O use smith chart. normalize z

$$Z = \frac{ZL}{20} = \frac{80-540}{100} = 0.8-0.45$$

so r=0.8, x=-0.4 And find the corresponders point on the chart.

3. use cal culation

At the smuce, smore and=1.52

"PL (9t the 18 = PL (4t the strad) = 0.2420 e 3256.

lbl. Ouse Smith chart

draw a circle, and use the opposite point on the circle.

@. read its rand x from the chart.
about 100+10j.

(a). Use accalculation

Sme it is quarter marelength

$$\frac{20}{21} = \frac{100^2}{80-400} = 100+500$$

input impedance at z=-18.75mm is 140+50j.

$$V_{m} = \frac{2m}{2h + 2s} \cdot V_{s} = V^{+} (1 + P_{L} V_{s})$$

$$P_{LS} = P_{LL} = \frac{2L - 20}{2L + 20} = \frac{80 + 40i}{18 - 4i} = 0.2425e^{i2} = 0.2425e^{i2}$$

$$\frac{80 - 40\dot{9}}{80 - 40\dot{9} + 100} \cdot 10 = V^{+} \left(1 + \frac{80 - 40\dot{9} - 100}{80 - 40\dot{9} + 100} \right)$$

$$= V^{+} \left(160 - \frac{80 - 40\dot{9} + 100}{80 - 40\dot{9} + 100} \right)$$

