi_{ext}/\Phi_0), \quad \Phi_{ext} = I_\Phi M. \end{aligned}$$

Presuming the coupling is not very strong ( $C_g \ll C_q, C_r$ ) it is possible also to include simple time-dependent driving terms for both subsystems:

$$\begin{aligned} \hat{\mathcal{H}}_r^d(t) &= \frac{C_\kappa V_\kappa(t)}{C_r + C_\kappa} \hat{Q}_r \propto f_r(t) i(\hat{a}^\dagger - \hat{a}) \otimes \hat{\mathbb{1}}_q, \\ \hat{\mathcal{H}}_q^d(t) &= \frac{C_e V_e(t)}{C_q + C_e} \hat{Q}_q \propto f_q(t) \hat{\mathbb{1}}_r \otimes \hat{n}, \end{aligned} \quad (2.2)$$

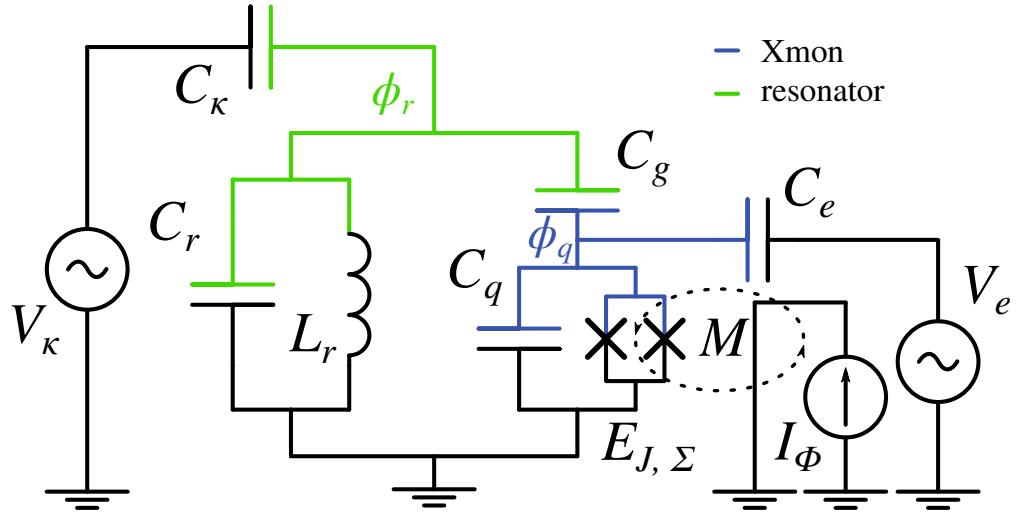
where  $f_{q,r}(t)$  are the effective values of the drive magnitude at time  $t$ .

### 2.2 Energy spectrum of the compound system

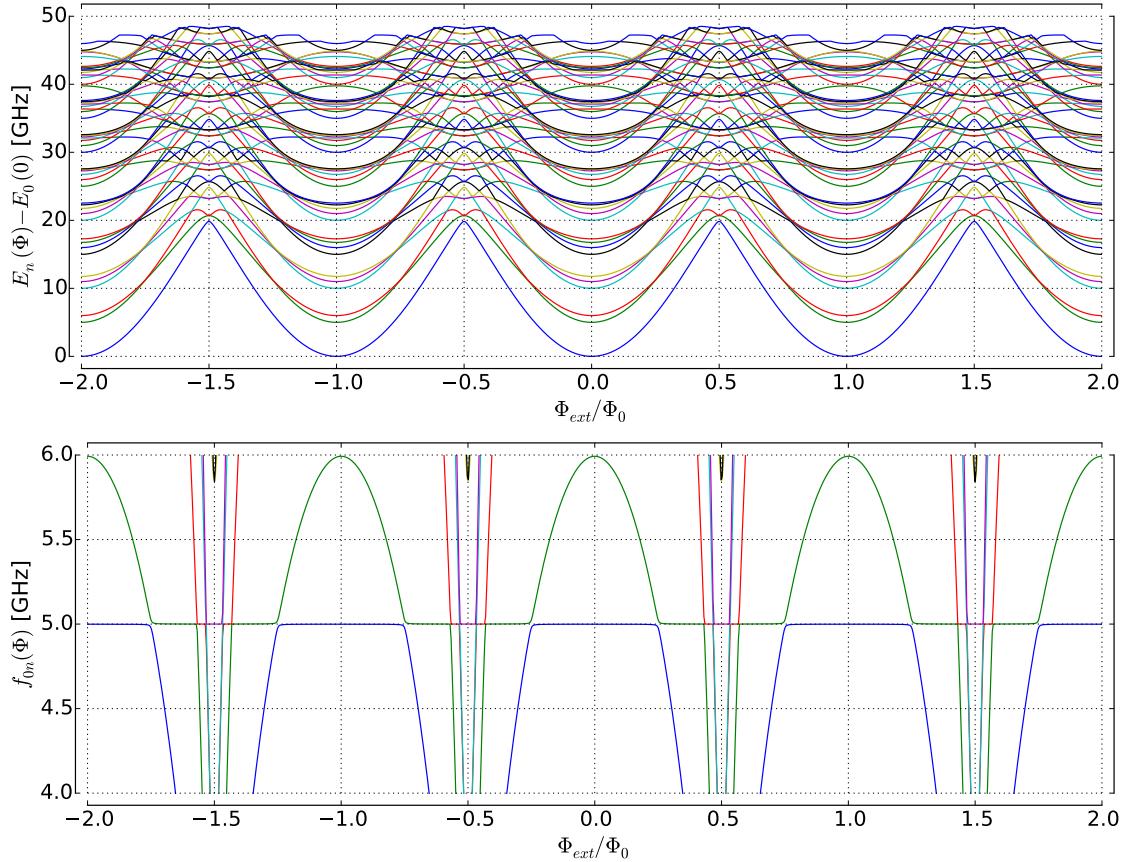
Using QuTiP<sup>7</sup> it is straightforward to solve the truncated matrix eigenproblem with the Hamiltonian (2.1). The results for the typical design values

$$C_\kappa = 5 \text{ fF}, \quad C_g = 2 \text{ fF}, \quad C_q = 90 \text{ fF}, \quad C_r = 500 \text{ fF}, \quad L_r = 2 \text{ nH},$$

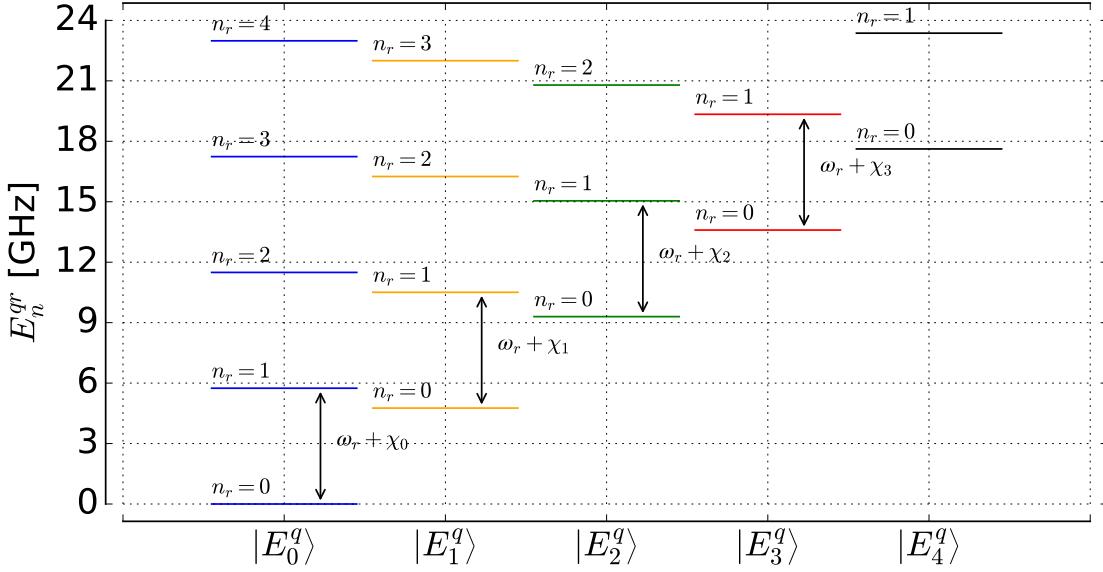
$$E_{J,\Sigma} = (h\nu_q + E_C)^2 / 8E_C \text{ for}^5 \nu_q = 6 \text{ GHz}$$



**Figure 1.8:** Equivalent circuit for coupled system of a tunable transmon qubit and a resonator. Colors show nodes (or branches) containing system's degrees of freedom according to M. Devoret's theory.<sup>6</sup>



**Figure 1.9:** Energy structure of the studied system depending on  $\Phi_{ext}$ .



**Figure 1.10:** Energy level diagram for the transmon-resonator system in the sweet spot when the detuning  $\Delta\omega = \omega_r - \omega_{ge}$  is positive.

can be observed in Fig. 1.9.

In Fig. 1.10 and Fig. 1.11 the energy structure of the compound system in the sweet-spot ( $\Phi_{ext} = 0$ ) is shown for two cases of positive and negative detuning. The dispersively shifted frequencies can be calculated from perturbation theory. For example, for the transition  $|0, g\rangle \rightarrow |1, g\rangle$  the shift is defined to the second order as

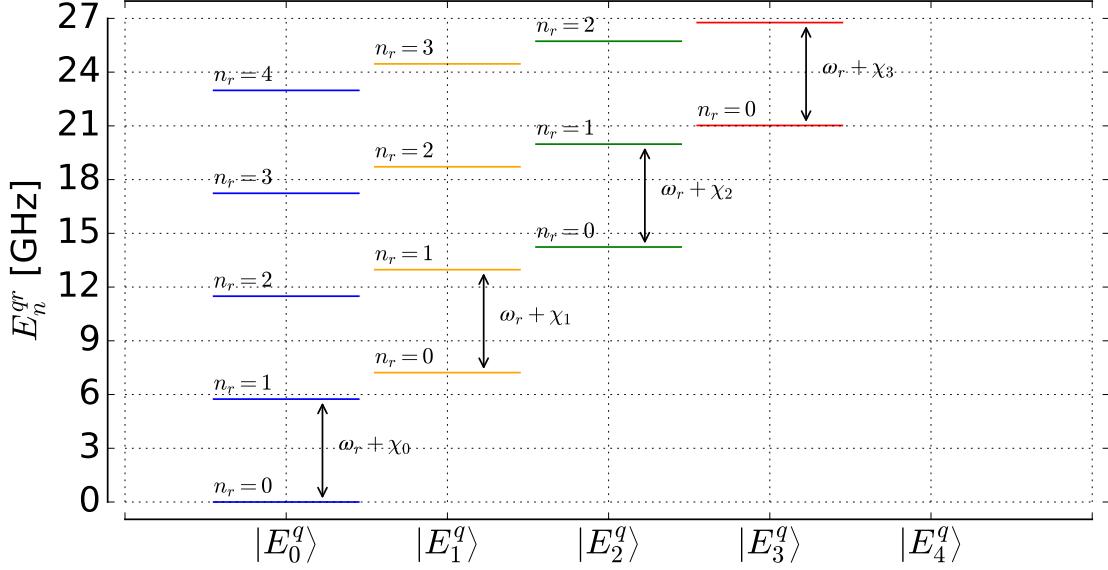
$$\begin{aligned}\chi_0 &= E_{1g}^{(1)} + E_{1g}^{(2)} - E_{0g}^{(1)} - E_{0g}^{(2)} \\ &= \langle 1, g | \hat{\mathcal{H}}_i | 1, g \rangle + \sum_{i,\alpha \neq 1,g} \frac{|\langle g, 1 | \hat{\mathcal{H}}_i | i, \alpha \rangle|^2}{E_{1g} - E_{i\alpha}} \\ &\quad - \langle 0, g | \hat{\mathcal{H}}_i | 0, g \rangle - \sum_{i,\alpha \neq 0,g} \frac{|\langle g, 0 | \hat{\mathcal{H}}_i | i, \alpha \rangle|^2}{E_{1g} - E_{i\alpha}}.\end{aligned}$$

As long as  $\hat{\mathcal{H}}_i$  mixes only adjacent resonator states the first order corrections vanish and so do the summations over  $i$ :  $\sum_{i,\alpha} \rightarrow \sum_{0,\alpha} + \sum_{2,\alpha} (\sum_{1,\alpha})$ . These sums then can be further truncated:

$$E_{1g}^{(2)} - E_{0g}^{(2)} \approx \frac{|\langle g, 1 | \hat{\mathcal{H}}_i | 0, e \rangle|^2}{\omega_r - \omega_{ge}} + \frac{|\langle g, 1 | \hat{\mathcal{H}}_i | 2, e \rangle|^2}{\omega_r - 2\omega_r - \omega_{ge}} - \frac{|\langle g, 0 | \hat{\mathcal{H}}_i | 1, e \rangle|^2}{-\omega_r - \omega_{ge}} \quad (2.3)$$

due to the selection rule of  $\hat{n}$ :  $\langle E_n^q | \hat{n} | E_{n+2k}^q \rangle = 0$ ,  $k \in \mathbb{Z}$  and the fast (exponential from numerics) decay of its matrix elements over distance between transmon energy eigenstates. It can be easily proven that last two elements of (2.3) are equal up to the factor of  $\sqrt{2}^2$  and final equation for  $\chi_0$  follows

$$\chi_0 = g^2 \left[ \frac{n_{ge}^2}{\omega_r - \omega_{ge}} - \frac{n_{ge}^2}{\omega_r + \omega_{ge}} \right]. \quad (2.4)$$



**Figure 1.11:** Energy level diagram for the transmon-resonator system in the sweet spot when the detuning  $\Delta\omega = \omega_r - \omega_{ge}$  is negative.

Similarly, dispersive shifts for the other two transmon states are derived:

$$\begin{aligned}\chi_1 &= g^2 \left[ \frac{n_{ef}^2}{\omega_r - \omega_{ef}} - \frac{n_{ef}^2}{\omega_r + \omega_{ef}} + \frac{n_{eg}^2}{\omega_r + \omega_{ge}} - \frac{n_{eg}^2}{\omega_r - \omega_{ge}} \right], \\ \chi_2 &= g^2 \left[ \frac{n_{fd}^2}{\omega_r - \omega_{fd}} - \frac{n_{fd}^2}{\omega_r + \omega_{fd}} + \frac{n_{fe}^2}{\omega_r + \omega_{ef}} - \frac{n_{fe}^2}{\omega_r - \omega_{ef}} \right],\end{aligned}$$

where  $g, e, f, d$  denote the first 4 energy eigenstates of the transmon,  $n_{\alpha\beta} = \langle \alpha | \hat{n} | \beta \rangle$  is the matrix element of  $\hat{n}$  and  $g = |\frac{\hat{\mathcal{H}}_i}{i(\hat{a}^\dagger - \hat{a}) \otimes \hat{n}}|$  is the coupling parameter which precedes the operator part in the interaction Hamiltonian. These formulas were compared to the numerical solution and have relative errors of less than 1%.

