

# **EE 240B – Fall 2019**

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## **Advanced Analog Integrated Circuits**

### **Lecture 8: Operational Transconductance Amplifiers (I)**

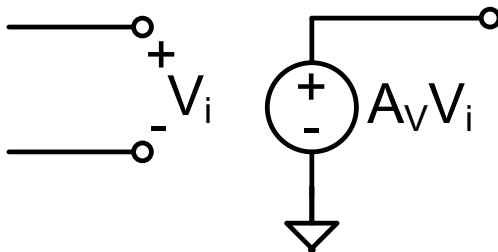
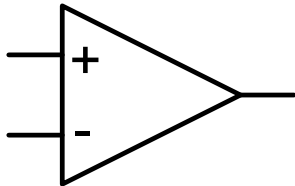


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# OpAmps and OTAs

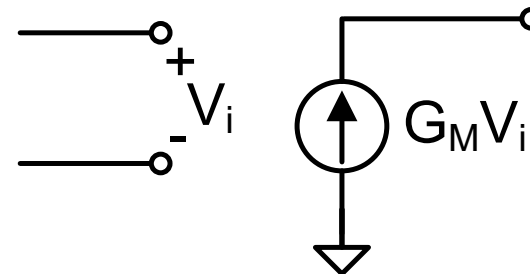
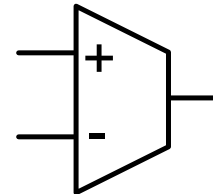
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## OpAmp



- High voltage gain, high input impedance
- Voltage source output (low impedance)

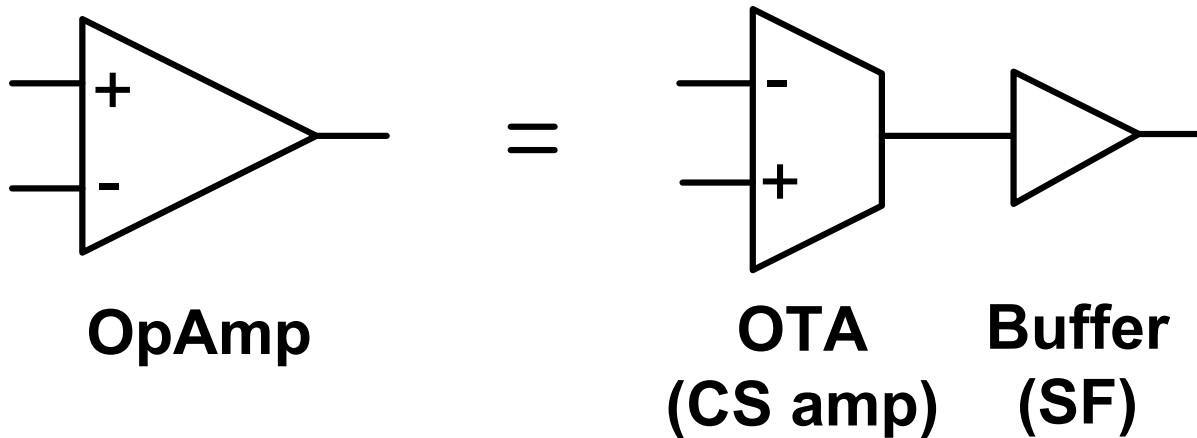
## OTA



- High “voltage” gain, high input impedance
- Current source output (high impedance)

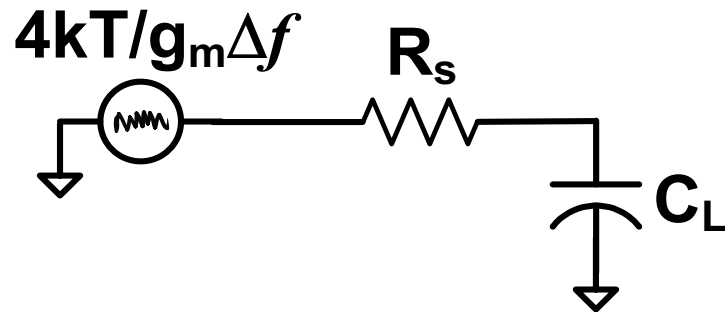
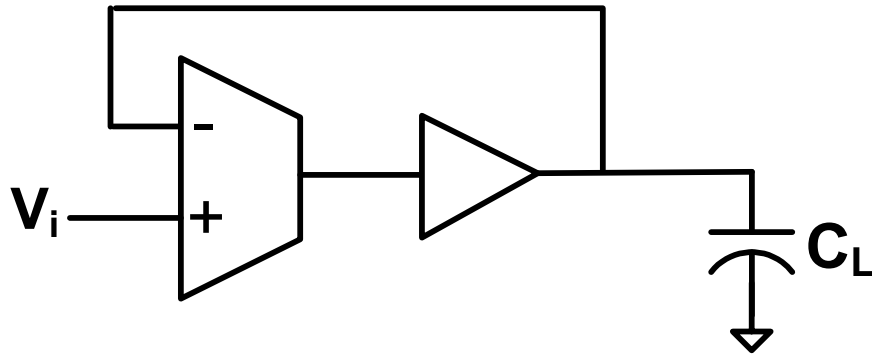
# Opamp & OTA in CMOS

