



Applied Subsystems Design Master's degree in Space and Aeronautical Engineering

Universitat Politècnica de Catalunya

Final Project

ADCS Final Project: Tracking "El Niño"

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1 Introduction

The objective of this project is to design and simulate an **Attitude Determination** and **Control System (ADCS)** capable of orienting a satellite so that one of its body axes (specifically, the **+Z body axis**) continuously points toward a **Point of Interest (POI)** located on Earth's surface — in this case, the city of **Quito (Ecuador)** — while the satellite completes an orbital revolution around the planet.

To achieve this, a complete **attitude dynamics and control simulation** was developed in **MATLAB**. The implemented model includes the following main elements:

- The **orbital motion** of the satellite in a **700 km circular equatorial orbit**, expressed in an **Earth-Centered Inertial (ECI)** frame.
- The **rotation of the Earth** at its real angular velocity, causing the position of the POI to evolve within the inertial frame over time.
- The **rotational dynamics** of the satellite, taking into account its **inertia tensor**, the presence of **constant disturbance torques**, and the **control torques** generated by the ADCS.
- A **Proportional–Derivative–Integral (PDI)** controller implemented using **quaternions**, which avoids the singularities associated with Euler angles and ensures smooth orientation transitions.

The purpose of the controller is to minimize both the attitude error (represented by the vector part of a quaternion) and the angular rate error, maintaining the satellite's +Z body axis aligned with the line-of-sight vector from the satellite to the POI at all times.

To obtain a physically consistent and visually illustrative simulation, the code includes:

- Realistic **orbital and rotational kinematics** for both the satellite and the Earth.
- A **feedforward rate estimation** term that anticipates the necessary rotational velocity, improving transient response.
- A **3D** graphical visualization showing the Earth, the orbit, the satellite, and its body-frame axes, making it possible to observe the pointing behavior in real time.
- A video export function that generates a complete orbital animation of approximately 10 seconds, preserving the true dynamics but accelerating playback for improved visualization.

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2 Results and Analysis

The simulation demonstrates the correct performance of the implemented ADCS. Throughout the orbital revolution, the satellite successfully maintains its +Z axis continuously pointing toward the Point of Interest (Quito), compensating for both its own orbital motion and the Earth's rotation.

2.1 Attitude Behavior

During the initial phase of the simulation, the controller progressively adjusts the satellite's orientation to align the +Z body axis with the line-of-sight vector toward the POI. The quaternion-based PDI controller provides a **stable**, **accurate**, **and oscillation-free** response, allowing smooth transitions between orientations without any singularities.

The **feedforward term** enhances the system's responsiveness by predicting the angular rate variations induced by orbital motion, thus reducing tracking delay.

2.2 Visual Tracking

In the 3D representation (Fig. 1) generated in MATLAB:

- The **Earth** is displayed as a rotating sphere, with its rotation axis aligned with the inertial Z-axis.
- The **satellite** moves along its orbit, represented as a dashed circular path.
- The **body-frame axes** (X, Y, and Z) are shown as colored arrows. Throughout the entire orbit, the **+Z** axis remains directed toward Quito, fulfilling the tracking objective.
- The line-of-sight vector (Sat→POI) updates dynamically, confirming the continuous alignment between the two directions.

The **control torques** remain within the defined saturation limits ($\pm 0.8 \text{ N} \cdot \text{m}$), demonstrating a realistic actuator capability. Despite the presence of a **constant disturbance torque**, the integral term of the controller effectively eliminates steady-state error, maintaining accurate and stable pointing throughout the simulation.

The full animation of the satellite attitude control simulation can be viewed at the following link:

Google Drive { $GO7_FinalProject$.

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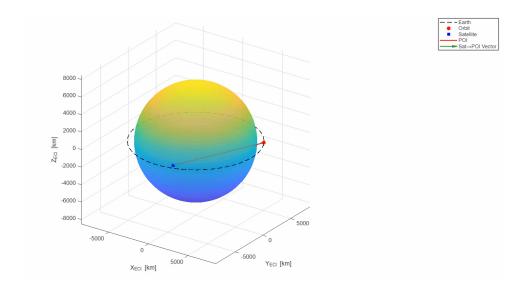


Figure 1: $+Z_{\text{body}}$ following POI (Quito).

