Forte Element Method unch Bovi - KI) WI) elemental statre equilibrium equation of local diplacements.

As sulate local and
1 should condition
Compatibility expodres condition to relate doced and global displacements
global angli
4 4 4 10 2 4 5 4
1,2 un = u,3 = u, = u,
$u_{1}^{2} = u_{1}^{2} = u_{1}^{3} = u_{1}^{4} = u_{1}^{3} = u_{2}^{2} = u_{1}^{2} = u_{2}^{3}$
5 4 5 - 110
u24= u25= u3
- 11
Equilibram of forces at nodes are
01 0 0 1.02.03.04= p P2+R2+R=R2
Ri= Ro, Ro+ Ri2+ Ri3+Ri4=R, R2+R2+R2+R2=R2
$-R_2^{9}+R_2^{5}=R_3$
Equilibration forces con be written as
1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Ro = Kiuo - Kiui - 1
No = 2,000 117 117
R1 = - K, 40+ K, 14, + K241 + K242 + K341 - K342+ K441 - K448
KI = - KINDT HOLL TO THE PARTY OF THE PARTY
R, z - K, Uo + [K, + K2 + K2 + Ku] U1 - (K2 + K3) U2 - KuU3
K, z - Kidor (Ki z - Kidor)
R2 = - K24, + K242 - K34, + K542 + K542 - K543
5 (r + K2 + K2 + KC 40 - X3)
R2 = - (1C3+K3) U, + (K2+K3+K5) U2 - K5 U3 -> 3
- B = = Kuu + Kuus - 16542 + K543 = - K441 - K542 + (ku+45)4
The state of the s
Equilibrium equation of system is (from equa-er)
Rolling Rolling Rolling
) R. (N. C. Fr. HOLLIN) - G. F. H.
of Ri b = - Ki (Ki + Ki + Ki) + - (Ke+ Ks) - Ky / U,
(F2) 0 - (C2+ K3) 1 K2+ K3+K5 - K5) 42
$ \begin{cases} R_0 \\ R_1 \\ R_2 \end{cases} = \begin{cases} K_1 \\ -K_1 \\ (K_1 + K_2 + K_3 + K_4) \end{cases} - (K_2 + K_3) - (K_4 + K_5) - (K_4) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} = \begin{pmatrix} K_1 \\ -K_2 + K_3 + K_4 \end{pmatrix} - (K_2 + K_3) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} = \begin{pmatrix} K_1 \\ -K_2 + K_3 \end{pmatrix} - (K_3 + K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} = \begin{pmatrix} K_1 \\ -K_2 \\ K_3 \end{pmatrix} - (K_3 + K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} - (K_3 + K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} - (K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} - (K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \\ K_3 \end{pmatrix} - (K_5) $ $ \begin{pmatrix} K_1 \\ K_2 \end{pmatrix} - (K_5) $ $ \begin{pmatrix} K_1$
- 1cs (Ku+1ks) (3)

Considering element O, D & . which are morable, the equilibrium legrection of system is written as - Ky (for the) + 1 (or the) + (By energy method was - was - was blockdone. WKT, Potential Energy & Krain Energy for each element T1= 1 K1 (u2-u1) - P1 u1 - R2 u21 (11) 72 = - 12 K2 (42 - 42) - Ri2u,2 - R22u22 13 = 1 12 K2 (423 - 43) - RB43 - R242 + (11-11) = 16 Tu = 1 ka (u2 - u14) - Ry quy - Rzy w24 75 = 1 K5 (425-45) - 18,5 45 - 1825 45 compatibility audition of local of global diplacement relation $u_1 = u_0$, $u_2 = u_1^2 = u_1^2 = u_1^2 = u_1^2 = u_2^2 = u$ R'= Ro, Ri R2 + R1 + R1 + R1, R2 = R2 + R2 + R25 R3 = R24+ R25 10 mothers 16 vortages (n) [3] = (1)

