
**Carbon dioxide capture, transportation
and geological storage — Carbon
dioxide storage using enhanced oil
recovery (CO₂-EOR)**

*Captage, transport et stockage géologique du dioxyde de carbone —
Stockage du dioxyde de carbone au moyen de la récupération assistée
du pétrole (RAP-CO₂)*





COPYRIGHT PROTECTED DOCUMENT

© ISO 2019

All rights reserved. Unless otherwise specified, or required in the context of its implementation, no part of this publication may be reproduced or utilized otherwise in any form or by any means, electronic or mechanical, including photocopying, or posting on the internet or an intranet, without prior written permission. Permission can be requested from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office
CP 401 • Ch. de Blandonnet 8
CH-1214 Vernier, Geneva
Phone: +41 22 749 01 11
Fax: +41 22 749 09 47
Email: copyright@iso.org
Website: www.iso.org

Published in Switzerland

Contents

Page

Foreword	v
Introduction	vi
1 Scope	1
1.1 Applicability	1
1.2 Non-applicability	1
1.3 Standard boundary	1
1.3.1 Inclusions	1
1.3.2 Exclusions	1
2 Normative references	2
3 Terms and definitions	2
4 Documentation	4
4.1 Purpose	4
4.2 Use of existing data	4
4.3 Initial documentation	5
4.4 Periodic documentation	5
5 EOR complex description, qualification, and construction	5
5.1 General	5
5.2 Geological characterization and containment assessment of the EOR complex	6
5.3 Description of the facilities within the CO ₂ -EOR project	6
5.4 Existing wells within the EOR complex	6
5.5 Operations history of the project reservoir	7
6 Containment assurance and monitoring within the EOR complex	7
6.1 Containment assurance and EOR operation management plan	7
6.1.1 EOR operations management plan	7
6.1.2 Initial containment assurance	7
6.1.3 Operational containment assurance	8
6.2 Monitoring program, methods, and implementation	8
6.2.1 Monitoring of potential leakage pathways	8
6.2.2 Monitoring methods	8
6.2.3 Monitoring program implementation	9
7 Well construction	9
7.1 New well construction	9
7.2 Well intervention	9
8 Quantification	10
8.1 General	10
8.2 Quantification principles	10
8.3 Quantification of input [m_{input}]	11
8.4 Quantification of loss	11
8.4.1 Quantification of operational loss [$m_{\text{loss operations}}$]	11
8.4.2 Leakage from facilities	12
8.4.3 Venting and flaring from operations	12
8.4.4 Entrained CO ₂ in products	12
8.4.5 Transfer of CO ₂	12
8.4.6 Loss from EOR complex	12
8.5 Allocation ratio for anthropogenic CO ₂	13
8.6 De minimis losses	13
8.7 Avoidance of double-counting	13
9 Recordkeeping and missing data	13
9.1 Record retention	13
9.2 Missing data procedures	13

10	Project termination	13
10.1	General	13
10.2	Periodic assurance of containment	14
10.3	Termination plan	14
10.4	Requisites for termination	14
10.5	CO ₂ -EOR project termination	14
10.6	Post termination	15
Annex A	(informative) Introduction to CO₂-EOR	16
Annex B	(informative) Example quantification calculation	33
Annex C	(informative) Unit conversion	41
Bibliography		42

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 265, *Carbon dioxide capture, transportation, and geological storage*.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

This is the first edition of the standard entitled: *Carbon dioxide capture, transportation and geological storage — Carbon dioxide storage using enhanced oil recovery (CO₂-EOR)*. The subject matter of this document is a new work product and does not cancel or replace any other documents in whole or in part related to the subject of CO₂-EOR.

Carbon dioxide enhanced oil recovery (CO₂-EOR) is a technique for increasing the recovery of hydrocarbons from an oil field.

The process involves using wells to inject volumes of CO₂ at pressures where the injected CO₂ usually mixes with the oil, changing the properties of the oil and enabling it to flow more freely to production wells. In most cases, a CO₂-EOR project is designed as a closed-loop system whereby some of the injected CO₂ is co-produced with the oil and then separated in above-ground recycling facilities prior to being reinjected into the oil reservoir. CO₂ that is injected into the project reservoir is contained as an inherent element of the injection and production operations, and this document requires that such containment be demonstrated. CO₂ that is injected and remains trapped in the project reservoir (or EOR complex) during and after oil production activities is not released to the atmosphere, and this trapping is referred to as “associated storage”. [Annex A](#) provides a detailed description of the CO₂-EOR process as presently used (and potential “next generation” uses) and the associated storage that occurs as an intrinsic part of those operations. Although methane is often present in EOR project reservoirs, this document does not specifically address methane or other greenhouse gases. The demonstration requirements for safe, long-term containment, however, address assessment of trapping and potential leakage pathways that would likely assure containment of methane as well as CO₂. As detailed in [Annex A](#), CO₂-EOR has been deployed internationally for several decades and has potential to expand. CO₂-EOR is commercially valuable today because it allows for the additional recovery of hydrocarbon resources while simultaneously trapping injected CO₂ for safe, long-term containment as a part of the process.

