

Assignment - 2

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1B110107

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$$(1) \quad R_0' = \begin{bmatrix} C_1 & C_2 & C_3 \\ \hat{C}_1 \cdot \hat{C}_0 & \hat{C}_1 \cdot \hat{R}_0 & \hat{C}_1 \cdot \hat{E}_0 \\ \hat{C}_2 \cdot \hat{C}_0 & \hat{C}_2 \cdot \hat{R}_0 & \hat{C}_2 \cdot \hat{E}_0 \\ \hat{C}_3 \cdot \hat{C}_0 & \hat{C}_3 \cdot \hat{R}_0 & \hat{C}_3 \cdot \hat{E}_0 \end{bmatrix}$$

Columns are C_1, C_2 & C_3 .

Q. Prove $\hat{C}_1 \cdot \hat{C}_2 = C_2 \cdot C_3 = C_3 \cdot C_1 = 0$

Let we write R_0' as:

$$R_0' = \begin{bmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{bmatrix}$$

Then

$$R_0'^T = \begin{bmatrix} a_1 & b_1 & c_1 \\ a_2 & b_2 & c_2 \\ a_3 & b_3 & c_3 \end{bmatrix}$$

For the rotation matrix: $R_0' \cdot R_0'^T = R_0'^T \cdot R_0' = I$

$$\Rightarrow R_0'^T \cdot R_0' = I$$

$$\begin{bmatrix} a_1 & b_1 & c_1 \\ a_2 & b_2 & c_2 \\ a_3 & b_3 & c_3 \end{bmatrix} \cdot \begin{bmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} a_1^2 + b_1^2 + c_1^2 & a_1 a_2 + b_1 b_2 + c_1 c_2 & a_1 a_3 + b_1 b_3 + c_1 c_3 \\ a_1 a_2 + b_1 b_2 + c_1 c_2 & a_2^2 + b_2^2 + c_2^2 & a_2 a_3 + b_2 b_3 + c_2 c_3 \\ a_1 a_3 + b_1 b_3 + c_1 c_3 & a_2 a_3 + b_2 b_3 + c_2 c_3 & a_3^2 + b_3^2 + c_3^2 \end{bmatrix} = I$$

$$c_1 c_2 = a_1 a_2 + b_1 b_2 + c_1 c_2 = 0$$

$$c_2 c_3 = a_2 a_3 + b_2 b_3 + c_2 c_3 = 0$$

$$c_1 c_3 = a_1 a_3 + b_1 b_3 + c_1 c_3 = 0$$

Hence columns are orthogonal.

(2) Show that $\det(R_o') = 1$

We know that for any matrix:

$$\det(R) = \det(R^T)$$

$$\text{also } \det(R \cdot R^T) = \det(R) \cdot \det(R^T)$$

for rotation matrix:

$$R \cdot R^T = I$$

$$\det(R \cdot R^T) = \det(I)$$

$$\det(R) \cdot \det(R^T) = 1$$

$$\therefore \det(R^T) = \det(R)$$

$$[\det(R)]^2 = 1$$

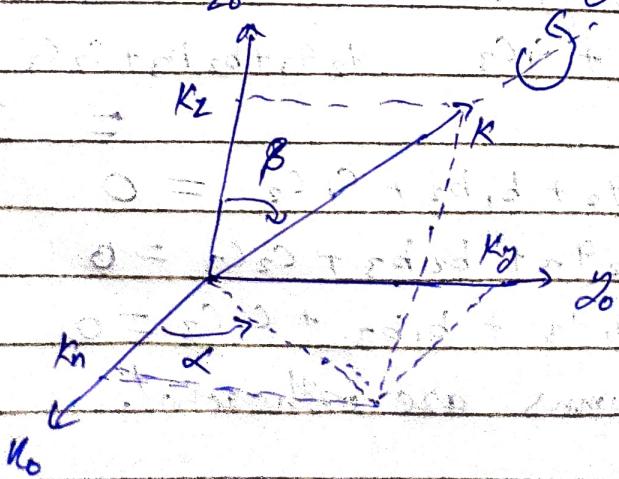
$$\det(R) = 1$$

(3.) Done.