$$= V^{+} \left(\frac{160 - 80\dot{9}}{80 - 40\dot{9} + 100} \right)$$

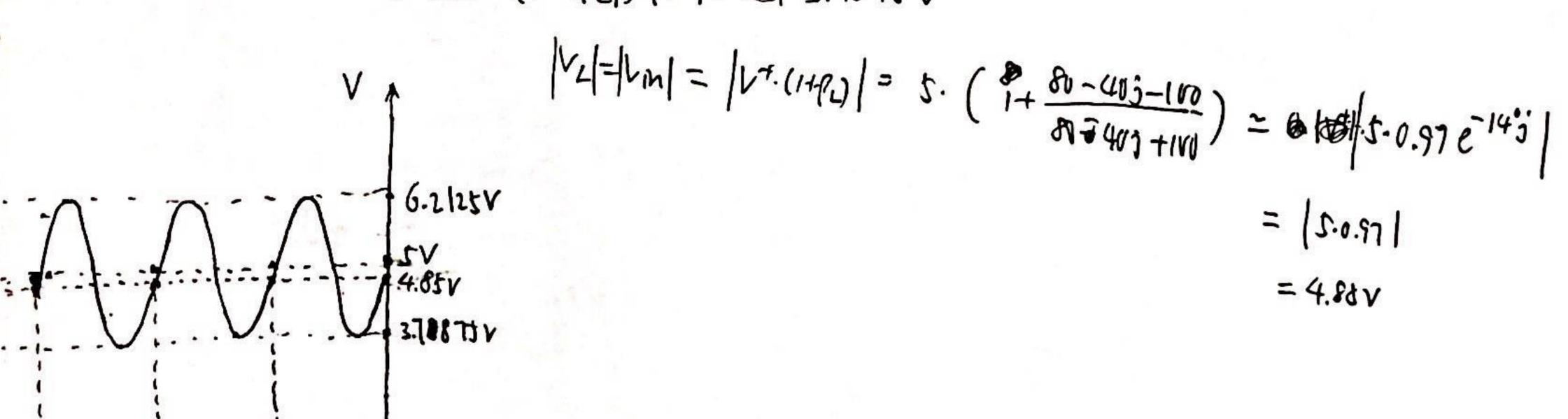
$$\therefore V^{+} = 5 \text{ V}$$

$$|V^{+}| = 5 \text{ V}$$

@ For SWR. just find from the Smith Chart. ASWR ~ 1.64

3. For SWR, Calculation.

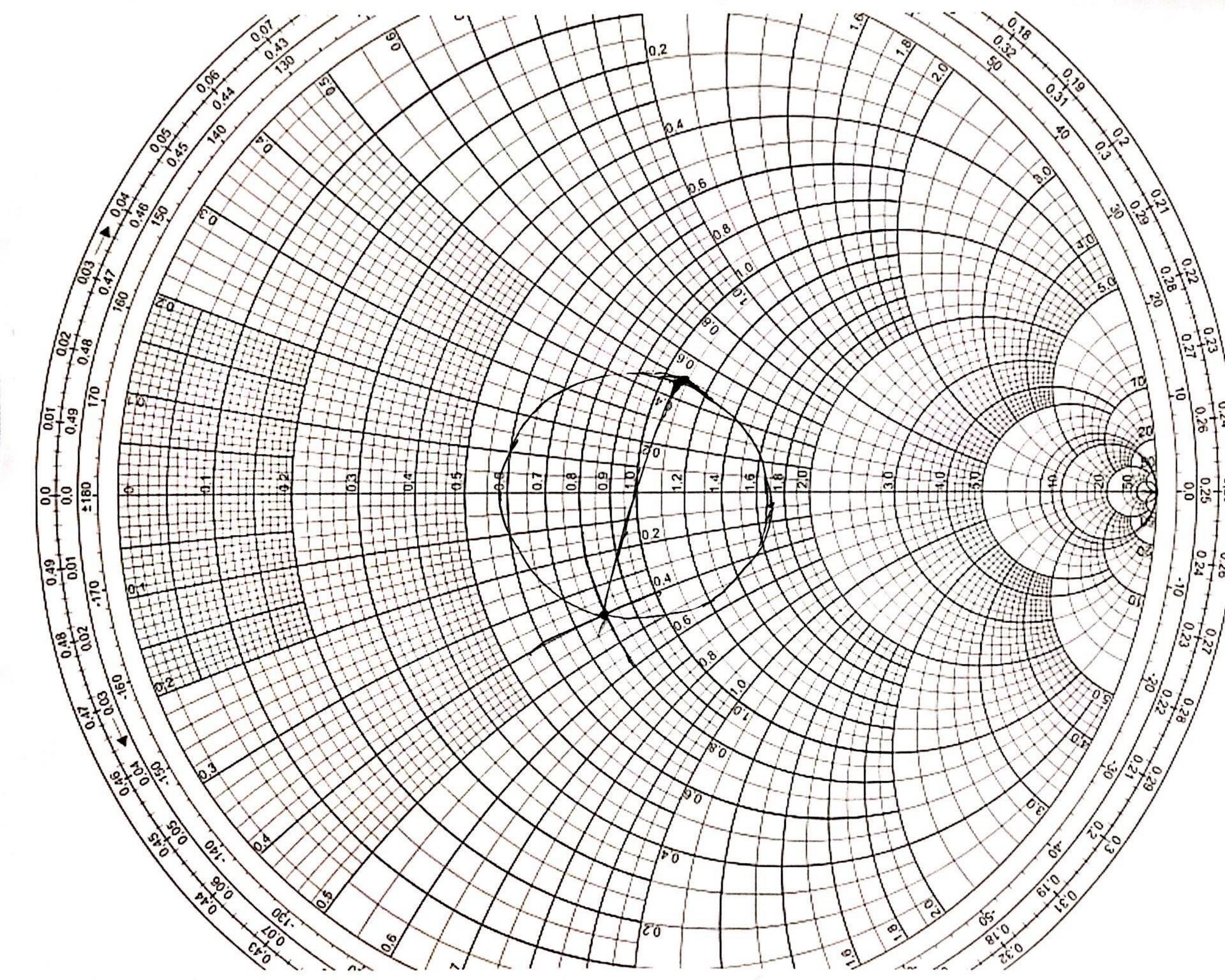
SWR=
$$\frac{1+1921}{1-1921} = \frac{1+0.2425}{1-0.2425} = 1.64$$



