

# Explanatory Document for `tms_2.m`: Battery Cooling Simulation

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# 1 Introduction

The `tms_2.m` script enhances `tms_1.m` by introducing a dynamic discharge profile (variable C-rates), PID control for cooling, and support for nominal (35°C) and worst-case (40°C) ambient conditions. It uses an RK4 solver instead of Euler for improved numerical accuracy and includes a Simulink fallback. The script models a 48V, 4kWh lithium-ion battery pack (13s10p) with a liquid cooling plate. This document explains each code section, highlighting improvements over `tms_1.m`.

## 2 Code Structure

The script is organized into:

- License and Environment Check
- Battery Pack Parameters
- Electrical Load Profile
- Cooling System Parameters
- Simulation (Nominal and Worst-Case)
- Results
- Plotting
- Local Function (RK4)
- Troubleshooting Notes

## 3 License and Environment Check

```
1 clear; clc; close all;
2
3 matlab_ver = ver;
4 simscape_licensed = license('test', 'Simscape');
5 simulink_licensed = license('test', 'Simulink');
6 fprintf('MATLAB Version: %s\n', matlab_ver(1).Version);
7 ...
8
9 use_simulink = simulink_licensed;
10 if use_simulink
11     try
12         add_block('simulink/Continuous/Integrator', 'test/Integrator');
13         ...
14     catch e
15         warning('Simulink Integrator block unavailable: %s. Using
16             numerical solver.', e.message);
17         use_simulink = false;
18     end
19 else
20     fprintf('Simulink not licensed. Using numerical ODE solver.\n');
```

Similar to `tms_1.m`, this section clears the workspace and checks for MATLAB, Simscape, and Simulink licenses. It tests the Simulink Integrator block (noting a change to `Continuous/Integrator`

from Commonly Used Blocks/Integrator) and sets `use_simulink` accordingly. The check ensures the script can run with or without Simulink.

## 4 Battery Pack Parameters

```

1 cell_voltage = 3.6; % Nominal voltage (V)
2 cell_capacity = 8.55; % Capacity (Ah, adjusted for ~4kWh)
3 cell_resistance_base = 0.007; % Base internal resistance (Ohm, 7 mOhm)
4 ...
5
6 num_series = 13; num_parallel = 10;
7 pack_voltage = num_series * cell_voltage; % 46.8V
8 pack_capacity = num_parallel * cell_capacity; % 85.5Ah
9 ...
10
11 rng(42);
12 cell_resistance = cell_resistance_base * (1 + 0.1 * (2 *
    rand(num_series, num_parallel) - 1));
13 avg_cell_resistance = mean(cell_resistance(:));
14
15 T_ambient_base = 35; T_ambient_worst = 40; T_max_limit = 45; T_runaway
    = 60;
16 T_coolant_in = 24; T_initial = 25;

```

This section refines `tms_1.m` by: - Reducing `cell_resistance` to 7 mOhm (more realistic) with  $\pm 10\%$  variation across cells, seeded for reproducibility. - Introducing a worst-case ambient temperature (40°C) and a thermal runaway threshold (60°C). - Lowering `T_coolant_in` to 24°C for stronger cooling.

The pack remains 13s10p, yielding 4kWh.

## 5 Electrical Load Profile

```

1 time_segments = [0 150 300 ... 3600];
2 c_rates = [0.5 2 1 3 0.5 ... 0.5]; % Aggressive cycle
3 current_total = c_rates * pack_capacity;
4 current_cell = current_total / num_parallel;
5
6 heat_gen_cell = zeros(1, length(c_rates));
7 for i = 1:length(c_rates)
8     heat_gen_cell(i) = (current_cell(i)^2) * avg_cell_resistance + 0.5;
9 end
10 total_heat = heat_gen_cell * num_series * num_parallel;

```

Unlike `tms_1.m`'s constant 2C discharge, this section defines a dynamic drive cycle with 25 segments (0–3600s) and C-rates varying between 0.5C and 3C. Heat generation is computed per segment using  $I^2R + 0.5$  W entropic heating, scaled for the entire pack. This models a more realistic, aggressive load.

## 6 Cooling System Parameters

```

1 pipe_surface_area = 0.2; h_conv_base = 1000; R_thermal = 0.02;
    tau_delay = 10;
2 m_dot = 0.02; Cp_coolant = 3500;

```

```

3
4 mass_factor = 1.2; ambient_noise_std = 1.0;
5
6 k_P = 120; k_I = 1.5; k_D = 25;

```

Improvements over `tms_1.m` include: - Increased `h_conv_base` (1000 W/m<sup>2</sup>-K) and reduced `R_thermal` (0.02 K/W) for better cooling. - Reduced `tau_delay` (10s) for faster response. - Added coolant flow (`m_dot` = 0.02 kg/s) and specific heat (`Cp_coolant` = 3500 J/kg-K) for outlet temperature calculation. - Replaced proportional control with PID (`k_P`, `k_I`, `k_D`) for tighter temperature tracking. - Increased `ambient_noise_std` to  $\pm 1^\circ\text{C}$ .

These changes enhance cooling realism and control.

