

Enhanced physics-informed neural networks (PINNs) for high-order power grid dynamics

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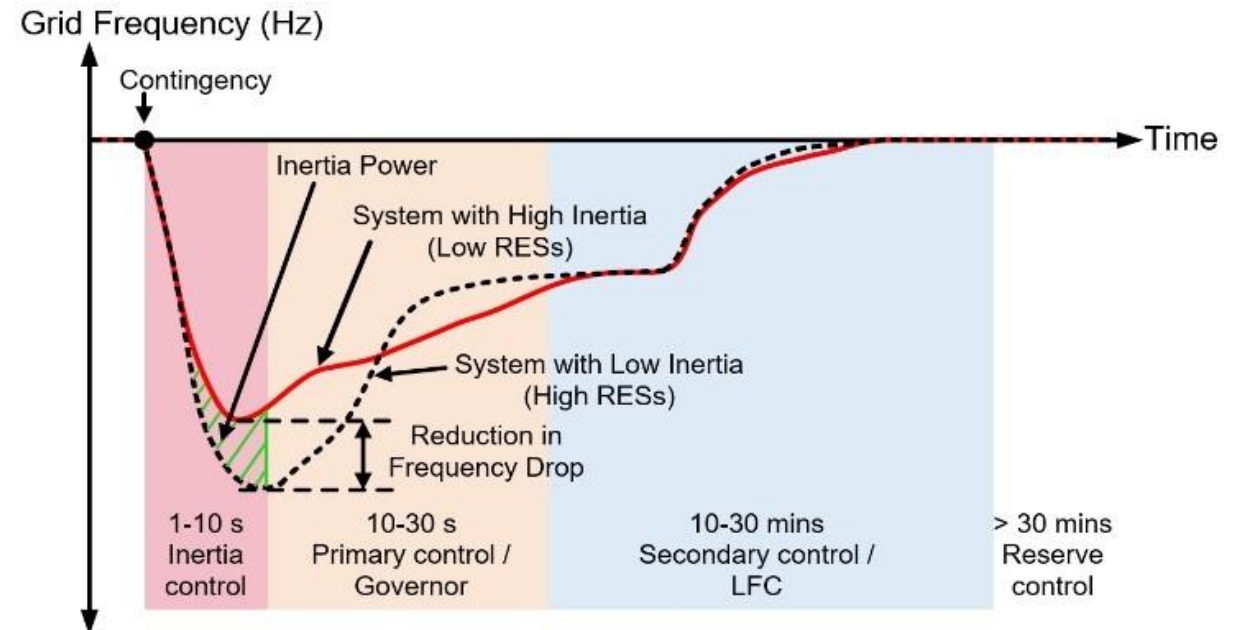
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*Work done as part of a research internship at X, the moonshot factory (formerly Google X)



Motivation

- Rapid power grid decarbonization
- Transition from fossil fuels to renewables
- Coal & natural gas plants are **synchronous generators (SGs)**
→ High inertia helps stabilize supply-demand imbalances
- Renewables (solar, wind) & batteries are **inverter-based resources (IBRs)**
→ Little to no inertia!
- Stability & reliability issues for the future grid



