

PART-A1. SLEW RATE + CAUSES:

Slew rate is maximum rate of change of output voltage with respect to time. Specified in V/ms.

REASON FOR SLEW RATE: Usually a capacitor within or outside an op-amp oscillation. This capacitor, which prevents the output voltage from fast changing input. The rate at which the volt across the capacitor increases $dv_c/dt = I/c$

Where: I is maximum amount furnished by op-amp

to capacitor C . Op amp should have either a higher current or small compensating capacitors.

2. IDEAL CHARACTERISTICS OF OP-AMP:

- Infinite voltage gain A .
- Zero output resistance R_o , so that the output can drive an infinite number of other drives.
- Infinite common mode rejection ratio, so that the output common mode noise voltage is zero.

- Infinite slew rate, so that output voltage changes occur simultaneously with input voltage changes.
- Infinite bandwidth so that any frequency signals from 0 to ∞ Hz can be amplified without attenuation.

PART-B

1. Explain the dc characteristics of op-amp.

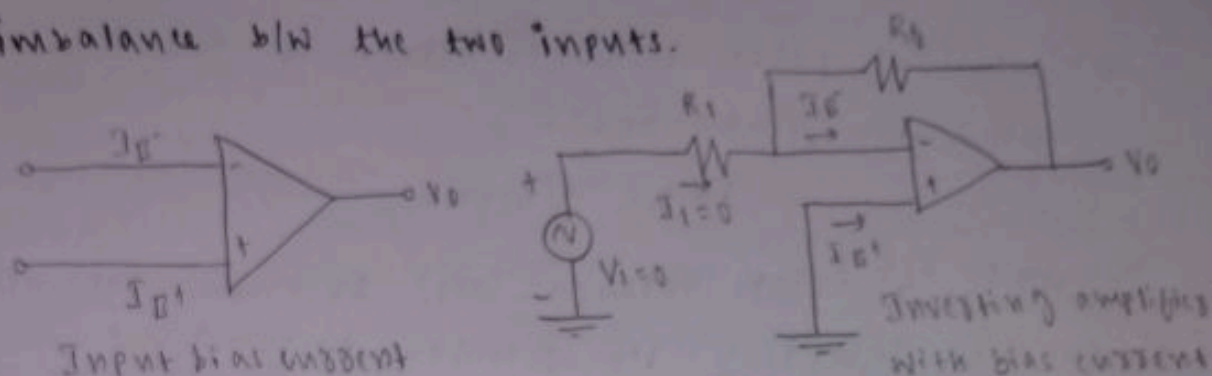
Dc output voltages are:

- Input bias current
- Input offset current
- Input offset voltage
- Thermal drift.

