

TCMT for Faraday-Rotation FWM in Isotropic $\chi^{(3)}$

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1 Maxwell wave equation in time domain and setup

We work in nonmagnetic media $\mu = \mu_0$ and split polarization into a linear part (absorbed into ϵ) and a nonlinear part \mathbf{P}_{NL} . The *time-domain* electric-field wave equation is

$$\nabla \times \nabla \times \mathbf{E}(\mathbf{r}, t) + \mu_0 \epsilon(\mathbf{r}) \partial_t^2 \mathbf{E}(\mathbf{r}, t) = -\mu_0 \partial_t^2 \mathbf{P}_{\text{NL}}(\mathbf{r}, t), \quad (1)$$

with the usual outgoing-radiation boundary conditions. For frequency components $e^{-i\omega t}$ this becomes

$$\nabla \times \mu_0^{-1} \nabla \times \mathbf{E}(\mathbf{r}, \omega) - \frac{\omega^2}{c^2} \epsilon(\mathbf{r}, \omega) \mathbf{E}(\mathbf{r}, \omega) = \omega^2 \mu_0 \mathbf{P}_{\text{NL}}(\mathbf{r}, \omega). \quad (2)$$

Fields and carriers. We consider five carriers with slowly varying envelopes (SVEA): pumps at $\omega_1 = \omega_p + \Delta/2$ and $\omega_2 = \omega_p - \Delta/2$, probe at ω_s , and probe-generated sidebands at $\Omega_{\pm} = \omega_s \pm \Delta$. Circular basis $\{\mathbf{e}^{(+)}, \mathbf{e}^{(-)}\}$ with $\mathbf{e}^{(+)} \cdot \mathbf{e}^{(-)} = 1$, $\mathbf{e}^{(\pm)} \cdot \mathbf{e}^{(\pm)} = 0$.

Polarizations. Counter-rotating pumps and probe:

$$\mathbf{E}^{(1)} = E_1 \mathbf{e}^{(+)}, \quad \mathbf{E}^{(2)} = E_2 \mathbf{e}^{(-)}, \quad \mathbf{E}^{(s)} = E_+ \mathbf{e}^{(+)} + E_- \mathbf{e}^{(-)},$$

with $|E_{\pm}| \ll |E_{1,2}|$. We keep only terms linear in the probe envelopes.

2 Eigenmodes and normalization

Let $\{\mathbf{u}_{\mu}(\mathbf{r}), \omega_{\mu}\}$ denote (quasi-normal) cavity eigenmodes solving the source-free frequency-domain problem

$$\nabla \times \mu_0^{-1} \nabla \times \mathbf{u}_{\mu}(\mathbf{r}) = \frac{\omega_{\mu}^2}{c^2} \epsilon(\mathbf{r}, \omega_{\mu}) \mathbf{u}_{\mu}(\mathbf{r}), \quad (3)$$

with outgoing-radiation boundary conditions. We expand the field near each carrier as

$$\mathbf{E}_{\mu}(\mathbf{r}, t) = x_{\mu}(t) \mathbf{u}_{\mu}(\mathbf{r}) e^{-i\omega_{\mu} t} + \text{c.c.}$$

We adopt the energy normalization

$$U_{\mu} = \frac{1}{4} \int \left[\epsilon \mathbf{u}_{\mu} \cdot \mathbf{u}_{\mu}^* + \mu_0 \mathbf{h}_{\mu} \cdot \mathbf{h}_{\mu}^* \right] dV = 1, \quad (4)$$

so that $|x_{\mu}|^2$ equals the energy stored in mode μ . *If $U_{\mu} \neq 1$ is used, then **all** nonlinear overlap coefficients below must be divided by U_{μ} accordingly.*

Modes and ports. Linear radiative/absorptive losses are captured by total decay rates κ_{μ} ; coupling to external ports p is described by rates $\kappa_{\mu,p}$ with $\kappa_{\mu} = \kappa_{\mu,i} + \sum_p \kappa_{\mu,p}$.

