

# Thermal boundary conditions

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# 1 Model

## 1.1 CMB - heat flux pattern

We impose a heat flux balance between the inner and the outer core boundary. The total influx at the ICB  $Q_i$  equals the total outflux  $Q_o$  at the CMB:

$$-Q_i = Q_o \quad (1)$$

$$\Leftrightarrow \int_{\Sigma_{\text{icb}}} \kappa \nabla T|_{\text{icb}} \cdot \mathbf{e}_r dS = \int_{\Sigma_{\text{cmb}}} \kappa \nabla T|_{\text{cmb}} \cdot \mathbf{e}_r dS \quad (2)$$

$$\Leftrightarrow \int_{\Sigma_{\text{icb}}} \left. \frac{\partial T}{\partial r} \right|_{\text{icb}} dS = \int_{\Sigma_{\text{cmb}}} \left. \frac{\partial T}{\partial r} \right|_{\text{cmb}} dS \quad (3)$$

For the spectral decomposition it is important to know, that only the 0th order spherical harmonic  $\mathcal{Y}_0^0$  yields values  $\neq 0$  when integrated over a closed surface  $\Sigma$ :

$$\int_{\Sigma} \frac{\partial T}{\partial r} dS = \int_{\Sigma} \left( \frac{\partial T}{\partial r} \right)_0^0 \mathcal{Y}_0^0 dS \quad (4)$$

with  $\left( \frac{\partial T}{\partial r} \right)_0^0$  being the spectral coefficient of degree and order 0.

$$\int_{\Sigma_{\text{icb}}} \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{icb}} \mathcal{Y}_0^0 dS = \int_{\Sigma_{\text{cmb}}} \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{cmb}} \mathcal{Y}_0^0 dS \quad (5)$$

$$\Leftrightarrow \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{icb}} r_i^2 = \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{cmb}} r_o^2 \quad (6)$$

This allows to formulate a simple relation between the mean radial temperature gradient at the inner and outer boundary.

$$\Leftrightarrow \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{icb}} = \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{cmb}} \frac{r_o^2}{r_i^2} = -\beta \frac{r_o^2}{r_i^2} = -\beta \frac{1}{a^2} \quad (7)$$

with  $\beta := - \left( \frac{\partial T}{\partial r} \right)_0^0 \Big|_{\text{cmb}}$  as prescribed temperature gradient at the CMB.

This relation allows us to formulate Neumann boundary conditions for the stationary temperature equation that has the form of a Laplace equation,

$$\nabla^2 T = 0 \quad (8)$$

since we have no internal sources.

$$\text{ICB: } \left. \frac{\partial T}{\partial r} \right|_{\text{icb}} = -\beta \frac{1}{a^2} \mathcal{Y}_0^0 \quad (9)$$

$$\text{CMB: } \left. \frac{\partial T}{\partial r} \right|_{\text{cmb}} = -\beta \mathcal{Y}_0^0 + \text{Amp}_l^m \mathcal{Y}_l^m \quad (10)$$

where  $\text{Amp}_l^m$  is the amplitude of the heat flux heterogeneity. The general solution of (8) in spherical coordinates reads

$$T = \sum_{l,m} [a_l^m r^l + b_l^m r^{-l-1}] \mathcal{Y}_l^m(\vartheta, \varphi) \quad (11)$$

and its radial derivative

$$\frac{\partial T}{\partial r} = \sum_{l,m} [l a_l^m r^{l-1} - (l+1) b_l^m r^{-l-2}] \mathcal{Y}_l^m(\vartheta, \varphi). \quad (12)$$

From (9) and (12) follows immediately for  $l = m = 0$

$$-b_0^0 r_i^{-2} = -\beta \frac{1}{a^2} \Rightarrow b_0^0 = \beta r_o^2 \quad (13)$$

and the algebraic equation

$$l a_l^m r_i^{l-1} - (l+1) b_l^m r_i^{-l-2} = 0 \quad (14)$$

for all  $l > 0$  and  $m > 0$ .

(10) and (11) together give another equation for the determination of  $a_l^m$  and  $b_l^m$ :

$$l a_l^m r_o^{l-1} - (l+1) b_l^m r_o^{-l-2} = \text{Amp}_l^m. \quad (15)$$

Since only a heat flux pattern with  $l = m = 2$  will be used here, (14) and (15) simplify to

$$\begin{pmatrix} 2r_o & -3r_o^{-4} \\ 2r_i & -3r_i^{-4} \end{pmatrix} \begin{pmatrix} a_2^2 \\ b_2^2 \end{pmatrix} = \begin{pmatrix} \text{Amp}_2^2 \\ 0 \end{pmatrix}. \quad (16)$$

In a nondimensional form, the solution (8) is

$$\hat{T} = \frac{T}{d\beta} = \left( \frac{a_0^0}{d\beta} + \frac{1}{(a-1)^2 \hat{r}} \right) \mathcal{Y}_0^0 + \frac{\text{Amp}_2^2}{\beta} \cdot \frac{2a^5 \hat{r}^3 - 3(a-1)^5 \hat{r}^2}{6(a-1)^4 (1-a^5)} \mathcal{Y}_2^2 \quad (17)$$

with  $a_0^0$  being an arbitrary integration constant that is chosen to be 0 in the following.