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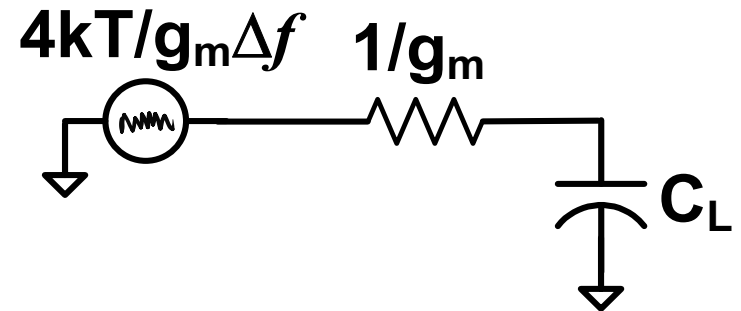
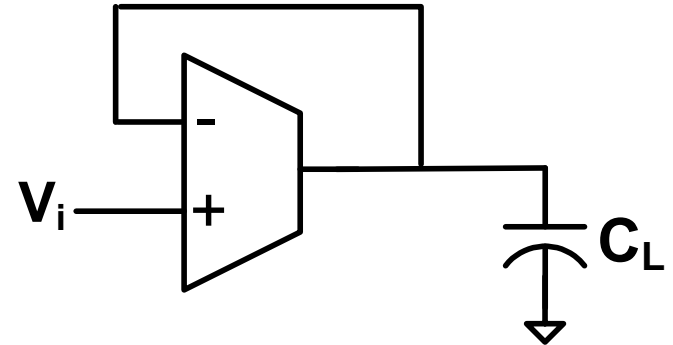
# Opamp vs. OTA Noise

## OpAmp



$$v_{o,n}^2 = \frac{4k_B T}{g_m} \frac{1}{4R_s C_L} = \frac{k_B T}{C_L} \frac{R_n}{R_s}$$

## OTA



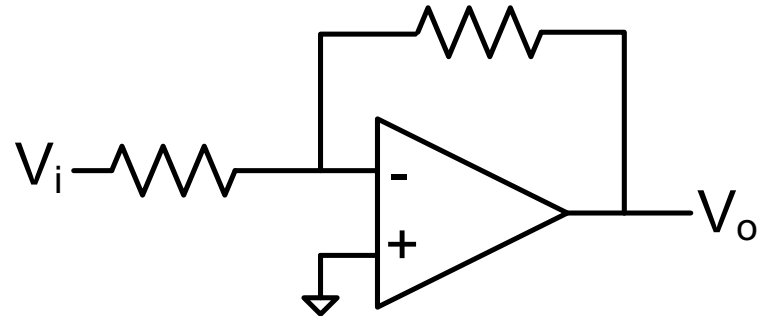
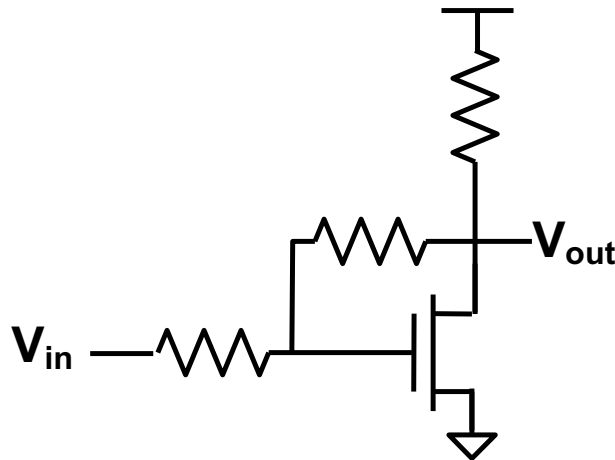
$$v_{o,n}^2 = \frac{k_B T}{C_L}$$

# **Simplest Single-Ended OTA**

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# Differential Input?

