

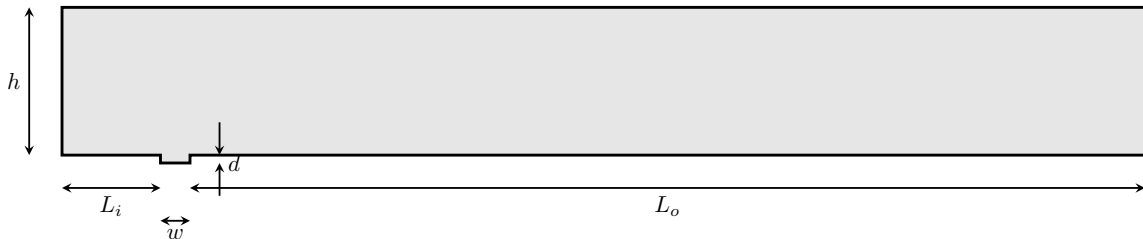
# IMPERIAL

## Summary 1st term 2025

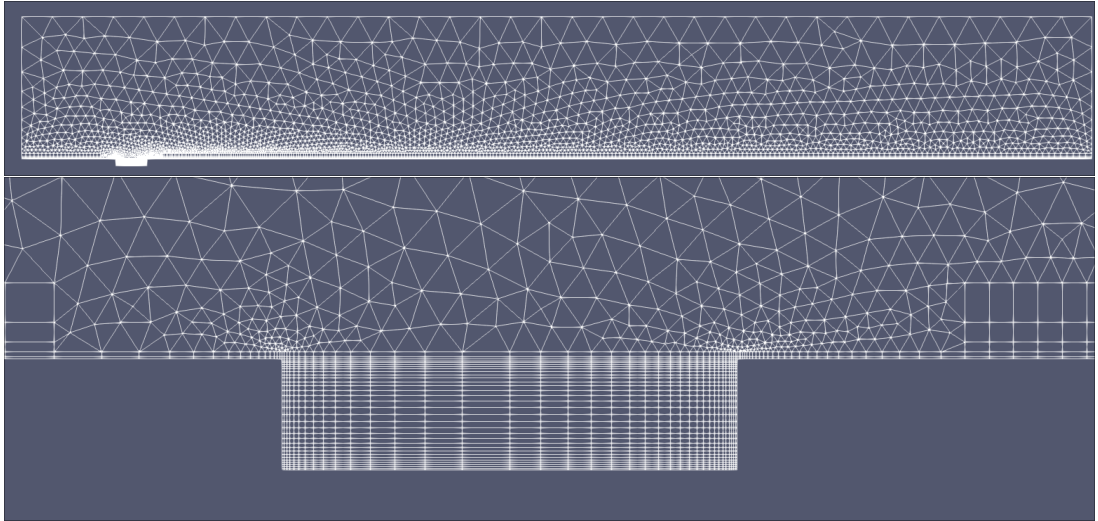
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April 2, 2025

# Domain

- $\delta^*$ : measured at the upstream edge of the gap in a surface free of discontinuities.
- $\text{Re}_{\delta^*} = 1000$
- $L_i = 50\delta^*$
- $L_o = 500\delta^*$
- $h = 75\delta^*$
- $d = 4\delta^*$
- $w \in A\delta^*$ ,  $A = \{10, \dots, 30\}$
- Inflow BC: Blasius profile
- Top BC: Far-field BC
- Wall BC: No-slip
- Outflow BC: Convective BC (Robin), or normal Neumann BC.



# Current mesh



## Study - range of $w$

- For  $w \leq 16.4\delta^*$ , we observe a steady state from nonlinear simulations (“global” attractor).
- As we increase  $w \geq 16.5\delta^*$ , we observe a divergent behavior. Thus, to do LSA with those cases we have to make use of Selective Frequency Damping (SFD) (e.g. control theory) to get a locally stable baseflow.
- **Conjecture:** the critical width at  $d = 4\delta^*$  lies in the interval  $(16.4\delta^*, 16.5\delta^*)$  (up to numerical sensitivity).

## Unstable baseflows



u-component of dns simulations with  $w = 16.5\delta^*$  at time  $t \sim 11\,500$ .