3 Isotropic $\chi^{(3)}$ tensor bookkeeping

For any frequency tuple Ξ we use the Maker–Terhune decomposition

$$\chi_{ijkl}^{(3)}(\Xi) = A(\Xi) \delta_{ij} \delta_{kl} + B(\Xi) \delta_{ik} \delta_{jl} + C(\Xi) \delta_{il} \delta_{jk}, \quad (5)$$

with distinct $\{A, B, C\}$ for each tuple; no Kleinman symmetry is assumed. Contractions are performed in the circular basis.

4 Counter-rotating pumps

4.1 Direct third-order polarization at ω_s

Keeping only terms linear in probe,

$$P_i^{(3)}(\omega_s) = \frac{3}{4} \varepsilon_0 \sum_{m \in \{s, 1, 2\}} \left[A_s^{(m)} \delta_{ij} \delta_{kl} + B_s^{(m)} \delta_{ik} \delta_{jl} + C_s^{(m)} \delta_{il} \delta_{jk} \right] E_j^{(s)} E_k^{(m)} E_l^{(m)*}, \quad (6)$$

where $A_s^{(m)} := A(-\omega_s; \omega_s, \omega_m, -\omega_m)$ and similarly for $B_s^{(m)}, C_s^{(m)}$. In $\{\mathbf{e}^{(+)}, \mathbf{e}^{(-)}\}$ this is diagonal:

$$\mathbf{P}^{(3)}(\omega_s) = P_+ \mathbf{e}^{(+)} + P_- \mathbf{e}^{(-)},$$

with P_+ containing $(A_s^{(1)} + B_s^{(1)})|E_1|^2 E_+$ and $(A_s^{(2)} + C_s^{(2)})|E_2|^2 E_+$, and P_- the $(+) \leftrightarrow (-)$ counterparts. Thus the *direct* Kerr action is circular-diagonal.

4.2 Probe sidebands at Ω_{\pm}

With $\Omega_{\pm} = \omega_s \pm \Delta$ and counter-rotating pumps one finds

$$\mathbf{P}^{(3)}(\Omega_+) = \frac{3}{4} \varepsilon_0 (B_+^{\text{sb}} + C_+^{\text{sb}}) E_1 E_2^* E_- \mathbf{e}^{(+)}, \quad (7)$$

$$\mathbf{P}^{(3)}(\Omega_-) = \frac{3}{4} \varepsilon_0 (B_-^{\text{sb}} + C_-^{\text{sb}}) E_2 E_1^* E_+ \mathbf{e}^{(-)}, \quad (8)$$

where, e.g., $B_+^{\text{sb}} := B(-\Omega_+; \omega_s, \omega_1, -\omega_2)$.

4.3 TCMT from Maxwell projection

Projecting (2) onto \mathbf{u}_{ν}^* and using (4) gives, under SVEA and RWA,

$$\dot{x}_{\nu} = (i\Delta_{\nu} - \frac{\kappa_{\nu}}{2})x_{\nu} + \sum_p \sqrt{\kappa_{\nu,p}} s_{\nu p, \text{in}} + F_{\nu}, \quad F_{\nu} = i \frac{\omega_{\nu}}{2U_{\nu}} \int \mathbf{u}_{\nu}^*(\mathbf{r}) \mathbf{P}_{\text{NL}}(\mathbf{r}, \omega_{\nu}) dV. \quad (9)$$

We now instantiate (9) for the five carriers with envelopes

$$\{A_1 \leftrightarrow \omega_1, A_2 \leftrightarrow \omega_2, a_{\pm} \leftrightarrow \omega_s, b_+ \leftrightarrow \Omega_+, b_- \leftrightarrow \Omega_-\}.$$