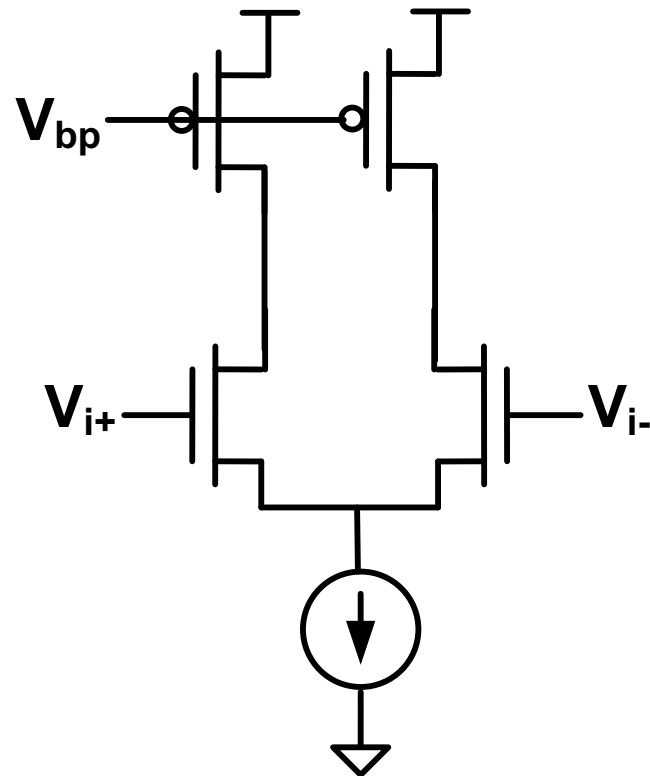
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- **Why use a differential input?**
  - Diff. version has extra device(s) – more power, noise, etc.
- **Real reason is systematic offset**
  - All voltages are relative
- **If used a differential input, often might as well use differential output too...**

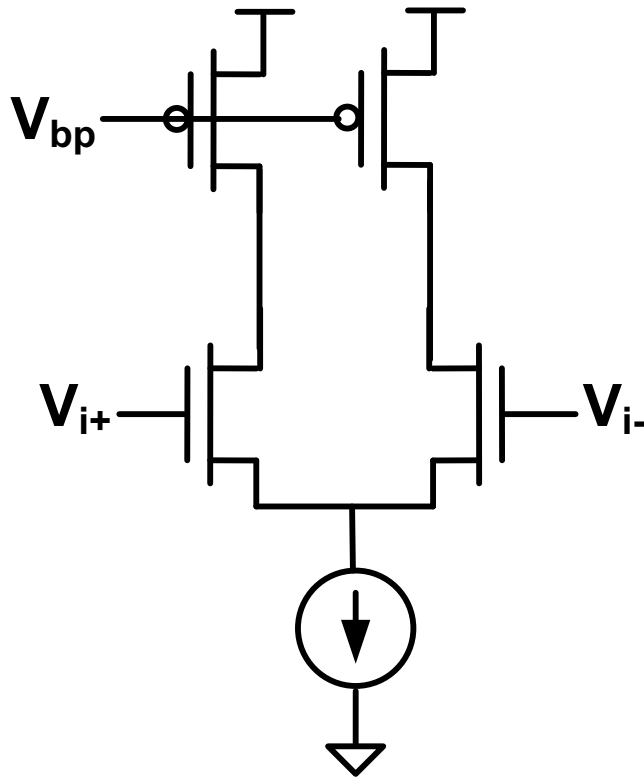
# Simple Diff. Input OTA

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# Simple Diff. Input OTA: Noise (1)

