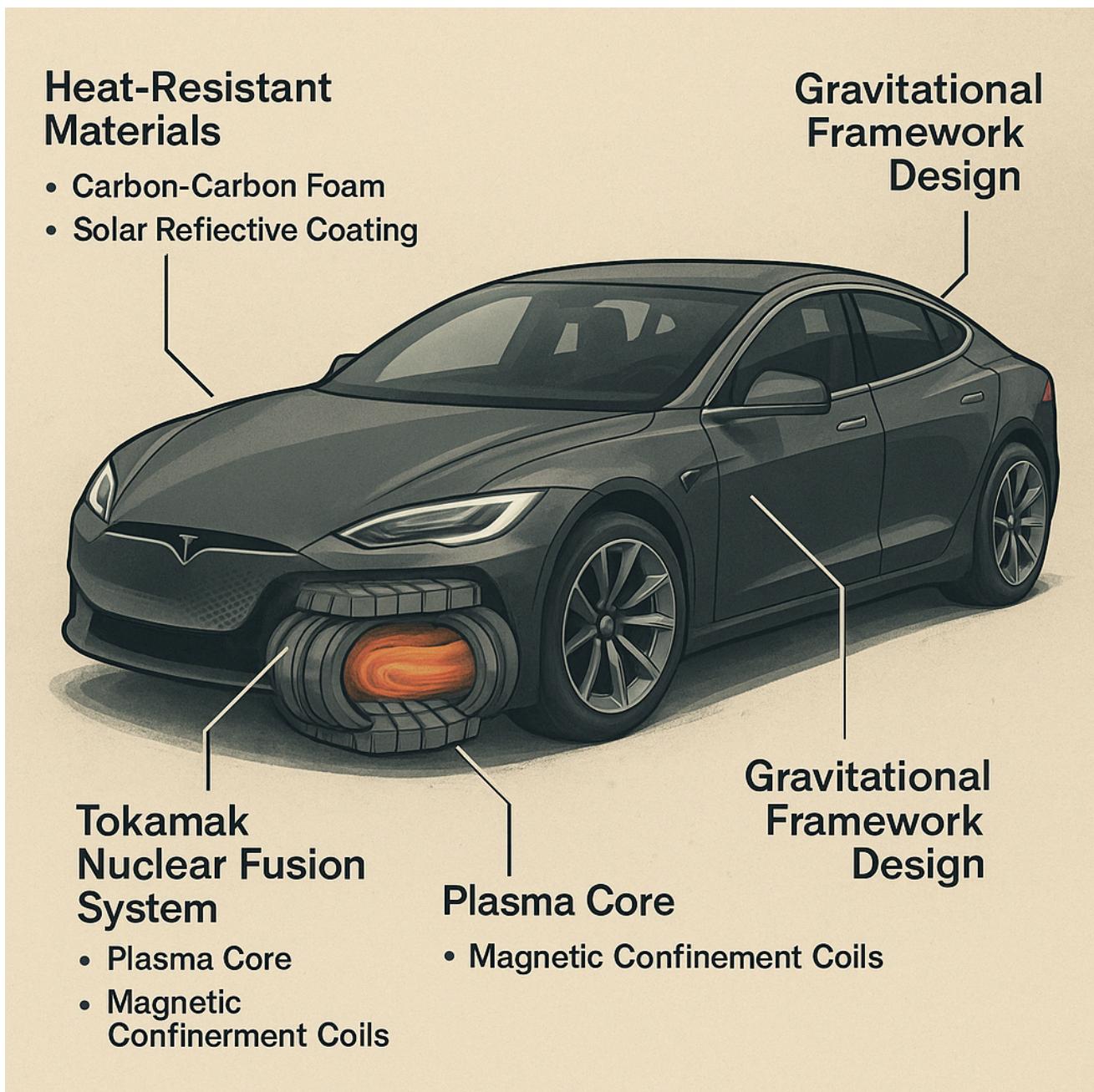


# *Technical Design Blueprint — Compact Tokamak Plasma Vehicle*

*(Plasma-powered Concept Car for Aerospace and Military Use)*

*Tesla Model S + Xilinx ZCU106 sensor fusion + FLIR Lepton integration — for a vehicle diagram. Tesla-like vehicle with a compact Tokamak plasma hybrid reactor — cross-sectional technical diagram.*



## *Prototype Concept: Plasma-Low Temperature Reactor Installation in Tesla Model S*

- *What plasma is, how it behaves, how it is studied, and how it can be controlled to achieve nuclear fusion (for example, energy similar to that produced by the Sun).*
- *It covers topics such as:*
- *Basic plasma physics: charged particles, electric and magnetic fields, and waves in plasma.*
- *Controlled fusion: how to reproduce nuclear reactions that occur in the Sun on Earth (with Tokamak reactors, Stellarator reactors, etc.).*

*Instruments and processes for studying plasma.*

### **Objective**

*Design and install a basic low-temperature plasma reactor prototype into a Tesla Model S to study alternative plasma-based propulsion and energy systems.*

### **Main Components**

#### **- Xilinx ZCU106 FPGA Board:**

*Acts as the real-time controller for plasma regulation, energy exchange monitoring, and sensor data processing.*

#### **- FLIR Lepton Thermal Sensors:**

*Embedded into the vehicle structure to monitor plasma temperature, magnetic fields, and heat distribution.*

#### **- Plasma Channeling System:**

*Composed of high-resistance ceramic composites, magnetic insulators, and multi-layer thermal shields to guide and contain the plasma at reduced temperatures.*

#### **- Power Interface:**

*Integrates the plasma energy output into the Tesla's main battery management system (BMS) through DC-DC converters.*

### **Key Functionalities**

#### **- Plasma Generation Unit:**

*Small-scale magnetic confinement system based on Tokamak principles, optimized for low-temperature, stable plasma behavior.*

#### **- Energy Harvesting:**

*Captures ionized particle flow and converts it into electrical energy to recharge batteries or assist in propulsion.*

- *Real-Time Monitoring:*

*ZCU106 runs adaptive algorithms to manage plasma density, temperature, and reactor containment.*

**Technical Challenges**

- *Thermal Management:*

*Preventing overheating and ensuring the vehicle's internal systems remain within operational limits.*

- *Magnetic Shielding:*

*Isolating sensitive electronics from plasma-induced electromagnetic fields.*

- *Plasma Stability:*

*Maintaining a continuous and controllable plasma state suitable for automotive-scale energy needs.*

**How can plasma be generated?**

Plasma = ionized gas (atoms from which electrons have been removed).

To generate it, it is usually done by:

- Heating a gas very strongly: at very high temperatures, electrons "escape" from the atoms.
- Applying strong electric fields: as in a plasma lamp or lightning.
- Applying powerful lasers or radiofrequency waves (as in laboratories or experimental reactors).

**Examples:**

- Lightning is plasma.
- Fire can contain small amounts of plasma (under certain conditions).
- Plasma reactors use electric and magnetic fields to create and confine it.

**What types of plasma exist?**

There are several ways to classify it, but the main ones are:

**Type of plasma Characteristics**

Thermal plasma: Electrons and ions at the same temperature. Very hot. E.g., interior of the Sun, electric arcs. Non-thermal plasma: Hot electrons but cold atoms. E.g., auroras, microwave plasma.

Natural plasma: Thunderstorms, northern lights, stars.

Artificial plasma: Laboratories, fluorescent lamps, experimental melters (Tokamaks).

## **Viability**

Although full plasma propulsion is still decades away, developing and testing plasma-assisted energy systems in existing EV platforms like Tesla models provides critical data for future transport innovations.

## **Future Integration**

- Hybrid propulsion combining electric and plasma energy.
- Space exploration vehicles capable of plasma energy harvesting.
- Integration of quantum control algorithms with plasma reactors. Conclusion

This prototype represents a stepping stone toward reducing dependence on fossil fuels, advancing plasma technology, and preparing for the next leap in human mobility and space exploration.

## **1. Theoretical Foundation (Francis F. Chen)**

To ground the exchange module in solid plasma physics, focus on these Chen chapters:

- **Chapter 2: Single-Particle Motion & Magnetic Confinement**

Understand how charged particles orbit field lines (Larmor radius, cyclotron frequency) to design your magnetic cusp injectors and ensure particles remain guided into the filters.