Transient stability analysis

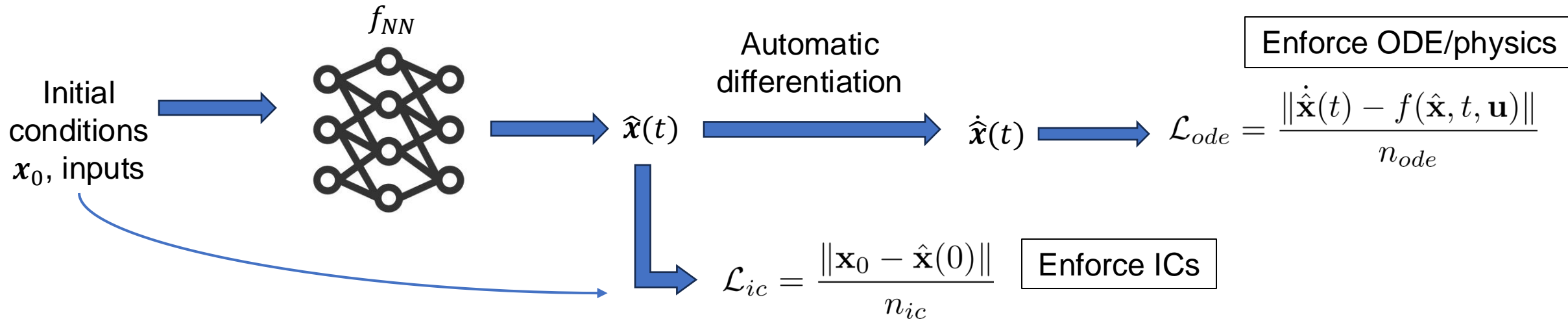
- Solve power system dynamics → Estimate grid frequency
- Crucial to assess transient stability esp. during disturbances (e.g. faults, line or generator outages, extreme weather)
- Involves systems of nonlinear ordinary differential equations (ODEs)
- Need to solve at very high resolution (milli- to micro-seconds)
- Cons of conventional numerical integration methods:
 - Expensive, may require small Δt for stability
 - Not scalable for the future distributed grid with millions of IBRs

Use physics-informed machine learning to directly predict ODE solutions & accelerate dynamic simulations with high accuracy

Physics-informed neural networks

- Approximate solution to initial value problem with neural network

$$\dot{\mathbf{x}} = f(\mathbf{x}, t, \mathbf{u}), \quad \mathbf{x}(0) = \mathbf{x}_0, \quad \hat{\mathbf{x}}(t) = f_{NN}(\mathbf{x}_0, t, \mathbf{u}; \boldsymbol{\theta})$$



- Minimize combined loss function to train PINN (with MLP layers)

$$\min_{\boldsymbol{\theta}} \mathcal{L}(\boldsymbol{\theta}) = \lambda_{ic} \mathcal{L}_{ic} + \lambda_{ode} \mathcal{L}_{ode}$$

Prior work and contributions

- A few papers have applied PINNs for power systems
- Most studies focus on dynamics of synchronous generators (SGs)
- Only 1 paper has considered PINNs for inverters
- Prior works generally use simplified or reduced order models
 - E.g. 2nd order swing equation for SG,
Or only 1 component of inverter (i.e. phase locked loop converter)
- **Our goal**: Develop enhanced PINNs that can be also applied to more complex, higher-order, & higher-dimensional ODE models
 - 4th order SG model
 - Full-order inverter model

Challenges with training PINN

- Difficult to train for higher-order, stiff ODE systems
- Ill-conditioned loss function, especially near optimum
 - Due to differential operator in ODE residual term
 - Many local minima & saddle points
- Curse of dimensionality
 - Expensive training & inference for higher-order ODEs
- Poor convergence, stability, and generalization issues

Proposed PINN enhancements

1. Initialize regularization weights $\lambda_{ic}, \lambda_{ode}$ using normalization strategies from multiobjective optimization
→ Based on *Utopia* and *Nadir* points in the Pareto set
2. Adaptively tune loss term weights during training
→ Based on intermediate values of their gradients
- (1) + (2) → Both losses have similar magnitudes & gradients
→ Balance learning ODE while also satisfying ICs
3. Sequence-to-sequence learning: PINN only predicts the very next time step instead of the whole time domain
4. Hyperparameter tuning & optimization
e.g. Combining optimizers: ADAM (1st order gradient-based method) followed by L-BFGS (2nd order, quasi-newton method)

Synchronous generator (sgPINN)

Model both SG and inverter using nonlinear state space approach:

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{R}(\mathbf{x}, \mathbf{u}) \text{ (matrix } \mathbf{R} \text{ captures all nonlinearities)}$$