4.4 Pumps

$$\dot{A}_1 = (i\Delta_1 - \frac{\kappa_1}{2})A_1 + \sum_p \sqrt{\kappa_{1,p}} s_{1p,\text{in}}, \quad \dot{A}_2 = (i\Delta_2 - \frac{\kappa_2}{2})A_2 + \sum_p \sqrt{\kappa_{2,p}} s_{2p,\text{in}}. \quad (10)$$

4.5 Probe at ω_s (direct Kerr)

Projecting the direct $\mathbf{P}^{(3)}(\omega_s)$ onto the probe mode profiles $\mathbf{u}_{s\pm}$ yields

$$\dot{a}_+ = \left[i\Delta_s - \frac{\kappa_s}{2}\right]a_+ + i\alpha_1|A_1|^2a_+ + i\alpha_2|A_2|^2a_+ + \sum_p \sqrt{\kappa_{s,p}^{(+)}} s_{sp,\text{in}}^{(+)}, \quad (11)$$

$$\dot{a}_- = \left[i\Delta_s - \frac{\kappa_s}{2}\right]a_- + i\tilde{\alpha}_1|A_1|^2a_- + i\tilde{\alpha}_2|A_2|^2a_- + \sum_p \sqrt{\kappa_{s,p}^{(-)}} s_{sp,\text{in}}^{(-)}, \quad (12)$$

with overlap coefficients (for $U_{s\pm} = U_{1,2} = 1$)

$$\alpha_1 = \frac{3\omega_s\varepsilon_0}{8} \int (A_s^{(1)} + B_s^{(1)}) |\mathbf{u}_{s+}|^2 |\mathbf{u}_{1+}|^2 dV, \quad \alpha_2 = \frac{3\omega_s\varepsilon_0}{8} \int (A_s^{(2)} + C_s^{(2)}) |\mathbf{u}_{s+}|^2 |\mathbf{u}_{2-}|^2 dV, \quad (13)$$

$$\tilde{\alpha}_1 = \frac{3\omega_s\varepsilon_0}{8} \int (A_s^{(1)} + C_s^{(1)}) |\mathbf{u}_{s-}|^2 |\mathbf{u}_{1+}|^2 dV, \quad \tilde{\alpha}_2 = \frac{3\omega_s\varepsilon_0}{8} \int (A_s^{(2)} + B_s^{(2)}) |\mathbf{u}_{s-}|^2 |\mathbf{u}_{2-}|^2 dV. \quad (14)$$

If $U_\mu \neq 1$, divide each coefficient by the corresponding U factors from (9).

4.6 Sidebands at Ω_{\pm} (generation)

Using $\mathbf{P}^{(3)}(\Omega_{\pm})$ and projecting onto $\mathbf{u}_{b\pm}$,

$$\dot{b}_+ = \left(i\Delta_{b+} - \frac{\kappa_{b+}}{2}\right)b_+ + i\zeta_+ (A_1 A_2^*) a_-, \quad (15)$$

$$\dot{b}_- = \left(i\Delta_{b-} - \frac{\kappa_{b-}}{2}\right)b_- + i\zeta_- (A_2 A_1^*) a_+, \quad (16)$$

with

$$\zeta_+ = \frac{3\Omega_+\varepsilon_0}{8} \int (B_+^{\text{sb}} + C_+^{\text{sb}}) (\mathbf{u}_{b+}^* \cdot \mathbf{u}_{1+}) (\mathbf{u}_{2-}^* \cdot \mathbf{u}_{s-}) dV, \quad (17)$$

$$\zeta_- = \frac{3\Omega_-\varepsilon_0}{8} \int (B_-^{\text{sb}} + C_-^{\text{sb}}) (\mathbf{u}_{b-}^* \cdot \mathbf{u}_{2-}) (\mathbf{u}_{1+}^* \cdot \mathbf{u}_{s+}) dV. \quad (18)$$