- **Chapter 3: Fluid Description of Plasmas**

Use the magnetohydrodynamic (MHD) equations (continuity, momentum, and energy) to size your heat-exchangers and electrodes, and to predict pressure gradients across the porous membranes.

- **Chapter 4: Plasma Diffusion & Transport**

Study cross-field diffusion rates to choose membrane pore sizes that balance retention time (for exchange) against plasma losses.

- **Chapter 5: Plasma Sheaths and Boundaries**

Key for designing the interface between hot plasma and solid materials—ensuring your graphene-oxide catalysts and tungsten mesh see controllable sheath potentials rather than destructive heat spikes.

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## **Vehicle Structure:**

### **1) Body Material:**

- a) *Ultra-light carbon-carbon composites* (inspired by Parker Solar Probe heat shield).
- b) *Titanium alloys* for skeleton reinforcement.
- c) *Reflective solar coating* for external thermal protection.

### **2) Plasma Reactor Chamber:**

- a) Encased in **multi-layer magnetic field shields** (using superconducting magnets).
- b) Inner walls: **Beryllium and Tungsten layers** to resist plasma erosion.

### **3) Thermal Insulation:**

- a) Vacuum insulation layer around the Tokamak core.
- b) Integration of **aerogel** and **ceramic composites**.

### **4) Radiation Shielding:**

- a) Graphene-based layers mixed with **boron carbide (B<sub>4</sub>C)** compounds.
- 

## **3. Energy Management:**

- 1) **Plasma Output** feeds high-efficiency **supercapacitors** and **solid-state batteries**.
  - 2) Direct plasma-to-electric converters (experimental).
  - 3) Autonomous cooling system with **liquid metal coolant loops**.
- 

## **4. Sensor Integration:**

### **01. Tesla-like sensor suite:**

- a. 8 Vision Cameras
- b. Front Radar

- c. 12 Ultrasonic Sensors
- d. IMU (accelerometer + gyroscope)
- e. High-precision GPS
- f. Sensor Fusion FPGA (e.g., Xilinx ZCU106, KCU116)

**02. Advanced aerospace sensors:**

- a. MEMS gravimetric detectors
  - b. Infrared/Thermal imaging arrays
- 

**5. Challenges (for illustration):**

- Plasma controls stability.
- Heat management under compact conditions.
- Neutron shielding in confined spaces.
- Minimizing reactor mass and electromagnetic interference.

**The real theoretical basis:**

1. how plasma behaves,
2. magnetic confinement,
3. basic transport equations,
4. concepts of temperature, pressure, and plasma stability.
5. It also explains the behavior in tokamaks and stellarators.

*Miniaturization Challenges for a Compact Tokamak Reactor in Vehicles*

**1. Plasma Control in Small Volume**

- Challenge: Maintain stable plasma at compact scales.
- Idea: Use superconducting micro-coils for precise magnetic confinement, inspired by stellarator techniques.

**2. Neutron Radiation Shielding**

- Challenge: Protect passengers and electronics from neutron emission.

- Idea: Multi-layer shielding combining lithium-based materials and boron carbide composites.

### **3. Thermal Management and Heat Dissipation**

- Challenge: Handle extreme localized temperatures (~10-50 million °C at plasma core).
- Idea: Inner carbon-carbon foam layers (Parker Probe material) + active liquid cooling around reactor walls.

### **4. Reactor Isolation System**

- Challenge: Fully isolate the reactor from the vehicle cabin and external environment.
- Idea:
  - Double magnetic containment layers.
  - Solid-state neutron absorbers.
  - Titanium alloy inner chambers with flexible graphene buffers.
  - Emergency plasma quenching system.

### **5. Fuel Storage and Safety**

- Challenge: Store deuterium/tritium safely and securely in vehicle scale.
- Idea: Metal hydride tanks operating at low pressures, cartridge-swappable for recharging.

### **6. Energy Conversion and Vehicle Integration**

- Challenge: Transform fusion energy into electrical and mechanical propulsion.
- Idea: Direct Magnetohydrodynamic (MHD) converters feeding high-efficiency motors.

### **7. Limiting Plasma Temperature for Practicality**

- Challenge: Prevent reaching stellar-like temperatures to ease material stress.
- Idea: Operate the reactor under 'low-confinement mode' (L-mode), achieving fusion at reduced plasma temperature (~50 million °C), still viable with advanced catalysts.

### **8. Lightweight Design Constraints**

- Challenge: Keep total mass under 600 kg (similar to Tesla Model S battery pack).
- Idea: Ultra-light composite structures based on carbon fiber + boron nitride nanoarchitectures.

### **Conclusion:**

A compact Tokamak reactor could provide a clean, near-infinite energy source for extreme mobility applications.

Control, isolation, and practical plasma handling are the keys to viable vehicular fusion systems.

The challenges of miniaturizing the tokamak reactor in a car, Including how to insulate the small reactor, And also considering the plasma's ability to be at extreme temperatures to be more practical (fuel -> energy -> car).

### ***1. Plasma Control in a Small Volume***

- Challenge: Maintain stable plasma in a small container.
- Proposal: Ultra-efficient superconducting coils, compact, high-precision magnetic fields, inspired by Stellarators.

### ***2. Neutron Radiation Shielding***

- Challenge: Protect occupants and electronic systems from neutron emissions from fusion.
- Proposal: Use of advanced absorbing materials (borides, liquid lithium) and structural layers based on doped carbon nanotubes.

### ***3. Extreme Heat Management and Dissipation***

- Challenge: Internal reactor temperatures exceed 100 million °C.
- Proposal: Active heat transfer using materials such as Parker Solar Probe's Carbon-Carbon Foam.

### ***4. Fuel Delivery and Storage***

- Challenge: Safely store deuterium/tritium in a car.
- Proposal: Low-pressure metal hydride cartridges, replaceable at service stations.

### ***5. Energy Conversion to Propulsion***

- Challenge: Efficiently convert fusion energy to electricity and then to motion.
- Proposal: Magnetohydrodynamic cycles or direct induction turbines to power electric motors.

### ***6. Accident Containment***

- Challenge: Prevent plasma or radiation leaks in the event of a crash.
- Proposal: Automatic reactor shutdown systems and solidified plasma containment chambers.

### ***7. Vehicle Integration and Weight***

- Challenge: The reactor should weigh no more than the current battery of a Tesla Model S (~600 kg).
- Proposal: Use of ultralight materials (structural graphene, magnesium boride compounds) for the chassis and reactor.



Ideas for the feasibility of solar plasma or inertial fusion plasma in objects/cars and space missions: A compact tokamak-like plasma reactor in a vehicle might seem like science fiction, but it offers several theoretical advantages that explain why we proposed it in this chat:

*Ultra-high energy density*

A fusion reactor releases millions of times more energy per unit of mass than fossil fuels or chemical batteries.

With a mini-tokamak, you would have a range of thousands of kilometers with very little "fuel" (deuterium/tritium), compared to hundreds of kilometers with a conventional electric car.

*Almost instant recharging*

Instead of hours on a charger, replenishing the small fusion fuel (a few grams of isotopes) would be enough to continue driving for days or weeks.

*Zero polluting emissions*

Fusion only produces and neutrons; with good shielding and neutron capture, there is no CO<sub>2</sub>, NO<sub>x</sub>, or solid particles. Ideal for sensitive urban environments.

*Extreme Thermal Management*

Using Parker Solar Probe-type materials, you can absorb and dissipate heat from the reactor (which operates at tens of millions of degrees at its core) without burning the chassis or damaging components.

