

OPEN POND PRODUCTION OF *ARTHROSPIRA PLATENSIS*

Microalgae (including cyanobacteria) are nowadays seen as a way to produce quality food and feed as well as high added value molecules. Among them, *Arthrospira platensis* has now reached commercial deployment (under the commercial name *Spirulina*). Several bioreactors can be used to grow this cyanobacterium, among them, open raceway ponds offer a cheap large scale solution (Fig. 1). Still, those bioreactors have two drawbacks. First water tends to evaporate, increasing the salinity of the growth medium which may be a source of stress for the cells. Second, they have to be operated at constant temperature, around the optimum for the microorganism (here, 35 °C). These two problems will be addressed hereinafter.

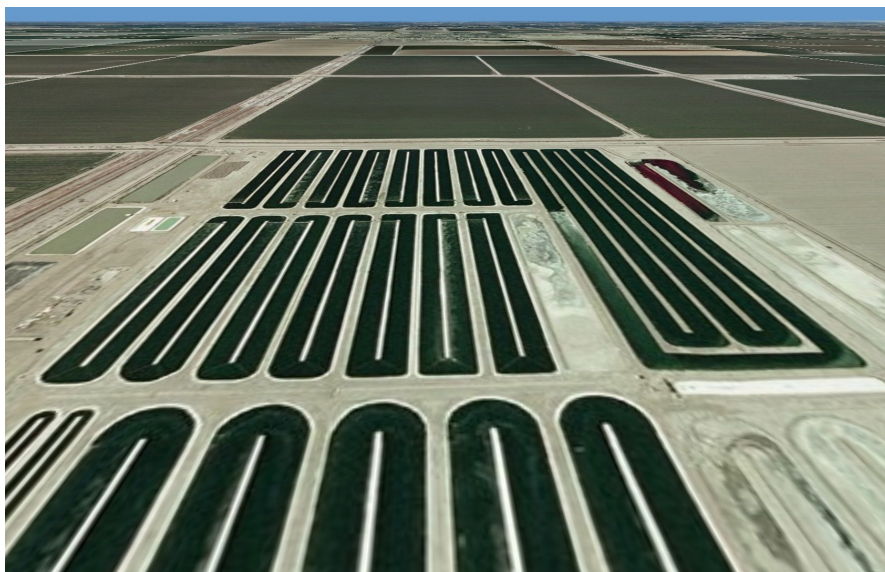


Fig. 1: picture of raceway open ponds (credit: Duke University, Nicholas School blogs)

Assumptions

Medium is assumed to be water

Medium is assumed to be at a constant temperature of 35 °C (T_{pond})

$v_{\text{wind}} = 20 \text{ km/h}$, wind velocity

Thermodynamic data

$T_{\text{air}} = 35 \text{ °C}$, average air temperature above the pond

$P^{\text{sat}}(35 \text{ °C}) = 5626.7 \text{ Pa}$, vapour pressure of water at 35 °C

$\nu_{\text{air}} = 1.64 \cdot 10^{-5} \text{ m}^2/\text{s}$, air viscosity at 35 °C

$D_{\text{water/air}} = 2.52 \cdot 10^{-5} \text{ m}^2/\text{s}$, water mass diffusivity in air

$D_{\text{water/pp}} = 2.00 \cdot 10^{-13} \text{ m}^2/\text{s}$, water mass diffusivity in polypropylene

$Y_{\infty} = 20 \%$, relative humidity far away from the pond ($Y_{\infty} = C_{\infty}/C^{\text{sat}}$)

$\alpha_{\text{water}} = 1.46 \cdot 10^{-7} \text{ m}^2/\text{s}$, water heat diffusivity

$C_{p_{\text{water}}} = 4183 \text{ J/kg/K}$, specific heat of water

Pond design and operation data

L = 50 m, length

l = 10 m, width

e = 0.30 m, depth

T = 35 °C, culture medium temperature

Coil heat exchanger data

T_{ech} = 50 °C, heating water inlet temperature

d_t = 2.54 cm, tube diameter

l_t = 10 m, tube length

Correlation list

Flat plate, forced convection:

Laminar flow -averaged

$$Sh_L = 0.664 Re_L^{1/2} Sc^{1/3} \text{ for } 0.6 < Sc < 60 \text{ and } Re < 5 \cdot 10^5$$

Combined laminar and turbulent flow -averaged

$$Sh_L = (0.037 Re_L^{4/5} - 871) Sc^{1/3} \text{ for } 0.6 < Sc < 60 \text{ and } 5 \cdot 10^5 < Re < 10^7$$