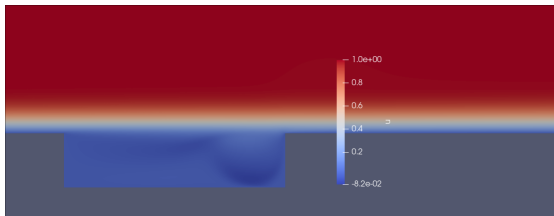


u-component of dns simulations with  $w = 26\delta^*$  at time  $t \sim 1500$  (old run with a short domain).

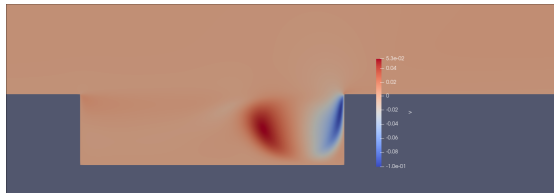
## Stable baseflows



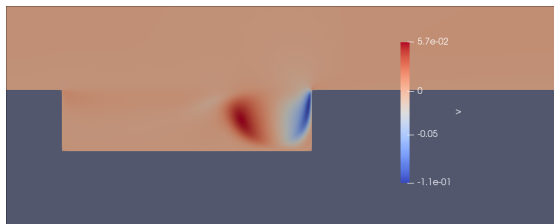
u-component natural baseflow with  $w = 15\delta^*$



u-component SFD baseflow with  $w = 16.5\delta^*$



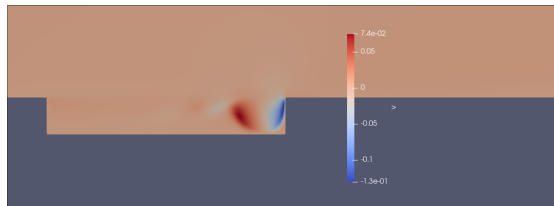
v-component natural baseflow with  $w = 15\delta^*$



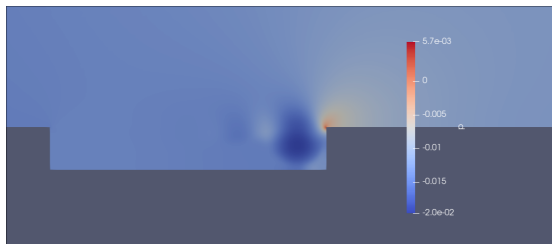
v-component SFD baseflow with  $w = 16.5\delta^*$



u-component SFD baseflow with  $w = 26\delta^*$



v-component SFD baseflow with  $w = 26\delta^*$



pressure SFD baseflow with  $w = 26\delta^*$

# Linear stability analysis

**Case**  $w = 15\delta^*$ . Most unstable mode:

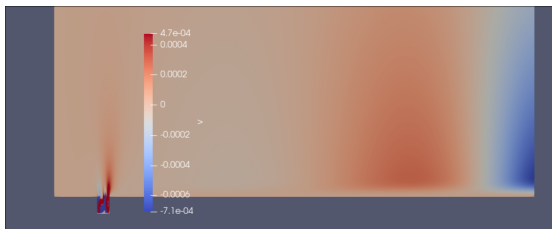
- Growth rate:  $-0.00279$
- Frequency:  $\pm 0.00304$

Comments:

- This is not a TS mode. We observe a huge mode in the BL.
- The magnitude of the fields is much higher inside the gap than on the BL (around 2-10 orders, depending on the x-position in the BL)



u-component of the most unstable eigenmode with  $w = 15\delta^*$  (domain scaled in the x-dir by 0.1)



v-component of the most unstable eigenmode with  $w = 15\delta^*$  (domain scaled in the x-dir by 0.1)



# Linear stability analysis

**Case**  $w = 16.5\delta^*$  (very similar to  $w = 15\delta^*$ ).

Most unstable mode:

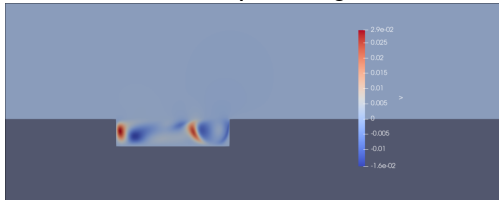
- Growth rate:  $-0.00258$
- Frequency:  $\pm 0.00276$

Comments:

- We do **not** observe a mode with positive growth rate, which suggests (up to numerical sensitivity and other possible errors) that the nature of the instability would be nonlinear instead of linear.



u-component of the most unstable eigenmode with  $w = 16.5\delta^*$  (emphasizing colors in the gap)



v-component of the most unstable eigenmode with  $w = 16.5\delta^*$  (emphasizing colors in the gap)

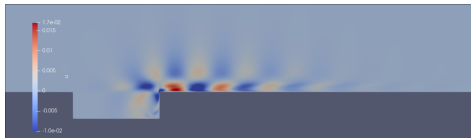
# Linear stability analysis

**Case**  $w = 26\delta^*$ . Most unstable mode:

- Growth rate: 0.00859
- Frequency:  $\pm 0.00887$

Comments:

- This mode looks like the result of an absolute instability in the gap because the amplitude of the waves decreases as they move downstream.



u-component of the most unstable eigenmode with  $w = 26\delta^*$  (domain scaled in the x-dir by 0.5)



v-component of the most unstable eigenmode with  $w = 26\delta^*$  (domain scaled in the x-dir by 0.5)

## Nature of the instability (work in progress)

- Runs doing global stability analysis from a baseflow just above the critical width where non-steadiness shows up on dns (e.g  $w_{\text{critical}}|_{d=4\delta^*} \in (16.4\delta^*, 16.5\delta^*)$ ) show eigenmodes with a **negative** growth rate.
- We did check that adding those modes to the baseflow as initial conditions in the nonlinear solver leads to a steady solution (we ran that for  $w = 16.5\delta^*$  and  $w = 18\delta^*$ ). This does **not** happen though for  $w = 26\delta^*$ .

## Coherence between DNS and LSA

Let

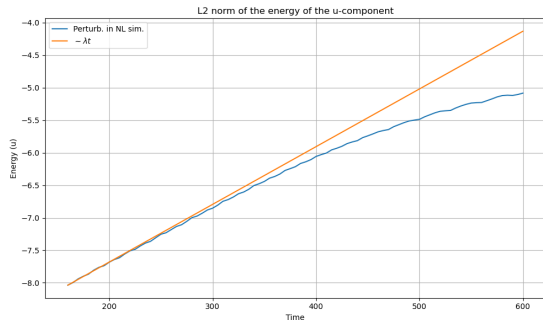
$$\varphi(\mathbf{t}; (\mathbf{u}_0, \mathbf{v}_0)) = (\varphi_u(\mathbf{t}; (\mathbf{u}_0, \mathbf{v}_0)), \varphi_v(\mathbf{t}; (\mathbf{u}_0, \mathbf{v}_0)))$$

the flow of NS eqs at time  $t$  with initial conditions  $(\mathbf{u}_0, \mathbf{v}_0)$ . Let  $(\mathbf{U}, \mathbf{V})$  be the baseflow of our system and  $(\tilde{\mathbf{u}}, \tilde{\mathbf{v}})$  the most unstable eigenmode with  $\lambda$  the respective growth rate. We plot the following quantities

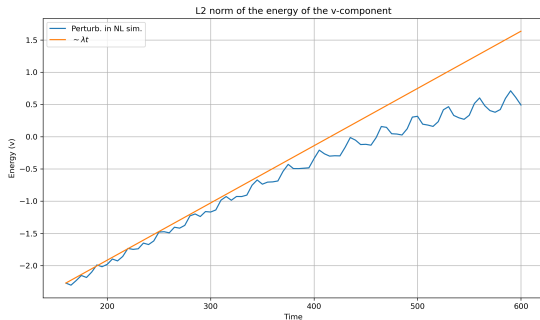
$$\begin{aligned} t &\mapsto \frac{\|\varphi_u(\mathbf{t}; (\mathbf{U} + \tilde{\mathbf{u}}, \mathbf{V} + \tilde{\mathbf{v}})) - \mathbf{U}\|_{L^2}}{\|\mathbf{U}\|_{L^2}} \\ t &\mapsto \frac{\|\varphi_v(\mathbf{t}; (\mathbf{U} + \tilde{\mathbf{u}}, \mathbf{V} + \tilde{\mathbf{v}})) - \mathbf{V}\|_{L^2}}{\|\mathbf{V}\|_{L^2}} \end{aligned}$$

for different  $w$ . This should tell us how the energy of the perturbation evolves in time. We compare this with the theoretical evolution of the energy based on LSA, which goes as  $\|\mathbf{u}_0\|_{L^2} e^{\lambda t}$  and  $\|\mathbf{v}_0\|_{L^2} e^{\lambda t}$ , respectively.