4.7 Cascaded back-mixing into the probe

The sidebands mix with the opposite pump pair to return to ω_s , producing *off-diagonal* probe drives:

$$\dot{a}_+ = \cdots + i\eta_- b_-, \quad \dot{a}_- = \cdots + i\eta_+ b_+, \quad (19)$$

with

$$\eta_+ = \frac{3\omega_s \varepsilon_0}{8} \int (B_+^{\text{mx}} + C_+^{\text{mx}}) (\mathbf{u}_{s-}^* \cdot \mathbf{u}_{2-}) (\mathbf{u}_{1+}^* \cdot \mathbf{u}_{b+}) dV, \quad (20)$$

$$\eta_- = \frac{3\omega_s \varepsilon_0}{8} \int (B_-^{\text{mx}} + C_-^{\text{mx}}) (\mathbf{u}_{s+}^* \cdot \mathbf{u}_{1+}) (\mathbf{u}_{2-}^* \cdot \mathbf{u}_{b-}) dV. \quad (21)$$

In the counter-rotating isotropic case the A -channel cancels in the cascade.

4.8 Adiabatic elimination of sidebands and effective coupling

If sidebands are fast ($|\Delta_{b\pm} - i\kappa_{b\pm}/2|$ large), set $\dot{b}_\pm \simeq 0$:

$$b_+ \simeq \frac{\zeta_+}{\frac{\kappa_{b+}}{2} - i\Delta_{b+}} (A_1 A_2^*) a_-, \quad b_- \simeq \frac{\zeta_-}{\frac{\kappa_{b-}}{2} - i\Delta_{b-}} (A_2 A_1^*) a_+.$$

Then the probe obeys

$$\begin{cases} \dot{a}_+ = \left[i(\Delta_s + \Phi_+) - \frac{\kappa_s}{2} \right] a_+ + i g_{\text{eff}} a_-, \\ \dot{a}_- = \left[i(\Delta_s + \Phi_-) - \frac{\kappa_s}{2} \right] a_- + i g_{\text{eff}}^* a_+, \end{cases} \quad (22)$$

with direct self-phase shifts $\Phi_+ = \alpha_1 |A_1|^2 + \alpha_2 |A_2|^2$ and $\Phi_- = \tilde{\alpha}_1 |A_1|^2 + \tilde{\alpha}_2 |A_2|^2$, and cascaded *mixing* strength

$$g_{\text{eff}} = \eta_+ \frac{\zeta_+}{\frac{\kappa_{b+}}{2} - i\Delta_{b+}} (A_1 A_2^*) = \eta_-^* \frac{\zeta_-^*}{\frac{\kappa_{b-}}{2} + i\Delta_{b-}} (A_1 A_2^*). \quad (23)$$

Polarization rotation of the probe arises from g_{eff} (off-diagonal coupling) and any circular-birefringent difference $\Phi_+ - \Phi_-$.

4.9 Ports and observables

For port p coupled to mode μ , the usual input-output relation is

$$s_{p,\text{out}} = \sum_{p'} C_{pp'} s_{p',\text{in}} + \sqrt{\kappa_{\mu,p}} x_\mu,$$

with unitary direct scattering matrix C fixed by energy conservation and time reversal. The transmitted/reflected Jones vector of the probe follows from a_\pm and yields the rotation angle.

Notes. (i) All overlap coefficients inherit the frequency-tuple labels of A, B, C ; no Kleinman symmetry is assumed. (ii) In homogeneous isotropic propagation, the dyadic Green tensor reduces to a diagonal scalar, which is consistent with the single-mode b_{\pm} description used here. (iii) If $U_{\mu} \neq 1$, remember to divide each nonlinear overlap by U_{μ} as indicated below (9).

