

| Dilan to orelate local and |
|--|
| Compatibility equation condition to orelate local and global displacements |
| slobal displacement |
| 3 2 |
| 2 1 13=44=4, U2=42=41=14 |
| $u_1^2 = u_2^2 = u_1^3 = u_1^4 = u_1$ $u_2^3 = u_2^2 = u_1^5 = u_2^3$ |
| |
| u ₂ ⁴ = u ₂ ⁵ = u ₃ |
| - II I I I I I I I I I I I I I I I I I |
| Equilibrance of forces out modes are |
| |
| Ri= Ro, Ro+ Ri2+ Ri3+ Ri4= R, R2+ R23+ Ri5= R2 |
| |
| R24+R25= R3 |
| () () () () () () () () () () |
| Equilibration forces con be written as |
| V= (1) (1) (1) (1) (1) (1) |
| Ro = Kino - Kini |
| |
| R = - K, 40+ K, 4, + K241 - K242 + K341 - K342+ K441- K448 |
| |
| R = - K, U0 + [K,+ K2+ K2+ Ku] U1 - (K2+K3) U2 - Kulls |
| |
| R2 = - K24, + K242 - K34, + K542 + K542 - K543 |
| Contraty, Markette |
| R2 = - (1C3+K3) U, + (K2+K3+K5) U2 - K5 U3 -> 3 |
| -B = - Kuu + Kuug - 16542 + K543 = -K441 - K542+ (ku+kg)4 |
| The state of the s |
| Fequilibrium equation of system is (from equation) |
| |
| Replace to the |
| $ \begin{cases} R_{0} \\ R_{1} \\ R_{2} \end{cases} = \begin{cases} R_{1} \\ -R_{1} \\ R_{1} \\ R_{2} \end{cases} + (R_{1} + R_{2} + R_{3} + R_{4}) \\ -R_{2} + R_{3} + R_{5} \end{cases} - R_{2} $ $ \begin{cases} R_{0} \\ -R_{2} + R_{3} \end{cases} + R_{2} $ $ \begin{cases} R_{1} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{1} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{1} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{2} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{3} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{2} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{3} \\ -R_{3} \end{cases} + R_{3} $ $ R_{3} \\ -R_{3} \end{cases} + R_{3} $ $ \begin{cases} R_{3} \\ -R_{3} \end{cases} + R_{3} $ $ R_{3} \\ -R_{3} \end{cases} + R$ |
| Re Contract - 1/2 / Unit |
| P3 0 -160 12 12 12 12 12 12 12 12 12 12 12 12 12 |
| (FS) (0 -124 - 1C5 Ku+1C5 (43) |

Considering element O, D & . which are movable, the equilibrium legrection of system is written as - Ky (for the) + 1 (or the) + (By energy method was - was - was blockdone. WKT, Potential Energy & Krain Energy for each element T1= 1 K1 (u2-u1) - P1 u1 - R2 u21 (11) 72 = - 12 K2 (422-42) - R242- R2422 13 = 1-12 (u23-u3) - RBu3-R2342 1(11-11) = 16 Tu = 1 ka (u2 - u1) - Ry quy - Rzy u24 75 = 1 K5 (425-45) - 18,5 45 - 1825 45 compatibility audition of local of global diplacement relation $u_1 = u_0$, $u_2 = u_1^2 = u_1^2 = u_1^2 = u_1^2 = u_2^2 = u$ Equilibrium fords, R'= Ro, Ri= R2+ R12+ R12+ R14, R2= R2+ R25 R3 = R24+R25 10 mothers 16 vortages (n) [a] = (a)