-225pm

-Itam

-7.5hm



2. (G).
$$z_{11} = \frac{V_1}{z_1}|_{\dot{u}=0}$$

$$Z_{11} = \frac{4}{2} \left(\frac{9}{2} \cdot \frac{1}{2} \right) \left[\frac{1}{2} + \frac{9}{2} + \frac{9}{2} \right] \left(\frac{1}{2} + \frac{9}{2} + \frac{9}{2} \right)$$
 (1) [L+R+(\frac{9}{2} | \frac{9}{2})] (1)

$$Z_{12} = Z_{21} = \frac{A^{2}}{2A + B}$$

$$A = \frac{G}{G} \frac{2}{3W} \frac{2}{3W} = \frac{2}{3WC + G}$$

$$= \frac{\left(\frac{2}{G} \frac{1}{3WC}\right)^{2}}{2 \cdot \left(\frac{2}{G} \frac{1}{3WC}\right) + 3WL + R}$$

$$= \frac{A^{2}}{3WC + G}$$

$$= \frac{2}{3WC + G}$$

$$\frac{1}{2} = \frac{\left(\frac{2}{4} \right) \frac{2}{3 \pi c} \left(\frac{2}{3 \pi c} \right) \left(\frac{2}{3 \pi c} \right) \left(\frac{2}{3 \pi c} \right) \left(\frac{2}{3 \pi c} \right)^{2}}{2\left(\frac{2}{4} \right) \frac{2}{3 \pi c} + 2 \pi c}$$

(More desprited organized firm is in (c))

2. (b).
$$\gamma = d + j\beta = \sqrt{(x' + jwL')}(G' + jwC')$$

$$V(2) = V^{+}e^{-\gamma z} + V^{-}e^{\gamma z} = V^{+}(e^{-\gamma z} + f_{e})e^{\gamma z})$$

$$i(z) = \frac{V^{+}}{70}e^{-\gamma z} - \frac{V^{-}}{20}e^{\gamma z} = \frac{V^{+}}{70}(e^{-\gamma z} - f_{e})e^{\gamma z})$$

$$Z_{11}(z) = \frac{V(2)}{i(z)} = \frac{1}{70}e^{-\gamma z}e^{-\gamma z} = \frac{1}{70}e^{-\gamma z}e^{-\gamma z}$$

$$Z_{11} = Z_{11}(-1) = \frac{1}{70}e^{-\gamma z}e^{-\gamma z}$$

$$V_{11} = Z_{11}(-1) = \frac{1}{70}e^{-\gamma z}e^{-\gamma z}$$

$$V_{12} = \frac{1}{70}e^{-\gamma z}e^{-\gamma z}e^{-\gamma z}$$

$$V_{13} = \frac{1}{70}e^{-\gamma z}e^{-\gamma z}e^{-\gamma$$

$$2_{12} = 2_{21} = \frac{V_{2}}{i_{1}} \Big|_{i_{2}=0}$$

$$i_{2} = i_{0}(0) = \frac{V_{1}}{20}(1-P_{2}) = 0 \quad \exists P_{2}=1$$

$$V_{21} = V(-1) = V^{+}(e^{\gamma A} + P_{2}e^{-\gamma A})$$

$$= V^{+}(e^{\gamma A} + P_{2}e^{-\gamma A})$$

$$i_{1} = i(-1) = \frac{V^{+}}{20}(e^{\gamma A} - P_{2}e^{-\gamma A})$$

$$= \frac{V^{+}}{20}(e^{\gamma A} - P_{2}e^{-\gamma A})$$

$$V_2 = V\omega) = V^{+}(1+\rho_c)=2V^{+}$$

$$\frac{1}{2} = \frac{1}{2} = \frac{1}{1} = \frac{1}$$

$$\frac{2}{e^{7L} - e^{-7R}} = \begin{bmatrix} \frac{1}{1 - e^{-2R}} \\ \frac{2}{1 - e^{-2R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L}} \\ \frac{2}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L}} \\ \frac{2}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L}} \\ \frac{2}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L}} \\ \frac{2}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L}} \\ \frac{2}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \\ \frac{e^{7L} - e^{-7R}}{e^{7L} - e^{-7R}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \\ \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \\ \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \\ \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \end{bmatrix} = \begin{bmatrix} \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \\ \frac{e^{7L} - e^{-7L}}{e^{7L} - e^{-7L}} \end{bmatrix} =$$