5 Co-rotating Pumps: Direct and Cascaded $\chi^{(3)}$ Paths in TCMT

We now take co-rotating pumps,

$$\mathbf{E}^{(1)} = E_1 \mathbf{e}^{(+)}, \quad \mathbf{E}^{(2)} = E_2 \mathbf{e}^{(+)}, \quad \Delta = \omega_1 - \omega_2, \quad \Omega_{\pm} = \omega_s \pm \Delta,$$

and the probe $\mathbf{E}^{(s)} = E_+ \mathbf{e}^{(+)} + E_- \mathbf{e}^{(-)}$ with $|E_{\pm}| \ll |E_{1,2}|$. The isotropic tensor is kept in Maker–Terhune form with tuple-dependent A, B, C and no Kleinman symmetry.

Direct Kerr at ω_s . As in the counter-rotating case, the direct third-order polarization is diagonal in $\{\mathbf{e}^{(+)}, \mathbf{e}^{(-)}\}$:

$$\mathbf{P}^{(3)}(\omega_s) = P_+^{\text{dir}} \mathbf{e}^{(+)} + P_-^{\text{dir}} \mathbf{e}^{(-)},$$

with

$$P_+^{\text{dir}} = \frac{3}{4}\varepsilon_0 \left[(A_s^{(s)} + C_s^{(s)})(|E_+|^2 + |E_-|^2)E_+ + 2B_s^{(s)}|E_-|^2E_+ + \right. \quad (24)$$

$$\left. (A_s^{(1)} + B_s^{(1)})|E_1|^2E_+ + (A_s^{(2)} + B_s^{(2)})|E_2|^2E_+ \right],$$

$$P_-^{\text{dir}} = \frac{3}{4}\varepsilon_0 \left[(A_s^{(s)} + C_s^{(s)})(|E_+|^2 + |E_-|^2)E_- + 2B_s^{(s)}|E_+|^2E_- + \right. \quad (25)$$

$$\left. (A_s^{(1)} + C_s^{(1)})|E_1|^2E_- + (A_s^{(2)} + C_s^{(2)})|E_2|^2E_- \right],$$

where $A_s^{(m)} := A(-\omega_s; \omega_s, \omega_m, -\omega_m)$ etc. (As before, with modal energy normalization $U_{\mu} \neq 1$, divide each nonlinear overlap coefficient by U_{μ} .)

Sideband generation at Ω_{\pm} . For co-rotating pumps, both circular components of the sideband polarization survive:

$$\mathbf{P}^{(3)}(\Omega_+) = \frac{3}{4}\varepsilon_0 E_1 E_2^* \left[(A_+^{\text{sb}} + B_+^{\text{sb}})E_+ \mathbf{e}^{(+)} + (A_+^{\text{sb}} + C_+^{\text{sb}})E_- \mathbf{e}^{(-)} \right], \quad (26)$$

$$\mathbf{P}^{(3)}(\Omega_-) = \frac{3}{4}\varepsilon_0 E_2 E_1^* \left[(A_-^{\text{sb}} + B_-^{\text{sb}})E_+ \mathbf{e}^{(+)} + (A_-^{\text{sb}} + C_-^{\text{sb}})E_- \mathbf{e}^{(-)} \right], \quad (27)$$

with, e.g., $A_+^{\text{sb}} := A(-\Omega_+; \omega_s, \omega_1, -\omega_2)$.

Sideband vectorization and compact TCMT We group the two circular polarizations of each arm into vectors

$$\mathbf{b}_+ = \begin{bmatrix} b_{+,+} \\ b_{+,-} \end{bmatrix} \leftrightarrow \Omega_+, \quad \mathbf{b}_- = \begin{bmatrix} b_{-,+} \\ b_{-,-} \end{bmatrix} \leftrightarrow \Omega_-, \quad \mathbf{a} = \begin{bmatrix} a_+ \\ a_- \end{bmatrix} \leftrightarrow \omega_s.$$

Here, $b_{\sigma,\tau}$ denotes the sideband at arm $\sigma \in \{+, -\}$ with circular polarization $\tau \in \{+, -\}$. We also allow a general *linear* 2×2 sideband block for each arm,

$$\mathbf{K}_{b\pm} \equiv \begin{bmatrix} \frac{\kappa_{b\pm,+}}{2} - i\Delta_{b\pm,+} & -i\Lambda_{b\pm} \\ -i\Lambda_{b\pm}^* & \frac{\kappa_{b\pm,-}}{2} - i\Delta_{b\pm,-} \end{bmatrix},$$

which captures distinct linewidths/detunings for $+$ and $-$ and any linear cross-polarization mixing ($\Lambda_{b\pm} = 0$ for an isotropic cavity without linear $+\leftrightarrow-$ coupling).

