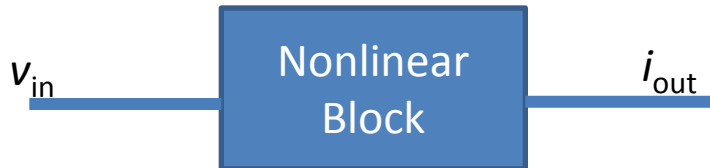


Today's Agenda (Nov. 1)

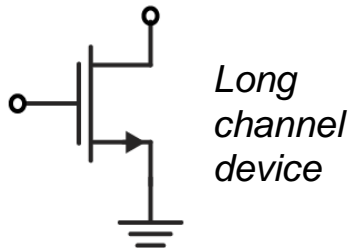
- Important Distortion Matrices
- IIP2 and IIP3 For Cascade Circuits
- Hw8: Distortion Analysis
- ADS Harmonic Balance Setup

Important Distortion Matrices



$$i_{\text{out}} \text{ (or } v_{\text{out}}) = a_1 v_{\text{in}} + a_2 v_{\text{in}}^2 + a_3 v_{\text{in}}^3 + \dots$$

Very Important: v_{in} and i_{out} are small-signal !!!



$$I_d = 0.5 \mu_n C_{\text{ox}} W/L (V_{\text{gs}} - V_{\text{th}})^2$$

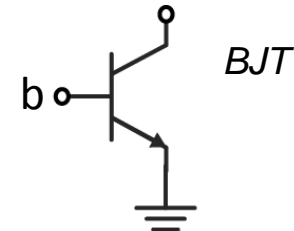
$$= 0.5 \mu_n C_{\text{ox}} W/L V_{\text{th}}^2 - \mu_n C_{\text{ox}} W/L V_{\text{th}} V_{\text{gs}} + 0.5 \mu_n C_{\text{ox}} W/L V_{\text{gs}}^2$$



$$I_d = 0.5 \mu_n C_{\text{ox}} W/L (V_{\text{gs0}} - V_{\text{th}} + v_{\text{in}})^2 =$$

$$0.5 \mu_n C_{\text{ox}} W/L (V_{\text{gs0}} - V_{\text{th}})^2 + \mu_n C_{\text{ox}} W/L (V_{\text{gs0}} - V_{\text{th}}) v_{\text{in}} + 0.5 \mu_n C_{\text{ox}} W/L v_{\text{in}}^2$$

$$\Rightarrow i_{\text{out}} = \mu_n C_{\text{ox}} W/L (V_{\text{gs0}} - V_{\text{th}}) v_{\text{in}} + 0.5 \mu_n C_{\text{ox}} W/L v_{\text{in}}^2$$



$$I_c \approx I_{\text{S0}} \exp(V_b/V_T)$$

$$= I_{\text{S0}} + I_{\text{S0}}/V_T V_b + I_{\text{S0}}/2V_T V_b^2 + I_{\text{S0}}/6V_T V_b^3 + \dots$$

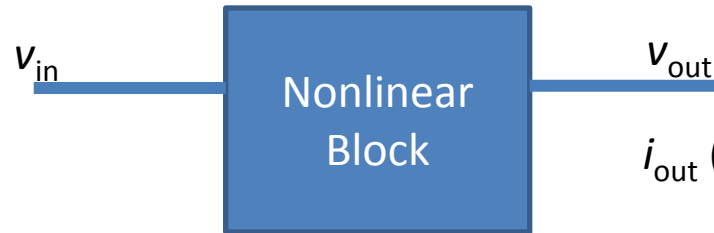


$$I_c \approx I_{\text{S0}} \exp[(V_b + v_{\text{in}})/V_T] = I_{\text{C0}} \exp(v_{\text{in}}/V_T)$$

$$= I_{\text{C0}} + I_{\text{C0}}/V_T v_{\text{in}} + I_{\text{C0}}/2V_T v_{\text{in}}^2 + I_{\text{C0}}/6V_T v_{\text{in}}^3 + \dots$$