2.3 Performance and Stability

The attitude error (vector part of the quaternion) decreases rapidly during the initial transient and remains close to zero for the rest of the simulation, confirming the **stability and robustness** of the control system. Similarly, the angular velocity smoothly converges to the desired value, and the torque commands remain **continuous and bounded**.

The final animation clearly illustrates the result: the satellite maintains its $+\mathbf{Z}$ axis directed toward the POI at all times, even as the Earth rotates and the satellite completes its orbital revolution. This demonstrates the correct performance of the implemented control algorithm.

3 Conclusions

The project successfully meets its main objective: developing a quaternion-based attitude control system capable of **tracking a fixed target on the Earth's surface** during the satellite's orbital motion.

The simulation accurately couples orbital kinematics, Earth's rotation, and satellite attitude dynamics, providing both **numerical** and **visual** validation of the control system's performance.

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The use of quaternions was essential to avoid singularities and guarantee smooth attitude representation, while the PDI control law ensured **precision**, **stability**, **and smooth tracking**. The inclusion of the feedforward term improved transient response, reducing delay and enhancing control efficiency.

Both the numerical results and the visual animation confirm that the satellite continuously maintains accurate pointing toward the Point of Interest throughout the entire orbit, satisfying the performance requirements expected from a functional ADCS.