There equation becomes,

$$K = \frac{1}{2} \left[K_1 \left[u_1 - u_0 \right]^2 + K_2 \left(u_1 - u_1 \right)^2 + K_3 \left(u_2 - u_1 \right)^2 + K_4 \left(u_3 - u_2 \right)^2 \right]$$
 $+ K_2 \left(u_1 - u_0 \right)^2 + K_2 \left(u_1 - u_1 \right)^2 + K_3 \left(u_2 - u_1 \right)^2 + K_4 \left(u_3 - u_2 \right)^2 + K_5 \left(u_3 - u_3 \right) + K_5 \left(u_3$

$$\begin{cases} R_{0} \\ R_{1} \\ R_{2} \\ R_{3} \end{cases} = \begin{cases} R_{1} & -K_{1} & 0 & 0 \\ -K_{1} & K_{1} + K_{2} + K_{3} + K_{4} & -(K_{2} + K_{3}) & -K_{4} \\ 0 & -(K_{2} + K_{3}) & K_{2} + K_{3} + K_{5} & -K_{5} \\ 0 & -K_{4} & -K_{5} & (K_{4} + K_{5}) \end{cases} \begin{cases} Q_{2} \\ Q_{2} \\ Q_{3} \\ Q_{4} \\ Q_{5} \\ Q_{5} \\ Q_{5} \\ Q_{6} \\ Q_{6} \\ Q_{6} \\ Q_{7} \\ Q_{8} \\ Q_{8}$$

for 3 devent

$$\begin{cases}
R_{1} \\
R_{2}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-(K_{2} + K_{3}) & K_{2} + K_{3} + 1K_{5} & -1C_{5} \\
-K_{4} & -K_{5}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3}
\end{cases} = \begin{cases}
K_{1} + K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4} \\
-K_{2} + K_{3} + 1K_{4} & -(K_{2} + K_{3}) & -K_{4}
\end{cases}$$

2. Matlab Code %..... % MATLAB codes for Finite Element Analysis % Discrete Systems.m % clear memory clear all % elementNodes: connections at elements elementNodes=[1 2;2 3;2 3;2 4;3 4]; % numberElements: number of Elements numberElements=size(elementNodes,1); % By using the MATLAB function size, that returns the number % of lines and columns of a rectangular matrix, we can detect % the number of elements by inspecting the number of lines of %matrix elementNodes. % numberNodes: number of nodes numberNodes=4; % for structure: % displacements: displacement vector % force : force vector % stiffness: stiffness matrix % initializing the matrices displacements=zeros(numberNodes,1); force=zeros(numberNodes,1); stiffness=zeros(numberNodes); % applied load at node 2 force(2)=1; force(3)=1; force(4)=1;

```
% computation of the system stiffness matrix
% We compute now the stiffness matrix for each element in turn and then assemble %
it in the global stiffness matrix.
for e=1:numberElements:
% elementDof: element degrees of freedom (Dof) elementDof=elementNodes(e,:)
stiffness(elementDof,elementDof)=stiffness(elementDof,elementDof)+[1-1;-11] end
% boundary conditions and solution
% prescribed dofs
prescribedDof=1; %
free Dof: activeDof
activeDof=setdiff([1:numberNodes],[prescribedDof]);
% solution
displacements=stiffness(activeDof,activeDof)\force(activeDof);
% positioning all displacements
displacements1=zeros(numberNodes,1);
displacements1(activeDof)=displacements;
% output displacements/reactions
outputDisplacementsReactions(displacements1, stiffness, numberNodes, prescribedDof)
outputDisplacementsReactions...
(displacements, stiffness, GDof, prescribedDof)
% output of displacements and reactions in
% tabular form
% GDof: total number of degrees of freedom of
% the problem %
displacements
disp('Displacements')
%displacements=displacements1; jj=1:GDof;
format
[jj' displacements]
% reactions
F=stiffness*displacements;
reactions=F(jj); disp('reactions')
[jj' reactions]
end
```

Stiffness ans

 $=4\times4$

Displacements

 $ans = 4 \times 2$

Reactions

 $ans = 4 \times 2$

1.0000 -3.0000

2.0000 1.0000

3.0000 1.0000

4.0000 1.0000

Displacements:

Displacement of node 2 = 3

Displacement of node 3 = 3.60

Displacement of node 4 = 3.80

Reaction Forces:

Reaction force at node 1 = -3

d. (b) Green
$$K_1 = K_2 = K_3 = K_4 = K_5 = 1 ...$$

R₁ = R₂ = R₃ = 1...

from equilibrium equatron of system.