Important Distortion Matrices

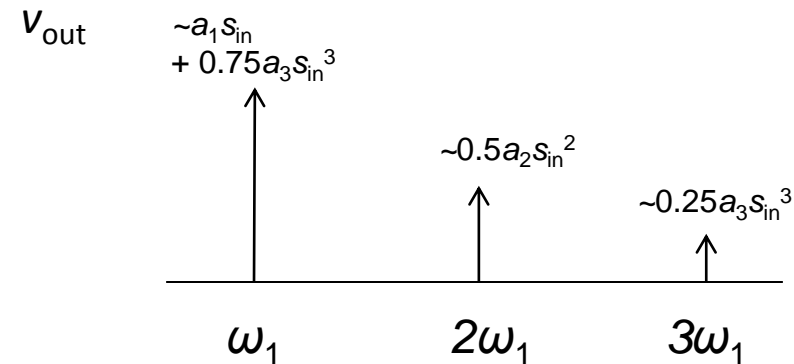


$$i_{\text{out}} \text{ (or } v_{\text{out}}) = a_1 v_{\text{in}} + a_2 v_{\text{in}}^2 + a_3 v_{\text{in}}^3 + \dots$$

v_{in} and i_{out} are small-signal !!!

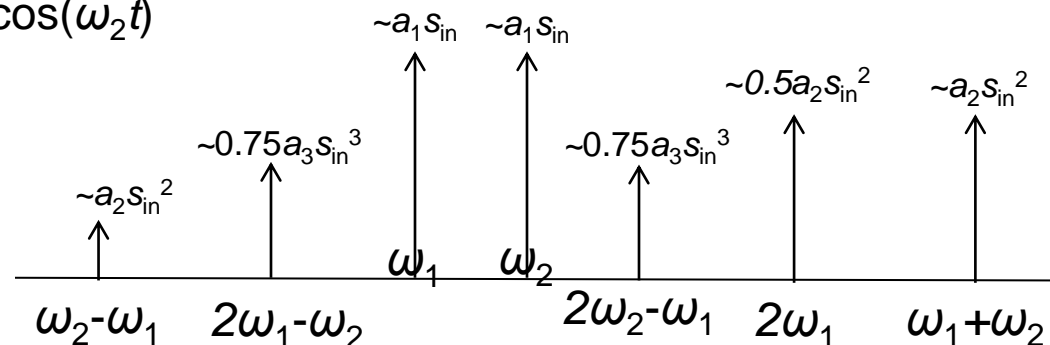
Single-Tone Excitation: $v_{\text{in}} = s_{\text{in}} \cos(\omega_1 t)$

- HD2 = $a_2 / (2a_1) \times s_{\text{in}}$
- HD3 = $a_3 / (4a_1) \times s_{\text{in}}^2$
- $\text{IP}_{1\text{dB}}$: $s_{\text{in}} = \sqrt{|4a_1| / |3a_3| \times 0.11}$

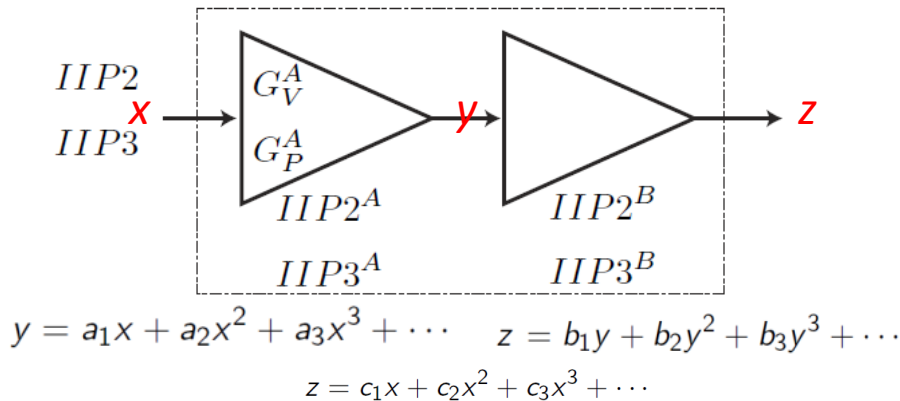


Two-Tone Excitation: $v_{\text{in}} = s_{\text{in}} \cos(\omega_1 t) + s_{\text{in}} \cos(\omega_2 t)$