Predict all 4 states

(i_d, i_q) : generator currents in the d-q coordinates

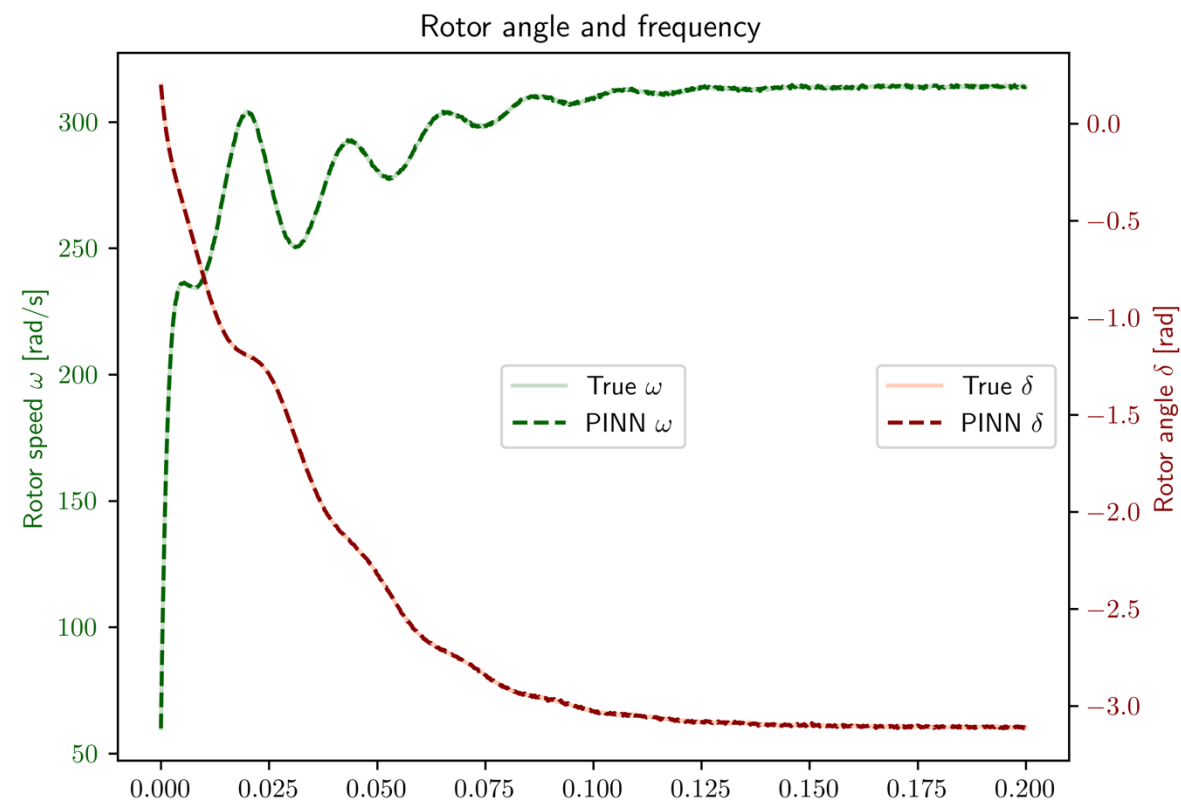
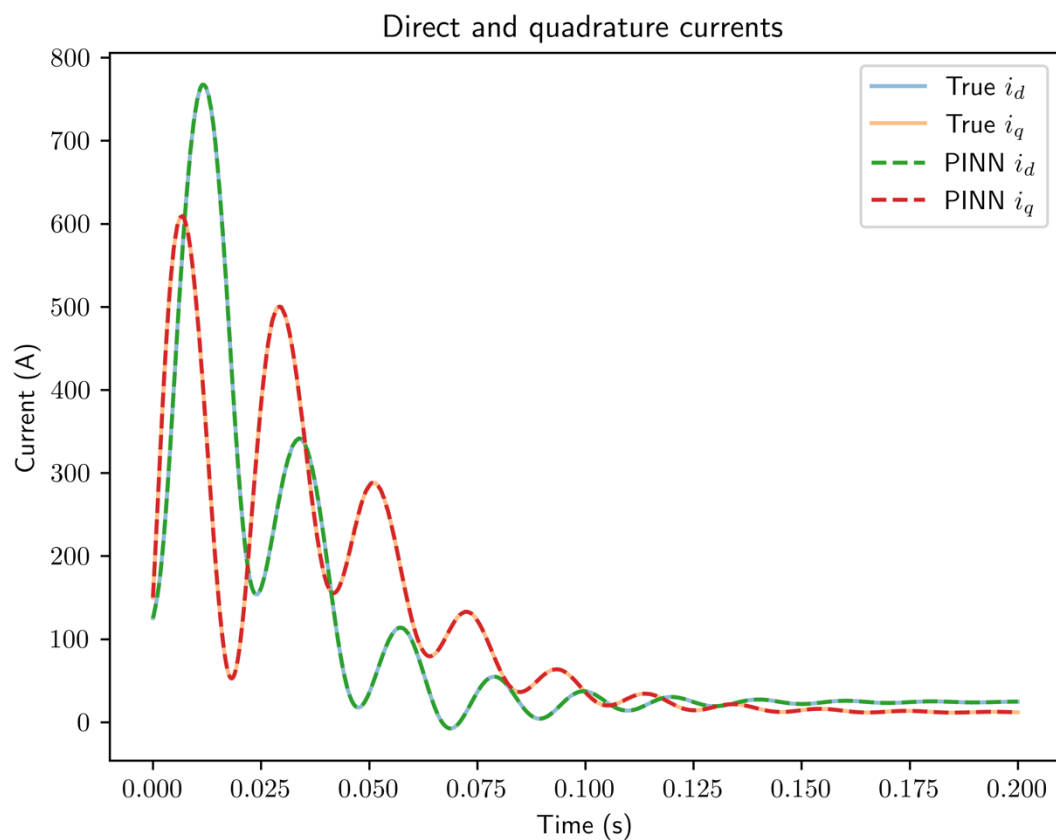
δ : angle difference