There equation becomes,

$$K = \frac{1}{2} \left[K_1 \left(u_1 - u_0 \right)^2 + \kappa_2 \left(u_2 - u_1 \right)^2 + \kappa_3 \left(u_2 - u_1 \right)^2 + \kappa_4 \left(u_3 - u_2 \right)^2 \right]$$
 $+ \kappa_2 \left(u_1 - u_0 \right)^2 + \kappa_2 \left(u_2 - u_1 \right)^2 + \kappa_3 \left(u_2 - u_1 \right)^2 + \kappa_4 \left(u_3 - u_2 \right)^2 + \kappa_5 \left(u_3 - u_3 \right)^2 + \kappa_5 \left(u_3 - u_3 \right) + \kappa_5 \left(u_3 - u$

$$\begin{cases} R_{0} \\ R_{1} \\ R_{2} \\ R_{3} \end{cases} = \begin{cases} R_{1} & -K_{1} & 0 & 0 \\ -K_{1} & K_{1} + K_{2} + K_{3} + K_{4} & -(K_{2} + K_{3}) & -K_{4} \\ 0 & -(K_{2} + K_{3}) & K_{2} + K_{3} + K_{5} & -K_{5} \\ 0 & -K_{4} & -K_{5} & (K_{4} + K_{5}) & W_{4} \end{cases}$$

$$\begin{cases} R_{0} \\ R_{1} \\ R_{2} \\ R_{3} \end{cases} = \begin{cases} R_{1} & -K_{1} & 0 & 0 \\ -K_{1} & K_{2} + K_{3} + K_{4} & -(K_{2} + K_{3}) & -K_{4} \\ 0 & -K_{4} & -K_{5} & (K_{4} + K_{5}) & W_{4} \end{cases}$$

$$\begin{cases} R_{0} \\ R_{1} \\ R_{2} \\ R_{3} \end{cases} = \begin{cases} R_{1} & -K_{1} & 0 & 0 \\ -K_{2} + K_{3} + K_{5} & -K_{5} \\ -K_{5} & -K_{5} & -K_{5} \\ -K_{4} & -K_{5} & -K_{5} \end{cases}$$

$$\begin{cases} R_{0} \\ R_{1} \\ R_{2} \\ R_{3} \end{cases} = \begin{cases} R_{1} & -K_{1} & 0 & 0 \\ -K_{2} + K_{3} & -K_{5} \\ -K_{5} & -K_{5} & -K_{5} & -K_{5} \\ -K_{5} & -K_{5} & -K_{5} & -K_{5} \\ -K_{5} & -K_{5} & -K_{5} \\ -K_{5} & -K_{5} & -K_{5} \\ -K_{5} & -K_{5} & -K_{$$

for 3 denent

$$\begin{cases}
R_{1} \\
R_{2}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-(K_{2} + K_{3}) & K_{2} + K_{3} + 1K_{5} & -1C_{5} \\
-K_{4} & -K_{5}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
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-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} + K_{4}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} + K_{4}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} + K_{4}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} + K_{4}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + K_{4} + 1K_{4} + 1K_{4} + 1K_{4} + 1K_{4}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{4} + 1K_{4} + 1K_{4} + 1K$$

2. Matlab Code

```
%.....
% MATLAB codes for Finite Element Analysis
% Discrete_Systems.m
% clear memory
clear all
% elementNodes: connections at elements
elementNodes=[1 2;2 3;2 3;2 4;3 4];
% numberElements: number of Elements
numberElements=size(elementNodes,1);
% By using the MATLAB function size, that returns the number
% of lines and columns of a rectangular matrix, we can detect
%the number of elements by inspecting the number of lines of
%matrix elementNodes.
% numberNodes: number of nodes
numberNodes=4;
% for structure:
% displacements: displacement vector
% force : force vector
% stiffness: stiffness matrix
% initializing the matrices
displacements=zeros(numberNodes,1);
force=zeros(numberNodes,1);
stiffness=zeros(numberNodes);
% applied load at node 2
force(2)=1;
force(3)=1;
force(4)=1;
```

```
% computation of the system stiffness matrix
% We compute now the stiffness matrix for each element in turn and then assemble
% it in the global stiffness matrix.
for e=1:numberElements;
% elementDof: element degrees of freedom (Dof)
elementDof=elementNodes(e,:);
stiffness(elementDof,elementDof)=stiffness(elementDof,elementDof)+[1-1;-11]
end
% boundary conditions and solution
% prescribed dofs
prescribedDof=1;
% free Dof: activeDof
activeDof=setdiff([1:numberNodes],[prescribedDof]);
% solution
displacements=stiffness(activeDof,activeDof)\force(activeDof);
% positioning all displacements
displacements1=zeros(numberNodes,1);
displacements1(activeDof)=displacements;
% output displacements/reactions
outputDisplacementsReactions(displacements1, stiffness, numberNodes, prescribedDof)
function outputDisplacementsReactions...
(displacements, stiffness, GDof, prescribedDof)
% output of displacements and reactions in
% tabular form
% GDof: total number of degrees of freedom of
% the problem
% displacements
disp('Displacements')
%displacements=displacements1;
ij=1:GDof; format
[jj' displacements]
% reactions
F=stiffness*displacements;
reactions=F(jj);
disp('reactions')
[jj' reactions]
end
```