*Continuous and Reliable Power Source*

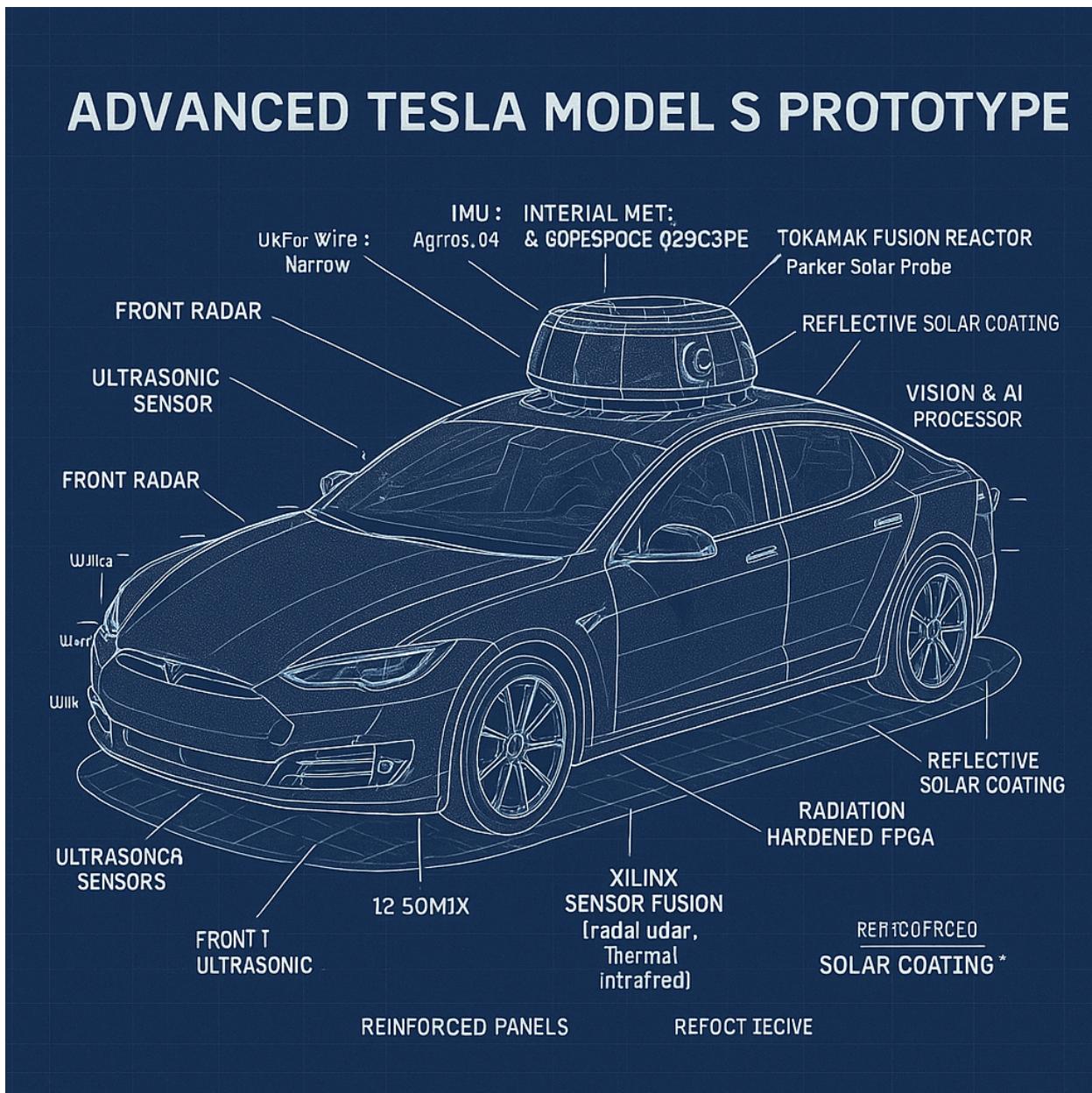
You're not dependent on the power grid or charging stations; your car is a portable power station, capable of powering not only the powertrain but also HVAC systems, sensors, AI, and electromagnetic shields.

*Power for Advanced Systems*

Spare energy for magnetic levitation technologies, plasma shields, energy weapons, or secondary propulsion (e.g., plasma pulses for extreme maneuvers).

## *Resilience in Special Missions*

For military or space applications, a mini-tokamak is lighter and more compact than a conventional generator and better withstands cosmic radiation or EMP attacks, thanks to its shielding and magnetic control systems. A note of realism: Miniaturizing a tokamak to automobile size is a huge challenge today: plasma control, neutron shielding, and heat management are still under investigation. But conceptually, a compact fusion reactor would offer a vehicle a clean, ultra-powerful, and self-contained energy source, forever changing advanced mobility.



## Design of mini plasma & sensors for tesla;

### 1 (Tesla Model S + Xilinx ZCU106 + FLIR Lepton Sensors)

A technical blueprint cross-sectional illustration of a Tesla Model S chassis. Show 8 exterior vision cameras (front, rear, and side views), one forward-looking radar at the nose, and 12 ultrasonic range sensors distributed around the body. Add small FLIR Lepton thermal imagers at the front corners, rear bumper, and sides. Draw wires or data lines from each sensor converging on a central **Xilinx ZCU106** sensor-fusion module inside the car. Annotate each camera, radar, ultrasonic sensor, thermal sensor, and the ZCU106 block with labels. Include arrows to indicate the data flow from sensors into the fusion unit.

### 2 (Tesla + Compact Tokamak Plasma Reactor)

A technical blueprint cross-section of a futuristic Tesla-like electric vehicle equipped with a compact tokamak fusion reactor mounted at the rear. Depict a toroidal fusion chamber (tokamak) with its vacuum vessel and magnetic confinement coils wrapped around a glowing deuterium-tritium plasma core. The reactor should be enclosed by **inner insulation** of carbon-carbon foam and an **outer shield** of boron-carbide ( $B_4C$ ). Draw insulated piping or ducts channeling the reactor's plasma/heat from the tokamak to an onboard heat exchanger or turbine that drives the electric drivetrain. Show hybrid electric motors on the axles receiving power from this system. Annotate all major parts with labels: "*Magnetic Coil*", "*Plasma Chamber*", "*Carbon-Carbon Insulation*", " *$B_4C$  Radiation Shield*", "*Plasma Pipe*", "*Heat Exchanger*", "*Electric Motor*", etc. Include arrows to indicate energy flow from the fusion core through the exchanger to the motors. Style the illustration as a monochrome engineering blueprint with crisp line-work and technical labeling.

#### Sensor Fusion System Integration Plan

- \*\*Sensors:\*\* 8 exterior cameras (surround-view) + 1 forward radar + 12 ultrasonic sensors, covering 360° around the vehicle. Multiple FLIR Lepton thermal cameras are mounted at key points (front corners, rear, sides) for infrared imaging.
- \*\*Fusion Module:\*\* Central AMD/Xilinx Zynq UltraScale+ \*\*ZCU106\*\* board inside the car aggregates all sensor data.
- \*\*Data Bus:\*\* Each sensor's data (video streams, radar return signals, ultrasonic ranges, thermal images) is sent to the ZCU106 over high-speed interfaces (e.g. MIPI CSI for cameras, CAN or Ethernet for radar, SPI/CAN for thermal).
- \*\*Processing:\*\* The ZCU106's SoC includes a quad-core ARM CPU cluster and FPGA

The FPGA fabric handles real-time signal pre-processing (image rectification, radar pulse processing, etc.), while the ARM CPU cores run the higher-level fusion algorithms and driving logic.

- **Output:** The fusion unit produces a combined environmental model (object positions, velocities, and thermal signatures) used by the Autopilot controller for navigation and safety.

### Plasma Hybrid System Design

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- **Tokamak Reactor:** A mini toroidal fusion chamber sits behind the rear axle. It includes a vacuum vessel containing a high-temperature deuterium-tritium plasma core, with superconducting magnetic field coils wrapped around it.

- **Insulation & Shielding:** The inner wall of the tokamak is lined with carbon-carbon composite foam to provide thermal insulation. The outer shell of the reactor is surrounded by boron-carbide ( $B_4C$ ) blocks, serving as a neutron and gamma

- **Energy Transfer:** Insulated pipes carry the reactor's plasma or high-temperature coolant to an onboard heat-exchange turbine system. (In the diagram, show fluid/plasma flow lines from the tokamak to the turbine.)

- **Drivetrain:** The turbine/generator converts fusion energy into electricity that powers the vehicle's electric motors (e.g. dual motors, one per axle). Show arrows indicating power flow from the reactor/turbine to the motors.

- **Labels:** Mark all key components on the blueprint: \*Magnetic Coils\*, \*Plasma Core\*, \*Vacuum Vessel\*, \*Insulation\*, \* $B_4C$  Shield\*, \*Pipes/Conduits\*, \*Heat Exchanger/Turbine\*, \*Electric Motors\*.

### Materials and Thermal Protection Choices

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- **Carbon-Carbon Foam:** Used as high-temperature thermal insulation on the reactor's inner wall (it has a very high melting point and is low-weight).