Sideband generation (vector form). Projecting the isotropic $\chi^{(3)}$ sideband polarizations onto the sideband modes gives

$$\dot{\mathbf{b}}_+ = -\mathbf{K}_{b+}\mathbf{b}_+ + i(A_1A_2^*)\mathbf{Z}^{(+)}\mathbf{a}, \quad \dot{\mathbf{b}}_- = -\mathbf{K}_{b-}\mathbf{b}_- + i(A_2A_1^*)\mathbf{Z}^{(-)}\mathbf{a}, \quad (28)$$

with 2×2 *generation* matrices

$$\mathbf{Z}^{(+)} = \begin{bmatrix} \zeta_{++}^{(+)} & \zeta_{+-}^{(+)} \\ \zeta_{-+}^{(+)} & \zeta_{--}^{(+)} \end{bmatrix}, \quad \mathbf{Z}^{(-)} = \begin{bmatrix} \zeta_{++}^{(-)} & \zeta_{+-}^{(-)} \\ \zeta_{-+}^{(-)} & \zeta_{--}^{(-)} \end{bmatrix}.$$

For *co-rotating* pumps in an isotropic medium the only nonzero entries are the *diagonals*

$$\zeta_{++}^{(+)} = \frac{3\Omega_+\varepsilon_0}{8U_{b+}} \int (A_+^{\text{sb}} + B_+^{\text{sb}}) (\mathbf{u}_{b+,+}^* \cdot \mathbf{u}_{1+}) (\mathbf{u}_{2+}^* \cdot \mathbf{u}_{s+}) dV, \quad (29)$$

$$\zeta_{--}^{(+)} = \frac{3\Omega_+\varepsilon_0}{8U_{b+}} \int (A_+^{\text{sb}} + C_+^{\text{sb}}) (\mathbf{u}_{b+,-}^* \cdot \mathbf{u}_{1+}) (\mathbf{u}_{2+}^* \cdot \mathbf{u}_{s-}) dV, \quad (30)$$

(and $\zeta_{+-}^{(+)} = \zeta_{-+}^{(+)} = 0$); similarly at Ω_- with the tuples $(-\Omega_-; \omega_s, \omega_2, -\omega_1)$. For *counter-rotating* pumps, $\mathbf{Z}^{(+)}$ and $\mathbf{Z}^{(-)}$ are diagonal but with only one nonzero element each: $b_{+,+} \leftarrow a_-$ and $b_{-,-} \leftarrow a_+$, exactly matching the contractions in your earlier note.

Back-mixing into the probe (vector form). Projecting the cascaded polarization onto the probe modes yields

$$\dot{\mathbf{a}} = \left[i(\Delta_s \mathbf{I} + \mathbf{\Phi}) - \frac{\kappa_s}{2} \mathbf{I} \right] \mathbf{a} + i(A_2 A_1^*) \mathbf{M}^{(+)} \mathbf{b}_+ + i(A_1 A_2^*) \mathbf{M}^{(-)} \mathbf{b}_- + (\text{probe inputs}), \quad (31)$$

with $\mathbf{\Phi} = \text{diag}(\Phi_+, \Phi_-)$ the direct (diagonal) Kerr shifts and 2×2 *mixing* matrices

$$\mathbf{M}^{(+)} = \begin{bmatrix} \eta_{+,+}^{(+)} & \eta_{+,-}^{(+)} \\ \eta_{-,+}^{(+)} & \eta_{-,-}^{(+)} \end{bmatrix}, \quad \mathbf{M}^{(-)} = \begin{bmatrix} \eta_{+,+}^{(-)} & \eta_{+,-}^{(-)} \\ \eta_{-,+}^{(-)} & \eta_{-,-}^{(-)} \end{bmatrix}.$$