Output

Stiffness

ans = 4×4

1 -1 0 0

-1 4 -2 -1

0 -2 3 -1

0 -1 -1 2

Displacements

ans =
$$4 \times 2$$

1.0000 0

2.0000 3.0000

3.0000 3.6000

4.0000 3.8000

Reactions

ans = 4×2

1.0000 -3.0000

2.0000 1.0000

3.0000 1.0000

4.0000 1.0000

Displacements:

Displacement of node 2 = 3

Displacement of node 3 = 3.60

Displacement of node 4 = 3.80

Reaction Forces:

Reaction force at node 1 = -3

2. (b) Green
$$K_1 = K_2 = K_3 = K_4 = K_5 = 1 ...$$

R₁ = R₂ = R₃ = 1.

from equilibrium equatron of system.

$$\begin{cases}
R_{0} \\
R_{1}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{1} & K_{1} + K_{2} + K_{3} & -(K_{2} + E_{3})^{3} & -K_{4} \\
0 & -(IC_{2} + K_{3}) & IC_{2} + K_{3} + K_{5} & -K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5} & -K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & K_{2} + E_{3}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & K_{2} + E_{3}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & K_{2} + E_{3}
\end{cases}$$

$$\begin{cases}
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C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & K_{2} + E_{3}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & K_{2} + E_{3}
\end{cases}$$

$$\begin{cases}
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C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2}
\end{cases}$$

$$\begin{cases}
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C_{3}
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$$\begin{cases}
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K_{1} - K_{2}
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$$\begin{cases}
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\end{cases} = \begin{cases}
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$$\begin{cases}
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\end{cases} = \begin{cases}
K_{1} - K_{2}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2}
\end{cases}$$