A Appendix

Matlab code used:

```
1 clear; clc; close all;
3 %% ADCS Final Project - Víctor González Martínez
5 % Global constants and parameters
_{6} G = 6.67430e-11; \% [m^{3}/(kg s^{2})]
      = 5.972e24;
                             % [kg]
                             % [m^3/s^2]
8 \text{ mu} = G*M;
9 Re = 6371e3;
                             % [m]
10 h
      = 700e3;
                             % [m]
                             % [m]
      = Re + h;
11 r
                             % [rad/s]
_{12} wE = 2*pi/86400;
14 % POI: Quito (lat=0°, lon=-78.467834°)
15 lat = deg2rad(0.0);
lon0 = deg2rad(-78.467834);
18 % Orbital dynamics
19 T_orbit = 2*pi*sqrt(r^3/mu);
                              % [s]
w = 2*pi/T_orbit;
                                 % [rad/s]
21
22 % Time
_{23} dt = 0.5;
                                 % [s]
t_end = T_orbit;
                                 % one complete orbit
25 t = 0:dt:t_end;
26
27 % Reference kinematics (ECI)
→ in ECEF (spherical Earth)
29
30 Rz = @(ang)[cos(ang) - sin(ang) 0;
                                                           % Rotation around
              sin(ang) cos(ang) 0;
31
                            0 1];
32
r_{sat}_{ECI} = 0(tt) r * [cos(w*tt); sin(w*tt); 0*tt+0];
                                                           % Satellite
   → position in ECI (equatorial orbit, 0° inclination)
35 poi_ECI = @(tt) Rz(wE*tt) * poi_ecef;
                                                           % POI in ECI (Earth
  → rotates with wE)
v_{\text{sat}} = 0(tt) w * r * [-\sin(w*tt); \cos(w*tt); 0];
                                                           % Satellite
  \rightarrow velocity in ECI
38 % Inertia of satellite (cube + 2 panels)
_{39} m_c = 500;
                                            % Cube mass
                                            % Cube sides
_{40} L = 2;
I_c = (1/6)*m_c*L^2 * eye(3);
                                           % Main body: cube 2x2x2 m
```

```
42
                                                  % Panel mass
_{43} m_p = 50;
ax = 0.1; by = 4; cz = 2;
                                                  % Panel dimensions
_{45} Ipx = (1/12)*m_p*(by^2 + cz^2);
46 Ipy = (1/12)*m_p*(ax^2 + cz^2);
_{47} Ipz = (1/12)*m_p*(ax^2 + by^2);
48 Ip_centroid = diag([Ipx, Ipy, Ipz]);
                                                % 1.05 m from body center
50 d = 1 + ax/2;
51 Ip_shift = diag([0, m_p*d^2, m_p*d^2]);
                                              % translation in X \rightarrow adds inertia on
52 Ip_body_each = Ip_centroid + Ip_shift;
54 I_total = I_c + 2*Ip_body_each;
                                              % approx ~ diag(500,477,577) kg m^2
55 I = I_total;
56 Iinv = diag(1./diag(I));
57
58 % Control parameters
59 \text{ Kp} = 0.6;
60 \text{ Kd} = 12.0;
61 \text{ Ki} = 0.005;
62
                                               % [N \cdot m]
63 \text{ tau_max} = 0.8;
64 tau_dist = [0.01; -0.02; 0.005];
                                               % [N \cdot m]
65 int_err = [0;0;0];
66
67 % Initial attitude
q = [1;0;0;0]; q = q/ norm(q);
                                               % quaternion [qw;qx;qy;qz]
omega = [0; 0; 0.05];
                                                % rad/s
70 \text{ omega_d = [0;0;0];}
                                                % desired angular rate
71
72 % === Figure setup ===
73 fig = figure('Color','w','Name','ADCS POI Tracking','NumberTitle','off');
74 ax = gca; hold(ax,'on'); grid(ax,'on'); axis(ax,'equal')
75 xlabel('X_{ECI} [km]'); ylabel('Y_{ECI} [km]'); zlabel('Z_{ECI} [km]');
  title('+Z_{body} following POI (Quito)');
  earth_T = hgtransform('Parent', ax);
78
79
  [Ns,^{\sim}] = deal(50);
80
  [xe, ye, ze] = sphere(Ns);
81
  earth_surf = surf(Re*xe/1e3, Re*ye/1e3, Re*ze/1e3, ...
                      'EdgeColor', 'none', 'FaceAlpha', 0.7, 'Parent', earth_T);
  colormap(parula);
84
85
86 theta = linspace(0, 2*pi, 400);
^{87} plot3(ax, (r/1e3)*cos(theta), (r/1e3)*sin(theta), 0*theta, 'k--',