### 3 Dynamics

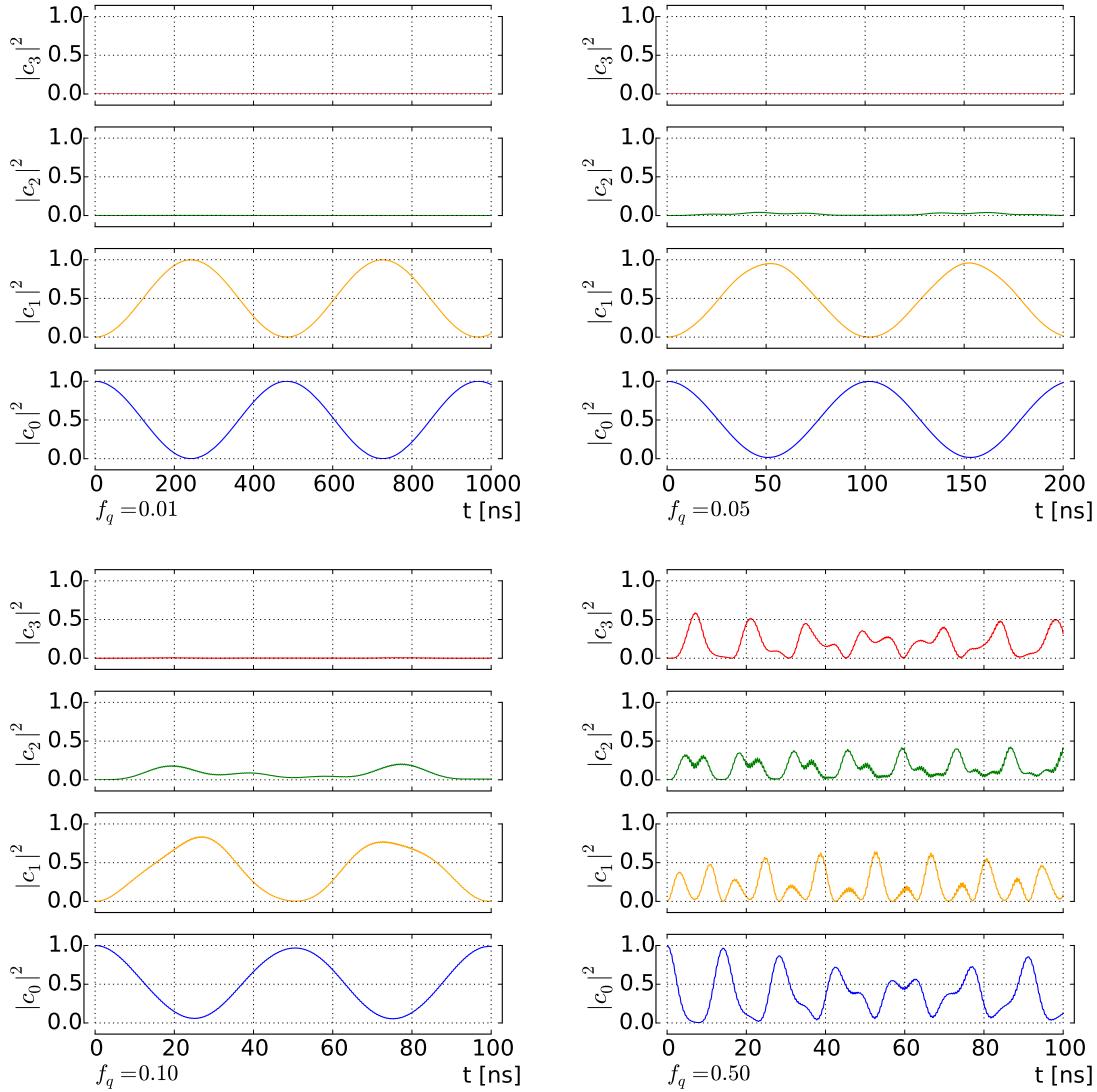
#### 3.1 Driving of an isolated transmon (Xmon)

To simulate the dynamics in the unitary case without taking into account the dissipative processes it is enough to solve the Schrödinger equation with the Hamiltonian (2.1) summed with the driving part (2.2). To consider the isolated qubit only it is sufficient to put  $C_g = 0$ . The final state after some time of the evolution  $t$  will be described with a Dyson series or a  $\hat{T}$ -exponent:

$$|\psi(t)\rangle = \hat{T} \exp \left\{ -\frac{i}{\hbar} \left( \hat{\mathcal{H}}t + \int_0^t \hat{\mathcal{H}}_q^d(\tau) d\tau \right) \right\} |E_0^q\rangle = \sum_k c_k(t) |E_k^q\rangle, \quad (3.1)$$

where  $|E_k^q\rangle$  denotes the  $k$ 's eigenstate of the qubit Hamiltonian. The simulation can also be reduced to a standard linear ODE solution which is also possible within QuTiP framework using the *mesolve* routine.

The result of such simulation can be observed in Fig. 1.12. As one can see when the driving amplitude (in GHz) becomes comparable to the anharmonicity of the transmon, significant leakage to higher states occurs.



**Figure 1.12:** Dynamics of the isolated driven transmon qubit with different drive strengths  $f_q = 0.01\text{-}0.5$  GHz, where  $f_q$  is an effective amplitude of the drive (2.2)  $f_q(t) = f_q \sin(\omega_{01}t)$ . It can be seen that significant distortions and leakage to higher levels occur when amplitude is too large.

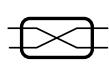
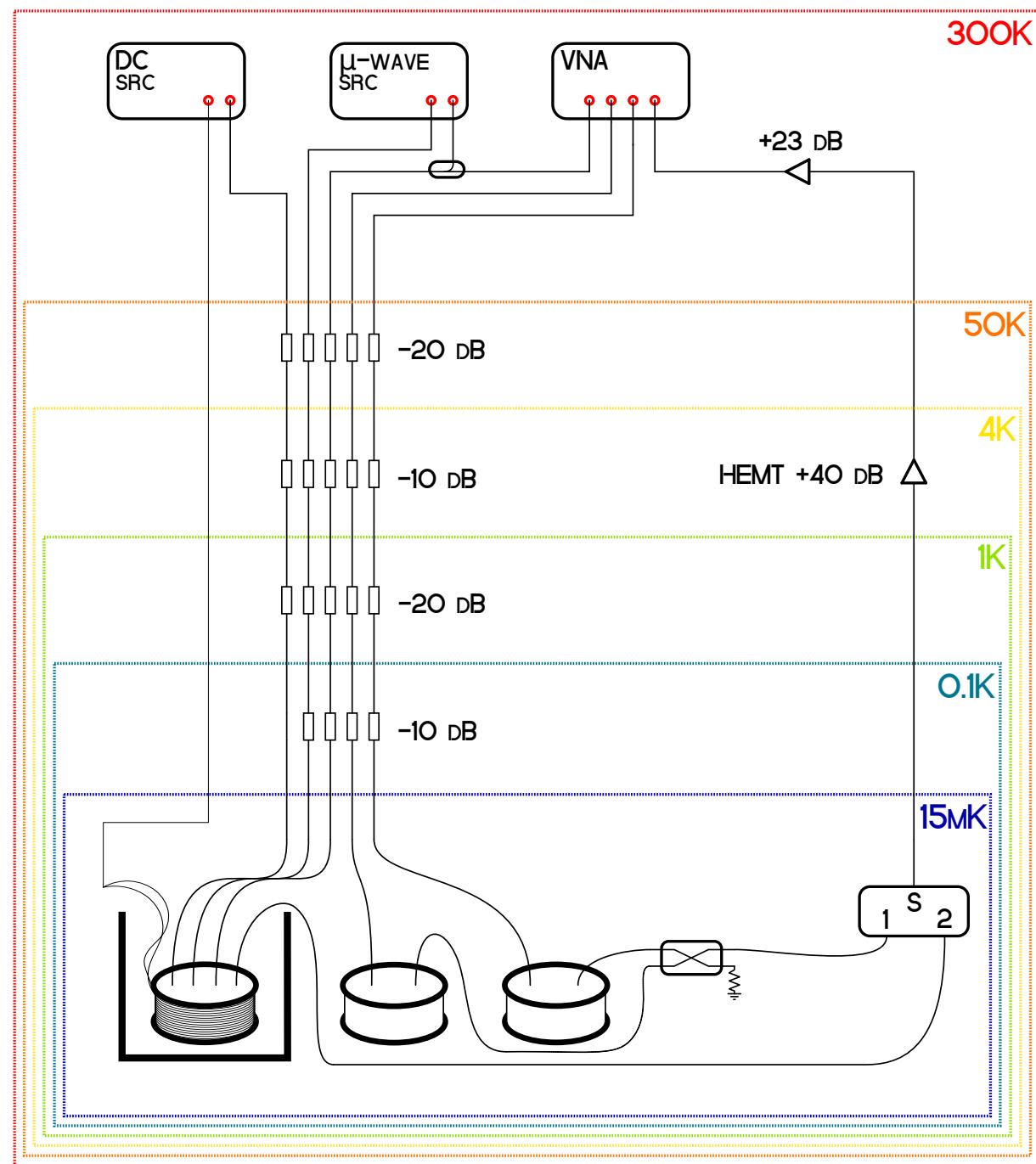
# Chapter 2

## Experimental methods

### 1 Experimental setup and equipment

### 2 Two-tone spectroscopy

This measurement is conducted with an additional high-power microwave tone from the microwave source, which induced the transitions from ground state of the system to higher levels and transition frequencies from there then were probed by the VNA. Practically this is realised by setting the VNA to measure single point at the shifted resonator frequency  $\omega_r + \chi_0$  (see Fig. 1.10) and then scanning the current in the coil and frequency on the  $\mu$ -wave source. When the frequency of the latter coincides with some allowed transition frequency of the system at given flux, the system leaves its ground state and the VNA is not probing a correct transition frequency any more. For example, if second tone has induced qubit  $ge$  transition, the correct resonator frequency would be  $\omega_r + \chi_1$  and the lowest transmission will be observed there (see Fig. 1.10 again). Thus, at  $\omega_r + \chi_0$  where the VNA is measuring the transmission would become higher than it was when the second tone missed the  $ge$  transition. In reality of course the situation is a bit more complicated as long as constant microwave tone induces Rabi oscillations between levels if it is resonant with the corresponding transition and after all the VNA will be probing transitions from the incoherent mixture of states  $\hat{\rho} = \frac{1}{2}[\lvert 0, g \rangle \langle 0, g \rvert + \lvert 0, e \rangle \langle 0, e \rvert]$ , however the transmission still ends up being higher when the second tone induces transitions from ground state. All said above can be applied also to the transmission phase, however the phase at resonance will become either higher or lower depending on the direction of the resonance shift as long as the phase behaves linearly around the resonance and is more sensitive. This method works well in the dispersive limit when the qubit-resonator detuning  $\Delta_\omega = \omega_r - \omega_{ge}$  is comparable to  $\omega_r, \omega_{ge}$ .



HYBRID COUPLER



ATTENUATOR

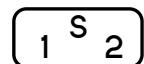
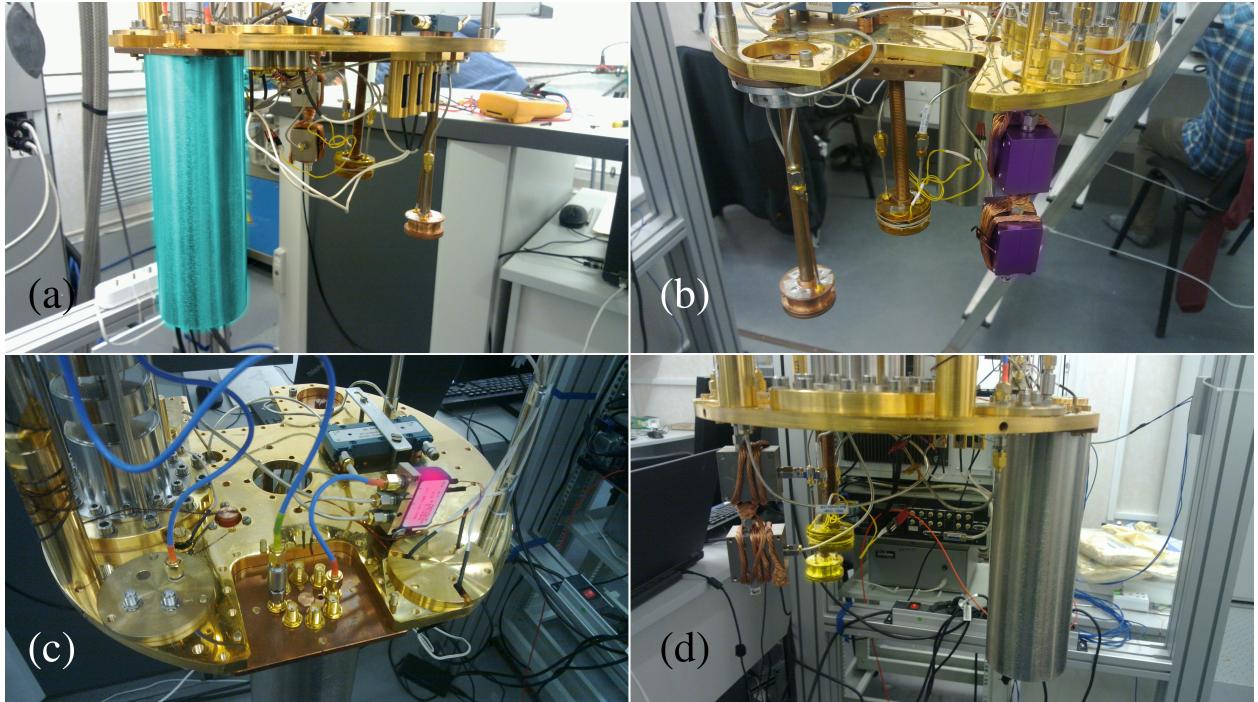
2-CHANNEL  
SWITCH

Figure 2.1



**Figure 2.2:** Example configuration of the 15 mK stage of the BF LD 250 fridge in the RQC lab at ISSP with three samples installed (with false colors added). **(a)** Front-bottom view of the 25 mK flange. Cyan color highlights the cylindric cryoperm shield inside which the sample holder resides. **(b)** Back view, violet color shows the circulators with a thick copper wire wrapped around them for thermalization. **(c)** Front-top view, where the 2-channel microwave switch is shown (magenta) and the hybrid coupler (blue, left in true color) used to measure several samples using only one low-noise HEMT amplifier. **(d)** Side view, the two unshielded sample holders similar to the one concealed under the shield from (a) are shown in yellow.

# Chapter 3

## Experimental results

### 1 Proof-of-concept design

#### 1.1 Geometry and parameters

The first sample that was measured was created from a proof-of-concept design, which was aimed at testing general properties of the simplest Xmon-based cQED systems. The easiest way to gain insight about the structure of the sample is to look at Fig. 3.1 where some of the main parts of its design are shown. The chip is 8 mm long and 4 mm wide and consists basically of six isolated qubit-resonator systems.

All of the resonators were  $\lambda/4$  with frequencies designed to be 6, 6.5, 6.9, 7, 7.1, 8 GHz for devices I-VI, respectively. Their coplanar parameters are  $7\ \mu\text{m}$  for the central wire width and  $4\ \mu\text{m}$  for the gaps.

The qubits were designed to be identical, with  $C_{\Sigma} \approx 80\ \text{fF}$  and  $I_{C,\Sigma} = 60\ \text{nA}$ , giving the  $\omega_{01}/2\pi \approx 7\ \text{GHz}$  at their flux sweet-spot ( $\Phi_{ext} = 0$ ) and anharmonicity of approximately  $-230\ \text{MHz}$ .