- IM2 = $a_2 / a_1 \times s_{\text{in}}$
- IIP2 = $s_{\text{in}} = a_1 / a_2$
- IM3 = $3a_3 / (4a_1) \times s_{\text{in}}^2$
- IIP3 = $s_{\text{in}} = \sqrt{|4a_1| / |3a_3|}$



IIP2 and IIP3 For Cascade Circuits



x , y , and z are voltage or current

$$\frac{1}{IIP2} = \frac{1}{IIP2^A} + \frac{a_1}{IIP2^B}$$

$$\frac{1}{IIP3^2} = \frac{1}{IIP3_A^2} + \frac{a_1^2}{IIP3_B^2}$$

IIP2 and IIP3 in the above formula are voltage or current

- Example 1: Suppose the input amplifiers of a cascade has $IIP2^A = +0$ dBm and a voltage gain of 20 dB. The second amplifier has $IIP2^B = +10$ dBm.

The formula has to be used in voltage domain!

case1

- $IIP2^A = 1$ mW which is 0.32V if the input is 50Ω
- $IIP2^B = 10$ mW which is 1V if the input is 50Ω
- voltage gain of 20 dB $\Rightarrow a_1 = 10$
- $IIP2 = (1/0.32 + 10/1)^{-1} = 0.076$ V or **-12.4 dBm**

case2

- $IIP2^A = 1$ mW which is 0.45V if the input is 100Ω
- $IIP2^B = 10$ mW which is 0.45V if the input is 10Ω
- voltage gain of 20 dB $\Rightarrow a_1 = 10$
- $IIP2 = (1/0.45 + 10/0.45)^{-1} = 0.041$ V or **-20.7 dBm**

IIP2 and IIP3 For Cascade Circuits

$$\frac{1}{IIP3^2} = \frac{1}{IIP3_A^2} + \frac{a_1^2}{IIP3_B^2}$$

IIP3 in the above formula are voltage or current

- LNA has an $IIP3^A = -10 \text{ dBm}$ and a power gain of 20 dB. The mixer has an $IIP3^B = -20 \text{ dBm}$.