$$\begin{cases}
R_{1} \\
R_{2}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{1} & K_{1} + K_{2} + K_{3} & -(K_{2} + K_{3})^{2} & -K_{4} \\
0 & -(K_{2} + K_{3}) & K_{2} + K_{3} + K_{5} & -K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
R_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5} & -K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{1} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{2} + K_{3} + K_{5}
\end{cases}$$

$$\begin{cases}
K_{2} \\
C_{3}
\end{cases} = \begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{2} & 0 & 0 \\
-K_{3}
\end{cases}$$

$$\begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{2} & 0 & 0 \\
-K_{3}
\end{cases}$$

$$\begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{3} & 0 & 0 \\
-K_{4} & 0 & 0 \\
-K_{3}
\end{cases}$$

$$\begin{cases}
K_{1} - K_{2} & 0 & 0 \\
-K_{3} & 0 & 0 \\
-K_{4} & 0 & 0 \\
-K_{3} & 0 & 0 \\
-K_{4} & 0 & 0 \\
-K_{5} & 0 & 0 \\
-K_{4} & 0 & 0 \\
-K_{5} &$$

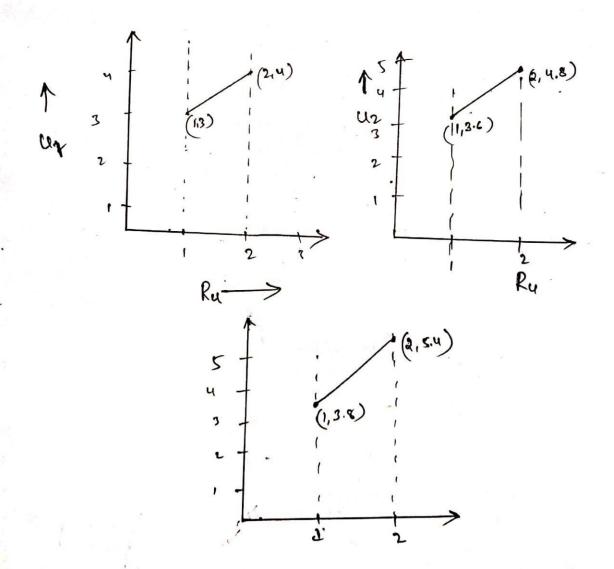
$$\begin{cases}
R_{0} \\
1 \\
1
\end{cases} = \begin{cases}
1 & -1 & 0 & 0 \\
-1 & 4 & -2 & -1 \\
0 & -2 & 3 & -1 \\
0 & -1 & -1 & 2
\end{cases}$$

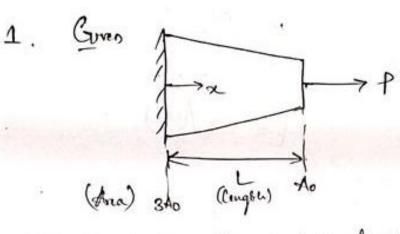
$$\begin{cases}
u_{1} \\
u_{2} \\
u_{3}
\end{cases} = \begin{cases}
u_{1} \\
u_{2} \\
u_{3}
\end{cases}$$

$$\vdots \quad \text{gived at e)}$$

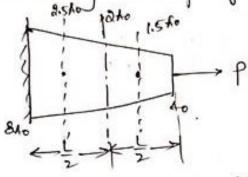
$$\begin{cases} \frac{1}{1} \\ \frac{1}{1} \\ \frac{1}{2} \\ \frac{$$

$$\begin{cases} u_1 \\ u_2 \\ \vdots \\ u_n \end{cases} = \begin{cases} 1 & 1 & 1 \\ 1 & 1.4 & 1.2 \\ 1 & 1.2 & 1.6 \end{cases} \begin{cases} 1 \\ 1 \\ 1 & 1.2 & 1.6 \end{cases}$$