- **Boron Carbide ( $B_4C$ ):** Selected for the outer radiation shield due to its hardness and excellent neutron-absorption

- **Refractory Alloys/Ceramics:** The tokamak vessel and piping employ tungsten alloys or ceramic composites to withstand plasma-level heat loads ( $\sim 10^8$ - $10^9$  K). These materials maintain strength and integrity under neutron bombardment.

- **Active Cooling:** Coolant loops (water or liquid metal channels) circulate around the reactor blanket to carry away residual heat. High-efficiency heat-exchanger radiators are implied to dump waste heat.

- **Safety:** Multi-layer insulation and reflective coatings on surrounding vehicle structure minimize heat leakage. All materials are chosen to minimize activation (long-lived radioactivity) and protect occupants from radiation.

Basic Connection Diagram

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Sensors -> ZCU106 (Fusion Processor) -> Tokamak Reactor -> Electric Motors

Future Viability Discussion

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- \*\*Current Status:\*\* Fusion power today is achieved only in massive experimental devices (e.g. ITER, hundreds of meters in size). No compact tokamak exists anywhere near car-scale.
- \*\*Past Efforts:\*\* For example, Lockheed Martin's "Compact Fusion Reactor" project aimed for a small prototype (announced 2014), but it was abandoned by

This underscores the difficulty of building a compact fusion engine.

- \*\*Technical Challenges:\*\* Major hurdles include attaining \*net-positive\* fusion energy, controlling a stable plasma, managing extreme thermal loads (millions of °C), and providing extremely heavy radiation shielding in a small space.
- \*\*Conclusion:\*\* A fusion-powered Tesla remains a theoretical concept. Making it real would require breakthroughs in fusion physics, advanced materials, and safety engineering far beyond current capabilities.

## Microwave Plasma Reactor Prototype for Vehicles (simpler and realistic)

### Project Name:

**Low-Cost Microwave Plasma Generator for Energy Research in Vehicles**

### Objective:

Design and build a small plasma generation system using microwave sources (e.g., modified microwave oven magnetrons) to create plasma inside a compact, controlled chamber embedded into a vehicle for experimental energy studies.

### Main Components:

- **Magnetron Microwave Source (2.45 GHz, ~1-2 kW)**
- **Waveguide and Resonant Cavity (stainless steel or copper chamber)**
- **Plasma Gas Injection System (argon or air at low pressure)**
- **Xilinx ZCU106 FPGA Board (for real-time sensor control and monitoring)**

- **Thermal Sensors** (FLIR Lepton or thermocouples to monitor heat)
- **Vehicle Battery Integration** (power supply adapted to vehicle system)

**Functionalities:**

- *Plasma generation at atmospheric or low pressure.*
- *Real-time monitoring of plasma parameters.*
- *Energy harvesting experiments (e.g., small thermoelectric generation or inductive plasma effects).*
- *Testing plasma's effect on vehicle thermal management.*

**Challenges:**

- *Controlling plasma ignition without damaging nearby vehicle electronics.*
  - *Ensuring thermal insulation around the plasma chamber.*
  - *Preventing microwave leakage (use of Faraday cage shielding).*
- 

***Combustion-Plasma Hybrid Reactor for Car Engines (linked to real combustion)***

**Project Name:**

***Plasma-Assisted Combustion System for Internal Combustion Engines (ICE)***

**Objective:**

*Develop a prototype system that injects plasma (arc or microwave plasma) into the air-fuel mixture of a combustion engine to improve ignition efficiency and reduce emissions.*

**Main Components:**

- **High-Voltage Plasma Injector** (arc plasma igniter or microwave plasma torch)

- **Control Unit** (*Xilinx ZCU106 FPGA for real-time ignition control*)
- **Temperature and Pressure Sensors** (*for closed-loop control*)
- **Modified Intake Manifold** (*to integrate plasma source*)
- **Power Interface** (*small DC-DC converter for plasma torch*)

**Functionalities:**

1. *Enhanced ignition at lean air-fuel ratios (better efficiency).*
2. *Faster, more uniform combustion.*
3. *Lower NO<sub>x</sub> and particulate emissions.*
4. *Real-time plasma regulation based on engine load and RPM.*

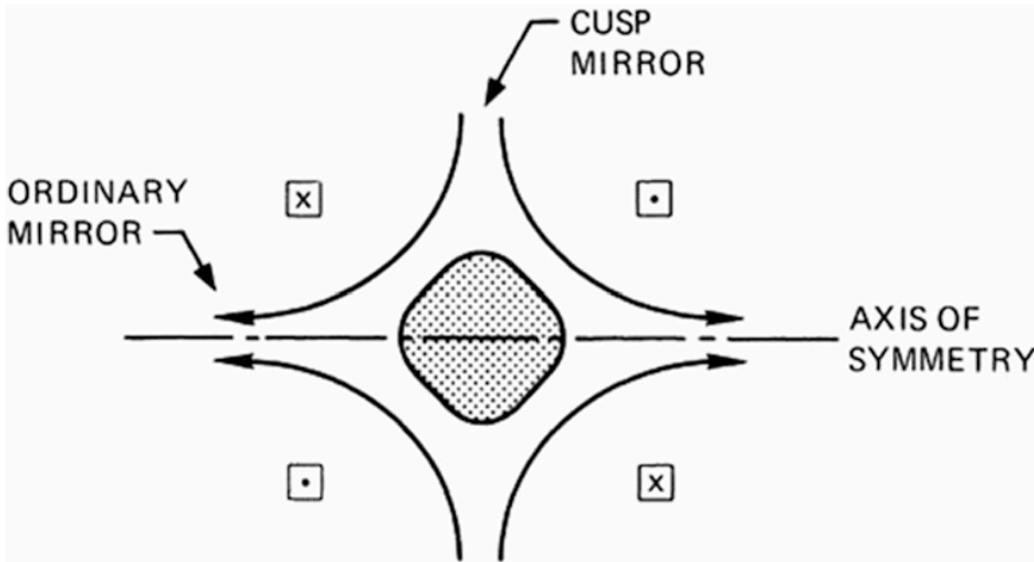
**Challenges:**

- *Safely integrating plasma devices with vehicle electronics.*
- *Managing heat from the plasma source.*
- *Avoiding plasma device degradation in harsh engine environments.*

Already being researched in automotive engineering (plasma-assisted combustion exists in experimental stages); a basic prototype could be made using spark plugs modified into mini plasma arcs.

(A) Magnetic Pumping. If the strength of  $B$  in a mirror confinement system is varied sinusoidally, the particles'  $v \perp$  would oscillate; but there would be no gain of energy in the long run. However, if the particles make collisions, the invariance of  $\mu$  is violated, and the plasma can be heated. In particular, a particle making a collision during the compression phase can transfer part of its gyration energy into  $v_k$  energy, and this is not taken out again in the expansion phase. (B) Cyclotron Heating. Now imagine that the  $B$  field is oscillated at the frequency  $\omega_0$ . The induced electric field will then rotate in phase with some of the particles and accelerate their Larmor motion continuously. The condition  $\omega = \omega_0$  is violated,  $\mu$  is not conserved, and the plasma can be heated. (C) Magnetic Cusps. If the current in one of the coils in a simple magnetic mirror system is reversed, a magnetic cusp is formed (Fig. 2.14). This configuration has, in addition to the usual mirrors, a spindle-cusp mirror extending over 360° in azimuth. A plasma confined in a cusp device is supposed to have better stability properties than that in an ordinary mirror. Unfortunately, the loss-cone losses are larger because of the additional loss region; and the particle motion is nonadiabatic. Since the  $B$  field vanishes at the center of symmetry,  $\omega_0$  is zero there; and  $\mu$  is not

preserved. The local Larmor radius near the center is larger than the device. Because of this, the adiabatic invariant  $\mu$  does not guarantee that particles outside a loss cone will stay outside after passing through the nonadiabatic region. Fortunately, there is in this case another invariant: the canonical angular momentum  $p\theta^{1/4}mr\nu\theta \propto A\theta$ . This ensures that there will be a population of particles trapped indefinitely until they make a collision:



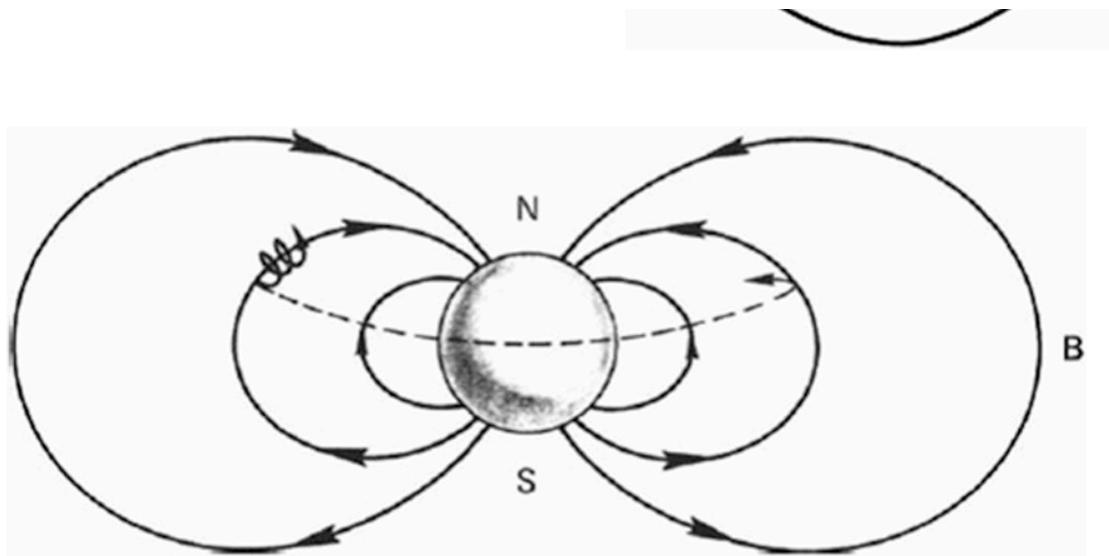
### Plasma confinement in a cusped magnetic field

The Second Adiabatic Invariant,  $J$  Consider a particle trapped between two magnetic mirrors: It bounces between them and therefore has a periodic motion at the “bounce frequency.” A constant of  $\beta$  this motion is given by  $mvkds$ , where  $ds$  is an element of path length (of the guiding center) along a field line. However, since the guiding center drifts across field lines, the motion is not exactly periodic, and the constant of the motion becomes an adiabatic invariant. This is called the longitudinal invariant  $J$  and is defined for a half-cycle between the two turning points

$$J = \int_a^b v_{||} ds$$

$J$  is invariant in a static, nonuniform  $B$  field; the result is also true for a slowly time-varying  $B$  field.

If the magnetic field were perfectly symmetric, the particle would eventually drift back to the same line of force. However, the actual field is distorted by such effects as the solar wind. In that case, will a particle ever come back to the same line of force



## ● Combined Project

Name:

Controlled Microwave Plasma Reactor with Magnetic Confinement Metrics

Objective:

Develop a **microwave plasma generator** embedded in a **small-scale vehicle system**, equipped with **magnetic control** to stabilize and study plasma dynamics via **adiabatic invariants ( $J$ )**.

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## 🌐 Project Structure

### 1. Plasma Generator (Microwave Source)

- Magnetron-based 2.45 GHz microwave plasma generator.
- Compact stainless steel resonant cavity.
- Argon or low-pressure air as plasma medium.

## 2. Magnetic Control System

- Helmholtz coils or custom solenoids surrounding the plasma chamber.
- Power electronics (PWM-controlled) for real-time B-field adjustment.
- FPGA (Xilinx ZCU106) reading plasma sensors and adjusting coil currents.

## 3. Plasma Monitoring and Adiabatic Metrics

- Sensors: B-field probes, Langmuir probes, thermocouples, optical sensors (emission spectroscopy).
- Real-time script calculating plasma metrics from kinetic equations.



## Plasma Magnetic Metrics Script

To prove the invariance of  $J$ :

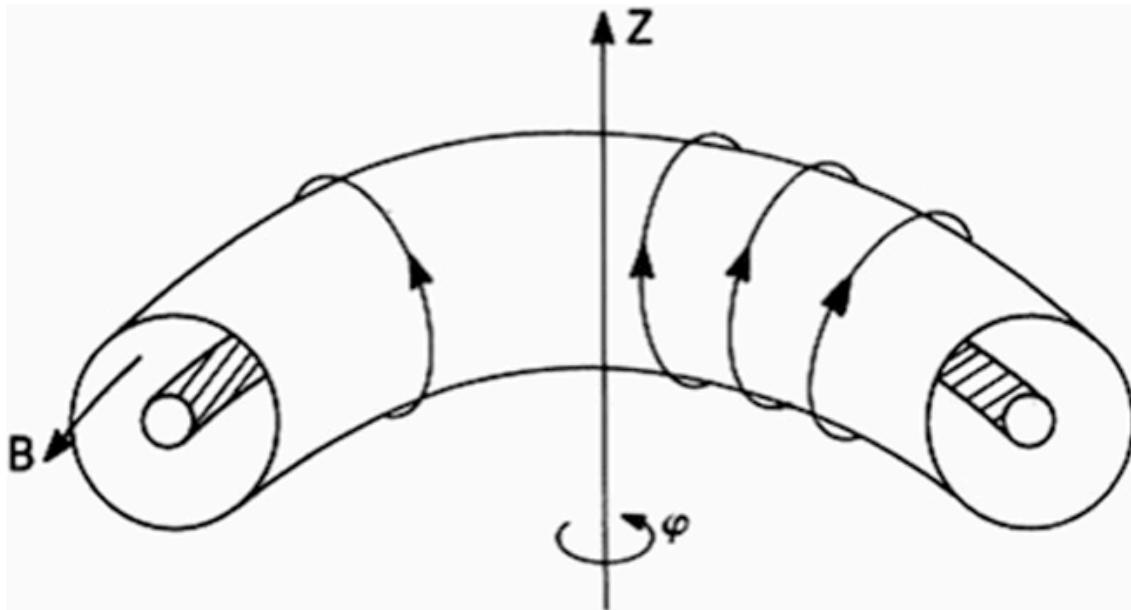
1.  $\delta s / R_c \propto \delta s_0 / R_{c0}$  – Guiding center drift correction.
2. From the drift velocity components:  
 $v_{gc} = (v \nabla B + vR) = (1/2) * (v \perp rL / B) * (\nabla B / B^2)$
3. Rate of change of  $\delta s$ :  
 $(1/\delta s) * (d(\delta s)/dt) = (1/2) * (m/q) * (v \perp^2 / B^3) * (B \cdot \nabla B) / R_c^2$
4. Parallel energy conservation:  
 $v_{||} = \sqrt((2/m) * (W - \mu B))$
5. Time derivative of  $v_{||}$ :  
 $(dv_{||}/dt) / v_{||} = (\mu/q) * (R_c B \cdot \nabla B) / (R_c^2 B^2)$
6. Combined conservation:  
 $d/dt (v_{||} \delta s) = 0 \Rightarrow v_{||} \delta s = \text{constant}$

Thus, under slow guiding center drift,  $J$  is conserved:

$$J = \int_a^b v_{||} ds = \text{constant}$$

[Microwave Plasma] → [Sensors] → [FPGA reads B,  $v\parallel$ ,  $v\perp$ ]  
 → [Compute J metrics] → [PID Controller for Coils] → [Adjust Magnetic Field B]

[Microwave Plasma] → [Sensors] → [FPGA reads B,  $v\parallel$ ,  $v\perp$ ]  
 → [Compute J metrics] → [PID Controller for Coils] → [Adjust Magnetic Field B]



#### PLASMA CONTROL MODEL - SCRIPT

##### 1. Magnetic Control Basis

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Guiding center drift leads to changes in segment  $\delta s$ .

Demonstrated:

$$d(\delta s)/dt + d(vk)/dt = 0 \quad \rightarrow \quad vk\delta s = \text{constant}$$

Thus, first invariant  $J = \int_a^b vk ds$  is constant under slow changes in B.

Important Equations:

$$v_{gc} = (1/2) v\perp r_L (B \times \nabla B) / B^2 + \dots \quad [\text{drift velocity components}]$$

$\delta s(t)$  evolves with drift, but  $vk\delta s$  remains invariant due to cancellation.

Applications:

- Magnetic bottle confinement
- Magnetic mirrors

- Controlled heating schemes

## 2. Third Adiabatic Invariant $\Phi$

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Slow guiding center drift defines a flux surface.