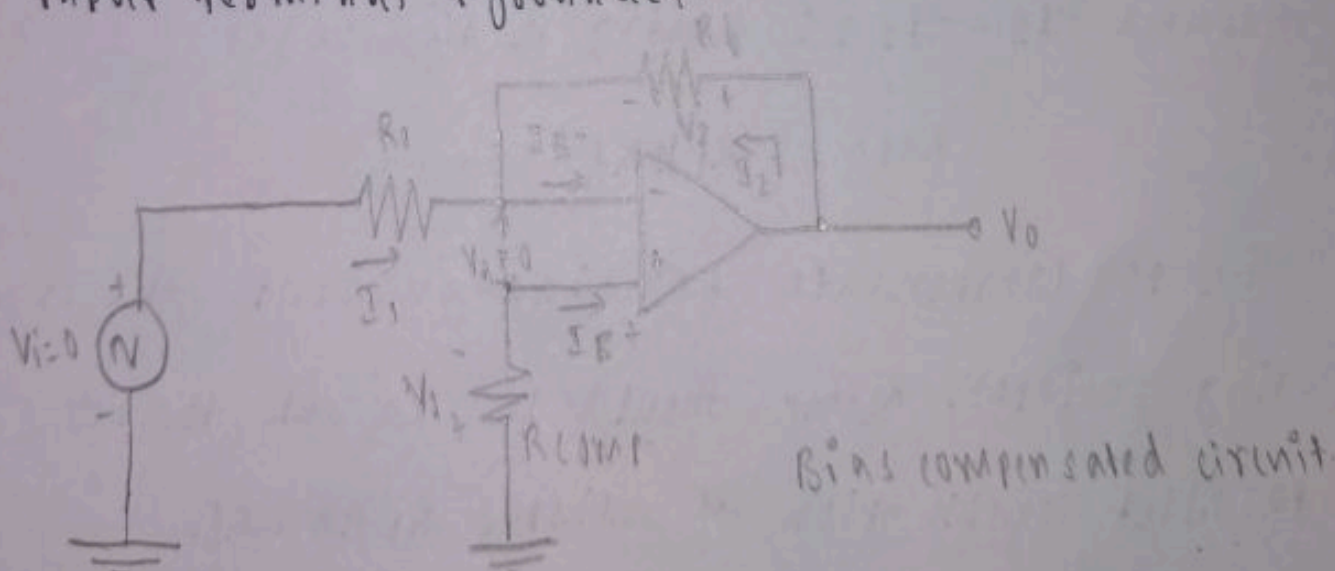
→ INPUT BIAS CURRENT:

- Op-amp's input is differential amplifier, which may be made of BJT or FET.
- In an ideal op-amp we assumed that no current is drawn from the input terminals the base currents entering into the inverting & non-inverting terminals.

- Even though both the transistors are identical, I_{B-} and I_{B+} are not exactly equal due to internal imbalance b/w the two inputs.



- Input voltage $V_i = 0V$, $I_B = \frac{I_{B+} + I_{B-}}{2}$. The output V_O should be ($V_O = 0$) but for $I_B = 500nA \Rightarrow V_O = 500nA \times 1M = 500mV$.
- The output is driven to 500mV with zero input because of bias currents
- This can be compensated by a compensation resistor R_{comp} has been added between the non-inverting input terminal & grounded.



current I_{B+} flowing through compensating resistor R_{comp} then by KVL, $V_0 = V_2 - V_1$ — (1)

By selecting proper value of R_{comp} V_2 can be cancelled with V_1 and $V_0 = 0$.

$$I_{B+} = V_1 / R_{comp} \quad \text{--- (2)}$$

The node 'a' is at voltage $(-V_1)$ because the voltage at the non-inverting i/p terminal is $(-V_1)$

$$I_1 = V_1 / R_1 \quad \text{--- (3)}$$

$$I_2 = V_2 / R_f \quad \text{--- (4)}$$

For compensation: V_0 should equal to zero: ($V_0 = 0, V_i = 0$)

from eq (3) $V_2 = V_1$ so,

$$I_2 = V_1 / R_f \quad \text{--- (5)}$$

KCL at node 'a' gives

$$I_{B-} = I_2 + I_1 = (V_1 / R_f) + (V_1 / R_1) / R_1 R_f \quad \text{--- (5)}$$

Assume $I_{B-} = I_{B+}$ & using (2) & (5) we get

$$R_{comp} = R_1 \parallel R_f \quad \text{--- (6)}$$

i.e. to compensate for bias current the compensating resistor, R_{comp} should be equal to the parallel combination of resistors R_1 and R_f .

INPUT OFFSET CURRENT:

→ Bias current compensation will work if both bias currents I_{B+} and I_{B-} are equal

→ Since the input transistor cannot be made identical. There will always be some small difference between I_{B+} and I_{B-} .

$$|I_{os}| = I_{B+} - I_{B-} \quad \text{--- (7)}$$

Offset current I_{os} for BJT op-amp is 200 nA & for FET op-amp is 10 pA . Even with bias current compensation, offset current will produce an output voltage when $V_i = 0$.

$$V_1 = I_{B+} R_{comp} \quad \text{--- (8)}$$

$$I_1 = V_1 / R_1 \quad \text{--- (9)}$$

KCL at node a gives,

$$I_2 = (I_{B-} - I_1) = I_{B-} - (I_{B+} R_{comp} / R_1)$$

$$\text{Again } V_0 = V_2 R_1 - V_1$$

$$V_0 = I_2 R_f - I_{B+} R_{comp}$$

$$V_0 = 1\text{ M}\Omega \times 200\text{ nA}$$

$$V_0 = 200\text{ mV with } V_i = 0$$

→ R_1 large the feedback resistor R_f must also be high, so as to obtain reasonable gain.