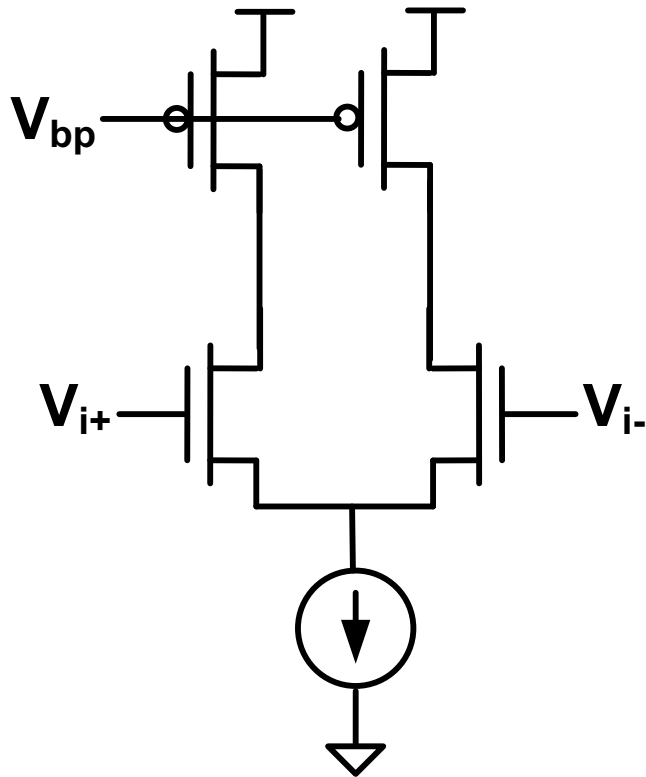
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# Simple Diff. Input OTA: Noise (2)

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# Simple Diff. Input OTA: Noise (2)

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# More Careful Look at Noise...

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# More Careful Look at Noise...

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# Real R vs. Current Source (1)

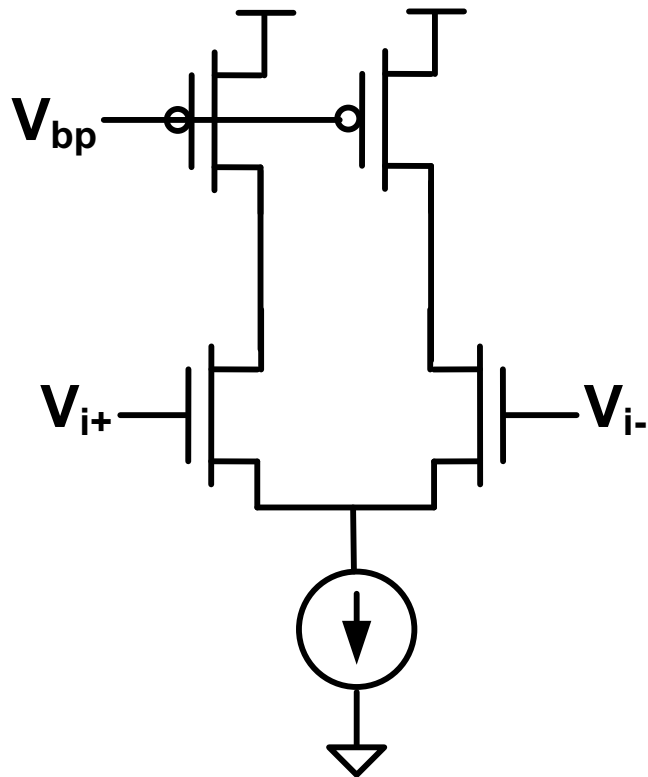
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# Real R vs. Current Source (2)