This document applies to quantifying and documenting the total CO₂ (and optionally the anthropogenic portion of the CO₂) that is stored in association with CO₂-EOR. The document recognizes that CO₂-EOR is principally an oil recovery operation. Associated with this oil recovery, however, safe and long-term CO₂ storage occurs. The absence of an accepted standard for demonstrating the safe, long-term containment of CO₂ in association with CO₂-EOR and documenting the quantity of associated stored CO₂ constitutes one of the barriers to the increased use of anthropogenic CO₂ in CO₂-EOR operations. The purpose of this document is to remove that barrier and thereby facilitate the exchange of goods and services related to the increased use and emissions reductions through associated storage by providing methods for demonstrating the safe, long-term containment of, and determining the quantity of CO₂ stored in association with CO₂-EOR. The document does not address the financial consequences that may or may not result from documenting storage of CO₂ in association with CO₂-EOR operations.

This document does not provide requirements for the selection, characterization or permitting of sites for CO₂-EOR projects because those sites are selected, characterized, and permitted pursuant to requirements and standards applicable to oil and gas exploration and production. Likewise, this document does not specify environment, health and safety protections or corrective action and mitigation requirements that are provided by the regulations and standards applicable to all hydrocarbon production operations. (A list of many of the existing standards applicable to CO₂ injection wells and oil and gas operations is presented in the Bibliography.) This document does provide requirements for demonstrating that the site in question is adequate to provide safe, long-term containment of CO₂, for demonstrating that the CO₂ flood is operated in a way to assure containment of the CO₂ in the EOR complex, and for quantifying associated storage.

This document provides for the quantification of the CO₂ that is stored in association with CO₂-EOR operations. The results of quantifications under this document could be used as input for calculations conducted in accordance with a number of other standards, protocols or programs for the quantification or reporting of greenhouse gas emissions, mitigation, or reductions, including those complying with ISO 14064-1, ISO 14064-2 and ISO 14064-3. Specifically, this document provides for the identification and quantification of CO₂ losses (including fugitive emissions) and quantification of the amount of CO₂

stored in association with CO₂-EOR projects. Such quantification could be used in a broader scheme for the quantification and verification of emissions and emission reductions over the entire carbon capture, transportation and storage chain. Specifically, using this document will provide quantification results that could be used as input to approaches described in ISO/TR 27915 for Quantification & Verification (Q&V). In addition, the quantification of CO₂ stored in association with a CO₂-EOR project pursuant to this document could be combined with the quantifications generated under ISO 27920, Carbon dioxide capture, transportation, and geological storage — Quantification and Verification, which is currently under development. The quantification of the storage associated with a CO₂-EOR project that occurs as part of a CCS project chain could be combined with the quantification of one or more capture, transportation and geological storage systems to produce a total quantification for the entire CCS project chain. Under some emissions quantification and reporting regimes, CO₂ quantities stored in association with CO₂-EOR are either treated as not emitted and excluded from calculations or subtracted as offsets.

Carbon dioxide capture, transportation and geological storage — Carbon dioxide storage using enhanced oil recovery (CO₂-EOR)

1 Scope

1.1 Applicability

This document applies to carbon dioxide (CO₂) that is injected in enhanced recovery operations for oil and other hydrocarbons (CO₂-EOR) for which quantification of CO₂ that is safely stored long-term in association with the CO₂-EOR project is sought. Recognizing that some CO₂-EOR projects use non-anthropogenic CO₂ in combination with anthropogenic CO₂, the document also shows how allocation ratios could be utilized for optional calculations of the anthropogenic portion of the associated stored CO₂ (see [Annex B](#)).

1.2 Non-applicability

This document does not apply to quantification of CO₂ injected into reservoirs where no hydrocarbon production is anticipated or occurring. Storage of CO₂ in geologic formations that do not contain hydrocarbons is covered by ISO 27914 even if located above or below hydrocarbon producing reservoirs. If storage of CO₂ is conducted in a reservoir from which hydrocarbons were previously produced but will no longer be produced in paying or commercial quantities, or where the intent of CO₂ injection is not to enhance hydrocarbon recovery, such storage would also be subject to the requirements of ISO 27914.

1.3 Standard boundary

1.3.1 Inclusions

The conceptual boundary of this document for CO₂ stored in association with CO₂-EOR includes:

- a) safe, long-term containment of CO₂ within the EOR complex;
- b) CO₂ leakage from the EOR complex through leakage pathways; and
- c) on-site CO₂-EOR project loss of CO₂ from wells, equipment or other facilities.

1.3.2 Exclusions

This document does not include the following:

- a) lifecycle emissions, including but not limited to CO₂ emissions from capture or transportation of CO₂, on-site emissions from combustion or power generation, and CO₂ emissions resulting from the combustion of produced hydrocarbons;
- b) storage of CO₂ above ground;
- c) buffer and seasonal storage of CO₂ below ground (similar to natural gas storage);
- d) any technique or product that does not involve injection of CO₂ into the subsurface; and
- e) emissions of any GHGs other than CO₂.

NOTE Some authorities might require other GHG components of the CO₂ stream to be quantified.

2 Normative references

There are no normative references in this document.

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

3.1 anthropogenic carbon dioxide

carbon dioxide that is initially produced as a by-product of a combustion, chemical, or separation process (including separation of hydrocarbon-bearing fluids or gases) where it would otherwise be emitted to the atmosphere (excluding the recycling of non-anthropogenic CO₂)

Note 1 to entry: The chemical symbol “CO₂” is synonymous with “carbon dioxide”. Accordingly, the two ways of writing out “carbon dioxide” and “CO₂” are used interchangeably in this document.

Note 2 to entry: If CO₂ that meets the definition of anthropogenic CO₂ is not included in a supplemental quantification of associated storage of anthropogenic CO₂ (e.g., because it was received and injected by a CO₂-EOR project prior to the quantification period) it will generally be treated as non-anthropogenic CO₂ in that quantification.