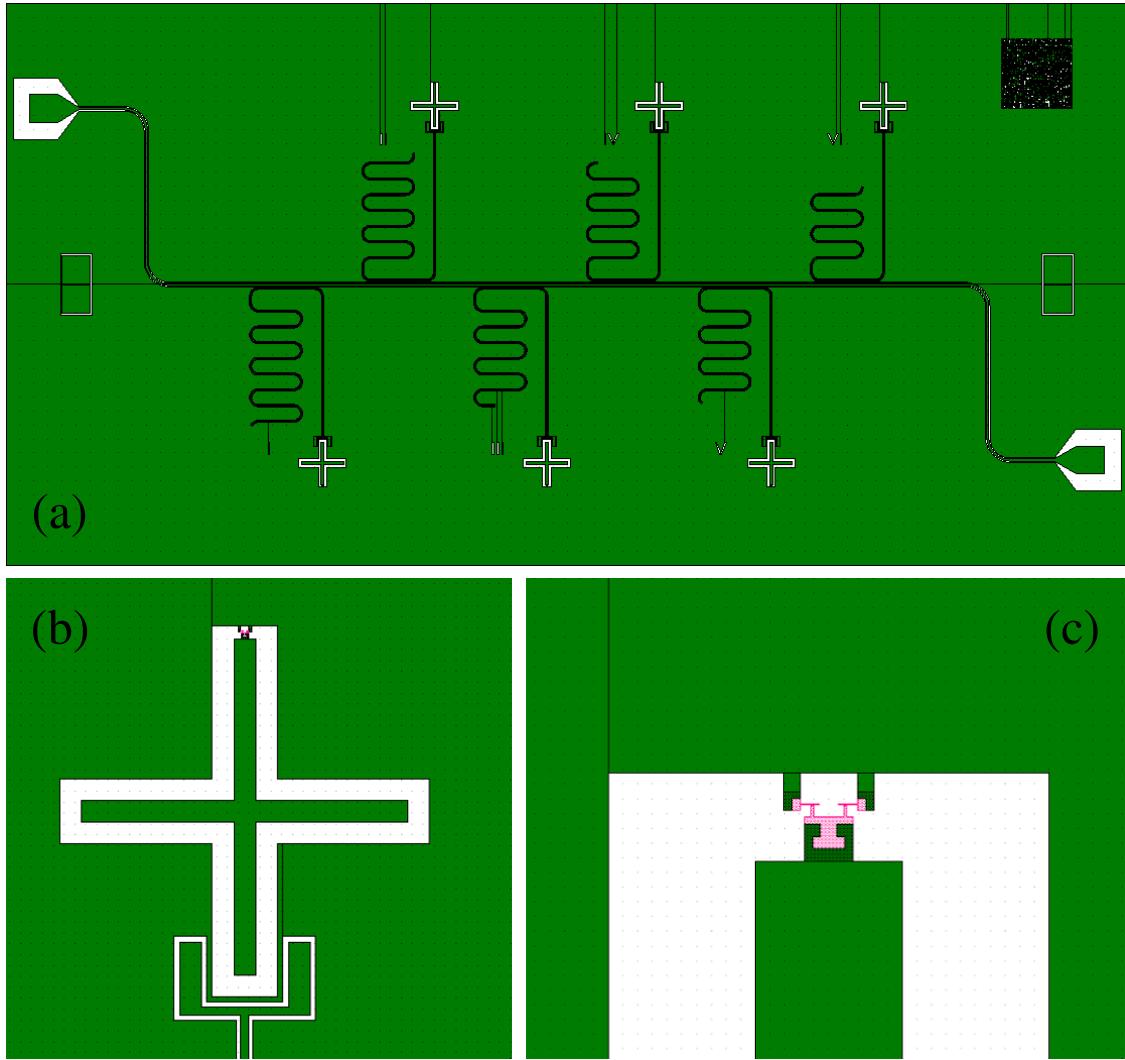
Two test structures at the sides of the chip were also included to allow direct DC measurement of the SQUIDs created during the shadow evaporation.

#### 1.2 Purposes and implementation

The main targets for the chip were:

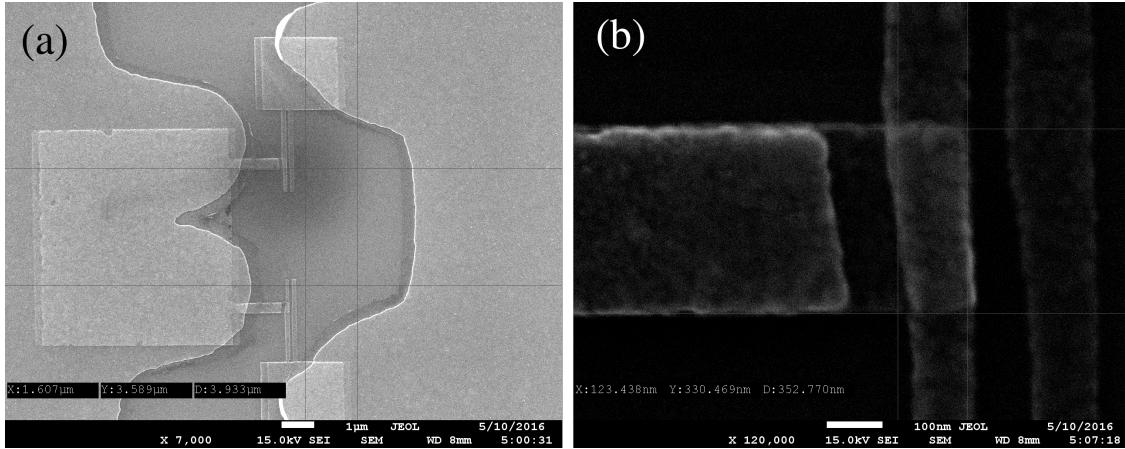
- (a) to check the measurement setup
- (b) to check the calculations for the frequencies and the coupling strengths
- (c) to roughly check the coherence of Xmons
- (d) to estimate the reproducibility of the junctions
- (e) to observe the AC-Stark shift
- (f) to observe high-power multiphoton transitions and sidebands

- (g) to check for the interesting effects caused by different resonator detunings at sweet-spot



**Figure 3.1:** (a) Large-scale image of the design used for the proof-of-concept sample. The chip (8x4 mm) consists of six  $\lambda/4$  CPW resonators coupled capacitively to the feedline each with an Xmon qubit at the open end. (b) Zoomed area around one of the qubits, showing its cross-shaped capacitor and the “claw” coupler of its resonator. (c) Zoom around one of the qubits’ SQUIDS. Pink areas denote the e-beam mask that was used for shadow evaporation.

The sample was fabricated in the cleanroom facility at MIPT, in a two-step process. Firstly, electron beam lithography was used to form the shadow evaporation mask for the pads with junctions and Al was shadow evaporated on the Plassys unit ( $\pm 7^\circ$ ). Secondly, the photolithography was used to pattern larger structures like the feedline, resonators and Xmons’ capacitors aligned with e-beam lithography and finally another layer of Al was deposited.



**Figure 3.2:** (a) SEM micrograph of the SQUID of one of the test structures on the chip. One can see that photo- and electron lithography are aligned, however fine structures Fig. 3.1 (c) were not resolved during the second step. (b) Enlarged view on one of the junctions (upper). Its area is approximately  $120 \times 330 \approx 0.4 \mu\text{m}^2$ , in the design it's  $0.3 \mu\text{m}^2$ .

### 1.3 Measurement setup

The sample was measured at ISSP in laboratory of RQC. Cryogenic equipment was represented by BlueFors LD250 dilution refrigerator, with base temperature of 16 mK. The microwave equipment included R&S ZNB 10 kHz-20 GHz vector network analyser, Agilent E8257D 100 kHz - 40 GHz analog signal generator. The sample was flux biased using Keithley 6221 current source.

Microwave line was thermalized with 60 dB of attenuation, additional 20 dB of attenuation were introduced on a directional coupler which added the second tone from the  $\mu$ -wave source. After leaving the sample the signal passed through two isolators and a hybrid coupler, which was used before to measure two samples during single cooldown. Finally, the signal was amplified with 4-8 GHz LNF amplifier at 4 K and a with a room-temperature amplifier.

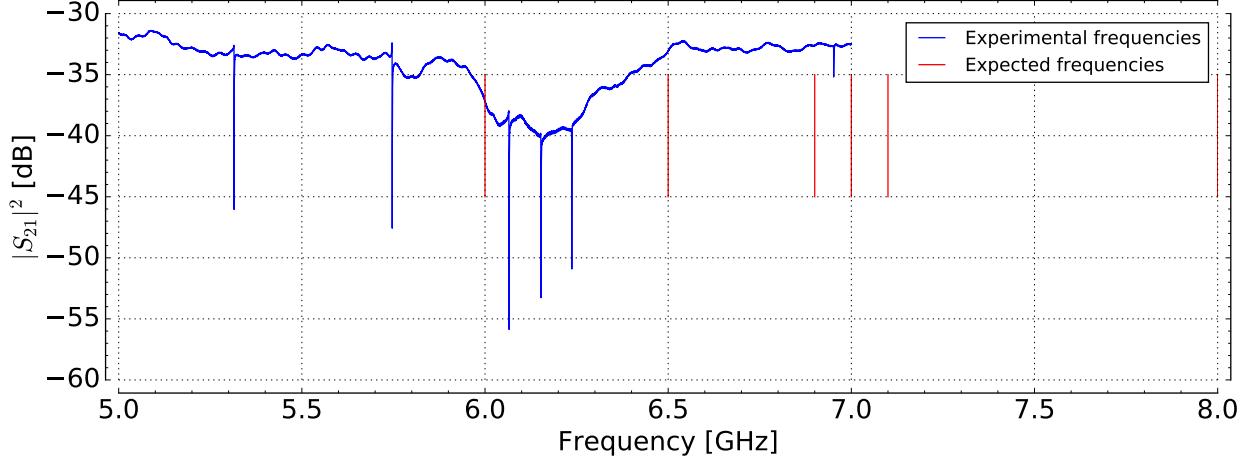
The sample holder that was used was designed for 10x10 mm chips, so the bondwires had a relatively large length of 1 mm which of course deteriorated the overall transmission. Chip lay directly on the copper disk of the bottom part of the sample holder with no hole carved under it. Around the sample holder a superconducting coil was wound which has been supplied using the current source mentioned above.

The magnetic shielding of the sample holder was achieved via a cryoperm shield. A superconducting shield was not installed in this run due to the lack of space inside the magnetic shield, which may have influenced the noise background.

### 1.4 Characterization of the resonators

As a first step of characterizing the sample a study of the resonances was performed. In Fig. 3.3 the power transmission through the cryostat is shown. It can be seen that in overall the transmission level is at approximately  $-35$  dB. As long as the amplifiers add 60 dB the

directional coupler and the hybrid coupler subtract 23 dB, it can be inferred that the sample in the sampleholder itself has approximately -10 dB transmission. This should be improved with better impedance matching to reduce noise. Secondly, there is a clear 300 MHz-wide dip in the transmission around 6.2 GHz, which should also be eliminated.



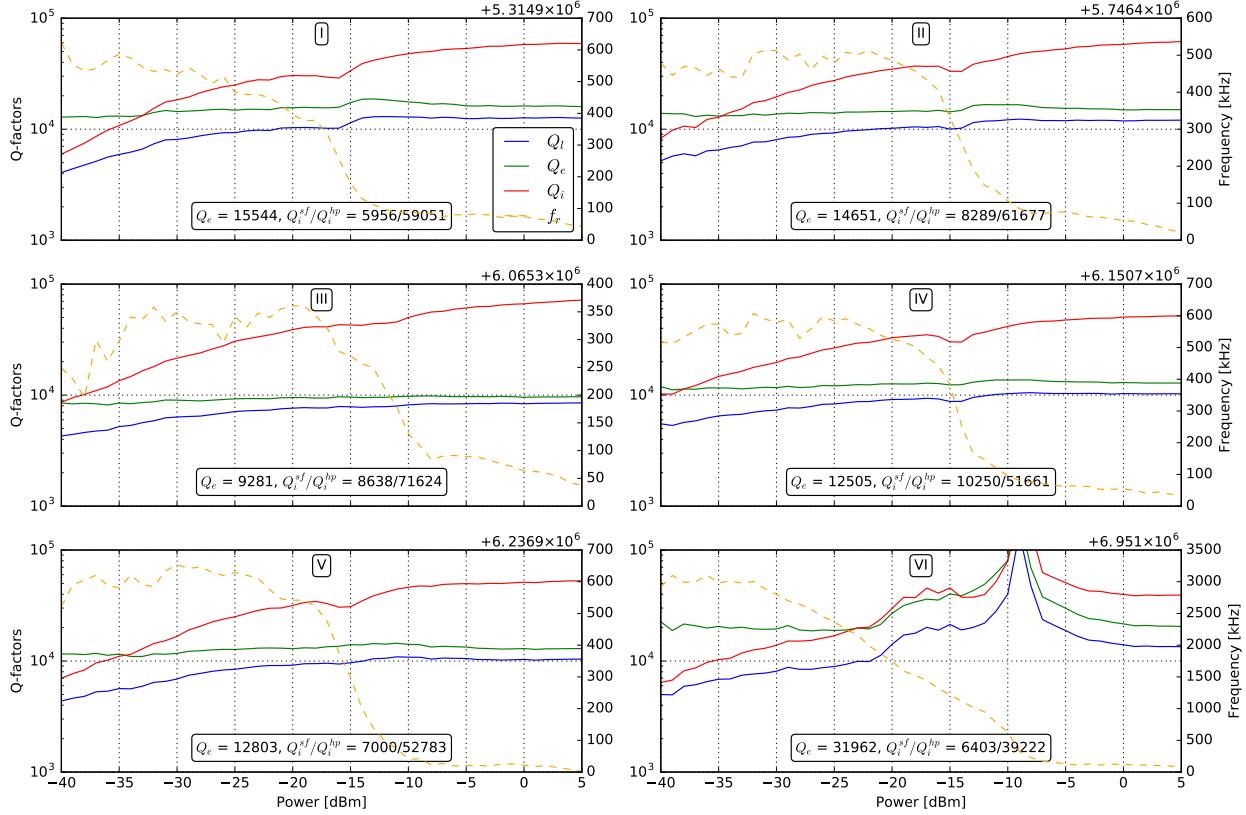
**Figure 3.3:** General view of the resonances. All six resonances are visible, however shifted far down in frequency. This shift is due to a mistake in the design which didn’t compensate for the “claw” couplers at the resonator ends.

All resonators are functional which can be seen from the presence of six sharp dips in transmission. The frequencies at which the dips occur are significantly lower than expected because there was a flaw in the macro code which draws the design. The frequency compensation routine made specifically to calculate the frequency shift<sup>8</sup> caused by the “claw” coupler at the end of the resonator was not executed, so the length of the resonators became larger than it should have been. At higher frequencies the phase shift of the “claw” is larger so the frequency discord is larger there.

Below the results obtained using the *circlefit*<sup>9</sup> fitting method are presented. Each peak from Fig. 3.3 was enlarged and scanned with a fine resolution and averaged to reduce noise (more averages on low and less on high powers). Then for each power complex  $S_{21}$  data for each scan area around a resonance was recorded.