ω : generator frequency

$$\begin{bmatrix} \dot{i}_d \\ \dot{i}_q \\ \dot{\omega} \\ \dot{\delta} \end{bmatrix} = \begin{bmatrix} -\frac{R_s}{L_s} & \omega & 0 & 0 \\ -\omega & -\frac{R_s}{L_s} & -\frac{m i_f}{L_s} & 0 \\ 0 & \frac{m i_f}{J} & -\frac{D_p}{J} & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} i_d \\ i_q \\ \omega \\ \delta \end{bmatrix} + \begin{bmatrix} \frac{V}{L_s} \sin \delta \\ \frac{V}{L_s} \cos \delta \\ \frac{T_m}{J} \\ -\omega_g \end{bmatrix}$$

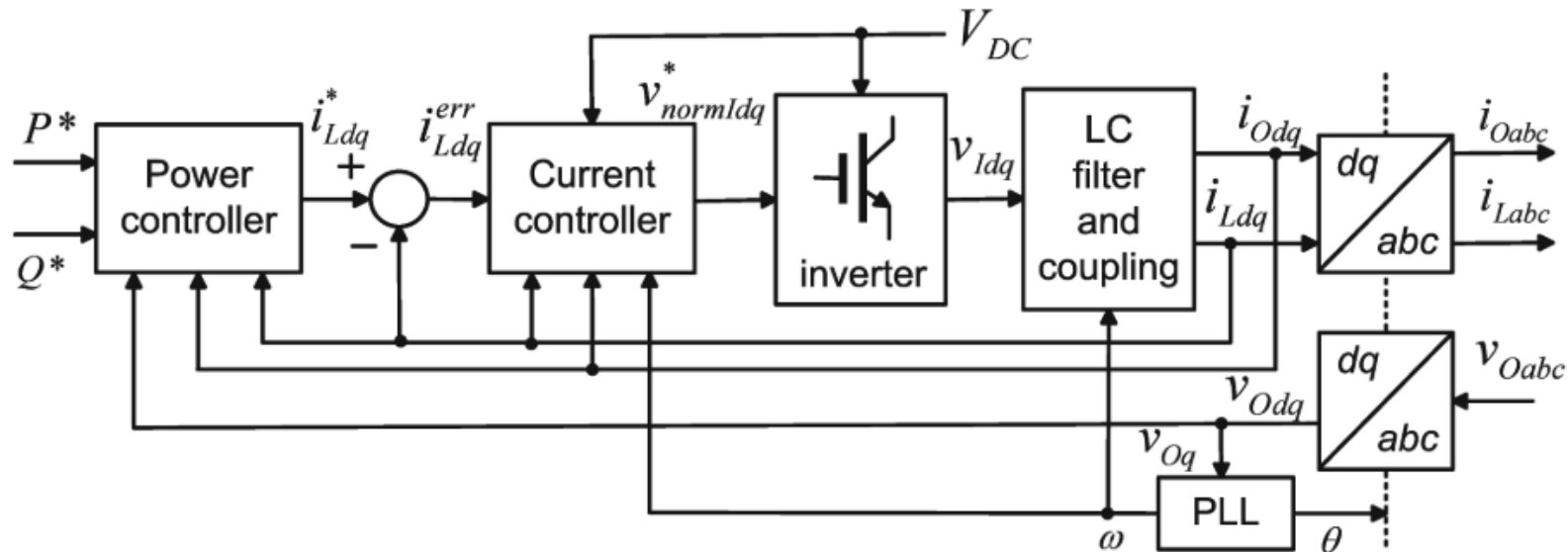
Parameter	Symbol	Value
Nominal Grid Frequency	ω_g	100π rad/sec
Stator Resistance	R_s	0.152Ω
Stator Inductance	L_s	4.4 mH
Damping Coefficient	D_p	10.14 Nm/(rad/sec)
Inertia Constant	J	0.02 Kgm ² /rad
Mechanical Torque	T_m	$[15.9 + D_p \omega_g]$ Nm
Nominal Voltage	V	$230\sqrt{3}$ Volts
Field Excitation Constant	m_{if}	-1.38 Voltsec