3.2 associated storage

CO₂ stored in association with CO₂-EOR (3.4) that occurs as an inherent result of a dedicated hydrocarbon production operation

Note 1 to entry: The requirements of this document are intended to ensure that CO₂ stored in association with a CO₂-EOR operation is stored as effectively as CO₂ stored in a geologic storage operation that complies with ISO 27914.

3.3 authority

competent governmental entity or entities with legal power to regulate or permit CO₂-EOR (3.4), to regulate storage of CO₂ in association with a CO₂-EOR (3.4) operation, or to regulate quantification of the storage of CO₂ in association with a CO₂-EOR (3.4) operation

3.4 CO₂ enhanced oil recovery CO₂-EOR

process designed to produce hydrocarbons from a reservoir using the injection of CO₂

Note 1 to entry: The process of CO₂ enhanced oil recovery is explained in detail in [Annex A](#)

3.5 CO₂ enhanced oil recovery project CO₂-EOR project

EOR complex (3.10), underground equipment, wells, surface or above seabed equipment, activities and rights necessary to an enhanced oil recovery operation, including any necessary or required surface or subsurface rights regulated by the authority

3.6 CO₂ injection well

well used to inject CO₂ into a *project reservoir* (3.19)

3.7**CO₂ stream**

stream consisting overwhelmingly of carbon dioxide

Note 1 to entry: The CO₂ stream typically includes impurities and may include substances added to the stream to improve performance of hydrocarbon recovery operation and/or to facilitate CO₂ detection.

[SOURCE: ISO 27917:2017, 3.2.10, modified — Note revised to added “to improve performance of hydrocarbon recovery operation”.]

3.8**containment**

status of CO₂ being confined within the *EOR complex* (3.10) by an effective *trap* (3.23) or combination of traps

3.9**containment assurance**

demonstration that the features and geologic structure of the *CO₂-EOR project* (3.5) are adequate to provide *safe, long-term* (3.21) *containment* (3.8) of CO₂, and that the CO₂ flood is operated in a way to assure containment of the CO₂ in the *EOR complex* (3.10)

3.10**EOR complex**

project reservoir (3.19), *trap* (3.23), and such additional surrounding volume in the subsurface as defined by the *operator* (3.16) within which injected CO₂ will remain in *safe, long-term* (3.21) *containment* (3.8)

3.11**injection-withdrawal ratio**

ratio, during a defined period, of the volume of all fluids and gases injected into the *project reservoir* (3.19) to the volume of all fluids and gases produced from the project reservoir as determined using consistent temperature and pressure conditions

3.12**leakage**

unintended release of CO₂ to the atmosphere or out of the *EOR complex* (3.10)

[SOURCE: ISO 27917:2017, 3.2.14, modified — Added to the atmosphere or out of the EOR complex.]

3.13**leakage pathway**

geological or artificial conduit for *leakage* (3.12) of CO₂ out of the *EOR complex* (3.10)

3.14**loss**

leakage (3.12), intended releases, and transfers of CO₂ from the *CO₂-EOR project* (3.5)

3.15**native CO₂**

CO₂ present and indigenous within the *project reservoir* (3.19) prior to hydrocarbon production or any CO₂ injection

Note 1 to entry: Native CO₂ is also known as “in situ CO₂”.

3.16**operator**

entity responsible for the *CO₂-EOR project* (3.5)

3.17

plug & abandon

permanently close a well or wellbore to prevent inter-formational movement of fluids into strata, into freshwater aquifers, and out of the well

Note 1 to entry: In most cases, a series of cement plugs is set in the wellbore, with an inflow or integrity test made at each stage to confirm hydraulic isolation.

3.18

post-termination

period of time after *termination* (3.22)

3.19

project reservoir

geologic reservoir in to which CO₂ is injected for production of hydrocarbons in paying or commercial quantities

3.20

quantification period

period of time during which *associated storage* (3.2) is being quantified

3.21

safe, long-term

period necessary for *associated storage* (3.2) to be considered environmentally safe by the system under which the quantification is being implemented

3.22

termination

process beginning with the cessation of quantification of *associated storage* (3.2), and ending with both the termination of hydrocarbon production from the *project reservoir* (3.19), and the plugging & abandonment of wells unless otherwise required by the *authority* (3.3)

3.23

trap

any feature or mechanism that alone or in combination provides *safe, long-term* (3.21) *containment* (3.8) below a low-permeability confining geologic layer (cap rock or seal), including in the pore spaces of the *EOR complex* (3.10) (physical, stratigraphic, or structural trapping), by capillary pressure from the water in the pore spaces between the rock (residual trapping), by dissolution in the in situ formation fluids (solubility), by hydrodynamic trapping, by adsorption onto organic matter or by reacting in geologic formations to produce minerals (geochemical trapping)

4 Documentation

4.1 Purpose

The provisions of this clause are intended to facilitate documentation of the safe, long-term containment, and the quantification of associated storage.

4.2 Use of existing data

Documentation and demonstration requirements throughout this document may be satisfied by information that has already been required, is held, approved by, and available from the authority, because in many cases EOR operations are addressed by existing oil and gas regulations. To the extent that information fully satisfies the requirements, has already been provided and is available from the authority, such information is not required to be developed again for purposes of this document. References to information that is available do not include information held by another entity but not available to the operator.