After all of the data had been obtained, the fitting procedure has been applied for every scan at each power. The full fitting process is described in depth in the original publication.<sup>9</sup> In practice the whole algorithm is encapsulated in several function calls of the library called *resonator tools* that the authors have kindly provided via GitHub. Fitting results are summarized in Fig. 3.4.

It is well-known<sup>10</sup> that for superconducting microwave resonators the internal quality factor experiences an increase in value when probed with higher power. This effect is believed to occur due to the presence of two-level defects or two-level systems (TLS) with a dipole moment in the areas of high electric fields which resonator creates. As long as TLSs have same frequency as the measured resonator and coupled strong enough, they will drain excitations from the resonator. However TLSs can only accommodate only one photon at a time; thus, at high probe powers they saturate and do no more participate in resonator relaxation.



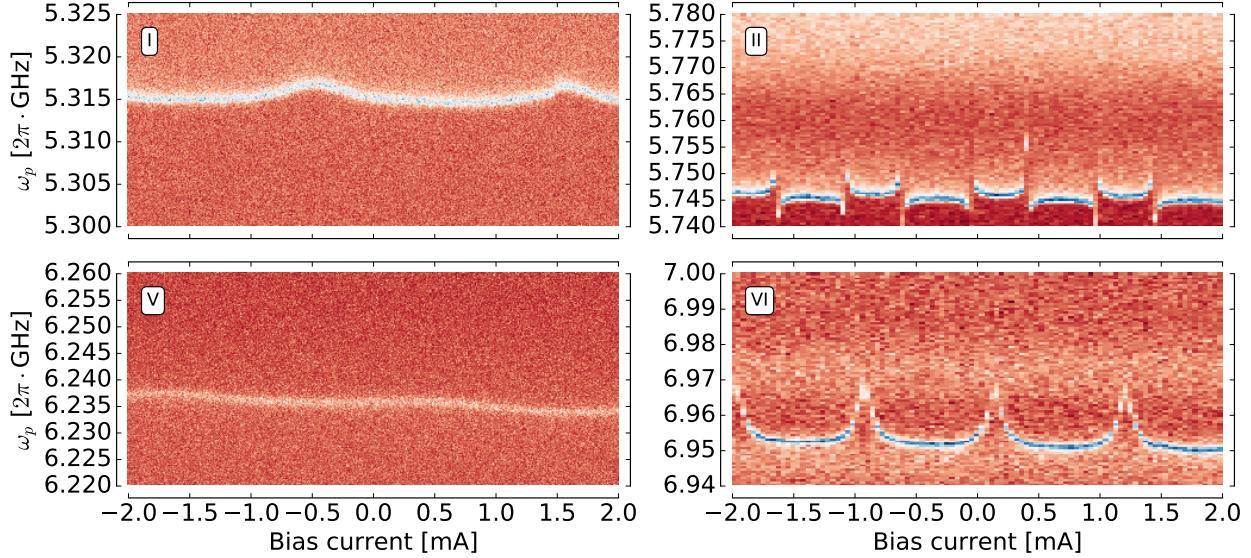
**Figure 3.4:** Various quality factors and frequencies depending on radiation power. Single photon limit is near -40 dBm on the VNA summed with 80 dB of attenuation, saturation limit near 5 dBm on the VNA. All devices show standard behaviour except for the VI<sup>th</sup> which loses its shape and cannot be fit correctly at powers above -20 dBm.

Therefore, an increase of the internal Q-factor is observed when the resonator is driven with strong microwave fields.

When the resonator is coupled to a weakly nonlinear quantum system like transmon its quality factor will depend strongly on the coherence time of the qubit when their frequencies are close (thus on the flux bias). Therefore, possibly the low (usual  $Q_i$  values for similar Al devices are around  $3 \cdot 10^4$ ) internal quality factor values of the resonators at single-photon level are determined by high dissipation in the qubits that were not detuned far enough in frequency.

## 1.5 Characterization of the whole cQED systems

From six systems on the chip only three were studied in detail partly due to lack of time and partly because the overall picture was more or less clear at that point. Firstly the behaviour of the resonators was investigated when the flux bias was being changed. This measurement revealed obvious periodic frequency oscillations in four devices from six, see Fig. 3.5. The other two devices didn't show any noticeable periodic flux dependence because one of the qubits (III) had a broken SQUID and the other (IV) probably was much lower in



**Figure 3.5:** Magnetic field influence on frequencies of four devices. Resonators III and IV didn't demonstrate any significant dependence on flux (not shown here).

frequency than its resonator.

Firstly system II was measured as long as it has shown the most prominent flux response of all. Then system VI was investigated and, finally, system I. For each of them a two-tone spectroscopy was performed and for II and VI a high-resolution single-tone one as well. Then the data was used to fit the parameters in the model (2.1) described in section 2. Accordingly, the graphs that are shown below are composed of the experimental spectra overlayed with theoretical curves obtained from numerical solution of the corresponding eigenproblems.

## System II

**Model.** Below all the experimental data will be provided for system II along with theoretical fits of the spectral lines that were observed using the model (2.1). Model parameters were fit based on all data on this system and are same for all figures in this section. Before turning to the comparison of the theoretical predictions and experimental results it would be useful to present the model parameters used for fitting which are summarized in Table 3.1.

Parameter	Value	Parameter	Value
$C_\kappa$	0 fF	$C_r$	444 fF
$C_g$	1.9 fF	$L_r$	1.72 nH
$C_q$	95 fF	$I_{C,\Sigma}$	69.5 nA
$E_C$	200 MHz	$E_{J,\Sigma}$	34.5 GHz

**Table 3.1:** Values of the main parameters defining the spectrum of the model (2.1).

From these values it's possible to calculate the coupling strength  $g \approx 19.6$  MHz between the qubit and the resonator, bare qubit frequency of  $\omega_{qe}^{(0)}/2\pi = 7.3$  GHz and bare res-

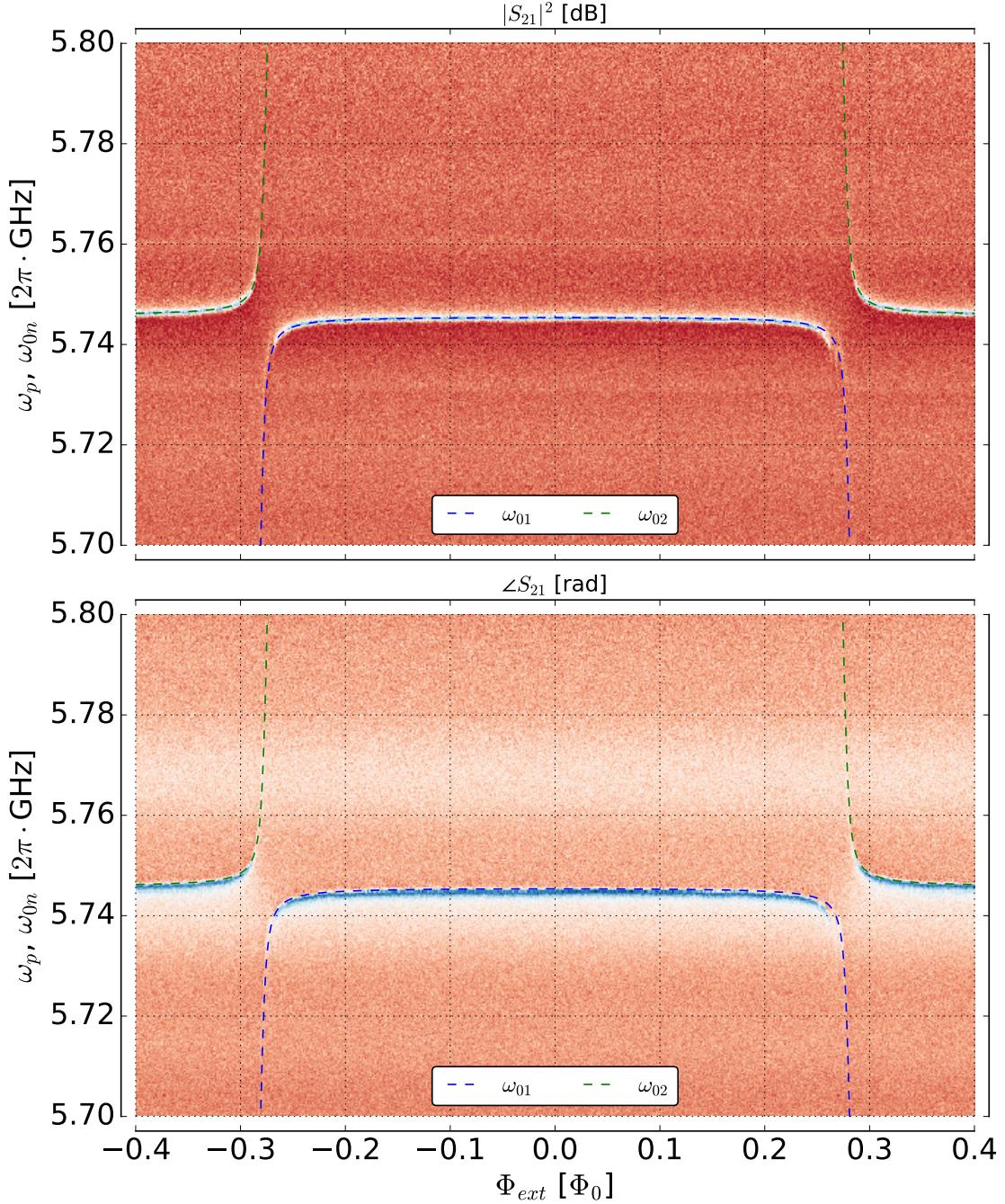
onator frequency  $\omega_r^{(0)} = 5.758$  GHz. In the coupled system these values are shifted strongly,  $\omega_{ge}/2\pi = 7.23$  GHz and  $\omega_r = 5.746$  GHz. These shifts are so large (much greater than what would be predicted by the usual dispersive shifts) because of the large value of the Xmon capacitance. Usually cQED systems are treated in the limit of large  $C_r \gg C_q, C_g, C_\kappa$  and in this case factors in the terms  $\hat{\mathcal{H}}_q, \hat{\mathcal{H}}_r$  from (2.1) can be reduced to their bare uncoupled values. This means the only difference from the uncoupled case is the term  $\hat{\mathcal{H}}_i$ , which defines the shifts from the uncoupled frequencies, which are in this case by definition equal to the dispersive shifts. In the studied case  $C_q \approx 0.25 C_r$  and cannot be neglected; thus, the interacting systems are not the same as before coupling, and only the full model (2.1) taking account of all capacitances can be used to obtain correct results. Despite that after acquiring the new parameters for the interacting systems from (2.1) the dispersive shifts may be calculated as usual.

The flux normalization on the x-axis was done using data from Fig. 3.5 (II) knowing the fact that  $\Phi_0$  should be the period of the pattern and that zero flux point is situated at the center of one of the lower branches.

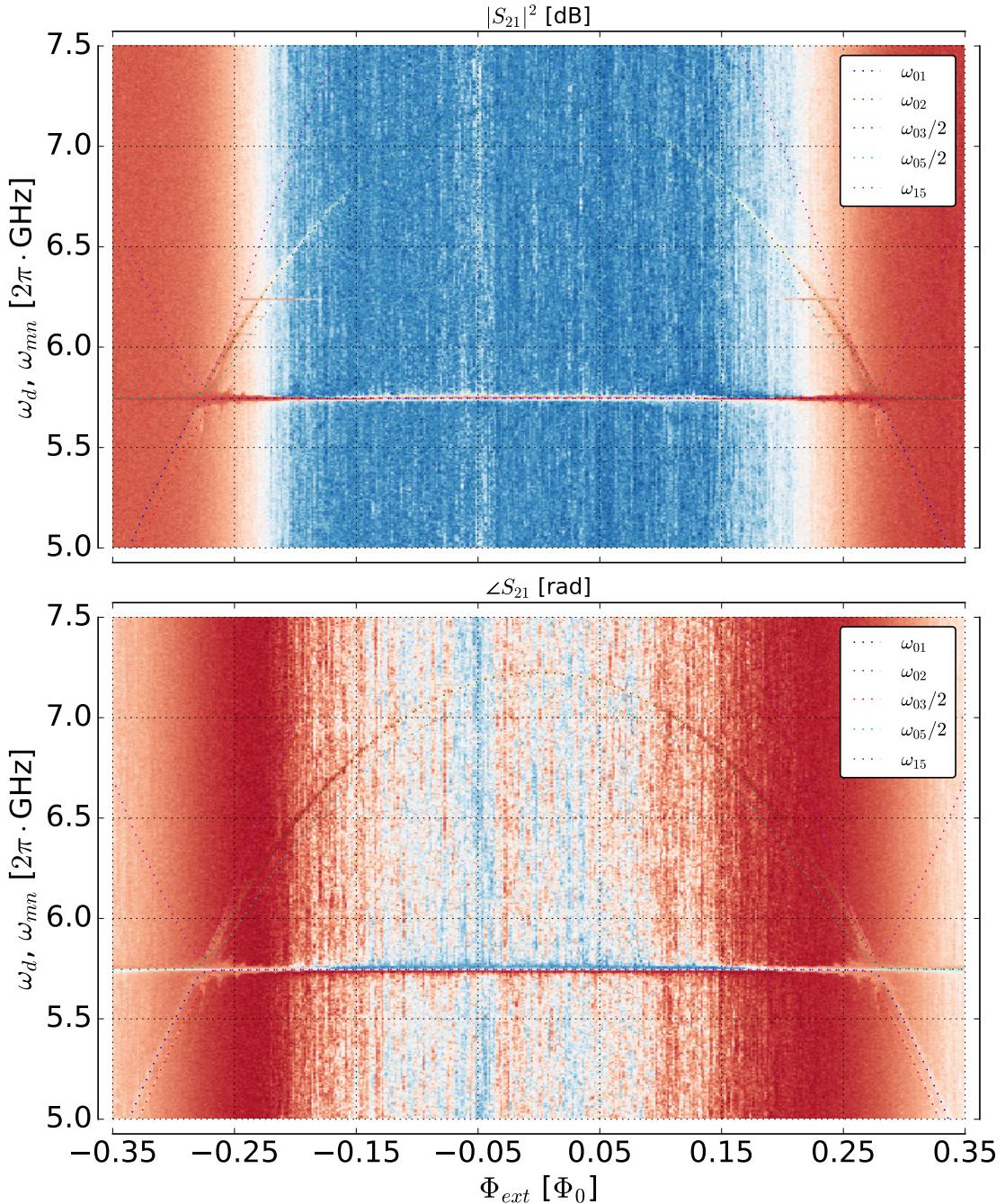
Below in the description of the figures a bit different notation for the transition frequencies may be used than those which denote the theoretical curves on the legends of the graphs. This is due to the fact that in the presence of coupling the qubit spectrum  $\omega_{ge}(\Phi_{ext})$  is shared between transitions  $\omega_{01}(\Phi_{ext})$  and  $\omega_{02}(\Phi_{ext})$  of the full Hamiltonian, so when we say  $\omega_{ge}(\Phi_{ext})$  we imply  $\omega_{01}(\Phi_{ext})$  and  $\omega_{02}(\Phi_{ext})$  for the cases of  $\Delta_\omega > 0$  and  $\Delta_\omega < 0$ , respectively.