In the *co-rotating, isotropic* case these are again diagonal,

$$\eta_{+,+}^{(+)} = \frac{3\omega_s \varepsilon_0}{8U_{s+}} \int (A_+^{\text{mx}} + B_+^{\text{mx}}) (\mathbf{u}_{s+}^* \cdot \mathbf{u}_{2+}) (\mathbf{u}_{1+}^* \cdot \mathbf{u}_{b+,+}) dV, \quad (32)$$

$$\eta_{-,-}^{(+)} = \frac{3\omega_s \varepsilon_0}{8U_{s-}} \int (A_+^{\text{mx}} + C_+^{\text{mx}}) (\mathbf{u}_{s-}^* \cdot \mathbf{u}_{2+}) (\mathbf{u}_{1+}^* \cdot \mathbf{u}_{b+,-}) dV, \quad (33)$$

(and $\eta_{+,-}^{(+)} = \eta_{-,+}^{(+)} = 0$); similarly for $\mathbf{M}^{(-)}$ with tuples $(-\omega_s; \Omega_-, \omega_1, -\omega_2)$. If the cavity exhibits linear circular mixing at the sideband (nonzero $\Lambda_{b\pm}$), $\mathbf{K}_{b\pm}$ accounts for it and the diagonality of $\mathbf{M}^{(\pm)}$ and $\mathbf{Z}^{(\pm)}$ still holds for an isotropic $\chi^{(3)}$.

Adiabatic elimination and effective probe coupling. When $\mathbf{K}_{b\pm}$ are “fast” (sidebands off-resonant or strongly damped), set $\dot{\mathbf{b}}_{\pm} \simeq \mathbf{0}$ in (28):

$$\mathbf{b}_+ \simeq i(A_1 A_2^*) \mathbf{K}_{b+}^{-1} \mathbf{Z}^{(+)} \mathbf{a}, \quad \mathbf{b}_- \simeq i(A_2 A_1^*) \mathbf{K}_{b-}^{-1} \mathbf{Z}^{(-)} \mathbf{a}.$$

Substituting into (31) gives

$$\dot{\mathbf{a}} = \left[i(\Delta_s \mathbf{I} + \mathbf{\Phi}) - \frac{\kappa_s}{2} \mathbf{I} \right] \mathbf{a} + i \mathbf{G}_{\text{eff}} \mathbf{a}, \quad (34)$$

$$\mathbf{G}_{\text{eff}} = \mathbf{M}^{(+)} \mathbf{K}_{b+}^{-1} \mathbf{Z}^{(+)} |A_1|^2 |A_2|^2 + \mathbf{M}^{(-)} \mathbf{K}_{b-}^{-1} \mathbf{Z}^{(-)} |A_1|^2 |A_2|^2. \quad (35)$$

In isotropic co-rotating pumps, $\mathbf{Z}^{(\pm)}$ and $\mathbf{M}^{(\pm)}$ are diagonal, so \mathbf{G}_{eff} acquires off-diagonal terms *only* through the linear sideband block $\mathbf{K}_{b\pm}^{-1}$ (i.e., via $\Lambda_{b\pm} \neq 0$) or through asymmetry between the two arms. In counter-rotating pumps, only a single element in each $\mathbf{Z}^{(\pm)}$ is nonzero, reproducing the simpler two-equation form in the main text.