Invariant:

$$\Phi = \oint \mathbf{B} \cdot d\mathbf{S} = \text{constant}$$

If magnetic field  $B$  varies slowly, the drift surface adjusts to preserve total flux.

Violation Example:

- Ionospheric hydromagnetic wave excitation:
  - Particle orbits resonate with B-wave phase.
  - Particle energy transfers into wave growth.

Key Insight:

$\Phi$  invariance is robust unless  $B$  fluctuates on timescales comparable to drift period.

## 3. Plasma Heating and Energy Gain

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Energy gain despite Lorentz Force ( $q \mathbf{v} \times \mathbf{B} \perp \mathbf{v}$ ):

- Compression:  $\mu = mv_{\perp}^2/(2B)$  constant  $\Rightarrow T_{\perp}$  increases with  $B$
- Radiofrequency waves ( $E \perp B$ ):
  - Polarization drift  $v_p$  necessary.
  - $v_p$  found from energy conservation:
 
$$d(1/2 mv_E^2)/dt = v_p \cdot E$$

## 4. Problems for Simulation/Validation

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[2.13] Derive  $T$  evolution from  $v_{kL}$  invariance.

[2.14] Explain energy gain under adiabatic compression.

[2.15] Derive polarization drift  $v_p$  from oscillating E-field energy.

[2.16] Analyze adiabaticity:

- $E \perp B$ ,  $\omega = 10^9$  rad/s,  $B = 1T$ .
- Electrons
  - Ions

[2.17] Proton acceleration:

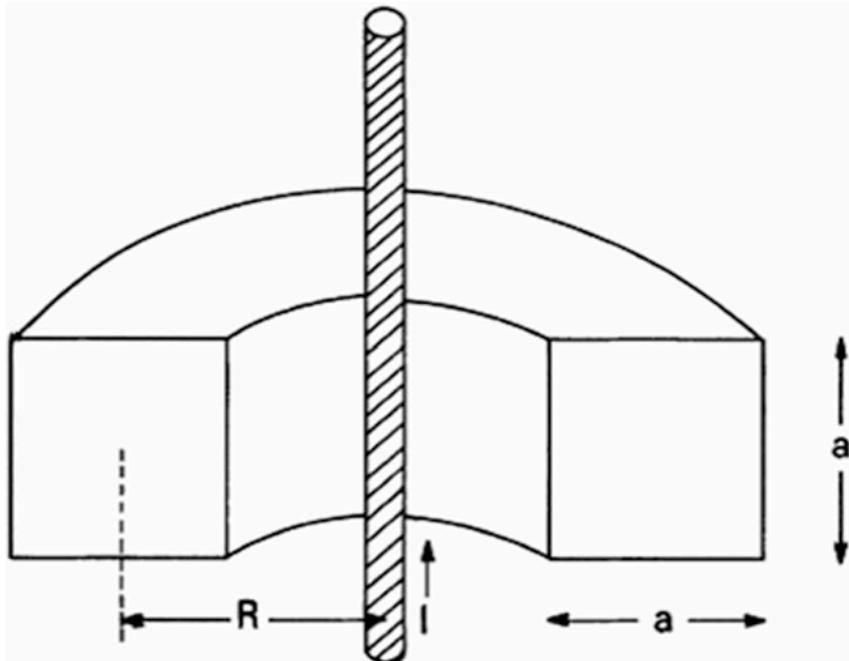
- Start:  $v_k = 0$ ,  $B: 0.1 T \rightarrow 1T$  (slow)
  - Elastic collision:  $v_{\perp} \rightarrow v_k$
  - Decrease  $B: 1T \rightarrow 0.1T$
- Find final proton energy.

[2.18] Plasma torus compression:

- B field:  $1T \rightarrow 3T$  in  $100\mu s$
- Show  $\mu$  invariance.

- Find final  $T_{\perp}$  and  $T_k$  for electrons and ions.

A uniform plasma is created in a toroidal chamber with square cross section, as shown. The magnetic field is provided by a current  $I$  along the axis of symmetry. The dimensions are  $a \approx 1$  cm,  $R \approx 10$  cm. The plasma is Maxwellian at  $KT \approx 100$  eV and has density  $n \approx 10^{19}$  m<sup>-3</sup>. There is no electric field



### *Plasma Theoretic -relations. Project (Tesla cars, space)*

- (a) Draw typical orbits for ions and electrons with  $v_k = 0$  drifting in the nonuniform  $B$  field.
- (b) Calculate the rate of charge accumulation (in coulombs per second) on the entire top plate of the chamber due to the combined  $v \nabla B$  and  $v R$  drifts. The magnetic field at the center of the chamber is 1 T, and you may make a large aspect ratio ( $R/a$ ) approximation where necessary.
- 2.20. Suppose the magnetic field along the axis of a magnetic mirror is given by  $B_z = B_0(1 + \alpha^2 z^2)$ .
- (a) If an electron at  $z = 0$  has a velocity given by  $v^2 = 3v_{\parallel}^2 + v_{\perp}^2$ , at what value of  $z$  is the electron reflected?
- (b) Write the equation of motion of the guiding center for the direction parallel to the field.
- (c) Show that the motion is sinusoidal, and calculate its frequency.

(d) Calculate the longitudinal invariant  $J$  corresponding to this motion.

2.21. An infinite straight wire carries a constant current  $I$  in the  $+z$  direction. At  $t = 0$ , an electron of small gyroradius is at  $z = 0$  and  $r = r_0$  with  $v_{\perp 0} = v k_0$ . ( $\perp$  and  $k$  refer to the direction relative to the magnetic field).

(a) Calculate the magnitude and direction of the resulting guiding center drift velocity.

(b) Suppose that the current increases slowly in time in such a way that a constant electric field in the  $z$  direction is induced. Indicate on a diagram the relative directions of  $I$ ,  $B$ ,  $E$ , and  $vE$ .

(c) Do  $v_{\perp}$  and  $vk$  increase, decrease, or remain the same as the current increases? Why?

## Chapter 3

### Plasmas as Fluids

#### 3.1 Introduction

In a plasma the situation is much more complicated than that in the last chapter; the  $E$  and  $B$  fields are not prescribed but are determined by the positions and motions of the charges themselves. One must solve a self-consistent problem; that is, find a set of particle trajectories and field patterns such that the particles will generate the fields as they move along their orbits, and the fields will cause the particles to move in those exact orbits. And this must be done in a time-varying situation. It sounds very hard, but it is not.

We have seen that a typical plasma density might be  $10^{18}$  ion-electron pairs per  $m^3$ . If each of these particles follows a complicated trajectory and it is necessary to follow each of these, predicting the plasma's behavior would be a hopeless task. Fortunately, this is not usually necessary because, surprisingly, the majority—perhaps as much as 80%—of plasma phenomena observed in real experiments can be explained by a rather crude model. This model is used in fluid mechanics, in which the identity of the individual particle is neglected, and only the motion of fluid elements is taken into account. Of course, in the case of plasmas, the fluid contains electrical charges. In an ordinary fluid, frequent collisions between particles keep the particles in a fluid element moving together. It is surprising that such a model works for plasmas, which generally have infrequent collisions. But we shall see that there is a reason for this.

In the greater part of this book, we shall be concerned with what can be learned from the fluid theory of plasmas. A more refined treatment—the kinetic theory of plasmas—requires more mathematical calculation than is appropriate for an introductory course. An introduction to kinetic theory is given in Chap. 7. In some plasma problems, neither fluid theory nor kinetic theory is sufficient to describe the plasma's behavior. Then one has to fall back on the tedious process of following the individual trajectories. Modern computers can do this, although they have only enough memory to store the position and velocity components for about  $10^6$  particles if all three dimensions are involved. Nonetheless, computer simulation plays an important role in filling the gap between theory and experiment in those instances where even kinetic theory cannot come close to explaining what is observed.