**Anticrossing spectrum.** Firstly, a high-resolution scan of one of the anticrossings from Fig. 3.5 (II) was obtained. The power level on the VNA was set to -40.0 dBm, which means around -120 dBm at the sample. It is presented in Fig. 3.6. It can be seen that a really good agreement between experiment and theory was attained. However there are some discrepancies that can be pointed out: a slight asymmetry of the left and right anticrossings and the reduced brightness of the main branch  $\omega_{01}$  on the right. It can be seen clearly from the data that additional multi-photon transitions or sidebands are visible similar to what have been observed before<sup>7</sup> which indicates that the power was higher than at the single-photon level. Theoretical curves for those transitions were not displayed because the picture becomes too crowded. It is not clear why this effect is stronger in the right anticrossing than in the left one. Further investigation is needed, because at that cooldown due to the setup limitations measurements at lower power were too time consuming because of the low transmission.

**Two-tone spectroscopy.** Next measurement was a standard two-tone spectroscopy. The results of such measurement at different second tone powers are presented. Firstly, the lowest possible power (-20 dBm) scan was acquired, it is shown in Fig. 3.7. It was not possible to set a lower power with the step attenuator of the  $\mu$ -wave source, however for studied system that power was low enough to observe only single-photon processes without apparent multi-photon transitions and sidebands around the qubit's degeneracy point. However due to the fact that the second tone was introduced from the feedline through the resonator the effective driving power was increasing when the qubit-resonator detuning was decreasing;



**Figure 3.6:** Anticrossing spectrum of system II with fitting lines obtained by numeric calculation from the model(2.1) (z-axis normalized). It can be seen that lower branch has some artefacts near the anticrossings which are caused by multiphoton and sideband transitions, signifying that probe power was not at single-photon level. The x-axis is normalized to one flux quantum through the SQUID of the Xmon.

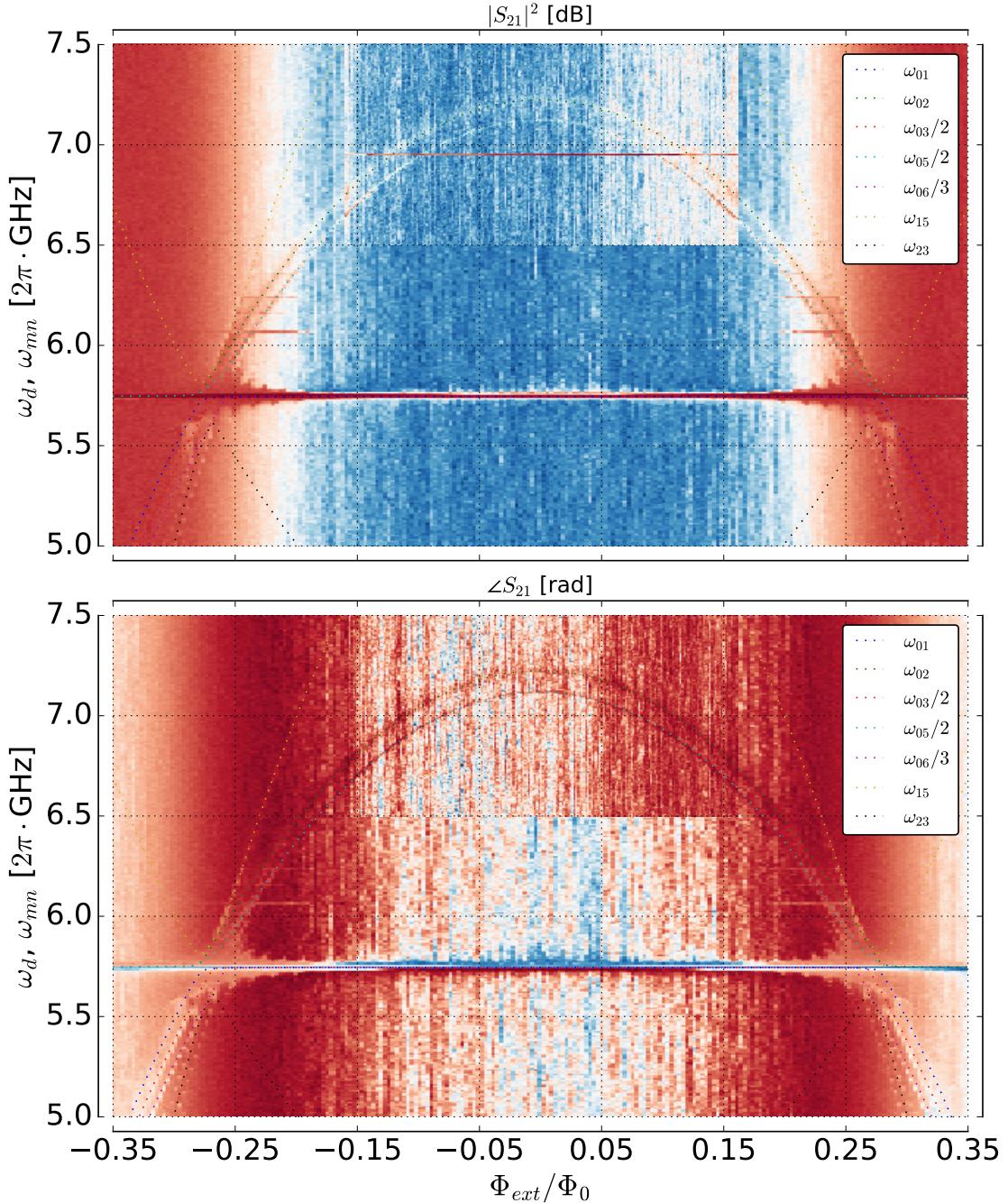


**Figure 3.7:** The two-tone spectrum of system II at -20 dBm power level on the  $\mu$ -wave source with fitting lines obtained from the model (2.1). Various transitions are visible, most pronounced are the horizontal resonator  $0n$  transition, the hyperbolic qubit  $ge$  transition ( $\omega_{01}$ ,  $\omega_{02}$ ) and lower branch of the hyperbolic two-photon  $gf$  transition ( $\omega_{03}/2$ ). Also a sideband  $|1, g\rangle \rightarrow |0, f\rangle$  is visible ( $\omega_{15}$ ).

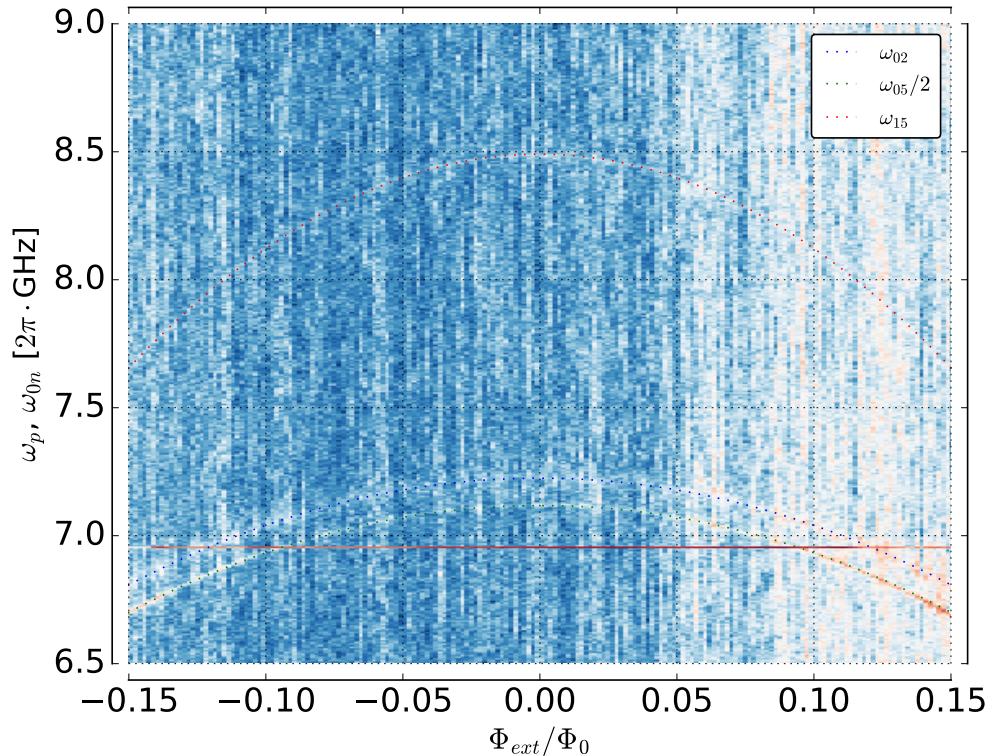
thus, some secondary transitions become visible near the anticrossing regions. For example, a sideband transition which uses one photon from a resonator and one photon from the incident microwave radiation ( $\omega_{15}$ ) is vaguely visible above the resonator line and a two-photon transition  $\omega_{gf}/2$  is clearly visible below it.

If the power of the second tone is increased, the probability of the transitions with lesser matrix elements also rises allowing to see these transitions more clearly. Such measurement yields a spectrum as in Fig. 3.8. It was done at -10 dBm; thus, a power 10 times higher than in the previous case was sent at the sample. Now the two-photon hyperbolic line  $\omega_{gf}$  under the main one  $\omega_{ge}$  is clearly visible (the upper complementary branch  $\omega_{05}/2$  of the previously visible transition  $\omega_{03}/2$ ). The upper branch of the sideband  $|1, g\rangle \rightarrow |0, f\rangle$  is visible also, see Fig. 3.9 for the scan around  $\Phi_{ext} = 0$ . Also there are two lines below the resonator at the sides of the graph whose origin is not clear. One of them might be the lower branch of that sideband (fit with  $\omega_{23}$  in Fig. 3.8), however it can be seen that the theoretical line is not very accurate there. The other line which is visible between  $\omega_{23}$  and  $\omega_{06}/3$  was not fit because no appropriate transition was found. Surely, one should be able to find it but this task looks hard enough to give it up.

Interestingly enough as well as the transition corresponding to the system's resonator some other narrow horizontal transitions are visible. Three of these lines are visible best of all around 6.1 GHz near the qubit line in Fig. 3.7 ( $|S_{21}^2|$ ) and near 7 GHz in the high-resolution area of Fig. 3.8 ( $|S_{21}^2|$ ). They correspond to the other resonators which lie higher in frequency. This effect was already observed before but was not thoroughly studied. At this moment it seems that the effect of changed transmission on the probe frequency when the other resonator is resonantly excited with large power (second tone power is  $10^4$ - $10^5$  times higher than the probe power) is not due to the coupling of the resonators but due to nonlinear effects or suppressed superconductivity in the Al film itself.



**Figure 3.8:** The two-tone spectrum of system II at -10 dBm power level on the  $\mu$ -wave source with fitting lines obtained from the model (2.1). More transitions are visible, new compared to Fig. 3.7 are the upper branch of the two-photon  $gf$  transition ( $\omega_{05}/2$ ), the lower branch of the three-photon  $gd$  transition ( $\omega_{06}/3$ ) and also the lower branch of the sideband  $|1, g\rangle \rightarrow |0, f\rangle$  ( $\omega_{23}$ ).



**Figure 3.9:** Zoomed area around the main qubit transition  $ge$ , two-photon transition  $gf$  and the sideband transition  $|1, g\rangle \rightarrow |0, f\rangle$  with fitting lines. Second tone power was -10 dBm, transmission amplitude is displayed.

## System VI

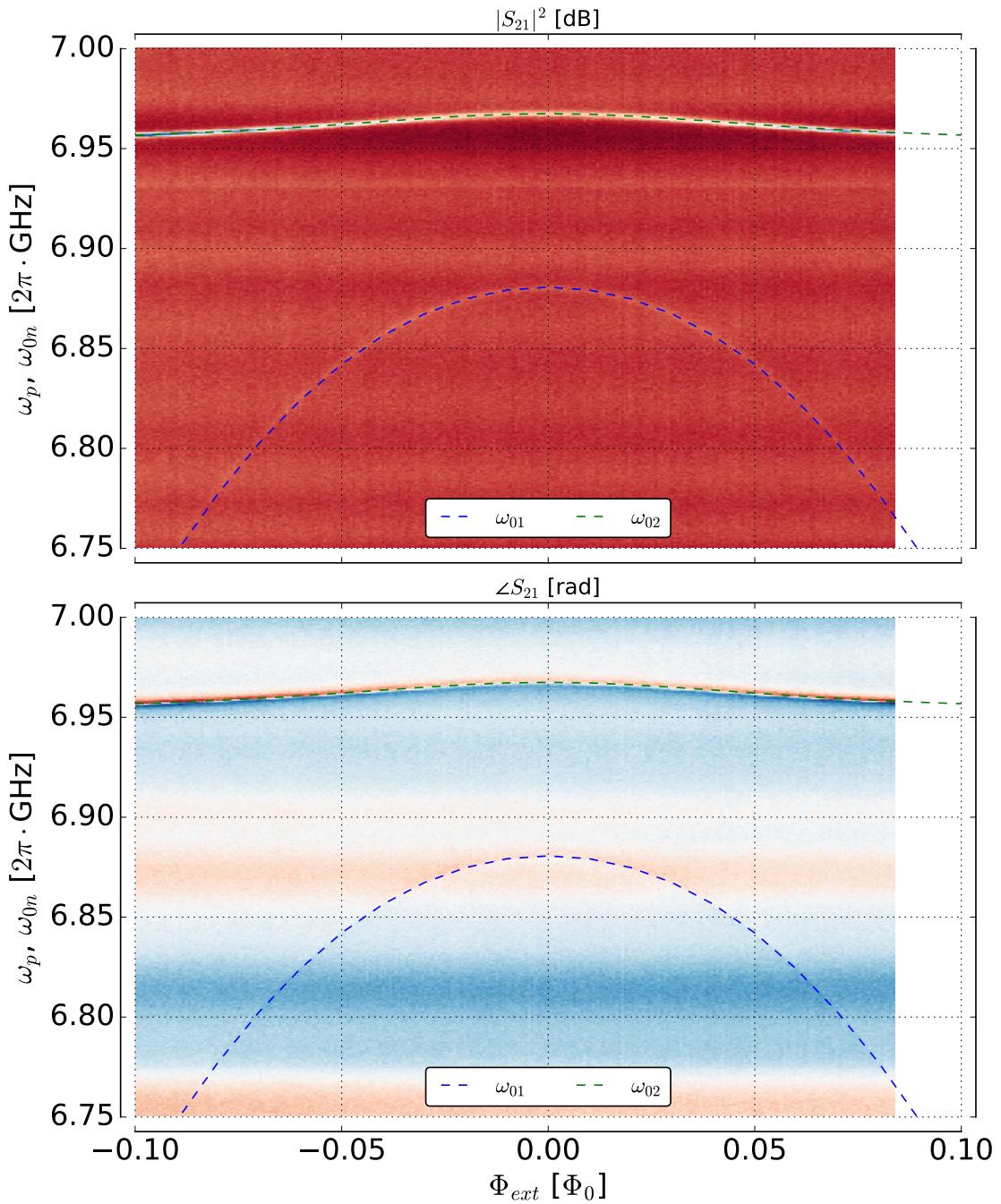
**Model.** Below all the experimental data will be provided for system VI along with theoretical fits of the spectral lines that were observed using the model (2.1). Model parameters were fit based on all data on this system and are same for all figures in this section. Before turning to the comparison of the theoretical predictions and experimental results it would be useful to present the model parameters used for fitting which are summarized in Table 3.2.