**Case**  $w = 26\delta^*$



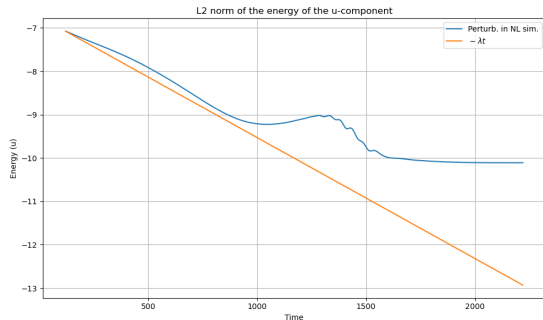
u-component



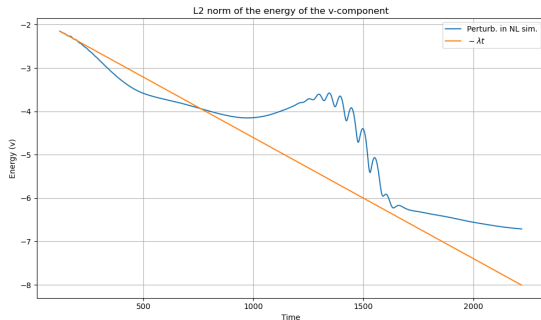
v-component

- We are plotting the log of the energy.
- Initially the nonlinear results fits well the linear prediction after which ( $t \sim 450$ ) the nonlinear effects start to contribute significantly.

**Case**  $w = 15\delta^*$  (similar to  $w = 16.5\delta^*$ )



u-component

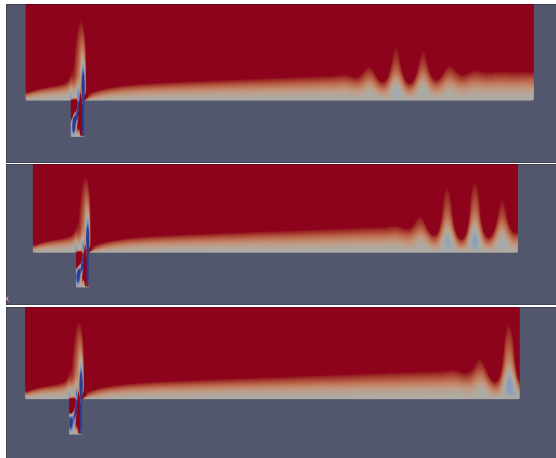
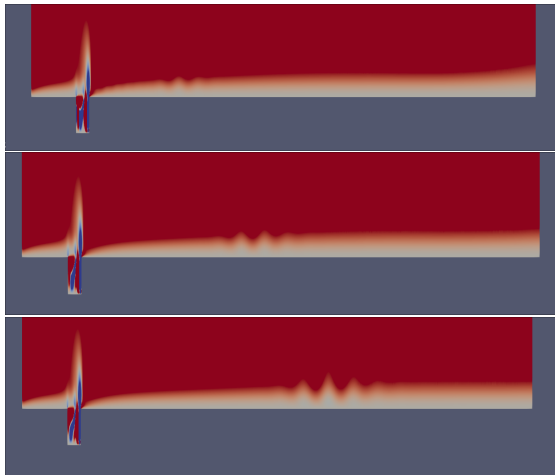


v-component

- We are plotting the log of the energy.
- The fit is less nicer, and we observe a weird bump appearing on the middle of the time interval considered.

# The bump

u-component the perturbed system at different times (domain scaled in the x-dir)



## The bump

- Looks like the modes may be providing the system with enough energy inside the gap to trigger the convective instability nature of the system. **Why?** The stable modes computed for  $w = 15\delta^*$  and  $w = 16.5\delta^*$  showed bigger magnitudes inside the gap than on the BL.



## Questions

- What range of  $d$  should we consider in the future?
- Should we first move to 3D case or to 2D compressible case?