## **3.2 Relation of Plasma Physics to Ordinary Electromagnetics**

### **3.2.1 Maxwell's Equations**

**In vacuum:**

$$\epsilon_0 \nabla \cdot E = \sigma$$

$$\nabla \cdot E = \partial B / \partial t$$

$$\nabla \cdot B = 0$$

$$\nabla \times B = \mu_0 j + \epsilon_0 \partial E / \partial t$$

**In a medium:**

$$\nabla \cdot D = \sigma$$

$$\nabla \cdot E = \partial B / \partial t$$

$$\nabla \cdot B = 0$$

$$\nabla \times H = j + \partial D / \partial t$$

$$D = \epsilon E$$

$$B = \mu H$$

(3.1) (3.2) (3.3) (3.4)

(3.5) (3.6) (3.7) (3.8)

(3.9) (3.10)

In Eqs. (3.5) and (3.8),  $\sigma$  and  $j$  stand for the “free” charge and current densities. The “bound” charge and current densities arising from polarization and magnetization of the medium are included in the definition of the quantities  $D$  and  $H$  in terms of  $\epsilon$  and  $\mu$ . In a plasma, the ions and electrons comprising the plasma are the equivalent of the “bound” charges and currents. Since these charges move in a complicated way, it is impractical to try to lump their effects into two constants  $\epsilon$  and  $\mu$ . Consequently, in plasma physics, one generally works with the vacuum equations (3.1)–(3.4), in which  $\sigma$  and  $j$  include all the charges and currents, both external and internal.

Note that we have used  $E$  and  $B$  in the vacuum equations rather than their counterparts  $D$  and  $H$ , which are related by the constants  $\epsilon_0$  and  $\mu_0$ . This is because the forces  $qE$  and  $j B$  depend on  $E$  and  $B$  rather than  $D$  and  $H$ , and it is not necessary to introduce the latter quantities as long as one is dealing with the vacuum equations.

### **3.2.2 Classical Treatment of Magnetic Materials**

Since each gyrating particle has a magnetic moment, it would seem that the logical thing to do would be to consider a plasma as a magnetic material with a permeability  $\mu_m$ . (We have put a subscript  $m$  on the permeability to distinguish it from the adiabatic invariant  $\mu$ .) To see why this is not done in practice, let us review the way magnetic materials are usually treated.

The ferromagnetic domains, say, of a piece of iron have magnetic moments  $\mu_i$ , giving rise to a bulk magnetization  $M = (1/V) \sum \mu_i$  per unit volume. This has the same effect as a bound current density equal to  $j_b = \nabla \cdot M$ .

In the vacuum equation (3.4), we must include in  $j$  both this current and the “free,” or externally applied, current  $j_f$ :

$$\mu_0 \nabla \times B = j_f + j_b + \epsilon_0 \partial E / \partial t$$

We wish to write Eq. (3.13) in the simple form:

$\nabla \times H = j_f + \epsilon_0 \partial E / \partial t$  by including  $j_b$  in the definition of  $H$ . This can be done if we let:

$$H = \mu_0^{-1} B + M$$

To get a simple relation between  $B$  and  $H$ , we assume  $M$  to be proportional to  $B$  or  $H$ :

$$M = \chi \square H$$

The constant  $\chi$  is the magnetic susceptibility. We now have:

$$B = \mu_0(1 + \chi) H = \mu_m H$$

This simple relation between  $B$  and  $H$  is possible because of the linear form of Eq. (3.16).

In a plasma with a magnetic field, each particle has a magnetic moment  $\mu_\chi$ , and the quantity  $M$  is the sum of all these  $\mu_\chi$ 's in  $1 \text{ m}^3$ . But we now have:

$$\mu_\chi = (mv \perp^2) / 2B$$

The relation between  $M$  and  $H$  (or  $B$ ) is no longer linear, and we cannot write  $B = \mu_m H$  with  $\mu_m$  constant. It is therefore not useful to consider a plasma as a magnetic medium.

### ***Classical Treatment of Dielectrics***

The polarization  $P$  per unit volume is the sum over all the individual moments  $p_i$  of the electric dipoles. This gives rise to a bound charge density

$$\sigma_b = \nabla \cdot P \quad (3.18)$$

In the vacuum equation (3.1), we must include both the bound charge and the free charge:

$$\epsilon_0 \nabla \cdot E = \sigma_f + \sigma_b$$

We wish to write this in the simple form

$$\nabla \cdot D = \sigma_f$$

by including  $\sigma_b$  in the definition of  $D$ . This can be done by letting

$$D = \epsilon_0 E + P$$

If  $P$  is linearly proportional to  $E$ ,

then  $\epsilon$  is a constant given by

$$P = \epsilon_0 \chi_e E$$

$$\epsilon = 1 + \chi_e \epsilon E \quad (3.19)$$

(3.20)

(3.21)

(3.22)

(3.23)

## 3.2 Relation of Plasma Physics to Ordinary Electromagnetics

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There is no a priori reason why a relation like Eq. (3.22) cannot be valid in a plasma, so we may proceed to try to get an expression for  $\epsilon$  in a plasma.

### 3.2.4 The Dielectric Constant of a Plasma

We have seen in Sect. 2.5 that a fluctuating E field gives rise to a polarization current  $j_p$ . This leads, in turn, to a polarization charge given by the equation of continuity:

$$\frac{\partial \sigma_p}{\partial t} + \nabla \cdot j_p = 0 \quad (3.24)$$

This is the equivalent of Eq. (3.18), except that, as we noted before, a polarization effect does not arise in a plasma unless the electric field is time varying. Since we have an explicit expression for  $j_p$  but not for  $\sigma_p$ , it is easier to work with the fourth Maxwell equation, Eq. (3.4):

$$\nabla \cdot B = \mu_0 j_f + j_p + \epsilon_0$$

$$-\epsilon E$$

We wish to write this in the form

$$\nabla \cdot B = \mu_0 j_f + \epsilon_- E$$

This can be done if we let

From Eq. (2.67) for  $j_p$ , we have

$$\epsilon = \epsilon_0 + j_p$$

$$-\epsilon E$$

$$\epsilon = \epsilon_0 + \rho$$

$$B^2$$

$$\text{or } \epsilon R$$

$$\epsilon \epsilon_0 = 1 + (3.25)(3.26)(3.27)$$

$$\mu_0 \rho c^2$$

$$B^2$$

(3.28)

This is the low-frequency plasma dielectric constant for transverse motions. The qualifications are necessary because our expression for  $j_p$  is valid only for  $\omega^2$   $\Omega^2 c^2$  and for E perpendicular to B. The general expression for  $\epsilon$ , of course, is very complicated and hardly fits on one page.

Note that as  $\rho \rightarrow 0$ ,  $\epsilon R$  approaches its vacuum value, unity, as it should. As  $B \rightarrow 1$ ,  $\epsilon R$  also approaches unity. This is because the polarization drift  $v_p$  then vanishes, and the particles do not move in response to the transverse electric field.

In a usual laboratory plasma, the second term in Eq. (3.28) is large compared with unity. For instance, if  $n = 10^{16} \text{ m}^{-3}$  and  $B = 0.1 \text{ T}$  we have (for hydrogen)

$$M_0 pc^2 B^2 = 4\pi \times 10^{-7} \times 10^{16} \times 1.67 \times 10^{-27} \times 9 \times 10^{16} \\ \times 0.1 (0.1)^2$$

= 189 This means that the electric fields due to the particles in the plasma greatly alter the fields applied externally. A plasma with large  $\epsilon$  shields out alternating fields, just as a plasma with small  $\lambda D$  shields out DC fields.

### Problems

- 3.1 Derive the uniform-plasma low-frequency dielectric constant, Eq. (3.28), by reconciling the time derivative of the equation  $\nabla D = \nabla \epsilon E$  ( ) = 0 with that of the vacuum Poisson equation (3.1), with the help of equations (3.24) and (2.67). 3.2 If the ion cyclotron frequency is denoted by  $\Omega_c$  and the ion plasma frequency is defined by  $\Omega_p = ne^2 / \epsilon_0 M^{1/2}$  where  $M$  is the ion mass, under what circumstances is the dielectric constant  $\epsilon$  approximately equal to  $\Omega^2 p / \Omega^2 c$ ?

## 3.3 The Fluid Equation of Motion

Maxwell's equations tell us what  $E$  and  $B$  are for a given state of the plasma. To solve the self-consistent problem, we must also have an equation giving the plasma's response to given  $E$  and  $B$ . In the fluid approximation, we consider the plasma to be composed of two or more interpenetrating fluids, one for each species. In the simplest case, when there is only one species of ion, we shall need two equations of motion, one for the positively charged ion fluid and one for the negatively charged electron fluid. In a partially ionized gas, we shall also need an equation for the fluid of neutral atoms. The neutral fluid will interact with the ions and electrons only through collisions. The ion and electron fluids will interact with each other even in the absence of collisions, because of the  $E$  and  $B$  fields they generate.