Parameter	Value	Parameter	Value
$C_\kappa$	0 fF	$C_r$	367 fF
$C_g$	1.8 fF	$L_r$	1.41 nH
$C_q$	95 fF	$I_{C,\Sigma}$	63.4 nA
$E_C$	200 MHz	$E_{J,\Sigma}$	31.5 GHz

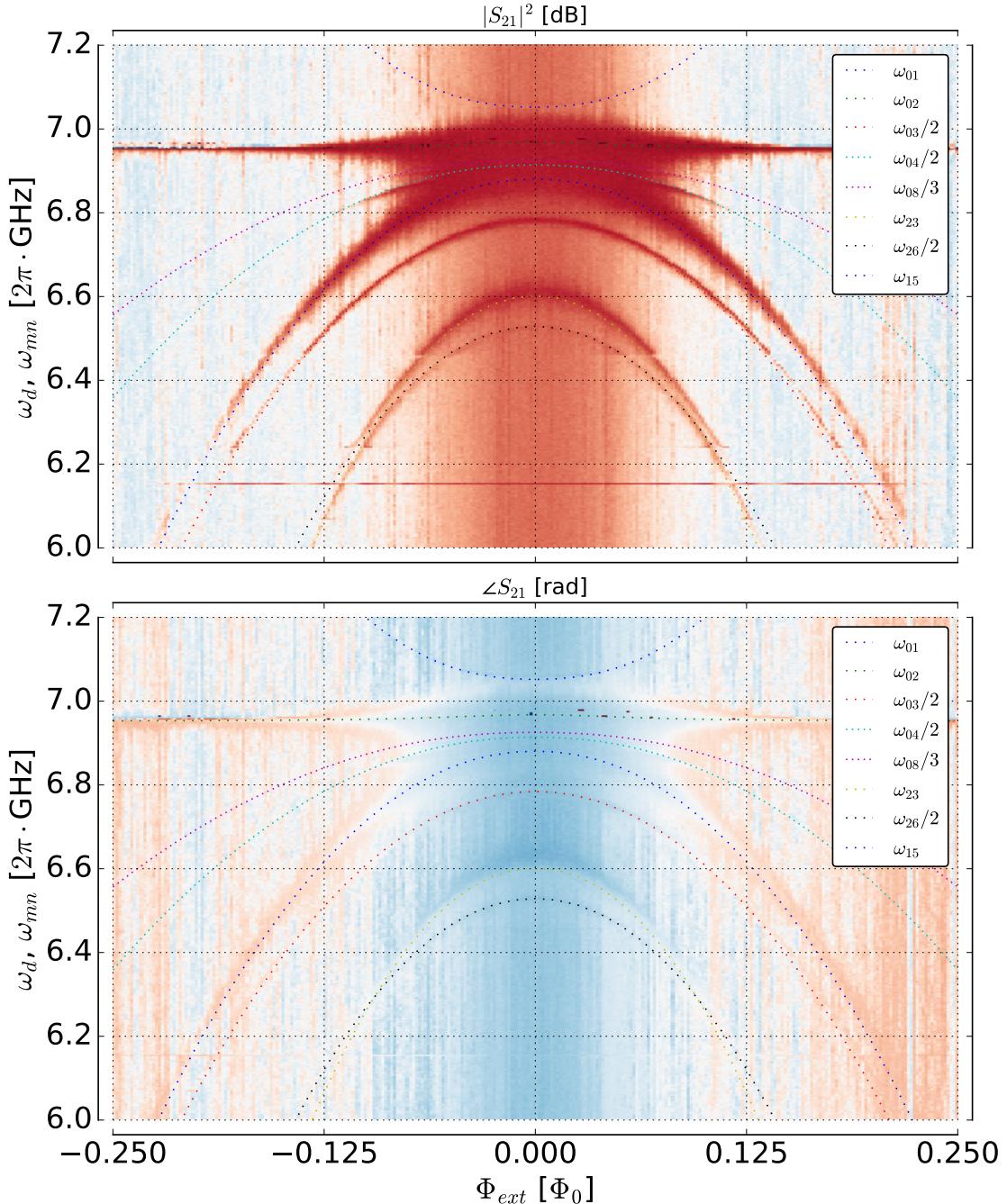
**Table 3.2:** Values of the main parameters defining the spectrum of the model (2.1).

**Anticrossing.** The anticrossing spectrum of the sixth system is presented in Fig. 3.10. It can be directly seen that the qubit is very close in frequency to its resonator; thus, the resonator line is bent slightly and the qubit line is looking ordinary. Using the theoretical model (2.1) these two lines were fit, and there's a good agreement between theory and data. It can be seen that at the degeneracy point, where the qubit is closest in frequency to the resonator, the resonator line becomes dimmer; it indicates that the qubit is less coherent than the resonator, reducing its Q-factor when approaching resonant interaction.

**Two-tone spectroscopy.** The results of the two-tone spectroscopy are presented in Fig. 3.11. It was performed at the lowest possible power of -20 dBm on the  $\mu$ -wave source, yet, due to a very small detuning of the qubit at the degeneracy point, the power in



**Figure 3.10:** Anticrossing spectrum for the 6<sup>th</sup> system (z-axis normalized) with fitting lines obtained from the model (2.1).

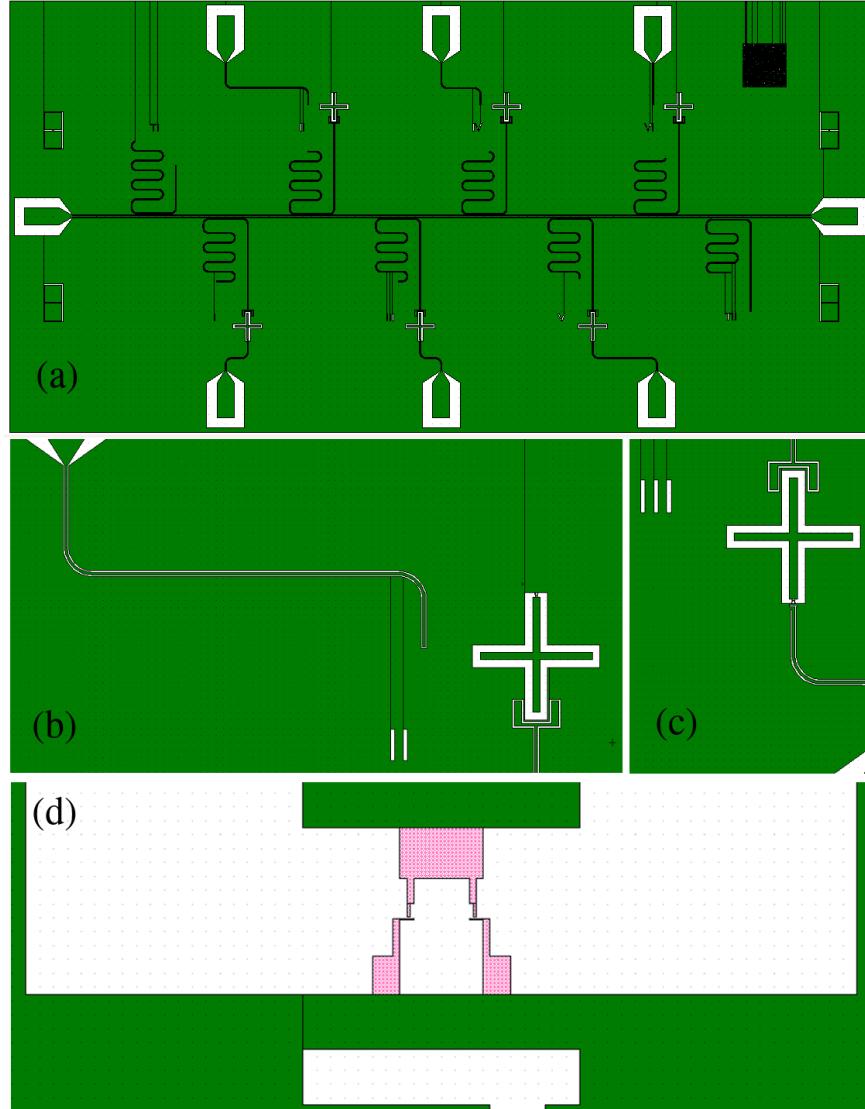


**Figure 3.11:** Two-tone spectrum of the 6<sup>th</sup> system (z-axis normalized) at -20 dBm on the  $\mu$ -wave source with fitting lines obtained from the model (2.1). As long as the qubit is very close to the resonator in frequency the effective driving power on it is very high, and thus a lot of sideband and multiphoton transitions are visible.

## 2 On-chip control lines testing design

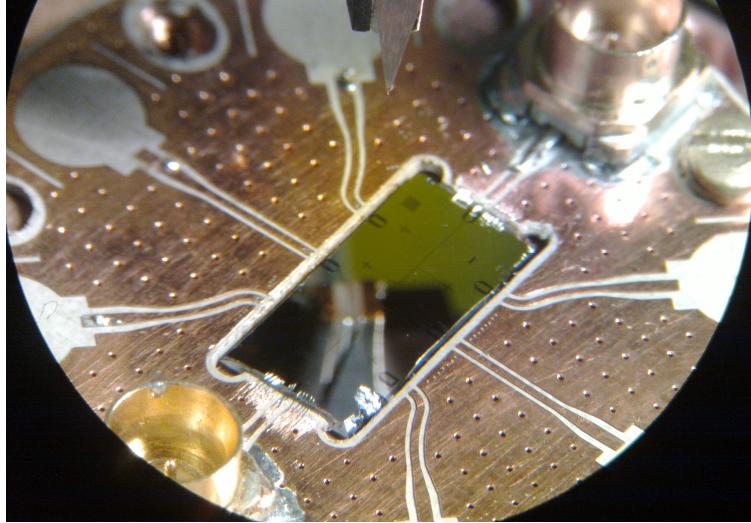
### 2.1 Geometry and parameters

The second design that was developed was intended to test the properties of the control lines, i.e. flux bias lines and microwave driving lines, implemented on the chip. The design is presented in Fig. 3.12 where some of its key features are highlighted. It's 10x5 mm.



**Figure 3.12:** (a) Large-scale image of the lines testing design. The chip (8x4 mm) consists of eight  $\lambda/4$  CPW resonators coupled capacitively to the feedline, six low- $Q_e$  with Xmon qubits at the open end and two high- $Q_e$  with no qubits. (b) Zoomed area around one of the qubits, showing the microwave antenna configuration. (c) Zoomed area around another qubit, showing the flux bias line. (d) Zoom around one of the qubits' SQUIDS. Pink areas denote the part of the mask which produces the SQUID and should be patterned with higher resolution.

Firstly, differently from the previous design, this design has more resonators, additional



**Figure 3.13:** Bonded Xmon Al BMSTU 1 in the PCB of the sample holder, as seen through the microscope of the bonding machine.

two (TI, TII, see Fig. 3.12(a)) were inserted at the ends of the main resonator-qubit array (I-VI). These resonators have high  $Q_e$  from their geometry to yield accurate results for possible high internal Q-factors.

Secondly, the frequencies of the devices were changed. The qubits still are all calculated to have the same frequency, but it's now 6 GHz, with  $C_{\Sigma} \approx 80$  fF and  $I_{C,\Sigma} = 40$  nA. The size of each junction in the qubit's SQUID is 100x200 nm<sup>2</sup>. The resonators had frequencies of 7, 7.1, 7.2, 7.3, 7.4, 7.5 GHz for the cQED systems I-VI, and the bare resonators TI and TII had 8 and 8.25 GHz, respectively.

Finally, as the main change made to the design, some coplanar control lines were introduced. For the upper qubits they are microwave antennas, i.e. open-ended coplanar line pieces, to induce transitions while for the lower qubits they are flux-bias lines to change the energy level structure of the devices. The lines were separated in such a way to make the design more fault-tolerant.

Four test structures at the sides of the chip were also included to allow direct DC measurement of the SQUIDs created during the shadow evaporation.

## 2.2 Implementation and purposes

The chip Xmon Al BMSTU 1 was made in a single-step process. It had a mask patterned with e-beam in the cleanroom facility at Bauman Moscow State Technical University (add recipe?), and then Al film was shadow-evaporated on Plassys in the RQC lab in ISSP, 25 and 45 nm thick. The substrate used was made of high-resistivity Si ( $> 6$  kOhm/cm).

One significant difference about this sample is that in fact it was fabricated with its twin in the center of a larger substrate (15x15 mm) which was previously patterned on the back side with a circular saw to allow the substrate to be cracked around the chips precisely. However, the process wasn't yet mastered and the twin chip was lost during the separation.

But nevertheless, the remaining sample fitted in the PCB cutout really well, and the method will be further improved.

Purposes for the design:

test resonator Q without qubits

test lines

test again the qubits' basic parameters

test improvement of the noise

test the half-sawing of the sample with following cracking

# Appendix A

## Pure dephasing or Does the density matrix really exist?

There are two ways of describing pure dephasing. One is developed from the system-bath approach (Lindbladian master equation) and the other comes from the stochastic Schrödinger equation. However the results of the latter deviate fundamentally from the results of the former for the experiment of spin-echo for a single qubit. Here this problem will be described in detail.

### 1 Quantum derivation of dephasing

For the derivation of this phase-destroying process in a quantum way the system-environment interaction Hamiltonian part is chosen as

$$\hat{\mathcal{H}}_{qe} = \hat{\sigma}_z \otimes \hat{O}_e,$$

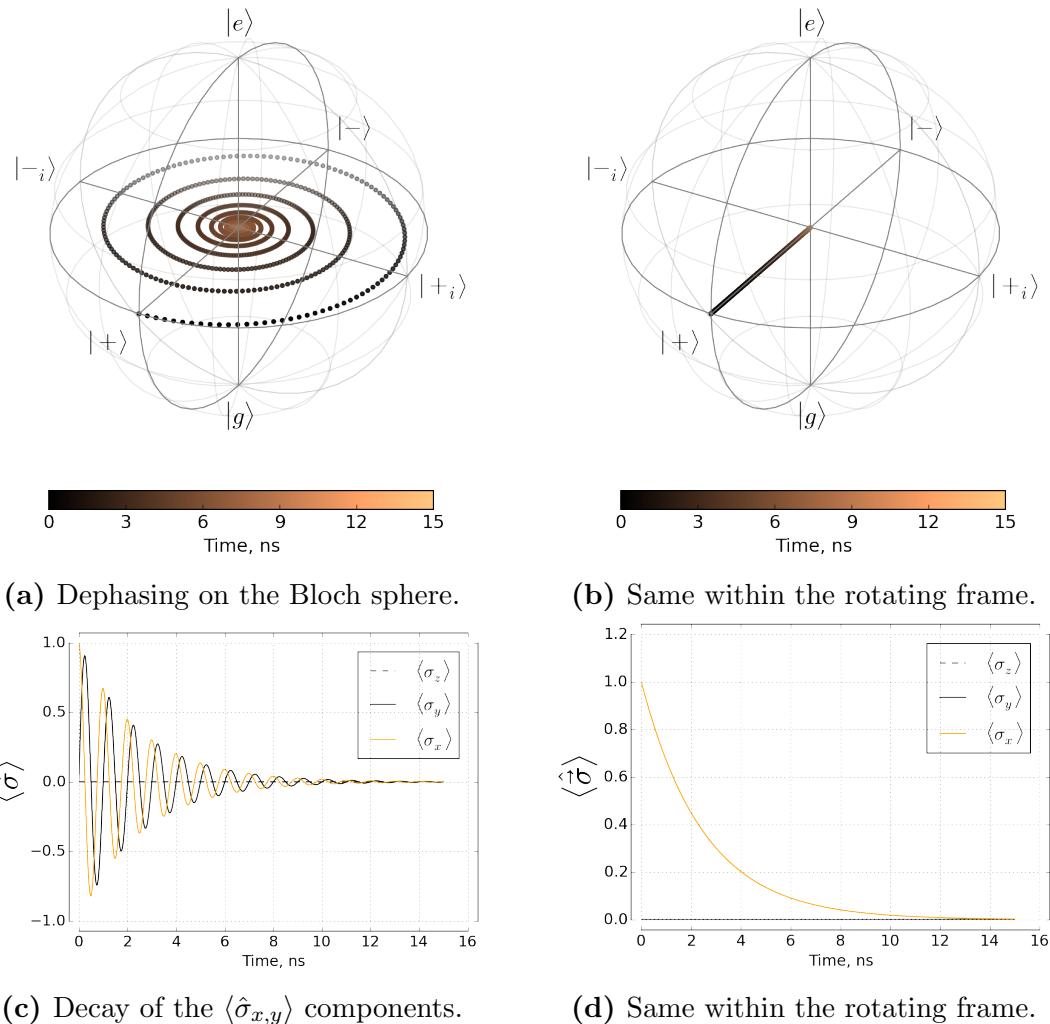
where  $\hat{O}_e$  is an arbitrary environment operator. From this interaction term a master equation is then developed:

$$\partial_t \hat{\rho}_s = \frac{i}{\hbar} [\hat{\rho}_s, \hat{\mathcal{H}}_s] + \gamma_\phi (\hat{\sigma}_z \hat{\rho}_s \hat{\sigma}_z - \hat{\rho}_s).$$