Preliminary sgPINN results



Inverter PINN model (invPINN)

- Complex grid-following inverter model with 17 total states



$$\mathbf{x} = [\theta \quad \Phi_{\text{PLL}} \quad i_{Ld}^* \quad i_{Lq}^* \quad q_{3Ld} \quad q_{3Lq} \quad q_{Ld}^{\text{err}} \quad q_{Lq}^{\text{err}} \quad i_{Ld} \quad i_{Lq} \quad i_{LO} \quad v_{Cd} \quad v_{Cq} \quad v_{CO} \quad i_{Od} \quad i_{Oq} \quad i_{OO}]^T$$

Inverter PINN model (invPINN)

$$A = \begin{bmatrix} 0 & K_I^{PLL} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -\sqrt{2}\omega_c & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \omega_c^2 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -\sqrt{2}\omega_c & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \omega_c^2 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 1 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R}{L} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R}{L} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{L} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{L} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{C} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{3R_G - R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{3R_G - R_{coupl}}{L_{coupl}} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

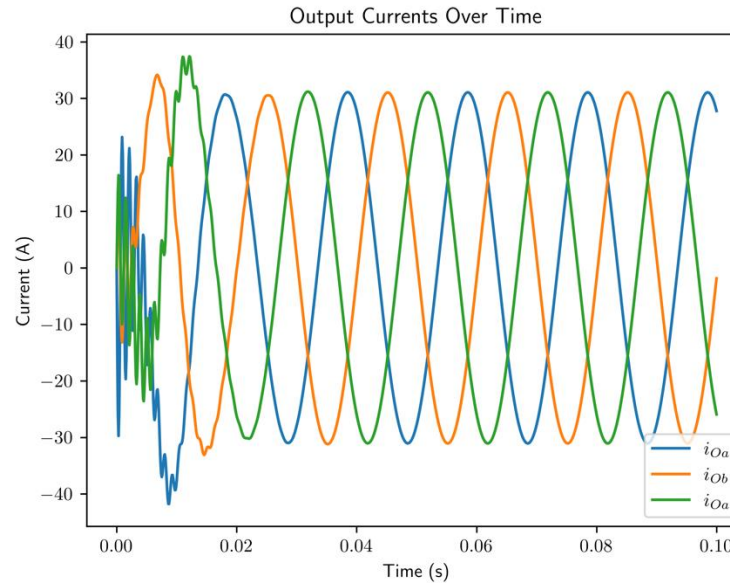
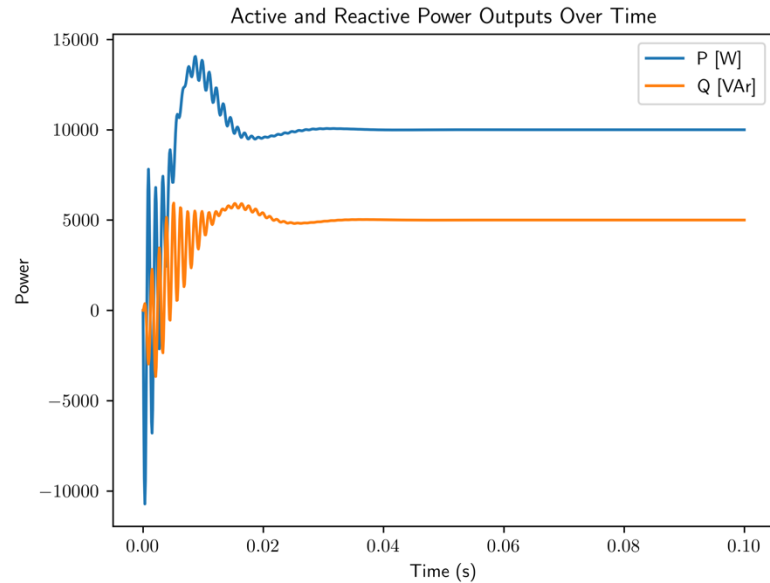
Nonlinear state space model:
 $\dot{\mathbf{x}}(t) = A\mathbf{x}(t) + R(\mathbf{x}, \mathbf{u})$