### 3.3.1 The Convective Derivative

The equation of motion for a single particle is

$$mdv/dt = qE + v \cdot B \quad (3.29)$$

## Plasmas as Fluids

### 3.3 The Fluid Equation of Motion

Assume first that there are no collisions and no thermal motions. Then all the particles in a fluid element move together, and the average velocity  $u$  of the particles in the element is the same as the individual particle velocity  $v$ .

The fluid equation is obtained simply by multiplying Eq. (3.29) by the density  $n$ :  
 $m n du/dt$

$$dt = qn E + u B$$

( ) (3.30)

This is, however, not a convenient form to use. In Eq. (3.29), the time derivative is to be taken at the position of the particles. On the other hand, we wish to have an equation for fluid elements fixed in space, because it would be impractical to do otherwise. Consider a drop of cream in a cup of coffee as a fluid element. As the coffee is stirred, the drop distorts into a filament and finally disperses all over the cup, losing its identity. A fluid element at a fixed spot in the cup, however, retains its identity although particles continually go in and out of it. To make the transformation to variables in a fixed frame, consider  $G(x, t)$  to be any property of a fluid in one-dimensional  $x$  space. The change of  $G$  with time in a

**frame moving with the fluid is the sum of two terms:**

$$dG(x,t) \\ dt = \partial G \partial t + \partial G \partial x dx \partial t = \partial G \partial t + ux \partial G \partial x$$

(3.31)

The first term on the right represents the change of  $G$  at a fixed point in space, and the second term represents the change of  $G$  as the observer moves with the fluid into a region in which  $G$  is different. In three dimensions, Eq. (3.31) generalizes to

$$dG \\ dt = \\ \partial G \\ \partial t + u \cdot \nabla \\ ( )G$$

(3.32)

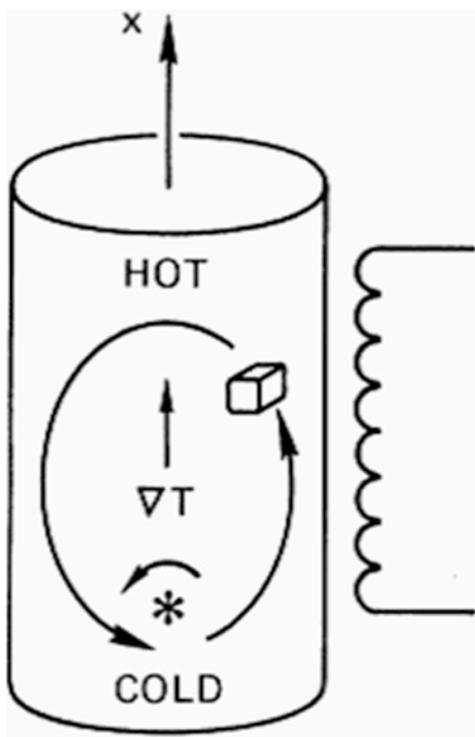
This is called the convective derivative and is sometimes written  $DG/Dt$ . Note that  $(u \cdot \nabla)$  is a scalar differential operator. Since the sign of this term is sometimes a source of confusion, we give two simple examples.

Figure 3.1 shows an electric water heater in which the hot water has risen to the top and the cold water has sunk to the bottom. Let  $G(x,t)$  be the temperature  $T$ ;  $\nabla G$  is then upward. Consider a fluid element near the edge of the tank. If the heater element is turned on, the fluid element is heated as it moves, and we have  $dT/dt > 0$ . If, in addition, a paddle wheel sets up a flow pattern as shown, the temperature in a fixed fluid element is lowered by the convection of cold water from the bottom.

**In this case, we have  $\partial T/\partial x > 0$  and  $ux > 0$ , so that  $u \cdot \nabla T > 0$ . The temperature change in the fixed element,  $\partial T/\partial t$ , is given by a balance of these effects,**

$$\partial T \\ dt = \\ dT \\ dt u \cdot \nabla T$$

It is quite clear that  $\partial T/\partial t$  can be made zero, at least for a short time.



### What industrial processes use plasma?

- Metal cutting: plasma cutters.
- Microchip manufacturing: plasma etching of semiconductors.
- Surface treatments: cleaning and modifying materials.
- Space propulsion: ion and plasma engines (satellite-type).
- Sterilization: cold plasma for disinfecting medical materials.

### How can a plasma similar to that of the Sun be generated?

1. To mimic solar plasma:
2. You need temperatures of millions of degrees (approximately  $10^7$  Kelvin).
3. Low density (more similar to a vacuum than air).
4. Magnetic confinement: very strong fields that trap the plasma.
5. Techniques:
6. Tokamak (like ITER in France, an international project).
7. Stellarator (another type of reactor).

8. *Inertial fusion (ultra-powerful lasers that compress small fuel pellets).*

### ***How can plasma be generated at low temperatures?***

Microwave (MW plasma):

We use a microwave generator (like the one in a modified kitchen microwave) to excite a gas.

1. *The gas (such as argon, helium, or low-pressure air) is ionized.*
2. *Cold plasma is formed: temperatures of 1000°C to 10,000°C in the gas, but the electrons are the ones that are super-hot, not the entire gas.*
3. *Example: plasma reactors for materials processing, or Plasma Electrodes in medicine.*
4. *Radiofrequency (RF plasma):*
5. *A radiofrequency field (e.g., at 13.56 MHz) is applied to an enclosed gas.*
6. *This also ionizes the gas → stable, low-temperature plasma.*
7. *Widely used in the electronics industry (chip manufacturing).*
8. *modulate the energy to obtain highly controlled plasmas.*

### ***Electric Arcs (Arc Plasma):***

1. Two electrodes create a powerful electric arc that ionizes the gas between them.
2. High-density plasma, it can be very hot if desired, or moderately hot if you control the current.
3. Used in plasma welding, hypersonic wind tunnels, and thermal generators.

### ***What gases would you use to generate this plasma?***

Argon (Ar) → Very easy to ionize, inexpensive.

Helium (He) → Stable, good thermal conductivity.

Nitrogen (N<sub>2</sub>) → Even cheaper, although it forms reactive species.

Hydrogen (H<sub>2</sub>) → For light fusion experiments (although it is more difficult to control).

 What advantage does this type of "cold" plasma have?  
You don't need to confine it to millions of degrees like in a Tokamak.

- *We can use it directly to:*
- *Generate small amounts of electrical energy.*
- *Improve the combustion of standard fuels.*

- Treat air or exhaust gases.

the electric dipoles. Giving rise to a bound charge density

$$\sigma_B = \nabla \cdot P \quad (3.18)$$

In the vacuum equation (3.1), we must include both bound charge and free .

$$\epsilon_0 \nabla E = \sigma_F + \sigma_B \quad (3.18)$$

Wher P is linearly proportional to, then  $\epsilon$  is consstant given by

$$\nabla D = \sigma_F \quad (3.20)$$

by including  $\sigma_B$  in the definition of D.

$$D = \epsilon_0 E + \bar{P} \quad (3.21)$$

### 3.2.4 Dielectric Constant of a Plasma

To be recen. see that in Sect. 2.5, a fluctuating E field gives nise to a polarization current  $j_P$ , Which leads t o a polarization charge given by the equation of con-

$$\partial \sigma_P + \nabla \cdot j_P = 0 \quad (3.22)$$

This is the equivalent of Eq. (318). except that, a polarization effect does not arise in a plasma unless the electric field is time varying, Since there is an exptict expression for  $j_P$  but not for  $\sigma_P$ .it is easier to work with the fourth Maxwell equation. Eq. (3.4)

$$\nabla \times B = \mu_0 (j_F + j_P + \epsilon_0 \epsilon \nabla \times E) \quad (3.25)$$

We wish to write this in the form  $\nabla \times B = \mu_0 (j_F + \epsilon \epsilon \nabla \times E)$

$$(3.26)$$

Which can be done if we let

$$\epsilon = \frac{\epsilon -}{\epsilon_0} + \frac{j_P}{\mu_0 \epsilon} \quad (3.27)$$

From Eq. (2.67) for i