The dynamics of this equation can be seen in Fig. A.1. At  $t \rightarrow \infty$  the state of the system is a totally mixed state:

$$\hat{\rho}_s(\infty) = \begin{pmatrix} \rho_{11}(0) & 0 \\ 0 & \rho_{22}(0) \end{pmatrix}.$$

Following the open system approach this should be understood as the consequence of the entanglement of the qubit with the environment. The same density matrix we will obtain trying to find out in which state is the qubit  $A$  when it's a part of a composite system  $A \otimes B$  of two qubits being in a Bell state  $|\Psi^+\rangle = \frac{1}{\sqrt{2}}(|0\rangle_A \otimes |1\rangle_B + |1\rangle_A \otimes |0\rangle_B)$ . From the quantum point of view, therefore, the process of dephasing is irreversible.



**Figure A.1:** Dephasing treated quantum-mechanically shows exponential decrease of the coherences of the density matrix.

## 2 Classical derivation of dephasing

The classical derivation will be presented below in detail. This method, just as in the case of interaction of an atom with a classical field, just includes an additional time-dependent term in the Hamiltonian, representing fluctuations of the system's parameters. For the pure dephasing this term looks like  $f(t)\hat{\sigma}_z$ , where  $f(t)$  is the random noise. It is possible to write down the evolution of the density matrix for such stochastic Schrödinger equation. Until specified, the unitary evolution will be discussed, although using density matrix. In the rotating frame:

$$\hat{\rho}_s(t) = \hat{U}^\dagger(t, 0) \hat{\rho} \hat{U}(t, 0),$$

where

$$\hat{U}(t, 0) = \hat{T} \exp \left\{ -\frac{i}{\hbar} \int_0^t f(\tau) \hat{\sigma}_z d\tau \right\}.$$

From the fact that  $\hat{\sigma}_z$  is diagonal it can be shown that

$$\begin{aligned} \hat{\rho}_s(t) &= \begin{pmatrix} \exp \left\{ \frac{i}{\hbar} \int_0^t f(\tau_1) d\tau_1 \right\} & 0 \\ 0 & \exp \left\{ -\frac{i}{\hbar} \int_0^t f(\tau_1) d\tau_1 \right\} \end{pmatrix} \cdot \\ &\quad \cdot \begin{pmatrix} 1/2 - N(0)/2 & \rho(0) \\ \rho^*(0) & 1/2 + N(0)/2 \end{pmatrix} \cdot \\ &\quad \cdot \begin{pmatrix} \exp \left\{ -\frac{i}{\hbar} \int_0^t f(\tau_2) d\tau_2 \right\} & 0 \\ 0 & \exp \left\{ +\frac{i}{\hbar} \int_0^t f(\tau_2) d\tau_2 \right\} \end{pmatrix}, \end{aligned}$$

where the integral variables  $\tau_1$  and  $\tau_2$ , coherence  $\rho(t)$  and inversion  $N(t)$  were introduced. From above it is obvious that

$$N(t) = N(0), \tag{2.1}$$

$$\rho(t) = \rho(0) \exp \left\{ \frac{2i}{\hbar} \int_0^t f(\tau) d\tau \right\}. \tag{2.2}$$

This equations can be visualized with numerical simulation, taking  $f(t)$  be, for instance, normally distributed. The phase will experience random drifts, which lead to random rotations of the Bloch vector on the equator of the sphere, see Fig. A.2 (a), (c).

However, we can now use the other side of the density matrix, the property for which it is also called statistical operator. Let's run the equation (2.2) many times and look at the statistically expected state of the observed system over time. The diagonal part will still stay the same, and for coherence we have (presuming Gaussian instantaneous distribution of  $f(t)$  and  $x(t) = \frac{2}{\hbar} \int_0^t f(\tau) d\tau$ ):

$$\langle \rho(t) \rangle = \rho(0) \int_{-\infty}^{+\infty} e^{ix} \mathbb{N}_{0,\sigma}(x) dx = \rho(0) e^{-\sigma^2/2} = \rho(0) e^{-\langle x^2 \rangle / 2} \tag{2.3}$$

$$= \rho(0) \exp \left\{ -\frac{2}{\hbar^2} \int_0^t \int_0^t \langle f(\tau_1) f(\tau_2) \rangle d\tau_1 d\tau_2 \right\}. \tag{2.4}$$

Presuming also that  $f(t)$  is a wide-sense stationary process  $\langle f(\tau_1)f(\tau_2) \rangle = K_f(\tau_2 - \tau_1) = \frac{1}{\sqrt{2\pi}} \int_{\mathbb{R}} S_f(\omega) e^{i\omega(\tau_2 - \tau_1)} d\omega$  where  $S_f(\omega)$  is the power spectral density of  $f(t)$ . Taking the time integrals with the exponents, finally we obtain

$$\langle \rho(t) \rangle = \rho(0) \exp \left\{ -\frac{2}{\sqrt{2\pi}\hbar^2} \int_{\mathbb{R}} W_t^R(\omega) S_f(\omega) d\omega \right\}, \quad W_t^R(\omega) = \frac{4 \sin^2(\frac{\omega t}{2})}{\omega^2} \quad (2.5)$$

It can be shown easily that (2.5) is an exponent for either a white noise ( $S_f(\omega) = S_f(0) = \text{const}$ ) or for a sufficiently large time  $t$  where

$$\frac{t}{2} \int_{\mathbb{R}} d(\omega t/2) \frac{\sin^2(\frac{\omega t}{2})}{(\omega t/2)^2} \bullet$$

acts as  $\frac{t\pi}{2}\delta(\omega) \bullet$ . In both these cases the pure dephasing rate  $\Gamma_2^*$  exists in the usual sense and  $\Gamma_2^* \propto S_f(0)$ . In case of, for example, the 1/f noise the decay curve will behave as  $e^{-t^2}$  in the vicinity of  $t = 0$ .

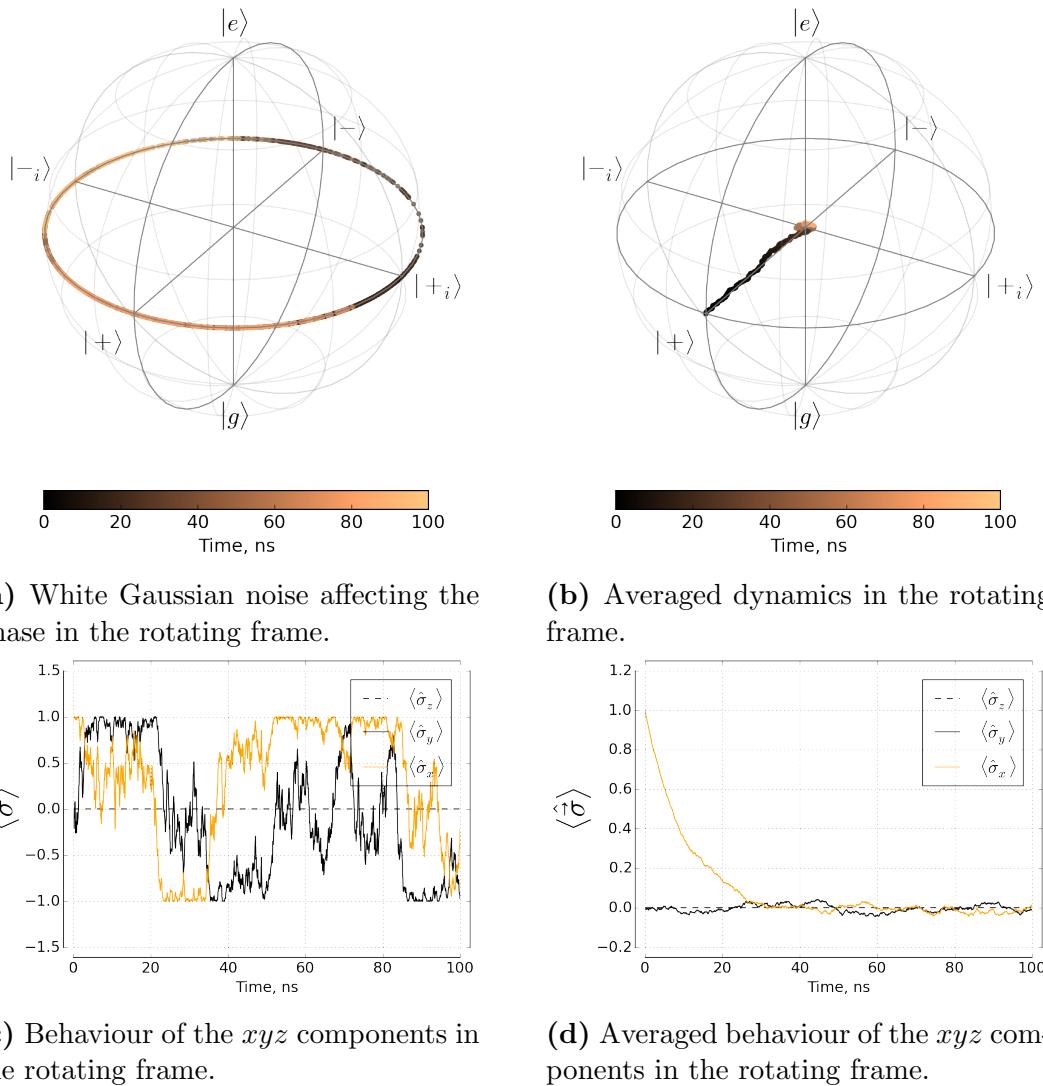
The averaged evolution for the white noise case can be observed in Fig. A.2 (b), (d). It is very similar to what can be seen in Fig. A.1. 1000 trajectories were used for averaging. In Fig. A.3 the simulation of the dynamics under the 1/f noise is shown. For the averaged case ((b), (d)) 2500 trajectories were used. One can see that a plateau is present for the yellow graph near  $t = 0$ , in accordance with theoretical predictions.

### 3 Spin-echo experiment

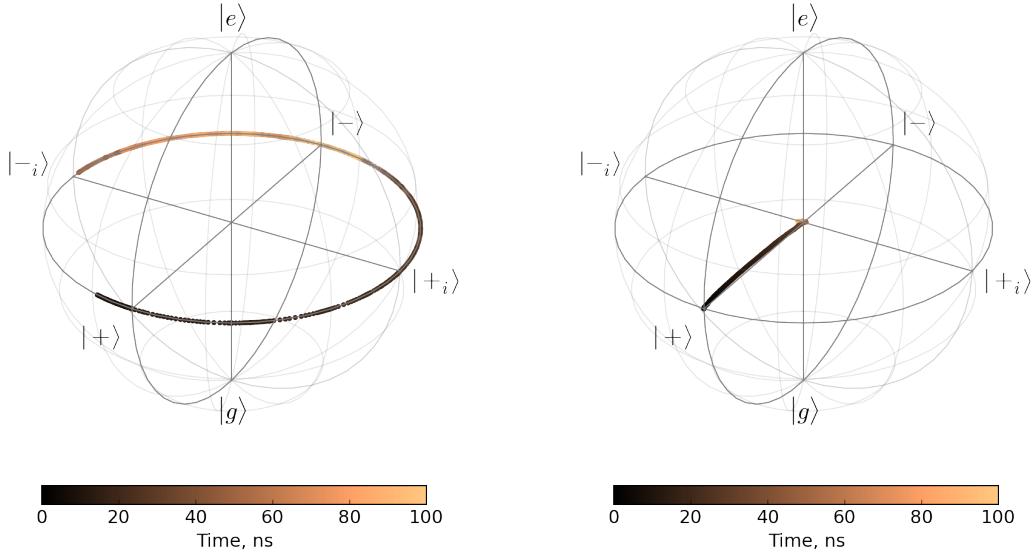
The spin-echo experiment in the simplest case (Hahn echo) is a modification of a Ramsey pulse sequence with an additional  $\pi_y$ -pulse right in between the  $\frac{\pi}{2}_x$  ones. The idea is that during the second period (after the  $\pi_y$ -pulse) slow components of the noise will cancel out the phase difference they've imposed during the first period. This can be understood easily in the limit of constant noise and infinitely fast rotations. There are also more sophisticated echo sequences such as CP, CPMG and UDD<sup>11</sup> which use more than one  $\pi_y$ -pulse during the free evolution, however for our case it is enough to regard the simplest Hahn echo.

Mathematically Hahn echo within the previous formulations acts as follows. Before the  $\pi_y$ -pulse at time  $t/2$  we have the same dynamics described by the (2.2). Then instantaneously the coherences of the density matrix are complex conjugated as a result of an infinitely fast  $\pi_y$ -pulse. This can be understood from the result of  $\pi_y$ -pulse on the Bloch sphere:  $\langle \hat{\sigma}_x \rangle = \rho + \rho^* \xrightarrow{\pi_y} \langle \hat{\sigma}_x \rangle$ ,  $\langle \hat{\sigma}_y \rangle = i(\rho - \rho^*) \xrightarrow{\pi_y} -\langle \hat{\sigma}_y \rangle$ ,  $\langle \hat{\sigma}_z \rangle = N \xrightarrow{\pi_y} \langle \hat{\sigma}_z \rangle$ . Finally, for the changed initial condition at  $t/2$  again evolution (2.2) is applied. Therefore, at the end of the period the coherence is defined as

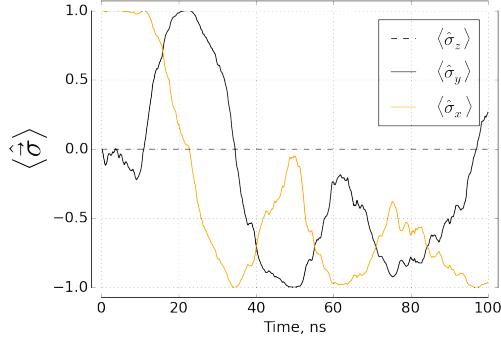
$$\rho(t) = \rho(0) \exp \left\{ -\frac{2i}{\hbar} \int_0^{t/2} f(\tau) d\tau + \frac{2i}{\hbar} \int_{t/2}^t f(\tau) d\tau \right\}.$$



**Figure A.2:** Classically treated pure dephasing for white noise.

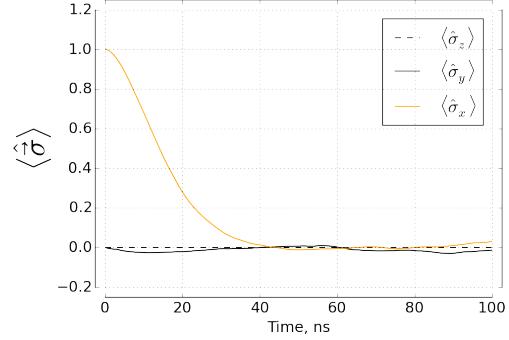


(a) 1/f Gaussian noise affecting the phase in the rotating frame.