4.3 Initial documentation

At the beginning of the quantification period, initial documentation shall be prepared and shall include:

- a) a description of the EOR complex and engineered systems (see [Clause 5](#));
- b) the initial containment assurance (see [6.1.2](#));
- c) the monitoring program (see [6.2](#));
- d) the quantification method to be used (see [Clause 8](#) and [Annex B](#)); and
- e) the total mass of previously injected CO₂ within the EOR complex at the start of quantification period (see [8.5](#) and [Annex B](#)).

The initial documentation shall be offered to the authority.

4.4 Periodic documentation

Periodic documentation should be prepared at least annually and shall provide the following information:

- a) the quantity of associated storage in specified units of CO₂ mass, or volumetric units convertible to mass, (see [8.2](#) m_{stored}) during the period covered by the documentation;
- b) the cumulative quantity of associated storage in specified units of CO₂ mass, or volumetric units convertible to mass, (see [8.2](#) m_{stored}) since the beginning of the quantification period;
- c) the formula and data used to quantify the mass of associated storage, including the mass of CO₂ delivered to the CO₂-EOR project and losses during the period covered by the documentation (see [Clause 8](#) and [Annex B](#));
- d) the methods used to estimate missing data and the amounts estimated as described in [9.2](#);
- e) the approach and method for quantification utilized by the operator, including accuracy, precision and uncertainties (see [Clause 8](#) and [Annex B](#));
- f) a statement describing the nature of validation or verification of the statement including the date of review, process, findings, and responsible person or entity; and
- g) source of each CO₂ stream quantified as associated storage (see [8.3](#)).

The periodic documentation shall be offered to the authority.

NOTE The operator can determine that more frequent recordkeeping and documentation are required to meet the goals or requirements of the CO₂-EOR project.

5 EOR complex description, qualification, and construction

5.1 General

A general EOR operations management plan shall be prepared and periodically updated; shall provide a description of the EOR complex and engineered system [see [4.3 a](#)], shall establish that the EOR complex is adequate to provide safe, long-term containment of CO₂ and shall include site-specific and other information pertaining to:

- a) geologic characterization of the EOR complex;
- b) a description of the facilities within the CO₂-EOR project;
- c) a description of all wells and other engineered features in the CO₂-EOR project; and

- d) the operations history of the project reservoir.

5.2 Geological characterization and containment assessment of the EOR complex

The general geologic characterization of the EOR complex shall be based on subsurface and other data collected at the site (augmented where appropriate with data from analogous fields), including any features that may affect safe, long-term containment of CO₂ and evidence of the integrity of the reservoirs and traps. The operator shall define the EOR complex in the geologic description to contain all likely subsurface locations to which the CO₂ could reasonably move beyond the project reservoir. For projects desiring to quantify associated storage, the geological characterization and engineering description shall provide evidence of the integrity of the reservoirs and traps that supports a conclusion that the EOR complex is suitable for safe, long-term containment. The description of the EOR complex should include, but not necessarily be limited to:

- a) general lithologic description of the stratigraphic column above the EOR complex;
- b) depth to the top of the EOR complex;
- c) thickness of the defined stratigraphy within the EOR complex;
- d) structural and geophysical properties;
- e) lateral boundaries and any spill points relevant to containment;
- f) hydraulic/petrophysical/geochemical/geomechanical properties;
- g) associated storage capacity of CO₂ in the project reservoir, recognizing that EOR operations are typically designed for maximum economic hydrocarbon production; and
- h) engineering data as described in [6.1.3](#).

5.3 Description of the facilities within the CO₂-EOR project

The description of the facilities within the CO₂-EOR project shall provide an overview of the equipment, downstream of the CO₂ custody transfer meter, used to handle CO₂ and production, including design specifications. This should typically include piping, separators, processing and dehydration equipment, pumps, compressors, and any other equipment relevant to CO₂ handling and production. It should specifically address vent, release, sampling, and metering points, including a description of metering accuracy and estimation techniques.

5.4 Existing wells within the EOR complex

The description of wells shall identify each well penetrating the EOR complex and shall provide evidence it has been constructed and/or plugged & abandoned in such a manner as to provide safe, long-term containment of CO₂. Such wells include injection, production, monitoring, temporarily abandoned, shut-in, and plugged & abandoned wells. The following information shall be provided where available:

- a) well name;
- b) unique well identifier;
- c) spud and completion dates;
- d) well status (e.g. injection, production, monitoring, temporarily abandoned, shut-in, plugged & abandoned);
- e) surface or seabed location;
- f) total and measured depth;
- g) plugging & abandonment information;

- h) well construction, completion, and well integrity technical details;
- i) significant equipment remaining in the well; and
- j) well intervention details and history.

In some cases, remote sensing methods or field or aerial surveys to locate old wells may be necessary.

5.5 Operations history of the project reservoir

The operations history of the CO₂-EOR complex should include:

- a) production and injection data for the project reservoir;
- b) temperature and pressure history, including current distribution;
- c) interaction with adjacent reservoirs;
- d) any known leakage incidents; and
- e) history of seismic activity.

