

## 10.4.7 PWM waveform harmonics

*Fourier series:*

$$i(t) = I_0 + \sum_{j=1}^{\infty} \sqrt{2} I_j \cos(j\omega t)$$

with

$$I_j = \frac{\sqrt{2} I_{pk}}{j\pi} \sin(j\pi D) \quad I_0 = DI_{pk}$$

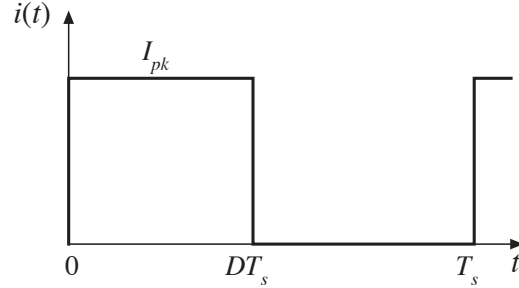
*Copper loss:*

$$\text{Dc} \quad P_{dc} = I_0^2 R_{dc}$$

$$\text{Ac} \quad P_j = I_j^2 R_{dc} \sqrt{j} \varphi_1 \left[ G_1(\sqrt{j} \varphi_1) + \frac{2}{3} (M^2 - 1) (G_1(\sqrt{j} \varphi_1) - 2G_2(\sqrt{j} \varphi_1)) \right]$$

Total, relative to value predicted by low-frequency analysis:

$$\frac{P_{cu}}{DI_{pk}^2 R_{dc}} = D + \frac{2\varphi_1}{D\pi^2} \sum_{j=1}^{\infty} \frac{\sin^2(j\pi D)}{j\sqrt{j}} \left[ G_1(\sqrt{j} \varphi_1) + \frac{2}{3} (M^2 - 1) (G_1(\sqrt{j} \varphi_1) - 2G_2(\sqrt{j} \varphi_1)) \right]$$



## Harmonic loss factor $F_H$

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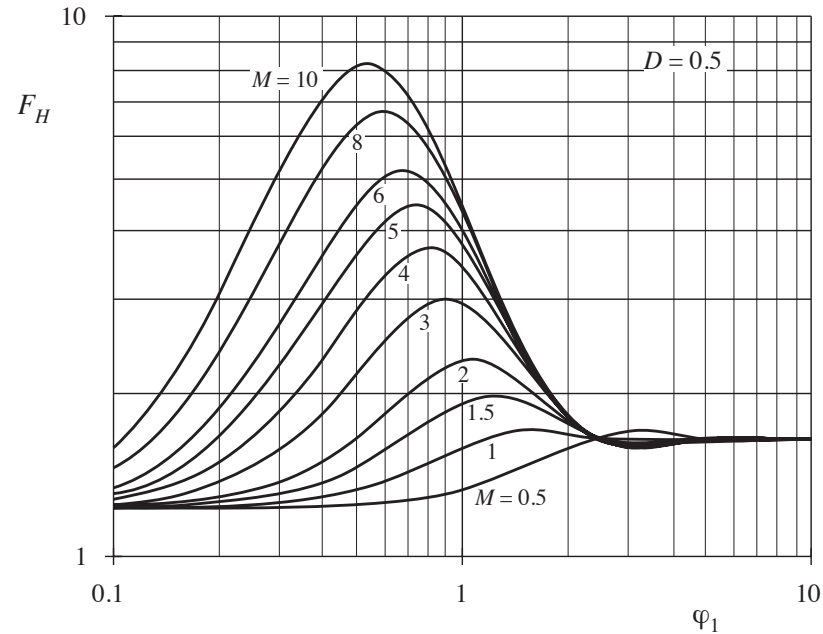
Effect of harmonics:  $F_H$  = ratio of total ac copper loss to fundamental copper loss