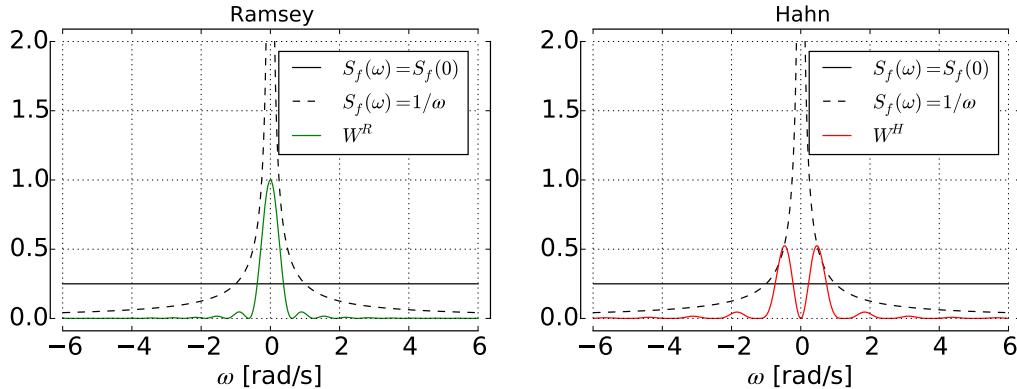
(c) Behaviour of the  $xyz$  components in the rotating frame.

(b) Averaged dynamics in the rotating frame.



(d) Averaged behaviour of the  $xyz$  components in the rotating frame.

**Figure A.3:** Classically treated pure dephasing for 1/f noise.



**Figure A.4:** Qualitative plot for noise PSD filtration at  $t = 10$  s.

Performing the ensemble averaging one can get

$$\langle \rho(t) \rangle = \rho(0) \exp \left\{ -\frac{2}{\hbar^2} \left\langle \left( \int_0^{t/2} f(\tau_1) d\tau_1 + \int_{t/2}^t f(\tau_2) d\tau_2 \right) \cdot \left( \int_0^{t/2} f(\tau_3) d\tau_3 + \int_{t/2}^t f(\tau_4) d\tau_4 \right) \right\rangle \right\}.$$

Expanding the brackets, again putting a Fourier transform of the power spectral density  $S_f(\omega)$  instead of the autocorrelation functions and factoring the expression back to the initial representation it is possible to obtain<sup>12</sup> the final expression for the coherence expectation:

$$\langle \rho(t) \rangle = \rho(0) \exp \left\{ -\frac{2}{\sqrt{2\pi}\hbar^2} \int_{\mathbb{R}} S_f(\omega) W_t^H(\omega) d\omega \right\}, \quad (3.1)$$

where

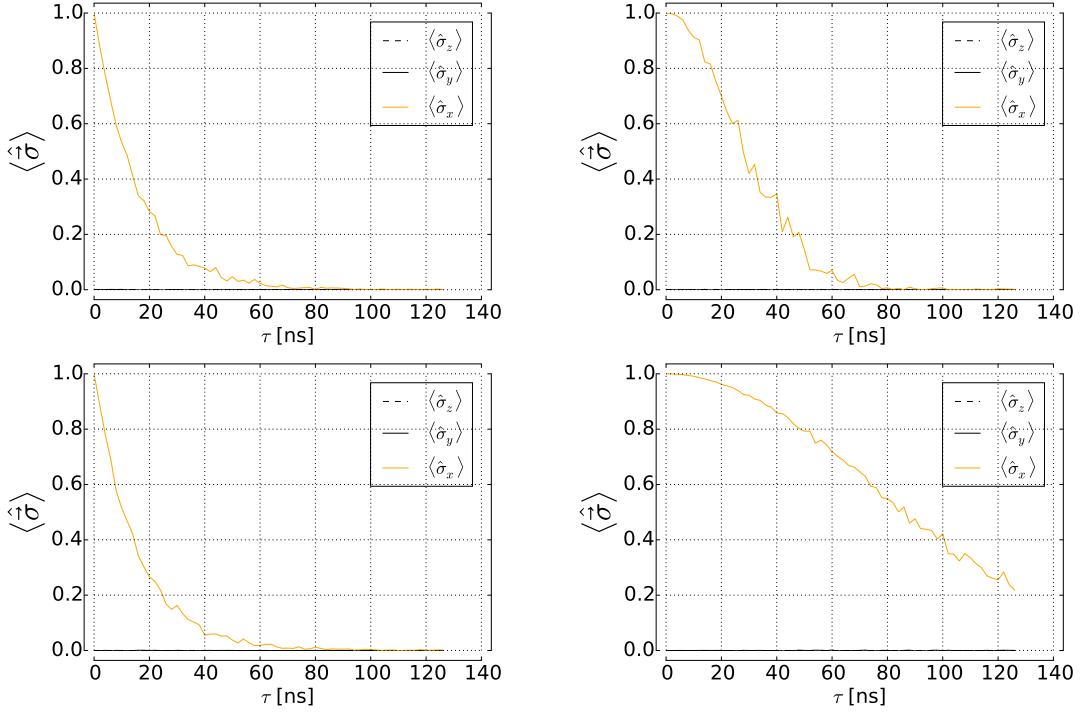
$$\begin{aligned} W_t^H(\omega) &= \left| - \int_0^{t/2} e^{i\omega\tau} d\tau + \int_{t/2}^t e^{i\omega\tau} d\tau \right|^2 \\ &= \left| 1 - 2e^{i\omega t/2} + e^{i\omega t} \right| \\ &= \left| \frac{(1 - e^{i\omega t/2})(1 + e^{i\omega t/2})(1 - e^{i\omega t/2})}{(1 + e^{i\omega t/2})} \right| \\ &= \tan^2(\omega t/4) \frac{4 \sin^2(\omega t/2)}{\omega^2}. \end{aligned}$$

It's obvious from (3.1) that the noise influence is now suppressed at low frequencies (compare with (2.5)) however it is enhanced at some higher frequency. This leads to inefficiency of Hahn echo and similar techniques when the noise is white and a good  $T_2^*$  improvement when it's 1/f, see Fig. A.5.

## 4 The problem (of Markovian MEs)

The interesting correspondence between quantum and classical derivation can be noted within the spin echo experiment. For the white noise both of the descriptions yield same results, the exponential decay of coherences with an equal rate. However the meanings of these two results are completely different. Quantum approach tells us that the density matrix will emerge even in a single experiment as a consequence of entanglement with the environment. Classical approach tells us that everything that happens to the system in a single experiment is unitary, and if we knew the noise beforehand, we would be able to find out what state the qubit ended his evolution in at every final time  $t$ . Classical description only knows that the noise is white, non-correlated – and this same idea is used in the derivation of the master equation when Markov approximation is applied.

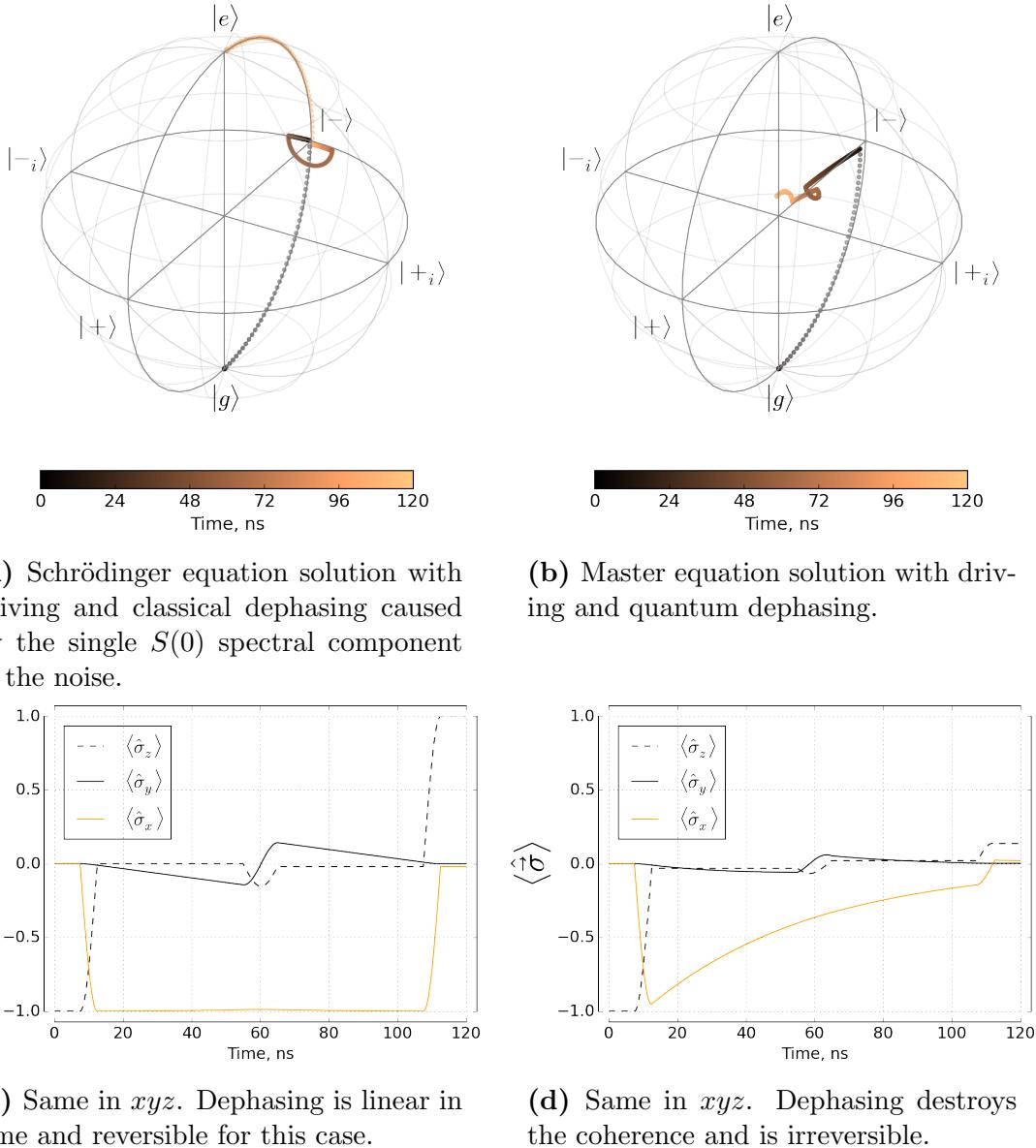
This correspondence is lucky, but what happens if the noise *is* correlated? The classical model now allows for (at least partially) reversible dynamics. In contrast, the entanglement



**Figure A.5:** Decoherence under white (left) and 1/f (right) noises with (bottom) and without (top) a refocusing  $\pi_y$ -pulse.

process is completely irreversible, so the quantum model should not simply entangle the system with the environment for the correlated bath.

At this point it is safe to say that density matrix really exists (that means it is not just a way to describe statistical distribution of states, but is the only approach to describe an open quantum system), but the quantum model of decoherence for the correlated noise should go beyond the Markovian master equations to keep up with experiments and naive (but still correct!) classical description.<sup>13</sup>



**Figure A.6:** Classical versus quantum spin-echo experiment modelling. Spin-echo can't cope with quantum noise.

# Bibliography

- <sup>1</sup> Coplanar waveguide resonators for circuit quantum electrodynamics / M. Goppl, A. Fragner, M. Baur et al. // Journal of Applied Physics. — 2008. — Vol. 104, no. 11. — P. 1–8. — 0807.4094. (referenced on p. [5 and 8])
- <sup>2</sup> Pozar D. M. Microwave Engineering, copyright 2012 by John Wiley & Sons. — Inc. (referenced on p. [5, 7 and 9])
- <sup>3</sup> Kiselev E. Design and Measurement of Superconducting Spiral Microwave Resonators : Ph. D. thesis / E. Kiselev. — 2013. (referenced on p. [7])
- <sup>4</sup> Bader S. The Transmon Qubit Theory. — 2013. (referenced on p. [10])
- <sup>5</sup> Charge insensitive qubit design derived from the Cooper pair box / J. Koch, Terri M. Yu, Jay M. Gambetta et al. — 2007. — P. 21. — 0703002. (referenced on p. [10])
- <sup>6</sup> Devoret M. H. Quantum fluctuations in electrical circuits // Les Houches, Session LXIII. — 1995. — URL: [http://www.physique.usherb.ca/tremblay/cours/PHY-731/Quantum\\_circuit\\_theory-1.pdf](http://www.physique.usherb.ca/tremblay/cours/PHY-731/Quantum_circuit_theory-1.pdf). (referenced on p. [11])
- <sup>7</sup> Johansson J. R., Nation P. D., Nori F. QuTiP: An open-source Python framework for the dynamics of open quantum systems. — 2011. — 1110.0573v2. (referenced on p. [10])
- <sup>8</sup> Sank D. T. Fast, Accurate State Measurement in Superconducting Qubits : Ph. D. thesis / D. T. Sank. — 2014. (referenced on p. [21])
- <sup>9</sup> Efficient and robust analysis of complex scattering data under noise in microwave resonators / S Probst, FB Song, PA Bushev et al. // Review of Scientific Instruments. — 2015. — Vol. 86, no. 2. — P. 024706. (referenced on p. [21])
- <sup>10</sup> Improving the coherence time of superconducting coplanar resonators / H Wang, M Hofheinz, J Wenner et al. // Applied Physics Letters. — 2009. — Vol. 95, no. 23. — P. 233508. (referenced on p. [21])
- <sup>11</sup> Dynamical decoupling and noise spectroscopy with a superconducting flux qubit / Jonas Bylander, Simon Gustavsson, Fei Yan et al. // Nature Physics. — 2011. — Vol. 7, no. 7. — P. 21. — 1101.4707. (referenced on p. [39])
- <sup>12</sup> Preskill J. Notes on noise. — URL: [http://www.theory.caltech.edu/people/preskill/papers/decoherence\\_notes.pdf](http://www.theory.caltech.edu/people/preskill/papers/decoherence_notes.pdf). (referenced on p. [42])

<sup>13</sup> Zurek Wojciech Hubert. Decoherence, einselection, and the quantum origins of the classical // *Reviews of Modern Physics*. — 2003. — Vol. 75, no. 3. — P. 715–775. — 0105127. (referenced on p. [43])