case1

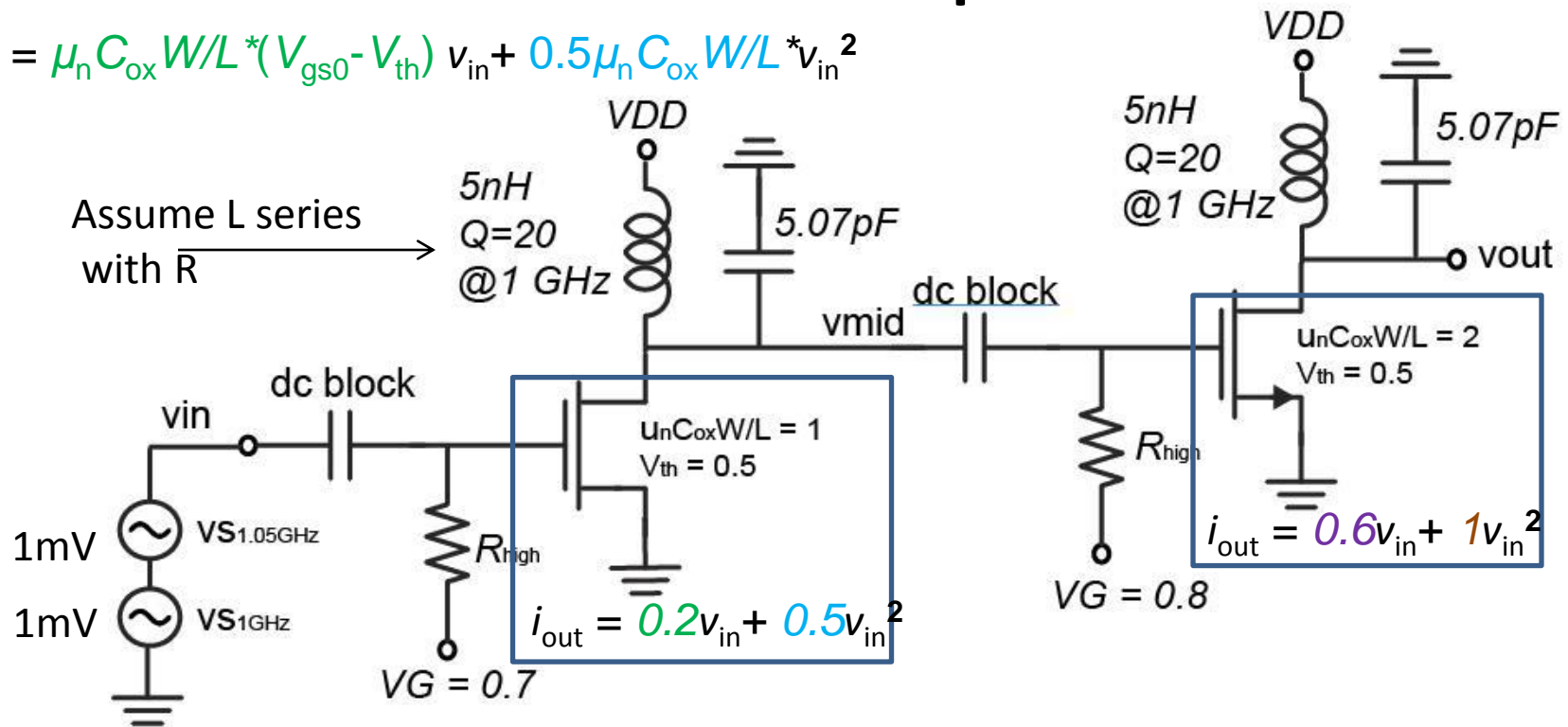
1. $IIP3^A = 0.1 \text{ mW}$ which is 0.1V if the input is 50Ω
 2. $IIP3^B = 0.01 \text{ mW}$ which is 32mV if the input is 50Ω
 3. power gain of 20 dB $\Rightarrow a_1 = 10$
 4. $IIP3^2 = (1/0.1^2 + 10^2/0.032^2)^{-1}$
- $\Rightarrow IIP3 = 3.2 \text{ mV}$ or **-40 dBm**

case2

1. $IIP3^A = 0.1 \text{ mW}$ which is 0.14V if the input is 100Ω
 2. $IIP3^B = 0.01 \text{ mW}$ which is 14mV if the input is 10Ω
 3. power gain of 20 dB $\Rightarrow a_1 = 32$
 4. $IIP3^2 = (1/0.14^2 + 32^2/0.014^2)^{-1}$
- $\Rightarrow IIP3 = 0.44 \text{ mV}$ or **-60 dBm**

HW Example

$$i_{out} = \mu_n C_{ox} W/L * (V_{gs0} - V_{th}) v_{in} + 0.5 \mu_n C_{ox} W/L * v_{in}^2$$



- $V_{mid_1.0GHz} \sim -0.2 * 1m * 628 = -0.125$
- $V_{mid_1.05GHz} \sim -0.2 * 1m * (135 - 270j) = -0.027 - 0.054j$
- $V_{mid_2.05GHz} \sim -0.5 * 1m * 1m * -20j = 1e-5j$
- $V_{mid_2.1GHz} \sim -0.5 * 0.5 * 1m * 1m * -20j = 5e-6j$
- $V_{mid_0.05GHz} \sim -0.5 * 1m * 1m * (1.6 + 1.6j) = -0.8u - 0.8uj$

