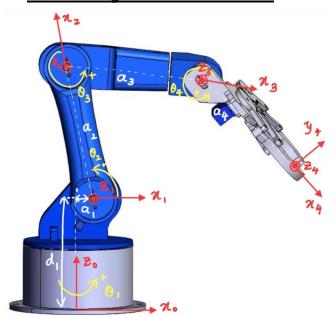
Robotics Mini Project: Kinematic Analysis of a Robot Arm

Team Members:

W.M.J.C. Kumara	190328V
B.S.V.W. Munasinghe	190397E
R.M.C.D.H. Ranasinghe	190498N

1. Frame Assignment and DH Table



Link	a_i	α_i	d_i	θ_i
1	1.3 <i>cm</i>	90°	9.5 <i>cm</i>	$ heta_1^*$
2	12 <i>cm</i>	0	0	$ heta_2^*$
3	12 <i>cm</i>	0	0	$ heta_3^*$
4	12.5 <i>cm</i>	0	0	$ heta_4^*$

2. Forward Kinematics

• Symbols have the following meanings.

$$C_i = \cos(\theta_i)$$
, $C_{ij} = \cos(\theta_i + \theta_j)$, $C_{ijk} = \cos(\theta_i + \theta_j + \theta_k)$
 $S_i = \sin(\theta_i)$, $S_{ij} = \sin(\theta_i + \theta_j)$, $S_{ijk} = \sin(\theta_i + \theta_j + \theta_k)$

• Transformation Matrices

$$A_{1} = \begin{bmatrix} C_{1} & 0 & S_{1} & 1.3C_{1} \\ S_{1} & 0 & -C_{1} & 1.3S_{1} \\ 0 & 1 & 0 & 9.5 \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{2} = \begin{bmatrix} C_{2} & -S_{2} & 0 & 12C_{2} \\ S_{2} & C_{2} & 0 & 12S_{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_{3} = \begin{bmatrix} C_{3} & -S_{3} & 0 & 12C_{3} \\ S_{3} & C_{3} & 0 & 12S_{3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{4} = \begin{bmatrix} C_{4} & -S_{4} & 0 & 12.5C_{4} \\ S_{4} & C_{4} & 0 & 12.5S_{4} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{4}^{0} = A_{1}A_{2}A_{3}A_{4} = \begin{bmatrix} C_{1}C_{234} & -C_{1}S_{234} & S_{1} & 12C_{1}(0.108333 + C_{2} + C_{23} + 1.04167C_{234}) \\ S_{1}C_{234} & -S_{1}S_{234} & -C_{1} & 12S_{1}(0.108333 + C_{2} + C_{23} + 1.04167C_{234}) \\ S_{234} & C_{234} & 0 & 9.5 + 12S_{2} + 12S_{23} + 12.5S_{234} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

3. Inverse Kinematics

Take the desired end position as $p_4^0 = [x \ y \ z]^T$.

Take the desired end effector orientation as $\theta_{orientation}$ and we get,

$$\theta_2 + \theta_3 + \theta_4 = \theta_{orientation}$$

Using the geometric relationship, we can take,

$$\theta_1 = atan2(y, x)$$
 or $\theta_1 = atan2(y, x) - \pi$

Using the transformation matrix T_4^0 and desired position p_4^0 ,

$$C_2 + C_{23} = \frac{x}{12C_1} - 0.108333 - 1.04167C_{234} = A$$

or

$$C_2 + C_{23} = \frac{y}{12S_1} - 0.108333 - 1.04167C_{234} = A$$

and

$$S_2 + S_{23} = \frac{z - 12.5S_{234} - 9.5}{12} = \mathbf{B}$$

Solving the above two equations we get,

$$C_3 = \frac{A^2 + B^2 - 2}{2} = l$$
 \rightarrow $S_3 = \pm \sqrt{1 - l^2}$

When $S_3 = \sqrt{1 - l^2}$,

$$\theta_3 = atan2\left(\sqrt{1-l^2},l\right) \ , \ \theta_2 = atan2\left(\frac{B(1+l)-A\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} \right) \cdot \frac{A(1+l)+B\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} = \frac{A(1+l$$

When $S_3 = -\sqrt{1 - l^2}$,

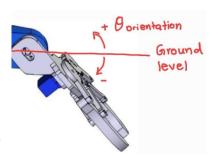
$$\theta_3 = atan2\left(-\sqrt{1-l^2},l\right) \ , \ \theta_2 = atan2\left(\frac{B(1+l)+A\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} \right) \frac{A(1+l)-B\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} = atan2\left(\frac{B(1+l)+A\sqrt{1-l^2}}{(1+l)^2+(1-l^2)}\right) \frac{A(1+l)-B\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} = atan2\left(\frac{B(1+l)+A\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} \right) \frac{A(1+l)-B\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} = atan2\left(\frac{B(1+l)+A\sqrt{1-l^2}}{(1+l)^2+(1-l^2)} \right)$$

Finally, we solve for θ_4 , Knowing that $\theta_{orientation}$ is the addition of all θ_2 , θ_3 , θ_4 .

$$\theta_4 = \theta_{orientation} - \theta_2 - \theta_3$$

- ➤ The solutions are filtered to obtain only one solution by considering the range of the physical joints of the arm. (Each joint is limited to rotate only 180 degrees)
- ➤ The limits for the angles defined by our team are as follows. (Convention is the same as used in the frame assignment)

Angle	Minimum	Maximum
$ heta_1^*$	0_{\circ}	180°
$ heta_2^*$	0°	180°
θ_3^*	-135°	0°
$ heta_4^*$	-90°	90°



4. Manipulator Jacobian

$$\begin{bmatrix} S_1(-1.3-12C_2-12C_{23}-12.5C_{234}) & C_1(-12S_2-12S_{23}-12.5S_{234}) & C_1(-12S_{23}-12.5S_{234}) & -12.5C_1S_{234}) \\ C_1(1.3+12C_2+12C_{23}+12.5C_{234}) & S_1(-12S_2-12S_{23}-12.5S_{234}) & S_1(-12S_{23}-12.5S_{234}) & -12.5S_1S_{234} \\ 0 & 12C_2+12C_{23}+12.5C_{234} & 12C_{23}+12.5C_{234} & 12.5C_{234} \\ 0 & S_1 & S_1 & S_1 \\ 0 & -C_1 & -C_1 & -C_1 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

5. Controlling the Arm