$$R(\mathbf{x}, \mathbf{u}) = \begin{bmatrix} K_P^{PLL} v_{Oq} \\ v_{Oq} \\ 0 \\ 0 \\ \frac{v_{Od} P^* - v_{Oq} Q^*}{v_{Od}^2 + v_{Oq}^2} \\ \frac{v_{Oq} P^* + v_{Od} Q^*}{v_{Od}^2 + v_{Oq}^2} \\ 0 \\ \frac{1}{L} v_{1d} + \omega i_{Lq} \\ \frac{1}{L} v_{1q} - \omega i_{Ld} \\ \omega v_{Cq} \\ -\omega v_{Cd} \\ -\frac{1}{L_{coupl}} v_{Od} + \omega i_{Oq} \\ -\frac{1}{L_{coupl}} v_{Oq} - \omega i_{Od} \end{bmatrix}$$

Parameter	Value
Nominal phase voltage	240 V
Grid frequency	50 Hz
Coupling impedance R_{coupl}, L_{coupl}	$(0.131 + j0.96) \Omega$
DC bus voltage	1000 V
Coupling filter	
Inductance L	1.35 mH
Capacitance C	50 μ F
Resistance R	0.056 Ω
Ground resistance R_G	100 Ω
Switching frequency ω_c	100 Hz
Reference active power P^*	10 kW
Reference reactive power Q^*	5 kVar
Current controller	
Proportional gain in branch d K_P^d	1
Integral gain in branch d K_I^d	460
Proportional gain in branch q K_P^q	1
Integral gain in branch q K_I^q	460
PLL	
Proportional gain K_P^{PLL}	2.1
Integral gain K_I^{PLL}	5000

Inverter simulations → invPINN challenges

- Poor performance & generalization for invPINN → Why?



- Higher order
- Predicting more states simultaneously
- Stiffer ODEs
- Need more careful parameter tuning to avoid numerical instability

Fast timescales also make training challenging

- Inverter transients settle down in less than 10-20 milliseconds
→ After which output powers track their reference setpoints
- But SG transients take around 100-200 milliseconds to settle down
- Inverter dynamics (smaller electrical time constants) much faster than SG (larger mechanical time constants)
- Under certain conditions and disturbances, inverters can have even faster transients (microseconds)

Next steps

- Improve generalization of sgPINN to diverse inputs & ICs
- Improve overall performance of invPINN
- Implement other types of layers in our PINNs e.g. RNN, LSTM
- Possible extensions for future work
 - Apply PINNs for ODE parameter estimation
 - Larger-scale studies with multiple SGs & IBRs
 - Bayesian PINNs for uncertainty quantification