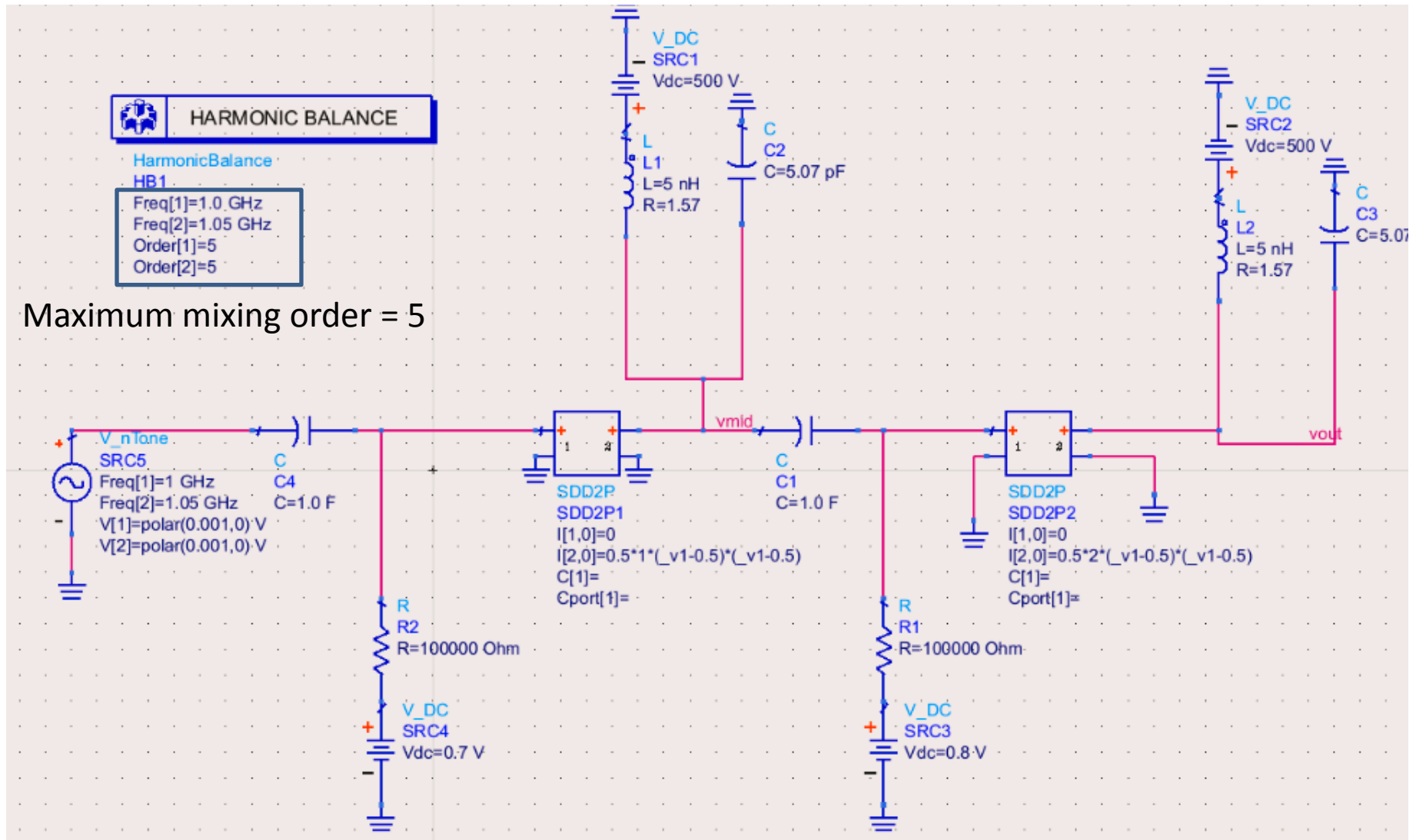
$$V_{o_1.0G} \sim -0.6 * -0.125 * 628 = 47 \text{ V (?!)}$$

$$V_{o_1.1GHz} \text{ from 4 and 1} \sim -1 * -0.125 * 5e-6j * (35 - 160j) = 1e-4 + 2.2e-5j$$

$$V_{o_1.1GHz} \text{ from 2 and 5} \sim -1 * (-0.027 - 0.054j) * (-0.8u - 0.8uj) * (35 - 160j) = -9.6e-6 - 5.7e-6j$$