2 (b) A // (A+B) =
$$\frac{\frac{2}{j_{NC+G}} \cdot (j_{NL} + j_{NL} + \frac{a_{NL}}{j_{NC+G}})}{\frac{2g}{j_{NC+G}} + j_{NL+B}} + \frac{a_{NL}}{j_{NC+G}} + \frac{a_{NL}}{j_{NC+G}} + \frac{a_{NL}}{j_{NC+G}} + \frac{a_{NL}}{j_{NL+B}} = \frac{2 \cdot [(j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}]^{k_{NL}}}{4(j_{NC+G}) + (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}} = \frac{4}{4(j_{NC+G}) + (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}} = \frac{4}{4(j_{NC+G}) + (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}} = \frac{2}{e^{NL} - e^{-NL}} = \frac{e^{NL} + e^{-NL}}{e^{NL} - e^{-NL}} = \frac{e^{NL} + e^{-NL}}{e^{NL} - e^{-NL}} = \frac{1}{2} (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}} + (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}}{e^{NL} - e^{-NL}} = \frac{1}{2} (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}} + \frac{1}{2} (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}}{e^{NL} - e^{-NL}} = \frac{1}{2} (j_{NL} + k_{N})(j_{NC+G})^{k_{NL}}}{e^{NL} - e^{-NL}} = \frac{2}{2} (j_{NL} + k_{N})(j_{NL} + k_{N})(j_{NL}$$

To-march each equation.

(in preto single mode

$$\frac{2 + 15wL + 12)(5wc+G)^{2}}{2(5wc+G) + \frac{1}{2}(5wL+12)Gwc+G)^{2}}$$

$$\frac{2}{2(5wc+G) + \frac{1}{2}(5wL+12)Gwc+G)^{2}}$$

$$\frac{2}{2(5wc+G) + \frac{1}{2}(5wL+12)(5wc+G)^{2}}$$

$$\frac{2}{2(5wc+G) + \frac{1}{2}(5wL+12)(5wc+G)^{2}}$$

$$\frac{2}{2(5wc+G) + \frac{1}{2}(5wL+12)(5wc+G)^{2}}$$

(d). From observation

$$\begin{cases} 2+\gamma^{2}\chi^{2} = 2+ \left(jvL+R\right)\left(jnC+G\right) \\ \frac{1}{2} \cdot (2+\frac{1}{3}\gamma^{2}\chi^{2}) = o\left(jwC+G\right) \cdot \left[2+\frac{1}{2}\left(jwL+R\right)\left(jwC+G\right)\right] \\ \cdot \left[\gamma L = F\left(\frac{1}{2} \cdot R+jwBL\right)\right] \int (P+jwL)\left(G+jwQ\right) = A\left(R'+jwBL'\right)\left(G'+jwC'\right) \cdot L \\ \frac{\gamma L}{\gamma_{0}} = jwC+G = G'(jwC'+G')L \\ \cdot \left[P=R'.L] \end{cases}$$

:.
$$A = A'.A$$
 (The 3rd order has coefficient mismatch, but 0.1.1, 2 order $C = C'.A$ match, so the approximation is very close)

 $A = A'.A$ (The 3rd order has coefficient mismatch, but 0.1.1, 2 order $A = A'.A$

So the model 13

so the opi model is a good approximation

3. (a)-Load impedance should be son.

$$P_{\text{max}} = \frac{1}{2} \left(\frac{V_{AP}}{2 \cdot 2R} \right)^2 \cdot I^2 = \frac{V_{PP}}{32} \cdot \frac{1}{502} = \frac{1}{32} \cdot \frac{1}{50} = 0.625 \text{ mW}$$

(d). Be
$$P_L = \frac{32-30}{32+30} = \frac{500-158.1}{500+158.1} = 0.52.$$

Let of be the divinition.

$$Z_{11} = Z_{1} \cdot \frac{1 + \rho_{L} e^{-23k(2+x)}}{1 - \rho_{L} e^{-23k(2+x)}} = 50 \cdot \frac{1 + 0.52 \cdot e^{-23kx}}{1 + 0.52 \cdot e^{-23kx}}$$

: frequency range from 505MHz ~ 1.495 per GHz.
The simulation yields same results.

Eqn P=0.5*dB(VL*VL/500/2)

