Turbulence Zeroth Law of Turbulence



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Energy balance relation

$$\frac{1}{2} \frac{d}{dt} \langle |\mathbf{u}|^2 \rangle = -\nu \langle \nabla_j u_i \nabla_j u_i \rangle + \langle \mathbf{u} \cdot \mathbf{f} \rangle$$
$$\frac{d}{dt} \mathcal{E} = -\epsilon + \mathcal{I}$$

Reynolds number and Nondimensional dissipation rate

$$\boxed{Re = \frac{UL}{\nu}}$$

$$\mathcal{C}_{\mathcal{D}}(Re) = \frac{\epsilon L}{U^3}$$

Laminar Estimate

$$\epsilon \propto \frac{\nu U^2}{L^2}$$
 $\mathcal{C}_{\mathcal{D}}(Re \to 0) = \frac{1}{Re}$



Flow behind an object

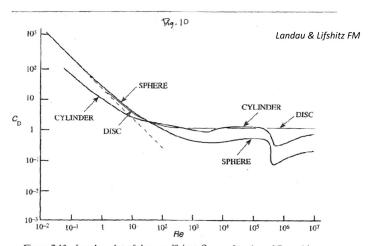


Figure 7.13 Log-log plot of drag coefficient $C_{\rm D}$ as a function of Reynolds Number Re for spheres, transverse cylinders, and face-on discs. The broken straight line represents Stokes's law.

Flow behind a grid

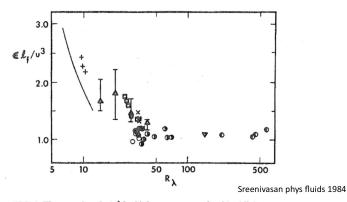
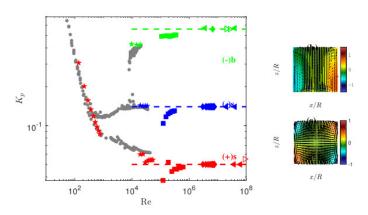


FIG. 1. The quantity $\epsilon L_f/u^3$ for biplane square-mesh grids. All data except + are for the initial period of delay, and are explained in Table I. + indicate typical data 13 in the final period of decay. — corresponds to Eq. (1).

Flow generated by propellers

VKS and SHREK experiment.



Flow in numerical simulations

Phys. Fluids, Vol. 15, No. 2, February 2003

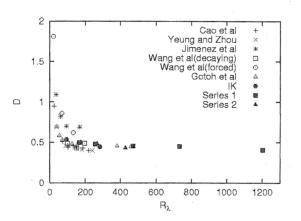


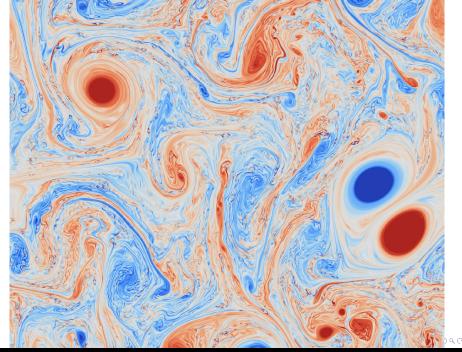
FIG. 3. Normalized energy dissipation rate D versus R from Ref. 5 data up to R 250), Ref. 3 , , and the present DNS databases , .

Zeroth law of turbulence

In the limit of infinite Re the normalized dissipation rate remains finite*

$$\mathcal{C}_{\mathcal{D}}^{\infty} \equiv \mathcal{C}_{\mathcal{D}}(Re \to \infty) = \lim_{Re \to \infty} \frac{\epsilon L}{U^3} > 0$$





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