6 Containment assurance and monitoring within the EOR complex

6.1 Containment assurance and EOR operation management plan

6.1.1 EOR operations management plan

The EOR operations management plan (see [5.1](#)) shall specify the procedures for field management, including:

- a) project data as described in [Clause 5](#), to be used for monitoring and quantification;
- b) engineering controls for injection and production;
- c) periodic assessment of reservoir performance as compared with expected behaviour in accordance with [6.1.3](#);
- d) assessment of containment by geologic features and engineering systems in accordance with [6.1.3](#);
- e) assessment and management of potential leakage pathway risks and monitoring technologies and procedures (see [6.1.3](#)), including definition of detection thresholds, that are sufficient to meet the requirements of [8.6](#);
- f) method of quantification of CO₂ below the detection threshold in accordance with [8.6](#);
- g) corrective measures for potential leakage or unexpected events;
- h) providing data for associated storage quantification; and
- i) developing a termination plan for the CO₂-EOR project that specifies criteria for termination and outlines the termination qualification process sufficient to meet the requirements of [Clause 10](#).

6.1.2 Initial containment assurance

The EOR operations management plan shall provide an initial containment assurance plan to identify and assess potential geologic, engineered, and engineering-affected leakage pathways that might lead to loss of CO₂ from the EOR complex.

6.1.3 Operational containment assurance

The EOR operations management plan shall provide operational containment assurance during the quantification period, based on engineering data encompassing such items as the results of reservoir management practices, including injection-withdrawal ratio monitoring, well integrity monitoring, pressure monitoring, monitoring of CO₂ movement within leakage pathways identified in the initial containment assurance and monitoring of pressure response within the boundary of the EOR complex. The operational containment assurance may include results from other monitoring. These results shall be used in periodically providing evidence of containment, including the supporting rationale.

Containment assurance and reservoir management shall be reviewed, and the EOR operation management plan shall be revised as necessary if changes occur that have the potential to adversely affect containment, which may include:

- a) unexpected changes in project performance that have potential to influence associated storage of CO₂;
- b) addition or abandonment of injection zones;
- c) change to the areal extent of the project reservoir;
- d) addition or abandonment of wells;
- e) anomalous change of injection-withdrawal ratio;
- f) development of reservoirs which are located above or below the project reservoir; or
- g) discovery of CO₂ beyond the boundary of the CO₂-EOR complex.

6.2 Monitoring program, methods, and implementation

6.2.1 Monitoring of potential leakage pathways

The monitoring program shall address the identified inventory of potential leakage pathways from the containment assurance plan [see [6.1.1 e\)](#)] to determine, for each potential leakage pathway, whether it is:

- a) not active and thus excluded from the monitoring program;
- b) not active, but might activate under operation of the CO₂-EOR project and is thus to be addressed by the monitoring program; or
- c) active.

The operator shall conduct the potential leakage pathway assessment in accordance with the EOR operation management plan or as required by the authority. A final leakage pathway assessment shall be conducted prior to project termination.

NOTE It is likely that the monitoring program could require collection of data prior to start of the quantification period and during the operational life of the project (see [5.5](#)).

6.2.2 Monitoring methods

The monitoring program shall describe tools, methods, applicability, and frequency for detecting and quantifying losses (see [8.4](#)). Details of the monitoring program and data assessed (including relevant data prior to the quantification period) shall be provided in the initial documentation (see [4.3](#)), along with the threshold beneath which there would be no detection. The method of quantification for quantities of CO₂ below the detection threshold shall be specified in the EOR operations management plan (see [8.6](#)).

6.2.3 Monitoring program implementation

The monitoring program shall be implemented to address facility and project losses in accordance with the EOR operations management plan (see 6.1) as applied to the inventory of potential leakage pathways (see 6.2.1). The monitoring program shall be reviewed and revised as EOR operational practices are modified.

7 Well construction

7.1 New well construction

A description of the new wells shall provide evidence that they are designed, constructed, and tested to provide safe, long-term containment of CO₂. Well materials, including metals, cements, and elastomers, shall be selected based on their ability to withstand the expected operational environment including the thermomechanical stress of operation and the geochemistry (including CO₂ where present) of the subsurface. At a minimum, wells that penetrate the EOR complex shall be cemented through each cap rock using cement that is suitable for the thermomechanical and geochemical environment for the safe, long-term containment of CO₂. To the extent not provided by other evidence of suitable construction (for example: reference to information that has been provided to the authority during permitting of CO₂-EOR operations), the following information shall be provided:

- a) well name;
- b) unique well identifier;
- c) spud date, completion date;
- d) status (e.g. injection, production, monitoring, temporarily abandoned, shut-in, plugged & abandoned);
- e) surface or seabed location;
- f) total and measured depth;
- g) well construction, completion, and well integrity technical details; and
- h) significant equipment remaining in the well.

7.2 Well intervention

A description of the well modifications shall provide evidence that they are designed, constructed, and tested to provide safe, long-term containment of CO₂. Well materials, including metals, cements, and elastomers, shall be selected based on their ability to withstand the expected operational environment including the thermomechanical stress of operation and the geochemistry (including CO₂ where present) of the subsurface. To the extent not provided by other evidence that the well modifications performed are suitable (for example: reference to information that has been provided to the authority during permitting of well intervention), the following information shall be provided:

- a) well name;
- b) unique well identifier;
- c) intervention type and date;
- d) status after intervention (e.g. injection, production, monitoring, temporarily abandoned, shut-in, plugged & abandoned);
- e) surface or seabed location;
- f) total and measured depth;

- g) plugging and abandonment information (if applicable);
- h) well intervention details; and
- i) significant equipment remaining in the well.

8 Quantification

8.1 General

The quantification of associated storage [m_{stored}] (see 8.2) includes calculation of loss (see 8.4) and shall be conducted as specified in the EOR operations management plan (see 6.1.1) at least annually. All factors and variables defined in Clause 8 shall be quantified and documented.