A Ports, Transmission/Reflection, and Polarization Rotation Angle

Input-output relations

For a mode μ coupled to one (left) and/or two (left/right) external waveguide ports with rates $\kappa_{\mu,L}, \kappa_{\mu,R}$, the standard input-output relations are

$$s_{L,\text{out}} = c_{LL} s_{L,\text{in}} + c_{LR} s_{R,\text{in}} + \sqrt{\kappa_{\mu,L}} x_\mu, \quad (36)$$

$$s_{R,\text{out}} = c_{RL} s_{L,\text{in}} + c_{RR} s_{R,\text{in}} + \sqrt{\kappa_{\mu,R}} x_\mu, \quad (37)$$

with a unitary direct-scattering matrix $C = [c_{pq}]$ fixed by energy conservation and time-reversal. For a single-ended cavity (only left port driven), $s_{R,\text{in}} = 0$ and $c_{LL} = -1$ (conventionally).

For the probe, one uses the two circular components $(+, -)$:

$$\mathbf{s}_{\text{out}} = C \mathbf{s}_{\text{in}} + \begin{bmatrix} \sqrt{\kappa_{s,L}^{(+)}} & 0 \\ 0 & \sqrt{\kappa_{s,L}^{(-)}} \end{bmatrix} \begin{bmatrix} a_+ \\ a_- \end{bmatrix} \quad (\text{left port}), \quad \text{and analogously for the right port.}$$

Transmission and reflection (single-ended example)

Driving from the left with circular components $\mathbf{s}_{\text{in}} = [s_{\text{in},+}, s_{\text{in},-}]^T$, the transmitted Jones vector is

$$\mathbf{t}(\omega_s) = \frac{\mathbf{s}_{R,\text{out}}}{\mathbf{s}_{\text{in}}} = C_R \mathbf{e}_L + \begin{bmatrix} \sqrt{\kappa_{s,R}^{(+)}} & 0 \\ 0 & \sqrt{\kappa_{s,R}^{(-)}} \end{bmatrix} (-\mathbf{M}^{-1}) \begin{bmatrix} \sqrt{\kappa_{s,L}^{(+)}} & 0 \\ 0 & \sqrt{\kappa_{s,L}^{(-)}} \end{bmatrix},$$

where $\mathbf{e}_L = [1, 0]^T$, C_R is the row of C for the right port, and

$$\mathbf{M} = \left[\frac{\kappa_s}{2} - i(\Delta_s \mathbf{I} + \Phi) \right] - i \mathbf{G}_{\text{eff}}$$

is the 2×2 dynamical matrix of the probe at steady state (with pumps fixed). The reflection matrix $\mathbf{r}(\omega_s)$ follows by replacing the right-port couplings by the left ones in the second factor and using C_{LL} in the direct term.

Polarization rotation angle from circular components

Let the transmitted probe Jones vector in the circular basis be $\mathbf{E}^{(\text{out})} = [E_+^{(\text{out})}, E_-^{(\text{out})}]^T$. Define the complex ratio

$$\rho = \frac{E_+^{(\text{out})}}{E_-^{(\text{out})}}.$$

The polarization ellipse satisfies

$$\text{rotation angle } \psi = \frac{1}{2} \arg(\rho), \quad \text{ellipticity angle } \chi = \frac{1}{2} \arcsin \left(\frac{|E_+^{(\text{out})}|^2 - |E_-^{(\text{out})}|^2}{|E_+^{(\text{out})}|^2 + |E_-^{(\text{out})}|^2} \right).$$

Equivalently, one may compute Stokes parameters

$$S_0 = |E_+|^2 + |E_-|^2, \quad S_1 = 2 \operatorname{Re}(E_+ E_-^*), \quad S_2 = 2 \operatorname{Im}(E_+ E_-^*), \quad S_3 = |E_+|^2 - |E_-|^2,$$

then $\psi = \frac{1}{2} \arctan 2(S_2, S_1)$ and $\chi = \frac{1}{2} \arcsin(S_3/S_0)$. For small rotation (nearly linear, $|E_+| \simeq |E_-|$), $\psi \simeq \frac{1}{2} \operatorname{Im}[\ln(\rho)]$.