    'LineWidth',1);
88
sat_h = plot3(ax, 0,0,0, 'ro', 'MarkerFaceColor','r', 'MarkerSize',6);
90 poi_h = plot3(ax, 0,0,0, 'bs', 'MarkerFaceColor','b', 'MarkerSize',6);
91 los_h = plot3(ax, [0 0], [0 0], [0 0], 'r-', 'LineWidth', 1.5);
```

```
92
 93 L_brf = 400;
      brf_x = quiver3(ax, 0,0,0, 0,0,0, 'LineWidth',1.5, 'MaxHeadSize',1.5);
       brf_y = quiver3(ax, 0,0,0, 0,0,0, 'LineWidth',1.5, 'MaxHeadSize',1.5);
       brf_z = quiver3(ax, 0,0,0, 0,0,0, 'LineWidth',1.5, 'MaxHeadSize',1.5);
 97
       legend({'Earth','Orbit','Satellite','POI','Sat→POI Vector'},
         → 'Location','bestoutside');
 99 view(35,25);
      x\lim(ax,[-1.2*r, 1.2*r]/1e3); y\lim(ax,[-1.2*r, 1.2*r]/1e3); z\lim(ax,[-1.2*r, 1.2*r]/1e3); zuin(ax,[-1.2*r, 1.2*r]/1e3); zuin(ax,[-1.2*r]/1e3); zuin(ax,[-1.2*r]
100
              1.2*r]/1e3);
101
       % VIDEO RECORDING SETUP
102
       outputPath = 'C:\Users\Víctor\Desktop\Máster\1º Cuatri\Applied Subsystems
         → Design\Assignments\Final Project\simulation_ADCS.mp4';
       v = VideoWriter(outputPath, 'MPEG-4');
104
       v.FrameRate = 30;
                                                   % playback fps
       open(v);
106
107
       % we want ~10 s total duration => 10*30 = 300 frames
       % number of steps in sim = numel(t)
       frameSkip = ceil(numel(t)/300);
110
111
       % Simulation
112
       err_hist = zeros(3, numel(t));
       tau_hist = zeros(3, numel(t));
115
       for k = 1:numel(t)
116
                 tk = t(k);
117
118
                 % Positions and velocities
119
                 rs = r_sat_ECI(tk);
120
                 rp = poi_ECI(tk);
121
                 vs = v_sat_ECI(tk);
122
                 % Earth rotation (visual)
124
                 set(earth_T, 'Matrix', makehgtform('zrotate', wE*tk));
125
126
                 % [Sat → POI] vector and desired +Z axis
127
                 los = (rp - rs); if norm(los) < eps, los = [0;0;1]; end
128
                 z_d = los / norm(los);
129
130
                 % Coherent yaw: x_d aligned with projected velocity
131
                 v_par = (dot(vs, z_d)) * z_d;
132
                 v_perp = vs - v_par;
133
                 if norm(v_perp) < 1e-6
134
                          up_ref = [0;0;1]; if abs(dot(z_d, up_ref)) > 0.97, up_ref = [1;0;0];
135
                          x_d = cross(up_ref, z_d); x_d = x_d / norm(x_d);
136
                 else
137
                           x_d = v_perp / norm(v_perp);
138
                 end
139
```

```
y_d = cross(z_d, x_d);
140
       R_d = [x_d, y_d, z_d];
141
       q_d = rotm2quat(R_d); q_d = q_d / norm(q_d);
142
143
       % Feedforward for desired rate
144
       rs_n = r_sat_ECI(tk+dt);
145
       rp_n = poi_ECI(tk+dt);
146
       vs_n = v_sat_ECI(tk+dt);
       los_n = rp_n - rs_n; if norm(los_n) < eps, los_n = [0;0;1]; end
148
       z_d_n = los_n / norm(los_n);
149
       v_{par_n} = (dot(v_{n, z_d_n})) * z_{d_n};
150
       v_perp_n = vs_n - v_par_n;
151
       if norm(v_perp_n) < 1e-6</pre>
152
            up_ref = [0;0;1]; if abs(dot(z_d_n, up_ref)) > 0.97, up_ref = [1;0;0];
153
            x_d_n = cross(up_ref, z_d_n); x_d_n = x_d_n / norm(x_d_n);
       else
155
            x_d_n = v_perp_n / norm(v_perp_n);
156
       end
       y_d_n = cross(z_d_n, x_d_n);
       R_d_n = [x_d_n, y_d_n, z_d_n];
159
       q_d_n = rotm2quat(R_d_n); q_d_n = q_d_n / norm(q_d_n);
160
161
       q_rel = quatMultiply(q_d_n, quatConj(q_d));
162
       if q_rel(1) < 0, q_rel = -q_rel; end
163
       omega_d = (2/dt) * q_rel(2:4);
164
165
       % Attitude error
166
       q_e = quatMultiply(q_d, quatConj(q)); q_e = q_e / norm(q_e);
167
       if q_e(1) < 0, q_e = -q_e; end
168
       e = q_e(2:4);
169
170
       % Control: P(e) - D(omega - omega_d) + I(e)
171
       int_err = int_err + e*dt;
172
       rate_err = omega - omega_d;
       tau_c = Kp*e - Kd*rate_err + Ki*int_err;
174
175
       % Saturation + anti-windup
176
       tau_c = max(min(tau_c, tau_max), -tau_max);
177
       for i=1:3
178