Data collected from monitoring a CO₂-EOR project can be used in the quantification of associated storage. Any loss of CO₂ in association with a CO₂-EOR project shall be characterized and quantified.

NOTE 1 In some jurisdictions, an authority might require the operator to document information related to project CO₂ emissions such as (a) incremental emissions from the CO₂-EOR project from power or heat generation, (b) electricity and heat which are imported and the carbon intensity of generation of power (direct or average grid carbon intensity, if available), and (c) exported electricity. Such additional information could be included in the periodical documentation and utilized as appropriate for additional quantification procedures but would not change the quantity of anthropogenic CO₂ stored in association with the CO₂-EOR project. ISO/TR 27915 describes several mechanisms/protocols which utilize quantification of such additional CO₂ emissions.

NOTE 2 Some operators could also quantify the anthropogenic portion of m_{stored} . An example quantification calculation for the anthropogenic portion is shown in Annex B.

8.2 Quantification principles

Any method of quantification used by the operator shall follow these quantification principles:

- a) The mass of CO₂ stored in association with CO₂-EOR [m_{stored}] shall be determined by subtracting loss from input [see Formula (1)].
- b) The manner by which associated storage is quantified shall assure completeness and preclude double counting. The CO₂ that is recycled and reinjected into the EOR complex shall not be quantified as associated storage. Loss from the CO₂ recycling facilities shall be quantified.
- c) Native CO₂ produced and captured in the CO₂-EOR project [m_{native}] should be quantified and documented and may be included in m_{input} if approved by the authority (see Note 2).
- d) The operator shall quantify any CO₂ that is subsequently produced from the EOR complex and transferred offsite (see 8.4.5).
- e) Quantification results shall be expressed either in units of mass or in volumetric units convertible to mass.

The method defined by Formula (1) should be used to document the associated storage of the mass of CO₂ [m_{stored}] within a defined period. m_{stored} should be calculated by quantifying the following variables:

$$m_{\text{stored}} = m_{\text{input}} - m_{\text{loss operations}} - m_{\text{loss EOR complex}} \quad (1)$$

- m_{input} ; the total mass of CO₂ m_{received} by the EOR project, approved m_{native} , (see 8.3);
- $m_{\text{loss operations}}$; the total mass of CO₂ loss from project operations (see 8.4.1 to 8.4.5); and
- $m_{\text{loss EOR complex}}$; the total mass of CO₂ loss from the EOR complex (see 8.4.6).

NOTE 1 In some jurisdictions $m_{\text{loss operations}}$ could be considered as fugitive emissions.

NOTE 2 Typically native CO₂ present in the project reservoir prior to starting a CO₂-EOR project is separated from produced hydrocarbons during production and emitted to the atmosphere. When hydrocarbon production progresses to CO₂-EOR and if recycling facilities are installed, the native CO₂ is no longer emitted, but is captured and retained for direct use by the CO₂-EOR project (see Figure 1) and is combined with the CO₂ received from other sources.

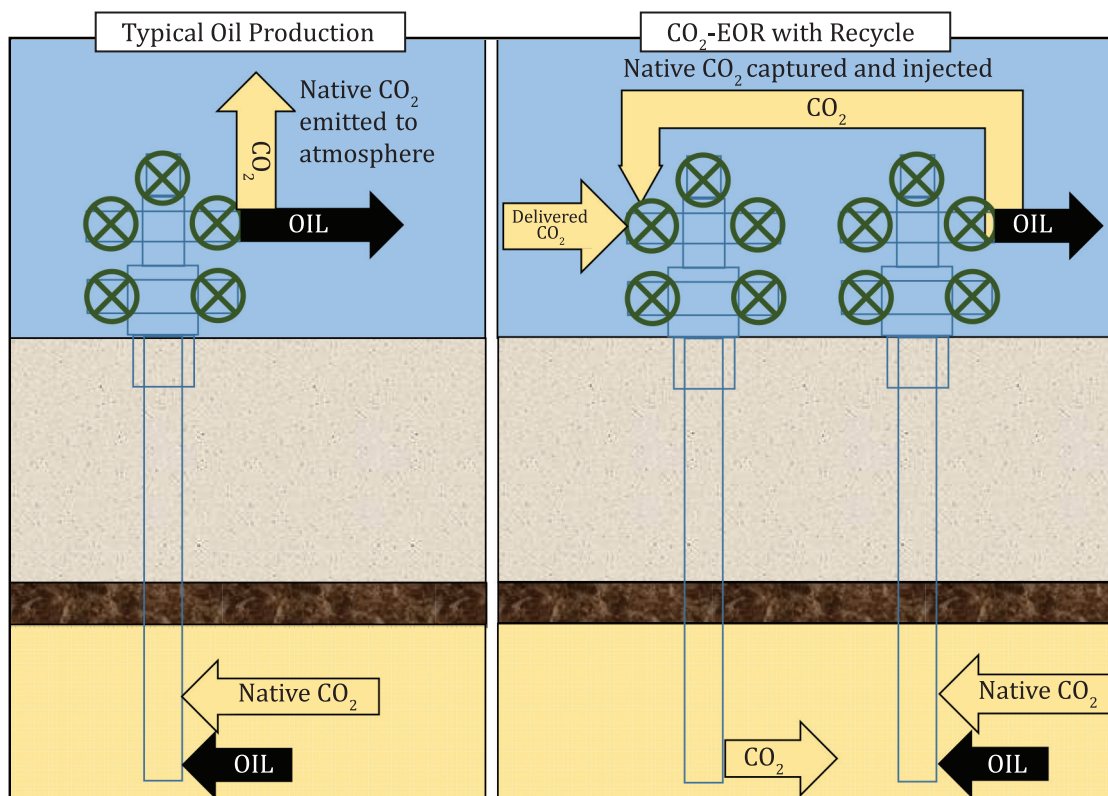


Figure 1 — Illustration of native CO₂, previously being emitted with typical production and now being captured and injected with CO₂-EOR (This diagram is to show movement of native CO₂ only and not meant to demonstrate production of other sources of CO₂)