→ The feedback network is a good solution. This will allow large feedback resistance, while keeping the resistance to ground low (in dotted line)

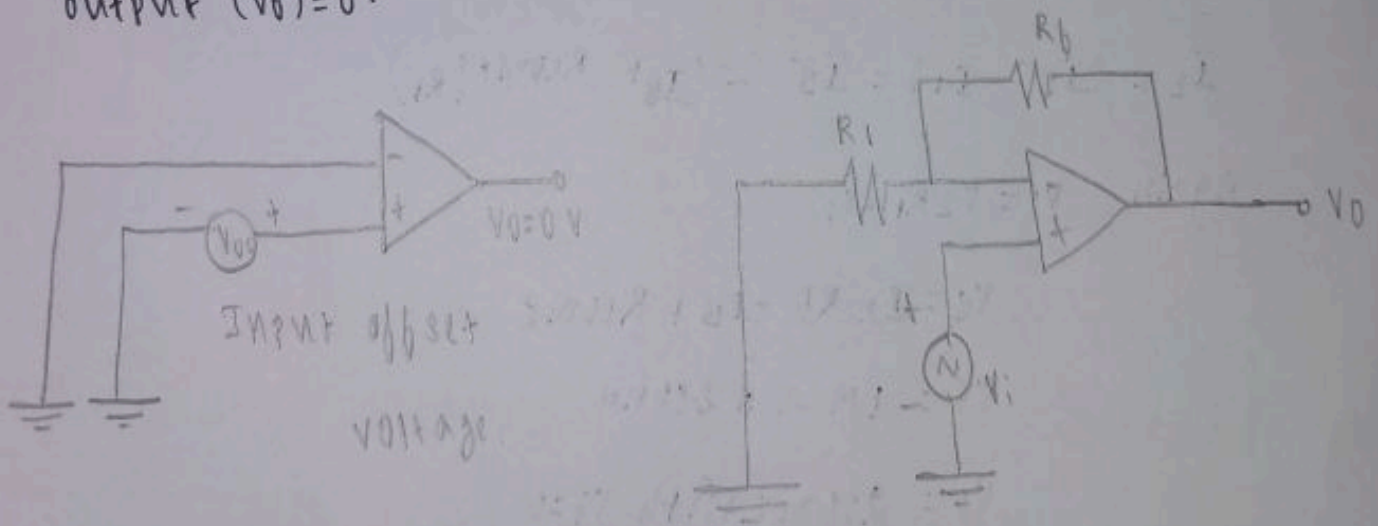
$$R_f = \frac{R_x^2 + 2R_x R_s}{R_s}$$

To design T-network $R_x < \sqrt{R_f / 2}$

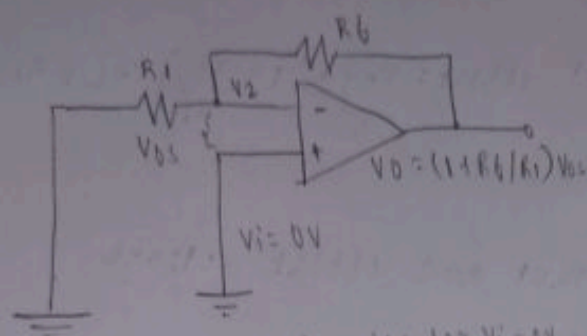
$$R_s = \frac{R_x^2}{R_f - 2R_x}$$

INPUT OFFSET VOLTAGE:

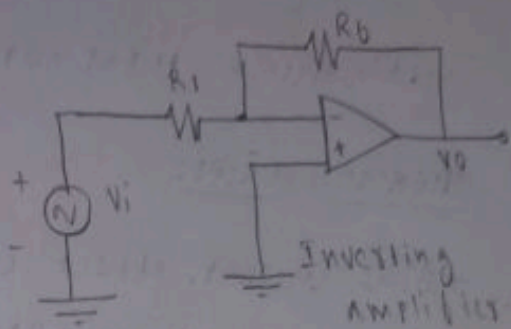
Above compensating techniques, it is found the output voltage still not be zero with zero input voltage. Imbalances inside the op-amp & one may have to apply a small voltage at the input terminal to make output $(V_o) = 0$.



Non-Inverting amplifier



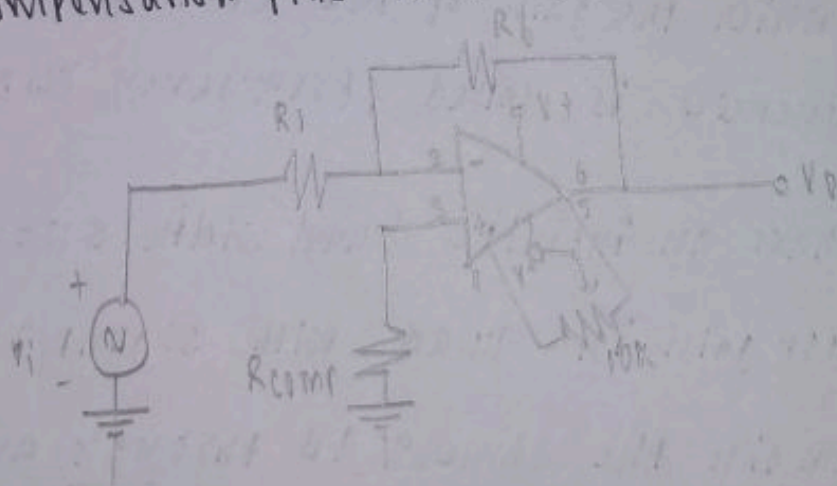
Equivalent circuit for $V_i = 0V$



Inverting amplifier

TOTAL OUTPUT OFFSET VOLTAGE:

Total output offset voltage could be either more or less than the offset voltage produced at the output due to input bias current or input offset voltage; this is maximum offset voltage at the output of an inverting and non-inverting amplifiers without any compensation technique used is given by many op-amps provide offset compensation pins to nullify the offset voltage.



Compensation circuit for offset voltage

With R_{comp} , total output offset: $V_{ot} = \left(1 + \frac{R_f}{R_i}\right) V_{os} + R_f I_B$

THERMAL DRIFT:

→ Bias current, offset current and offset voltage change with temperature

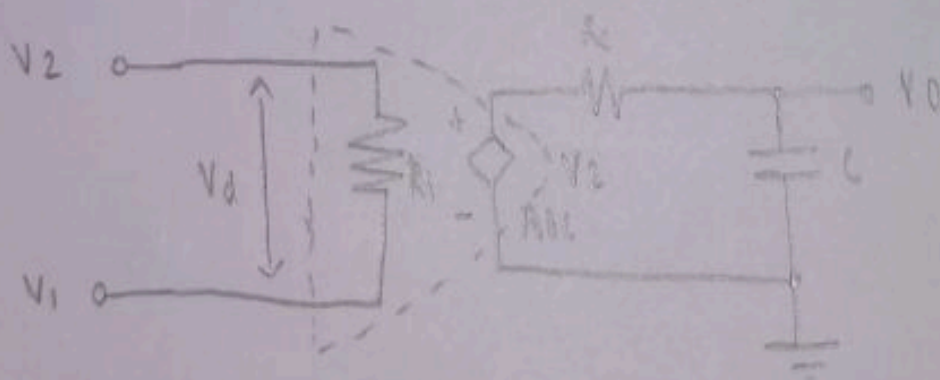
→ A circuit nulled at 25°C may not remain, so when the temperature rises to 35°C . This is called drift.