Tube, forced convection:

Turbulent flow

$$Nu_D = 0.023 Re_D^{4/5} Pr^{0.3}, \text{ for } L/D > 10, 0.6 < Pr < 160 \text{ and } 10^4 < Re_D$$

Laminar flow

$$Nu_D = 3.66$$

With dimensionless number being expressed as

$$Re_L = \frac{v L}{\nu}, Sc_{\text{water/air}} = \frac{\nu_{\text{air}}}{D_{\text{water/air}}}, Sh_L = \frac{k_L L}{D_{\text{water/air}}}, Pr = \frac{\nu_{\text{water}}}{\alpha_{\text{water}}}, Nu_L = \frac{h L}{\lambda_{\text{water}}}$$

where L is the characteristic length (width, length, diameter depending on the case).

Objectives of the TD

- Assess evaporation
- Size overnight heating system

Part 1: Managing evaporation

1. Calculate the Reynolds number for both axial and transverse wind configurations.
2. Calculate the Sherwood numbers for both axial and transverse wind configurations.
3. Calculate the rates of evaporation for both axial and transverse wind configurations.

For that we have to combine the equations of slides 6.6 and 6.7 :

$$J_s = -\frac{D_s}{\eta} (C_i - C_\infty) \text{ and } k = -\frac{D_s}{\eta} \text{ thus } J_s = -k (C_i - C_\infty) \text{ in kg/m}^2/\text{s (that should then be multiplied by par } A_{\text{pond}})$$

4. Compute the evaporated fraction pond content over 8 hours per day during the 10 days that lasts a culture. From now on, we will consider an averaged evaporation flow rate

In order to avoid excessive evaporation, a polypropylene sheet (200 μm thickness) has been placed on top of the pond.

5. Estimate water diffusion time through the polypropylene sheet. Conclude on the efficiency of this material as a barrier.

Part 2: Thermal management

The sheet induces a thermal forcing of $Q_{\text{rad}} = 100 \text{ W/m}^2$ at midday in the summer while there is no wind (worst case scenario).

1. How long would it take for the pond temperature to increase of 5 $^{\circ}\text{C}$. Conclude on the need to manage this additional heat.

While daytime additional heat does not seem to be a problem, night heat loss may have to be considered. Assuming purely radiative loss with a clear sky night, the thermal loss can be expressed $Q_{\text{loss}} = 0.90 \times 5.67 \cdot 10^{-8} (T_{\text{pond}}^4 - T_{\text{space}}^4)$, in W/m^2 , where $T_{\text{space}} = 3 \text{ K}$.

2. Compute the value of this lost power and the temperature decrease of the pond over 8 hours.

In order to counter this temperature, some fatal heat coming from a nearby boiler can be used. To transfer this heat to the pond, two coil heat exchangers are installed in the pond (Fig. 2).

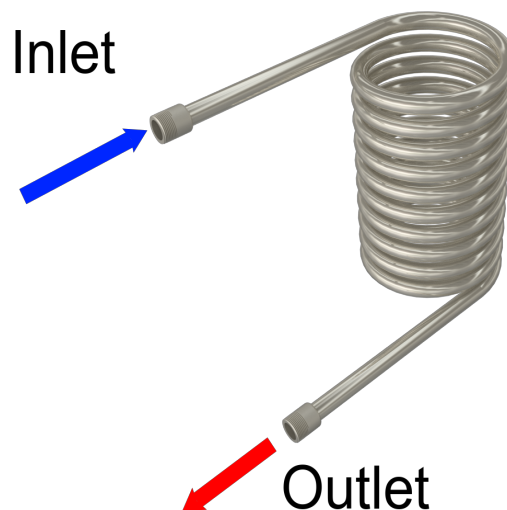


Fig. 2: Coil heat exchanger (credit deltahydro.com)

3. Draw a heat balance over the temperature water circulating inside of the heat exchanger assuming the pond temperature is constant over the coil.

Hints: considered a small size element of fluid, dz . Describe heat transfer with $h(T(z) - T_{\text{pond}})$ formulation.

4. Integrate the former expression to obtain the heat flux exchange over the coil as a function of the flow rate and the heat exchange coefficient.

5. Bearing in mind that turbulent flow are much more efficient at transferring heat, compute the flow rate that should be pumped through the coil.

Hint: You may start by substituting the heat transfer coefficient by its dependency over the flow rate in the former expression.

Then, use a plot of the transferred heat versus flow rate to obtain the desired operating condition.