8.3 Quantification of input [m_{input}]

The total CO₂ received at the custody transfer meter by the EOR project [m_{received}] shall be documented. The CO₂ stream received (including CO₂ transferred from another CO₂-EOR project) shall be metered. The native CO₂ recovered and included as m_{native} shall be documented.

CO₂ delivered to multiple CO₂-EOR projects shall be allocated among those CO₂-EOR projects. This allocation may be accomplished by contract. The sum of the quantities of allocated CO₂ shall not exceed the total quantities of CO₂ received.

NOTE Some operators could also quantify the anthropogenic portion of m_{input} (see 8.5).

8.4 Quantification of loss

8.4.1 Quantification of operational loss [$m_{\text{loss operations}}$]

The operator shall quantify the total mass of CO₂ loss from project operations within a defined period.

The $m_{\text{loss operations}}$ is composed of the following variables:

- Loss of CO₂ due to leakage from production, handling and recycling CO₂-EOR facilities (infrastructure including wellheads) [$m_{\text{loss leakage facilities}}$];

- b) Loss of CO₂ from venting/flaring from production operations [$m_{\text{loss vent/flare}}$];
- c) Loss of CO₂ due to entrainment within produced gas/oil/water when this CO₂ is not separated and reinjected [$m_{\text{loss entrained}}$]; and
- d) Loss of CO₂ due to any transfer of CO₂ outside the CO₂-EOR project [$m_{\text{loss transfer}}$].

$m_{\text{loss operations}}$ may be calculated using [Formula \(2\)](#):

$$m_{\text{loss operations}} = m_{\text{loss leakage facilities}} + m_{\text{loss vent/flare}} + m_{\text{loss entrained}} + m_{\text{loss transfer}} \quad (2)$$

NOTE [Formula \(2\)](#) is evaluated over a period of time in accordance with the documenting periods (see [4.4](#)).

8.4.2 Leakage from facilities

The CO₂ loss from facilities (including wellheads) shall be quantified and documented. The total CO₂ leakage should be measured when possible. Leakage shall be estimated when not measured. The operator shall describe in the initial documentation how the loss is quantified and whether leakage is measured or estimated [$m_{\text{loss leakage facilities}}$].

NOTE Leakage is likely to be extremely small or zero in well managed operations; however, quantification of leakage is required.

8.4.3 Venting and flaring from operations

Venting of gases including CO₂ can be necessary during emergencies, planned maintenance activities or well intervention operations. The vented total mass of CO₂ shall be quantified based on the metered mass (if planned) or estimated mass (if unplanned).

The mass of any CO₂ released through the flare line excluding combustion products, shall be quantified as loss.

The summation of vented or flared loss shall be the mass of total CO₂ vented and flared [$m_{\text{loss vent/flare}}$].

8.4.4 Entrained CO₂ in products

CO₂-EOR produces oil, gas and brine from the project reservoir into which CO₂ is injected. Entrained CO₂ is the mass not completely separated from the produced streams and that exists in solution after the separation of gas and liquid at the surface facilities. The entrained CO₂ is considered a loss when the oil is sold or when the produced water is not reinjected into the reservoir.

The operator shall quantify and document the CO₂ loss by entrainment [$m_{\text{loss entrained}}$].

8.4.5 Transfer of CO₂

Any CO₂ transferred out of the CO₂-EOR project shall be quantified through metering and documented as loss from the project [$m_{\text{loss transfer}}$]. Any CO₂ transferred out of a CO₂-EOR project may be transferred and quantified as associated storage in another CO₂-EOR project or quantified as CO₂ stored in a geological storage project.

NOTE For any CO₂ transferred from one CO₂-EOR project to another CO₂-EOR project, an alternative approach could be to obtain approval of the authority to enlarge the CO₂-EOR project to include both projects, meaning that no transfer or loss of CO₂ would occur.

8.4.6 Loss from EOR complex

The operator shall describe the procedures used to detect and characterize the total CO₂ leakage from the EOR complex. All CO₂ leakage shall be quantified and documented as loss [$m_{\text{loss EOR complex}}$].

8.5 Allocation ratio for anthropogenic CO₂

If only the mass of anthropogenic CO₂ will be considered for m_{stored} , the operator should devise and document an anthropogenic CO₂ allocation ratio for all the terms described in 8.1 to 8.4.6 and these allocation ratios may be utilized as appropriate for additional quantification procedures. These allocation ratios should be documented based on the fraction of the anthropogenic CO₂ of the total CO₂. Annex B presents an example of how such allocation ratios can be used to quantify the anthropogenic portion of CO₂ associated storage (see B.4).

The previously injected volume of CO₂ within the EOR complex at the start of quantification period [$m_{\text{previous injection}}$], which is required to be documented in the initial documentation may be utilized to derive the allocation ratio [see 4.3 e) and Annex B].