$$K_{2} + K_{3}
\end{cases}$$

$$\begin{cases}
K_{1} - K_{2}
\end{cases}$$

$$K_{2} + K_{3}
\end{cases}$$

$$K_{3} + K_{3}
\end{cases}$$

$$K_{2} + K_{3}
\end{cases}$$

$$K_{3} + K_{3}
\end{cases}$$

$$K_{4} + K_{3}
\end{cases}$$

$$K_{2} + K_{3}
\end{cases}$$

$$K_{3} + K_{3}
\end{cases}$$

$$K_{4} + K_{3}
\end{cases}$$

$$K_{3} + K_{3}
\end{cases}$$

$$K_{4} + K_{3}$$

$$K_{4} + K_{3}
\end{cases}$$

$$K_{4} + K_{3}$$

$$K_{4} + K_{4}$$

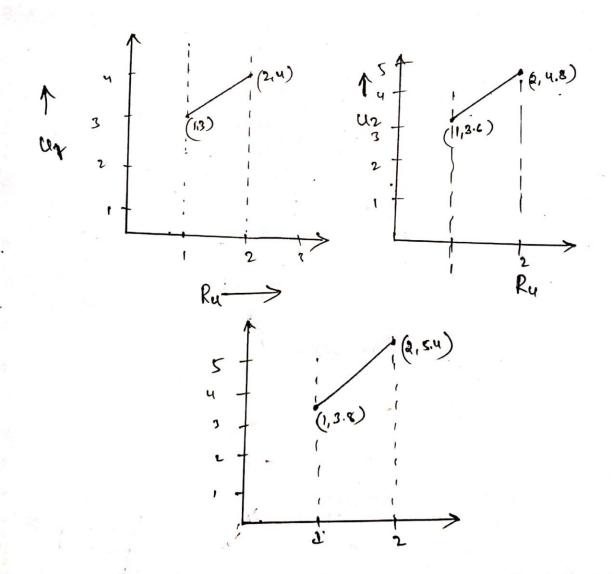
$$K_{4} + K$$

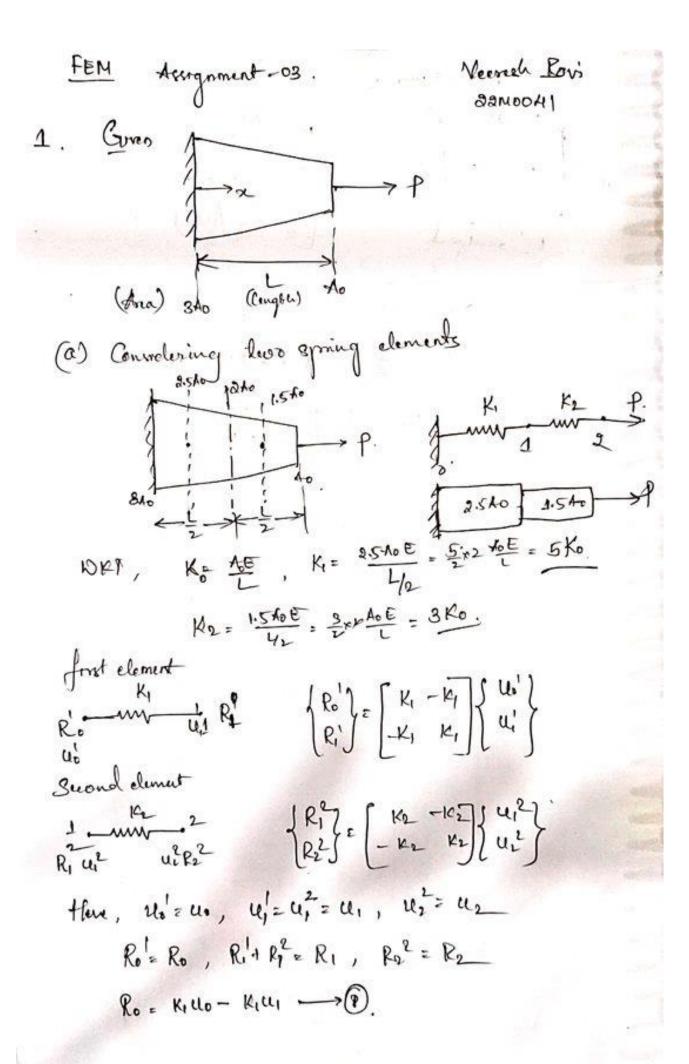
$$\begin{cases}
R_0 \\
1 \\
1
\end{cases} = \begin{cases}
1 & -1 & 0 & 0 \\
-1 & 4 & -2 & -1 \\
0 & -2 & 3 & -1 \\
0 & -1 & -1 & 2
\end{cases}$$

$$\begin{cases}
Q_1 \\
Q_2 \\
Q_3
\end{cases} = \begin{cases}
Q_1 \\
Q_3 \\
Q_3 \\
Q_3
\end{cases} = \begin{cases}
Q_1 \\
Q_3 \\$$

$$\begin{cases} \frac{1}{1} \\ \frac{1}{1} \\ \frac{1}{2} \\ \frac{$$

$$\begin{cases} u_2 \\ u_2 \\ \\ u_3 \\ \end{cases} = \begin{cases} \frac{1}{1} & \frac{1}{14} & \frac{1}{12} \\ \frac{1}{1} & \frac{1}{14} & \frac{1}{12} \\ \frac{1}{1} & \frac{1}{14} & \frac{1}{14} \\ \frac{1}{14} & \frac{1}{14} & \frac{1}{14} & \frac{1}{1$$





$$R_{1} + R_{1}^{2} = R_{1} = -K_{1} u_{0} + K_{1} u_{1} + K_{2} u_{1} - K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{0} + (K_{1} + K_{2}) u_{1} - K_{2} u_{2}$$

$$R_{2} = R_{2} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{3} = R_{1} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{4} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{5} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{6} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{7} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{7} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{8} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{4} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{5} = -K_{1} u_{1} + K_{2} u_{$$

b. Exact 501°,
$$u = \frac{PL \, Qu(3)}{2 \, EAD} = 0.5493 \, P/R_0$$

Perentage (1/1) error = 0.5493 - 0.54421 \$100.