(a) Convolering levo spring elements



NET, K: 4 - 5K0 - 5K2 - 5K0

frost element

Ki

Ro

ui

Ri

Second element

Here, u'zu, u'zu, z'zu, u'z uz Roz Ro, Ri+ Roz Ri, Roz = Rz

$$R_{1} + R_{1}^{2} = R_{1} = -K_{1} u_{0} + K_{1} u_{1} + K_{2} u_{1} - K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{0} + (K_{1} + K_{2}) u_{1} - K_{2} u_{2}$$

$$R_{2} = R_{2} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{3} = R_{1} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{4} = -K_{2} u_{1} + K_{2} u_{2}$$

$$R_{5} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{6} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{7} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{7} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{8} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{1} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{2} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{3} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{4} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{5} = -K_{1} u_{1} + K_{2} u_{2}$$

$$R_{5} = -K_{1} u_{1} + K_{2} u_{$$

b. Exact 501°,
$$u = \frac{PL \, Qu(3)}{2 \, EAD} = 0.5493 \, P/R_0$$

Perentage (1/1) error = 0.5493 - 0.54421 \$100.

- 0.928 10 error for 4 spring clements

- 0.5493 - 0.5333 ×100

- 0.5493

- 2.912 1. error for 2 spring clements

C. Matlab code for determining the displacement at end of the bar for linear elements

```
clc;
clear all;
A1 = 30;
A2 = 10;
1 = 100;
P = 100;
E = 200000;
n = input('Input array of number of elements')
disp_at_end = [];
for i = 1:length(n)
    node = zeros(n(i),2);
    for j = 1:n(i)
        node(j,:) = [j j+1];
    end
    le = 1/n(i);
    n1 = max(node,[],'all');
    force = zeros(n1,1);
    stiffness = zeros(n1);
    displacement = zeros(n1,1);
    g = 1;
    h = setdiff(1:n1,g);
    r = n1;
    force(r,1) = P;
    reduced_force = force(h, :);
    for j = 1:n(i)
         t = 3 - (((2*j)-1)/n(i));
         T = (E*A2*t)/le;
         r = node(j,1); % left node no. of element j
```

```
s = node(j,2); % right node no. of element j
         stiffness(r,r) = stiffness(r,r) + T;
         stiffness(s,s) = stiffness(s,s) + T;
         stiffness(r,s) = stiffness(r,s) - T;
         stiffness(s,r) = stiffness(s,r) - T;
    end
    disp_nodes = g;
    f nodes = setdiff(1:n1,disp nodes);
    f_stiffness = stiffness;
    f_stiffness = f_stiffness(:,f_nodes);
    f_stiffness = f_stiffness(f_nodes,:);
    unknown_disp = inv(f_stiffness)*reduced_force;
    for j = 1:length(f_nodes)
        displacement(f_nodes(j)) = unknown_disp(j);
    disp_at_end(end+1) = displacement(n1);
    fprintf('\nLinear elements %d',n(i));
    fprintf('Displacement is %d',displacement(n1))
end
X = n;
Y = disp at end;
plot(X,Y);
grid on;
xlabel('Number of Elements')
ylabel('Dispacements at end')
```

Output

Input array of number of elements [2 4 6 8 10]

n =

2 4 6 8 10

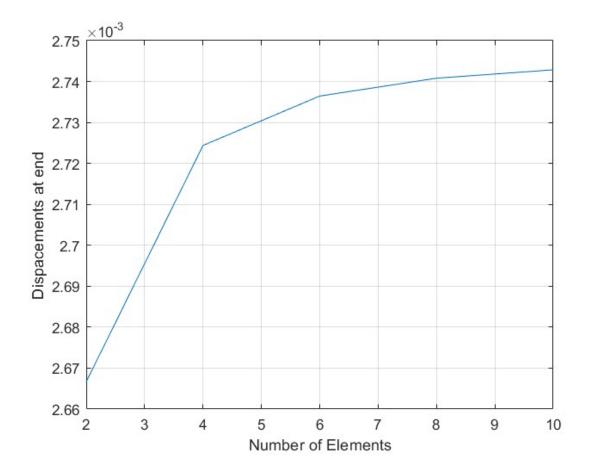
Linear elements 2 Displacement is 2.666667e-03

Linear elements 4 Displacement is 2.724387e-03

Linear elements 6 Displacement is 2.736453e-03

Linear elements 8 Displacement is 2.740812e-03

Linear elements 10 Displacement is 2.742855e-03



1) **f.**

As the number of elements increases, the accuracy tends to increase but at certain point for linear elements analysis the rate of convergence is decreasing as number of elements is increasing.