$$V_{o_1.1GHz} \sim 1e-4 + 2.2e-5j$$

ADS Harmonic Balance Setup



Maximum mixing order = 5

Assume solution space: $m \cdot 1.05 + n \cdot 1 \quad |m| + |n| < 6$

ADS Harmonic Balance Setup

freq	(vmid)	freq	(vout)
m=1, n=-1 0.0000 Hz	499.969 + j0.000	0.0000 Hz	499.844 + j0.000
m=2, n=-2 50.00 MHz	-7.889E-7 - j7.854E-7	50.00 MHz	-0.015 + j0.005
m=1, n=-1 100.0 MHz	4.033E-19 - j9.720E-21	100.0 MHz	-3.862E-11 - j8.091E-11
m=-2, n=3 900.0 MHz	-3.181E-17 - j4.531E-17	900.0 MHz	-3.431E-15 + j3.261E-15
m=-1, n=2 950.0 MHz	1.316E-16 + j2.155E-16	950.0 MHz	-1.036E-4 - j5.779E-5
m=0, n=1 1.000 GHz	-0.125 + j0.008	1.000 GHz	46.758 - j6.139
m=1, n=0 1.050 GHz	-0.023 + j0.052	1.050 GHz	-6.436 - j7.291
m=2, n=-1 1.100 GHz	-2.026E-49 + j2.337E-48	1.100 GHz	9.356E-5 + j3.659E-5
m=3, n=-2 1.150 GHz	-6.539E-17 + j1.890E-16	1.150 GHz	-1.264E-14 - j5.860E-15
m=-1, n=3 1.950 GHz	-1.031E-17 - j3.303E-18	1.950 GHz	9.163E-11 - j8.805E-11
m=0, n=2 2.000 GHz	-4.457E-8 + j5.229E-6	2.000 GHz	0.020 + j0.162
m=1, n=1 2.050 GHz	-7.832E-8 + j1.004E-5	2.050 GHz	0.133 + j0.051
m=2, n=0 2.100 GHz	-3.459E-8 + j4.831E-6	2.100 GHz	0.024 - j0.020
m=3, n=-1 2.150 GHz	1.854E-18 + j1.183E-18	2.150 GHz	7.002E-11 + j7.162E-11
m=-1, n=4 2.950 GHz	-8.433E-18 + j2.624E-17	2.950 GHz	-2.199E-16 - j4.119E-17
m=0, n=3 3.000 GHz	-1.184E-18 + j2.102E-17	3.000 GHz	7.682E-6 - j4.189E-7
3.050 GHz	-3.487E-18 + j4.037E-18	3.050 GHz	1.590E-5 - j3.911E-6
3.100 GHz	4.690E-19 + j4.651E-18	3.100 GHz	9.533E-6 - j6.240E-6
3.150 GHz	5.769E-18 + j3.468E-18	3.150 GHz	1.281E-6 - j2.764E-6
3.200 GHz	1.106E-18 + j2.423E-17	3.200 GHz	-6.728E-17 - j9.321E-18
4.000 GHz	0.000 + j0.000	4.000 GHz	2.046E-12 - j1.144E-10
4.050 GHz	1.340E-18 - j4.749E-18	4.050 GHz	7.421E-12 - j4.334E-10
4.100 GHz	7.339E-19 + j1.269E-17	4.100 GHz	1.010E-11 - j6.161E-10
4.150 GHz	5.686E-18 - j2.858E-17	4.150 GHz	6.117E-12 - j3.895E-10
4.200 GHz	1.431E-18 - j2.952E-18	4.200 GHz	1.390E-12 - j9.244E-11
5.000 GHz	2.019E-19 - j1.082E-17	5.000 GHz	1.038E-16 - j3.888E-17
5.050 GHz	3.661E-18 + j1.075E-17	5.050 GHz	-3.087E-17 + j2.804E-17
5.100 GHz	0.000 + j0.000	5.100 GHz	-4.442E-17 - j1.739E-20
5.150 GHz	3.593E-18 + j1.969E-18	5.150 GHz	-2.747E-18 - j1.043E-21
5.200 GHz	1.641E-19 + j3.036E-17	5.200 GHz	-1.078E-16 - j3.004E-17
5.250 GHz	-1.480E-18 - j7.660E-18	5.250 GHz	3.022E-17 + j7.226E-18