→ Offset current drift is expressed in $\text{nA}/^\circ\text{C}$.

2. Explain the frequency response of op-amp with its equivalent circuit?

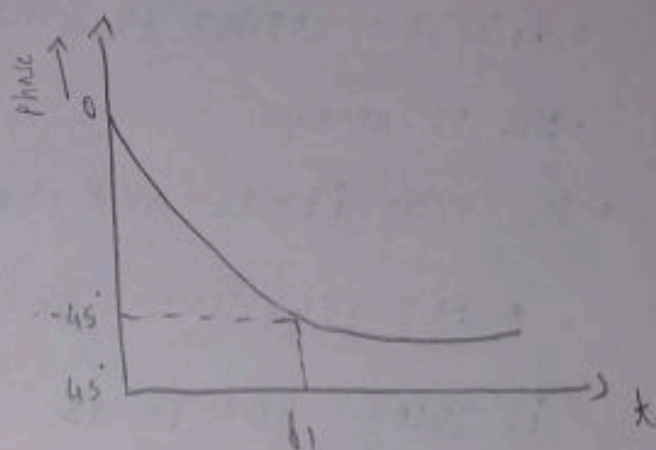
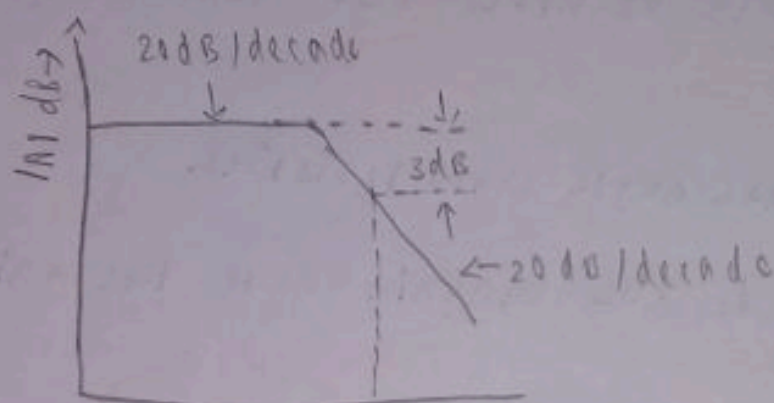
- The variation in operating frequency all cause variations in gain magnitude and its phase angle.
- The manner in which the gain of the op-amp responds to different frequencies is called frequency response.
- op-amp should have an infinite bandwidth $BW = \infty$ (i.e.) if its open loop gain is 90dB with signal its gain should remain the same 90dB through audio and onto high radio frequency.
- op-amp gain decreases at higher frequency to decrease gain after a certain frequency reached.

- There must be a capacitive component in the equivalent circuit of the op-amp.
- For an op-amp with only one break frequency all the capacitors effects can be represented by a single capacitor.
- There is one pole due to $R_o C$ and one -20 dB/decade .
- Open loop voltage gain of an op-amp with only one corner frequency is obtained.
- f_c is the corner frequency or upper 3 dB frequency of the op-amp.
- The magnitude and phase angle characteristics:
 - * For frequency $f \ll f_c$ the magnitude of the gain is $20 \log A_{OL}$ in dB
 - * At frequency $f = f_c$ the gain is 3 dB down from the dc value of A_{OL} in dB. This frequency f_c is called corner frequency.



Equivalent circuit of practical circuit

- For the phase characteristics that the phase angle is zero at frequency $f=0$.
- At the corner frequency f_1 the phase angle is -45° (lagging & at infinite frequency the phase angle is -90°)
- If frequency is taken as the decade below the corner frequency and infinite frequency is one decade above the corner frequency.



Frequency response of op-amp.

Roll off rate of op-amp gain