## 7 Simulation (Nominal Case)

```

1 mCp = mass_factor * cell_mass * num_series * num_parallel *
  cell_specific_heat;
2 T_max = NaN; T_final = NaN; T_coolant_out = NaN;
3 temp_profile = []; time_data = []; runaway_flag = false;
4
5 if use_simulink
6     model_name = 'BatteryCoolingModel';
7     ...
8     set_param(model_name, 'StopTime', '3600', 'Solver', 'ode23t', ...);
9     try
10         sim(model_name);
11         temp_var = evalin('base', 'TempData');
12         ...
13         T_coolant_out = T_coolant_in + Q_cool_avg / (m_dot *
            Cp_coolant);
14     catch e
15         ...
16     end
17 else
18     t = 0:0.01:3600; dt = 0.01;
19     T = zeros(size(t)); T(1) = T_initial;
20     Q_cool_delayed = 0; integral_error = 0; prev_error = 0;
21     T_coolant_out_sum = 0;
22     for j = 2:length(t)
23         total_heat_t = interp1(time_segments, total_heat, t(j-1),
            'previous');
24         T_ambient = T_ambient_base + ambient_noise_std * randn();
25         k1 = thermal_dynamics(...);
26         k2 = thermal_dynamics(...);
27         k3 = thermal_dynamics(...);
28         k4 = thermal_dynamics(...);
29         T(j) = T(j-1) + (dt/6) * (k1 + 2*k2 + 2*k3 + k4);
30         ...
31         T_coolant_out_sum = T_coolant_out_sum + Q_cool;
32     end
33     T_coolant_out = T_coolant_in + (T_coolant_out_sum / length(t)) /
        (m_dot * Cp_coolant);
34 end

```

The nominal case (35°C ambient) is simulated using: - **Simulink**: A model with PID control, coolant delay, and nonlinear cooling, similar to `tms_1.m` but with enhanced blocks (e.g., PID

Controller). It calculates coolant outlet temperature. - **RK4 Solver**: Replaces Euler with RK4 for higher accuracy, using four slope estimates per step. Heat is interpolated from the drive cycle, and PID control adjusts cooling dynamically.

The RK4 solver is a significant upgrade, improving stability and precision.

## 8 Simulation (Worst-Case)

```

1 T_max_worst = NaN; T_final_worst = NaN; runaway_flag_worst = false;
2 if use_simulink
3     ...
4     set_param([model_name '/AmbientBase'], 'Value',
5               num2str(T_ambient_worst));
6     ...
7 else
8     t = 0:0.01:3600; dt = 0.01;
9     T = zeros(size(t)); T(1) = T_initial;
10    ...
11    T_ambient = T_ambient_worst + ambient_noise_std * randn();
12    ...
end

```

The worst-case simulation (40°C ambient) reuses the nominal case logic, updating only the ambient temperature. It ensures the cooling system can handle harsher conditions.

## 9 Results

```

1 fprintf('\nNominal Case (Ambient = %.0f C):\n', T_ambient_base);
2 ...
3 if T_max <= T_max_limit && ~isnan(T_max)
4     ...
5 end
6 if runaway_flag
7     warning('Thermal runaway risk detected: Temperature exceeded
8             %.0f C.', T_runaway);
9 end

```

Results are printed for both cases, including maximum and final temperatures, coolant temperatures, and stability checks (within 45°C and  $\pm 1^\circ\text{C}$  of ambient). A runaway flag warns if temperatures exceed 60°C.

## 10 Plotting

```

1 figure('Name', 'Temperature Profile');
2 plot(time_data, temp_profile, 'b-', 'LineWidth', 2, ...);
3 ...
4 plot([0 3600], [60 60], 'k:', 'LineWidth', 1.5, 'DisplayName',
5       'Runaway Threshold (60 C)');

```

The plot is similar to `tms_1.m` but adds a 60°C runaway threshold line and focuses on the nominal case. It uses a traditional `figure` instead of a GUI.

## 11 Local Function (RK4)

```
1 function dT = thermal_dynamics(T, t, total_heat_t, T_ambient,
   T_coolant_in, ...
2     h_conv_base, pipe_surface_area, R_thermal, k_P, k_I, k_D, ...
3     integral_error, prev_error, Q_cool_delayed, dt, tau_delay, mCp)
4     ...
5     dT = (total_heat_t - Q_cool_delayed) / mCp;
6 end
```

The `thermal_dynamics` function computes the temperature derivative for RK4, incorporating PID control, nonlinear cooling, and coolant delay. It's more complex than `tms_1.m`'s Euler-based dynamics.

## 12 Troubleshooting Notes

```
1 % If cell temperature does not stabilize near ambient (35 C      1 C
   or 40 C      1 C ):
2 % 1. Increase h_conv_base (e.g., 1100 W/m^2-K) or pipe_surface_area
   (e.g., 0.3 m^2).
3 % ...
4 % 12. Ensure file is named correctly (e.g., 'tms_2.m').
```

These notes suggest tuning cooling parameters and checking the environment, with a focus on RK4 and PID adjustments.

## 13 Summary

The `tms_2.m` script improves `tms_1.m` with a dynamic drive cycle, RK4 solver, PID control, and dual ambient conditions. It lacks a GUI, which is added in `tms_3.m`, but provides robust thermal modeling.