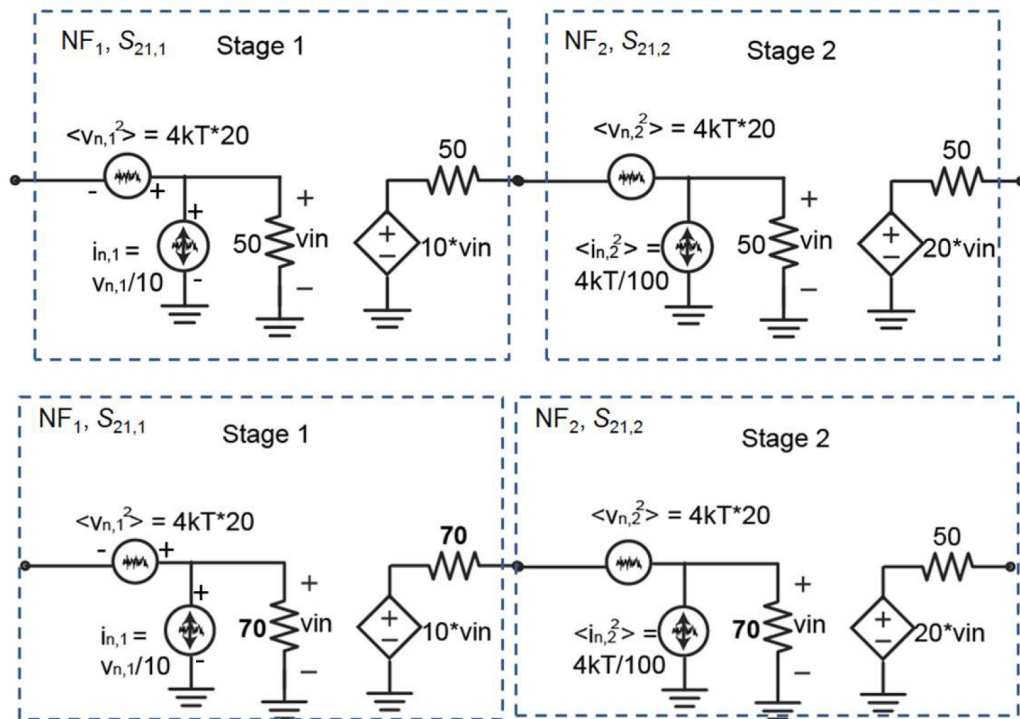


# EE142 Problem Set 7

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## 1 Noise Figure of Cascade Blocks and Lossy Transmission Line



- (a) For the above two cascade circuits, calculate the power gains and noise figures for each stage (i.e.  $S_{21,1}, S_{21,2}, NF_1, NF_2$ ) and the two stage circuits ( $S_{21,total}, NF_{total}$ ). The resistors are assumed to be noiseless.

### 1.a Cascade 1

For the first cascade's stage 1, we begin by input referring the noise sources and collapsing the voltage and current noise into  $\overline{v_{eq}^2}$ . From lecture:

$$\overline{v_{eq}^2} = \overline{v_n^2} + \overline{i_n^2} R_s^2 + 2 \cdot R_s \cdot \overline{v_n i_n}$$

$$F = 1 + \frac{N_{amp,i}}{N_s} = 1 + \frac{\overline{v_{eq}^2}}{\overline{v_s^2}}$$

Assume we are calculating noise figure in a  $50\Omega$  environment,  $R_s = 50\Omega$  and  $\overline{v_s^2} = 4kTR_s$ . We assume that all noise sources represented are defined as *spot noise*. Furthermore, we *don't* assume that  $\overline{v_n^2}$  and  $\overline{i_n^2}$  are uncorrelated, and include covariance terms when needed.

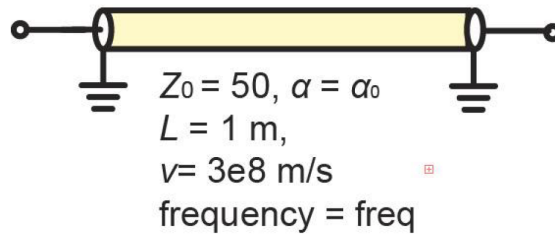
$$i_{n,1} = v_{n,1}/10 \rightarrow \overline{i_{n,1}^2} = \overline{v_{n,1}^2}/100$$

$$F_1 = 1 + \frac{\overline{v_{eq,1}^2}}{\overline{v_s^2}} = \frac{4kT \cdot 20 + 4kT \cdot 0.2 \cdot 50^2}{4kT \cdot R_s} = 10.4$$

$$NF_1 = 10 \cdot \log(F_1) = 23.42 \text{ dB}$$

(b) Is the formula  $NF_{total} = NF_1 + \frac{NF_2 - 1}{|S_{21,1}|^2}$  applicable?

(c) For a lossy transmission line illustrated below, derive its noise figure.



Starting with the definition of  $F$ :

$$F = \frac{SNR_i}{SNR_o} = \frac{P_{sig}/\overline{v_{n,s}^2}}{P_{sig} \cdot \text{loss}/\overline{v_{n,s}^2} \cdot \text{loss}^2}$$

$$F = \frac{1}{\text{loss}}$$

where 'loss' represents the power loss of the transmission line in steady state from input to output. This is simple to compute, assuming that the line is driven with a source impedance of  $Z_0$  with a mean squared noise voltage of  $4kTZ_0$  and terminated with a noiseless load of  $Z_0$ .

$$\text{Power @ Load} = V_+ e^{-\gamma l} \cdot \frac{1}{Z_0} e^{-\gamma l} V_+ |_{l=0} = \frac{V_+^2}{Z_0}$$

$$\text{Power @ Source} = V_+ e^{-\gamma l} \cdot \frac{1}{Z_0} e^{-\gamma l} V_+ |_{l=-l} = \frac{V_+^2 e^{2\gamma l}}{Z_0}$$

$$\text{Power @ Load} / \text{Power @ Source} = e^{-2\gamma l}$$

$$F = \frac{1}{e^{-2\gamma l}} = e^{2\gamma l}$$

We know the propagation constant  $\gamma = \alpha + j\beta$ . Because the velocity of the line is at the speed of light, the imaginary term goes to zero and  $\gamma$  is dominated by  $\alpha$ .

$$F = e^{2\alpha_0 L}$$

The noise figure seems frequency independent, but any real line has  $\beta = \frac{2\pi}{\lambda}$ .

- (d) If the tline is used to connect the above two cascade circuits to the  $50\Omega$  source (e.g. antenna), what will be the new total noise figures

## 2 Matching for Low Noise Versus Matching for High Gain

*In this problem, your answers should be functions of frequency.*

- (a) For a simplified common-source model shown below (with noise sources drawn) derive the input referred noise voltage and noise current.