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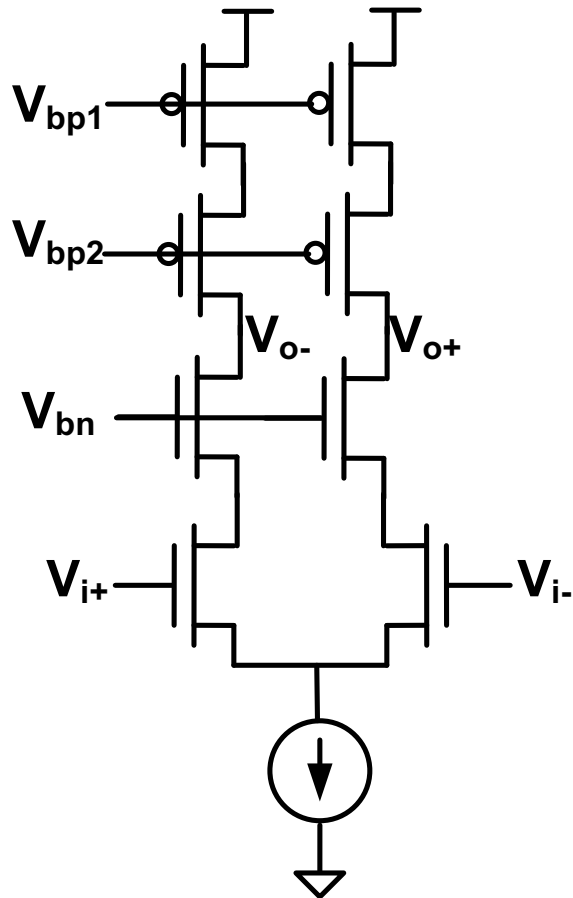
# Limitations of Simple OTA

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# Telescopic Cascoded OTA

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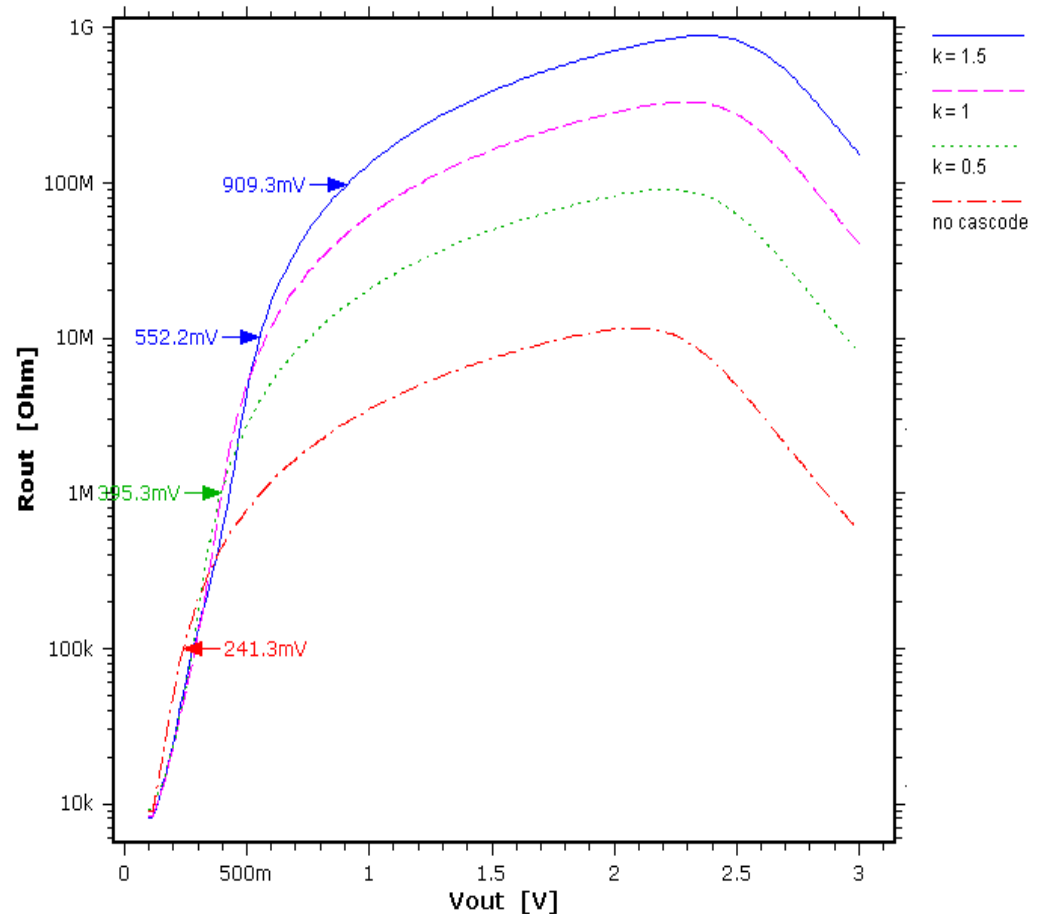




# Why Cascoding Helps

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# Cascode Sizing for $r_o$



# Cascode Noise?

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# Cascode Noise?

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# More Complete Analysis

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# More Complete Analysis

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# Cascode Sizing

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