(4.) Rotation about an arbitrary axis k .

$$k = [k_x, k_y, k_z]^T \quad (\text{in frame } O_0x_0y_0z_0)$$

Rotation matrix = $R_{k,\theta} \Rightarrow$ rotation of θ degree about axis k .



$$R_{K,\theta} = R_{z,\alpha} R_{y,\beta} R_{z,\theta} R_{y,-\beta} R_{z,-\alpha}$$

for unit vector k :

$$\sin \alpha = \frac{k_x}{\sqrt{k_x^2 + k_y^2}}, \cos \alpha = \frac{k_z}{\sqrt{k_x^2 + k_y^2}}$$

$$\sin \beta = \sqrt{k_x^2 + k_y^2}, \cos \beta = k_z$$

$$R_{K,\theta} = \begin{bmatrix} k_x^2 v_\theta + c_\theta & k_x k_y v_\theta - k_z s_\theta & k_x k_z v_\theta + k_y s_\theta \\ k_x k_y v_\theta + k_z s_\theta & k_y^2 v_\theta + c_\theta & k_y k_z v_\theta - k_x s_\theta \\ k_x k_z v_\theta - k_y s_\theta & k_y k_z v_\theta + k_x s_\theta & k_z^2 v_\theta + c_\theta \end{bmatrix}$$

$$\text{where } v_\theta = \cos \theta = 1 - c_\theta$$

Calculation of θ and k vector for rotation matrix:

⇒ Components of rotation matrix R are σ_{ij}

$$\text{then } \theta = \cos^{-1} \left(\frac{\text{Tr}(R) - 1}{2} \right)$$

$$\text{for } 3 \times 3 \text{ matrix } \theta = \cos^{-1} \left(\frac{\sigma_{11} + \sigma_{22} + \sigma_{33} - 1}{2} \right)$$

$\text{Tr} = \text{trace of } R$

$$k_i = \frac{1}{2 \sin \theta} \begin{bmatrix} \sigma_{32} - \sigma_{23} \\ \sigma_{13} - \sigma_{31} \\ \sigma_{21} - \sigma_{12} \end{bmatrix}$$

$$R_{K,\theta} = R_{-K,-\theta}$$

$$15. \quad R S(a) R^T = S(Ra)$$

Left hand side:

$$\Rightarrow R S(a) R^T$$

We know that $S(a)b = a \times b$

also for orthogonal matrix R :

$$R.(a \times b) = Ra \times Rb$$

$$\Rightarrow R S(a) R^T = R.(a \times R^T)$$

$$= Ra \times R.R^T$$

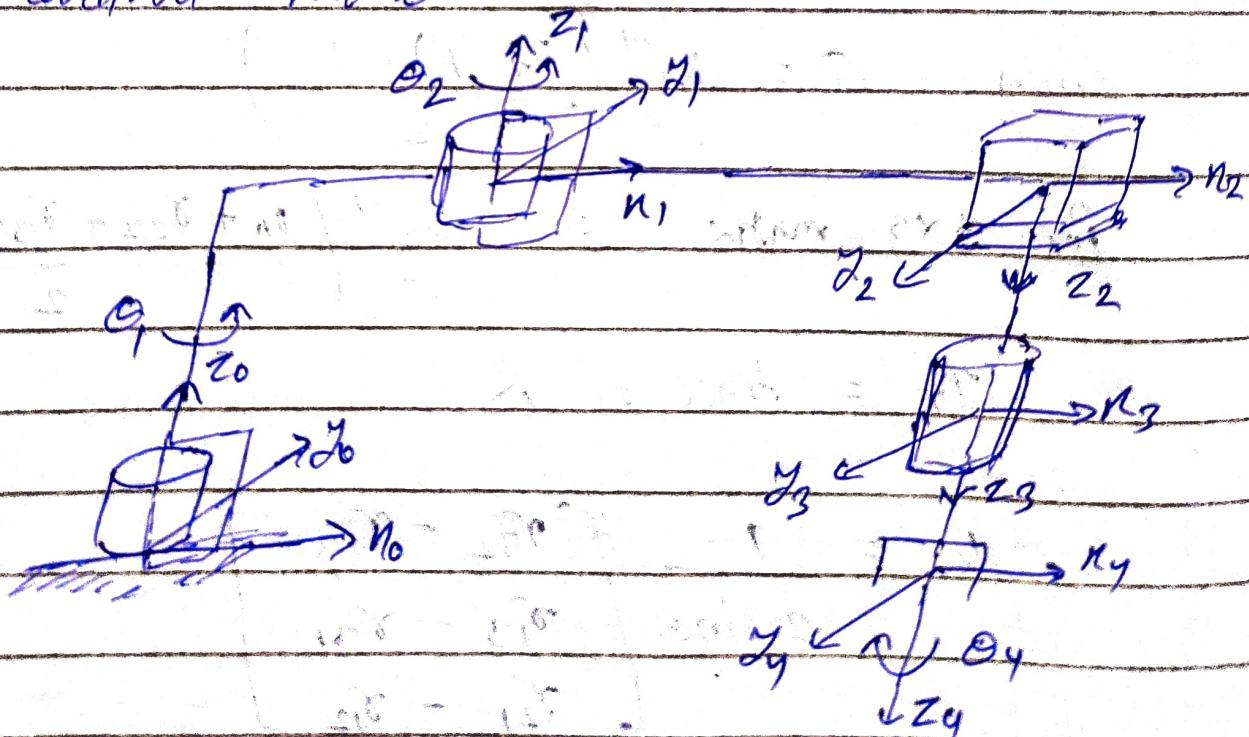
$$= Ra \times I$$

$$= S(Ra) \cdot I$$

$$\underline{R S(a) R^T = S(Ra)}$$

16. SCARA manipulator:

Coordinate frames:



(10.