- 0.928 10 error for 4 spring clements

- 0.5493 - 0.5333 ×100

- 0.5493

- 2.912 1. error for 2 spring clements

C. Matlab code for determining the displacement at end of the bar for linear elements

```
clc;
clear all;
A1 = 30;
A2 = 10;
1 = 100;
P = 100;
E = 200000;
n = input('Input array of number of elements')
disp_at_end = [];
for i = 1:length(n)
    node = zeros(n(i),2);
    for j = 1:n(i)
        node(j,:) = [j j+1];
    end
    le = 1/n(i);
    n1 = max(node,[],'all');
    force = zeros(n1,1);
    stiffness = zeros(n1);
    displacement = zeros(n1,1);
    g = 1;
    h = setdiff(1:n1,g);
    r = n1;
    force(r,1) = P;
    reduced_force = force(h, :);
    for j = 1:n(i)
         t = 3 - (((2*j)-1)/n(i));
         T = (E*A2*t)/le;
         r = node(j,1); % left node no. of element j
```

```
s = node(j,2); % right node no. of element j
         stiffness(r,r) = stiffness(r,r) + T;
         stiffness(s,s) = stiffness(s,s) + T;
         stiffness(r,s) = stiffness(r,s) - T;
         stiffness(s,r) = stiffness(s,r) - T;
    end
    disp_nodes = g;
    f nodes = setdiff(1:n1,disp nodes);
    f_stiffness = stiffness;
    f_stiffness = f_stiffness(:,f_nodes);
    f_stiffness = f_stiffness(f_nodes,:);
    unknown_disp = inv(f_stiffness)*reduced_force;
    for j = 1:length(f_nodes)
        displacement(f_nodes(j)) = unknown_disp(j);
    disp_at_end(end+1) = displacement(n1);
    fprintf('\nLinear elements %d',n(i));
    fprintf('Displacement is %d',displacement(n1))
end
X = n;
Y = disp at end;
plot(X,Y);
grid on;
xlabel('Number of Elements')
ylabel('Dispacements at end')
```

Output

Input array of number of elements [2 4 6 8 10]

n =

2 4 6 8 10

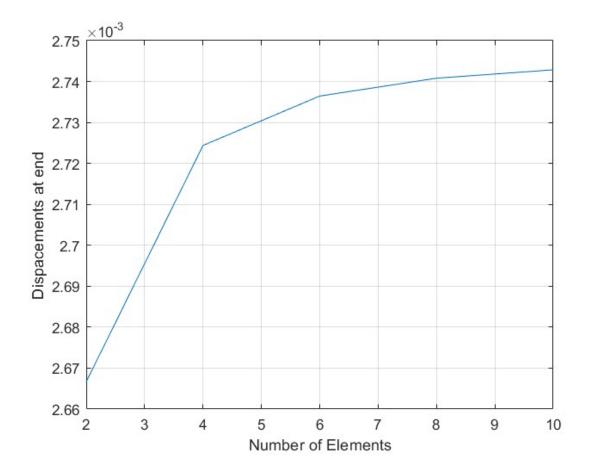
```
Linear elements 2 Displacement is 2.666667e-03

Linear elements 4 Displacement is 2.724387e-03

Linear elements 6 Displacement is 2.736453e-03

Linear elements 8 Displacement is 2.740812e-03

Linear elements 10 Displacement is 2.742855e-03
```



1) **f.**

As the number of elements increases, the accuracy tends to increase but at certain point for linear elements analysis the rate of convergence is decreasing as number of elements is increasing.