$$F_H = \frac{\sum_{j=1}^{\infty} P_j}{P_1}$$

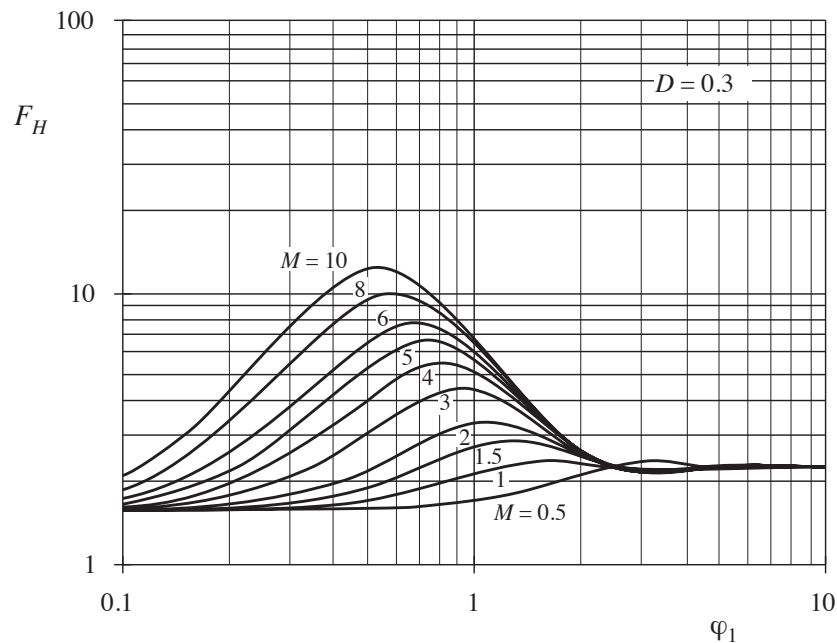
The total winding copper loss can then be written

$$P_{cu} = I_0^2 R_{dc} + F_H F_R I_1^2 R_{dc}$$

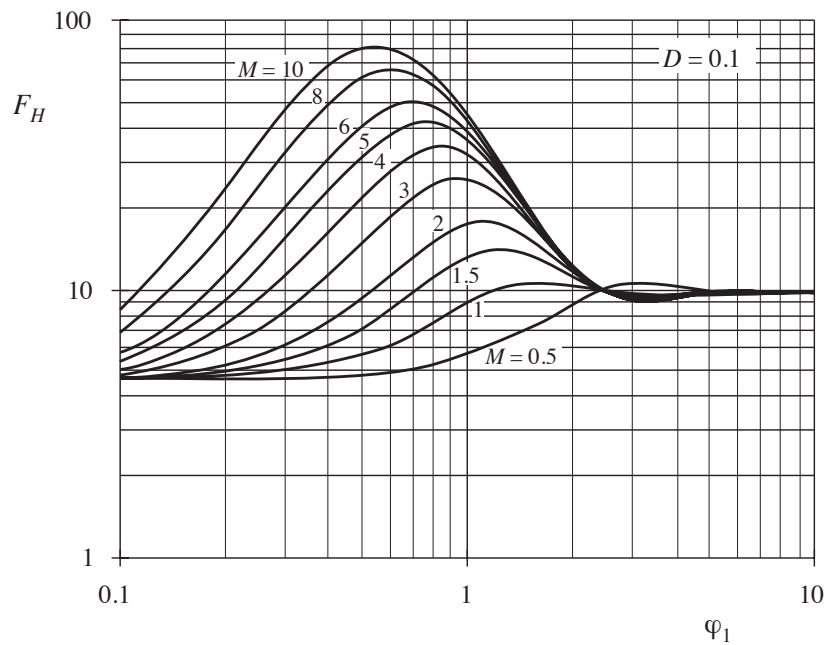
## Increased proximity losses induced by PWM waveform harmonics: $D = 0.5$



## Increased proximity losses induced by PWM waveform harmonics: $D = 0.3$



## Increased proximity losses induced by PWM waveform harmonics: $D = 0.1$



## Discussion: waveform harmonics

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- Harmonic factor  $F_H$  accounts for effects of harmonics
- Harmonics are most significant for  $\varphi_1$  in the vicinity of 1
- Harmonics can radically alter the conclusion regarding optimal wire gauge
- A substantial dc component can drive the design towards larger wire gauge
- Harmonics can increase proximity losses by orders of magnitude, when there are many layers and when  $\varphi_1$  lies in the vicinity of 1
- For sufficiently small  $\varphi_1$ ,  $F_H$  tends to the value  $1 + (\text{THD})^2$ , where the total harmonic distortion of the current is

$$\text{THD} = \frac{\sqrt{\sum_{j=2}^{\infty} I_j^2}}{I_1}$$