Gearboxes in Robots :

(1. Planetary Gearheads: These are used in high precision motion control applications that require high torque to volume ratio, high torsional stiffness and low backlash.

(2. Strain wave gearing (Harmonic gearing)):

These are very light weight with zero backlash and high gear ratio. It has coaxial input and output shaft. Good for repeatable tasks.

(3. Cycloidal drive:

These are used to reduce speed. These has compact size with zero backlash.

Q1. For the SCARA Program in Q.6:

$$\theta_1 = \begin{bmatrix} q_1 c_1 \\ q_1 s_1 \\ 0 \end{bmatrix}, \quad \theta_2 = \begin{bmatrix} q_1 c_1 + q_2 c_{12} \\ q_1 s_1 + q_2 s_{12} \\ 0 \end{bmatrix}$$

$$\theta_3 = \begin{bmatrix} q_1 c_1 + q_2 c_{12} \\ q_1 s_1 + q_2 s_{12} \\ d_3 \end{bmatrix}, \quad \theta_4 = \begin{bmatrix} q_1 c_1 + q_2 c_{12} \\ q_1 s_1 + q_2 s_{12} \\ d_3 - d_4 \end{bmatrix}$$

$$\mathbf{T} = \begin{bmatrix} z_0 \times (\theta_4 - \theta_0) & z_1 \times (\theta_4 - \theta_1) & z_2 & z_3 \times (\theta_4 - \theta_3) \\ z_0 & z_1 & 0 & z_3 \end{bmatrix}$$

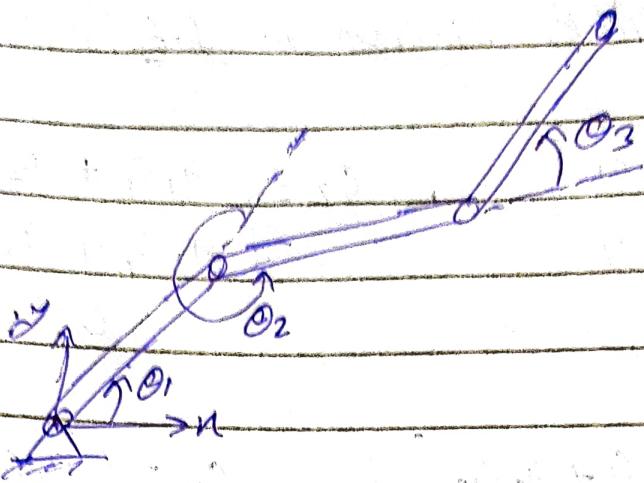
$\therefore z_3$ and $(\theta_4 - \theta_3)$ are parallel

$$z_3 \times (\theta_4 - \theta_3) = 0$$

$$\Rightarrow z_0 = z_1 = k = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, \quad z_2 = z_3 = -k = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix}$$

$$\Rightarrow \mathbf{T} = \begin{bmatrix} -q_1 s_1 - q_2 s_{12} & -q_2 s_{12} & 0 & 0 \\ q_1 c_1 + q_2 c_{12} & q_2 c_{12} & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix}$$

Q3.



$$O_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad O_1 = \begin{bmatrix} q, c, \\ q, s, \end{bmatrix}$$

$$O_2 = \begin{bmatrix} q, c_1 + q_2 c_{12} \\ q, s_1 + q_2 s_{12} \end{bmatrix}, \quad O_3 = \begin{bmatrix} q, c_1 + q_2 c_{12} + q_3 c_{123} \\ q, s_1 + q_2 s_{12} + q_3 s_{123} \end{bmatrix}$$

$$\mathcal{T} = \begin{bmatrix} Z_0 \times (O_3 - O_0) & Z_1 \times (O_3 - O_1) & Z_2 \times (O_3 - O_2) \\ Z_0 & Z_1 & Z_2 \end{bmatrix}$$

where $Z_0 = Z_1 = Z_2 = k = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

$$\mathcal{T} = \begin{bmatrix} -q_1 s_1 - q_2 s_{12} - q_3 s_{123} & -q_2 s_{12} - q_3 s_{123} & -q_3 s_{123} \\ q_1 c_1 + q_2 c_{12} + q_3 c_{123} & q_2 c_{12} + q_3 c_{123} & q_3 c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$