            if abs(tau_c(i)) >= tau_max*0.999
179
                int_err(i) = int_err(i) - e(i)*dt*0.5;
180
            end
       end
182
183
       % Rotational dynamics
       omega_dot = Iinv * (tau_c + tau_dist - cross(omega, I*omega));
185
       omega = omega + omega_dot*dt;
186
187
       % Quaternion kinematics
188
       q_{dot} = 0.5 * [ 0
                                -omega';
189
                         omega
                                 -skew(omega) ] * q;
190
```

```
q = q + q_dot*dt; q = q / norm(q);
191
192
       % --- Graphics update ---
193
       set(sat_h, 'XData', rs(1)/1e3, 'YData', rs(2)/1e3, 'ZData', rs(3)/1e3);
194
       set(poi_h, 'XData', rp(1)/1e3, 'YData', rp(2)/1e3, 'ZData', rp(3)/1e3);
195
       set(los_h, 'XData', [rs(1) rp(1)]/1e3, ...
196
                   'YData', [rs(2) rp(2)]/1e3, ...
197
                   'ZData', [rs(3) rp(3)]/1e3);
198
199
       R_cb = quat2rotm(q); ex = R_cb(:,1); ey = R_cb(:,2); ez = R_cb(:,3);
200
       x0 = rs(1)/1e3; y0 = rs(2)/1e3; z0 = rs(3)/1e3;
201
       set(brf_x, 'XData', x0, 'YData', y0, 'ZData', z0, ...
202
                   'UData', L_brf*ex(1), 'VData', L_brf*ex(2), 'WData',
203
                    \rightarrow L_brf*ex(3));
                   'XData', x0, 'YData', y0, 'ZData', z0, ...
204
       set(brf_y,
                   'UData', L_brf*ey(1), 'VData', L_brf*ey(2), 'WData',
205
                    \rightarrow L_brf*ey(3));
       set(brf_z,
                   'XData', x0, 'YData', y0, 'ZData', z0, ...
206
                    'UData', L_brf*ez(1), 'VData', L_brf*ez(2), 'WData',
207

    L_brf*ez(3));
208
       err_hist(:,k) = e;
209
       tau_hist(:,k) = tau_c;
210
       % draw frame occasionally (skip frames to make 10s video)
212
       if mod(k, frameSkip) == 0
213
            frame = getframe(fig);
214
            writeVideo(v, frame);
215
       end
216
   end
217
218
   % END VIDEO RECORDING
   close(v);
220
   disp(' Simulation video saved successfully at:');
   disp(outputPath);
222
223
   % Helper functions
224
   function S = skew(v)
225
   S = [ 0 -v(3) v(2);
         v(3) 0
                    -v(1);
227
        -v(2) v(1)
                     0];
228
   end
229
   function gout = quatMultiply(q1, q2)
   w1=q1(1); x1=q1(2); y1=q1(3); z1=q1(4);
232
   w2=q2(1); x2=q2(2); y2=q2(3); z2=q2(4);
233
234
   qout = [ w1*w2 - x1*x2 - y1*y2 - z1*z2;
             w1*x2 + x1*w2 + y1*z2 - z1*y2;
235
             w1*y2 - x1*z2 + y1*w2 + z1*x2;
236
             w1*z2 + x1*y2 - y1*x2 + z1*w2];
237
   end
238
239
```

```
function qconj = quatConj(q)
   qconj = [q(1); -q(2); -q(3); -q(4)];
241
242
243
   function q = rotm2quat(R)
^{244}
   tr = trace(R);
245
   if tr > 0
246
        S = sqrt(tr+1.0)*2;
247
        qw = 0.25*S;
248
        qx = (R(3,2)-R(2,3))/S;
249
        qy = (R(1,3)-R(3,1))/S;
250
        qz = (R(2,1)-R(1,2))/S;
251
   else
252
        if (R(1,1) > R(2,2)) && (R(1,1) > R(3,3))
253
            S = sqrt(1.0 + R(1,1) - R(2,2) - R(3,3))*2;
254
            qw = (R(3,2)-R(2,3))/S;
255
            qx = 0.25*S;
256
            qy = (R(1,2)+R(2,1))/S;
257
            qz = (R(1,3)+R(3,1))/S;
258
        elseif (R(2,2) > R(3,3))
259
            S = sqrt(1.0 - R(1,1) + R(2,2) - R(3,3))*2;
260
            qw = (R(1,3)-R(3,1))/S;
261
            qx = (R(1,2)+R(2,1))/S;
262
            qy = 0.25*S;
263
            qz = (R(2,3)+R(3,2))/S;
264
        else
265
            S = sqrt(1.0 - R(1,1) - R(2,2) + R(3,3))*2;
266
            qw = (R(2,1)-R(1,2))/S;
267
            qx = (R(1,3)+R(3,1))/S;
268
            qy = (R(2,3)+R(3,2))/S;
269
            qz = 0.25*S;
270
        end
271
   end
272
   q = [qw; qx; qy; qz];
   if q(1) < 0, q = -q; end
   q = q / norm(q);
276
   function R = quat2rotm(q)
278
   qw=q(1); qx=q(2); qy=q(3); qz=q(4);
279
   R = [1-2*(qy^2+qz^2), 2*(qx*qy - qz*qw), 2*(qx*qz + qy*qw);
280
         2*(qx*qy + qz*qw), 1-2*(qx^2+qz^2), 2*(qy*qz - qx*qw);
281
         2*(qx*qz - qy*qz), 2*(qy*qz + qx*qw), 1-2*(qx^2+qy^2)];
282
   end
283
```