For any quantification of the anthropogenic portion of CO₂ associated storage, the allocation ratio should be documented for CO₂ transferred out of a CO₂-EOR project that will be quantified as associated storage in another CO₂-EOR project or quantified as CO₂ stored in a geological storage project.

8.6 De minimis losses

The operator should specify for each monitoring method (i.e. meter type, technology, etc.) the threshold beneath which there would be no detection. For quantification purposes, calculations may use either some fraction of the detection threshold or nil, subject to authority requirements.

8.7 Avoidance of double-counting

The operator shall detail how CO₂ that is produced, captured, recycled and injected in the CO₂-EOR project is quantified and how that quantification assures completeness and precludes double-counting of CO₂.

Transfer of CO₂ from one CO₂-EOR project to another CO₂-EOR project should not be double counted for purposes of quantification in associated storage.

9 Recordkeeping and missing data

9.1 Record retention

Records supporting documentation as described in Clauses 4 to 10 of this document shall be retained for the duration of the operator's involvement in the CO₂-EOR project. Such supporting documentation shall be offered to the authority after termination of the lease/permit pertaining to the CO₂-EOR project.

9.2 Missing data procedures

The operator shall specify the procedures used to estimate monitoring, sampling and testing data for periods during which actual data are unavailable, such as periods of maintenance, equipment failure, or power outages. These procedures should avoid overestimations of the amounts of CO₂ stored.

10 Project termination

10.1 General

This clause provides requirements for the termination and documentation of a CO₂-EOR project that are in addition to the existing permitting, regulatory, and contractual framework that generally define the rules for safe and secure termination of hydrocarbon recovery projects. Compliance shall be demonstrated as part of the termination process through documentation provided to the authority or in the final periodic documentation under 4.4.

10.2 Periodic assurance of containment

If injection of the anthropogenic CO₂ ceases and the CO₂-EOR project continues to operate for hydrocarbon extraction purposes, periodic documentation (see [4.4](#)) shall be provided as defined by the operations management plan or authority until CO₂-EOR project termination is completed.

NOTE CO₂ injection cessation is discussed further in [Annex A](#).

10.3 Termination plan

The operator shall develop a termination plan for the CO₂-EOR project that specifies criteria for termination and documents the termination qualification process. This plan shall be developed to coincide with the initial documentation statement; shall be reviewed regularly; and shall be updated as appropriate during the project operation. The plan should specify:

- a) criteria that confirm compliance with the containment assurance and EOR operations management plan requirements of [Clause 6](#);
- b) the termination process and anticipated timing;
- c) monitoring consistent with requirements of [6.1](#) and [6.2](#);
- d) corrective measures to address potential leakage pursuant to [6.1.1 e\)](#) and g); and
- e) provisional plans for site decommissioning, including plans for plugging & abandonment of wells and decommissioning of facilities as referenced in [5.2](#) and [7.2 g\)](#).

10.4 Requisites for termination

Relying on CO₂ quantification, monitoring and operational information collected within the project, the operator shall satisfy the following requisites to demonstrate proper termination and compile them in the termination documentation:

- a) the absence of detectable leakage (see [6.2](#)) or open conduits to the surface out of the EOR complex, and that the injected CO₂ is, at the time of project termination, safely contained;
- b) compliance with all well decommissioning and plugging requirements for all CO₂-EOR project wells [see [7.2 g\)](#)], that wells do not allow fluid movement out of the EOR complex, and that the CO₂-EOR project wells do not pose a leakage risk;
- c) the injected CO₂ is safely contained with sufficient documentation of the characteristics of the EOR complex and operational history of the CO₂-EOR project to demonstrate long-term stability and predictability of the associated storage;
- d) risks and uncertainties relating to the associated storage of CO₂ were managed throughout the EOR project life; and
- e) facilities and ancillary equipment associated with the CO₂-EOR project have been removed, except those required to be retained by lease or contractual obligations, integral to other operations, or intended for different uses which may be left in place with approval of the authority.

The termination documentation shall describe the location of the injected CO₂. The termination documentation shall be offered to the authorities after termination of the CO₂-EOR project.

10.5 CO₂-EOR project termination

CO₂-EOR project termination is completed when all of the following occur: cessation of CO₂ injection, cessation of hydrocarbon production from the project reservoir, and wells are plugged & abandoned unless otherwise required by the authority.

10.6 Post termination

Assurance of safe, long-term containment shall consider fluid movement to ensure that leakage out of the EOR complex is unlikely. Some jurisdictions might require post-termination monitoring or follow up activities.

NOTE Regulatory requirements for project termination (or closure) and transfers of responsibility exist in some jurisdictions that could apply to CO₂-EOR projects. An example of such requirements is the EU CCS Directive: DIRECTIVE 2009/31/EC OF THE EUROPEAN PARLIAMENT AND OF THE COUNCIL of 23 April 2009 on the geological storage of carbon dioxide and amending Council Directive 85/337/EEC, European Parliament and Council Directives 2000/60/EC, 2001/80/EC, 2004/35/EC, 2006/12/EC, 2008/1/EC and Regulation (EC) No 1013/2006 (See Bibliography).

Annex A (informative)

Introduction to CO₂-EOR

A.1 General

[Annex A](#) provides background information on CO₂ Enhanced Oil Recovery (CO₂-EOR) determined to be relevant to discussion of storage associated with, and incidental to CO₂-EOR, based on current operations. It does not attempt to provide information on how to design and optimize an economic project. Additionally, many of the concepts discussed herein are applicable to other types of hydrocarbon bearing reservoirs.

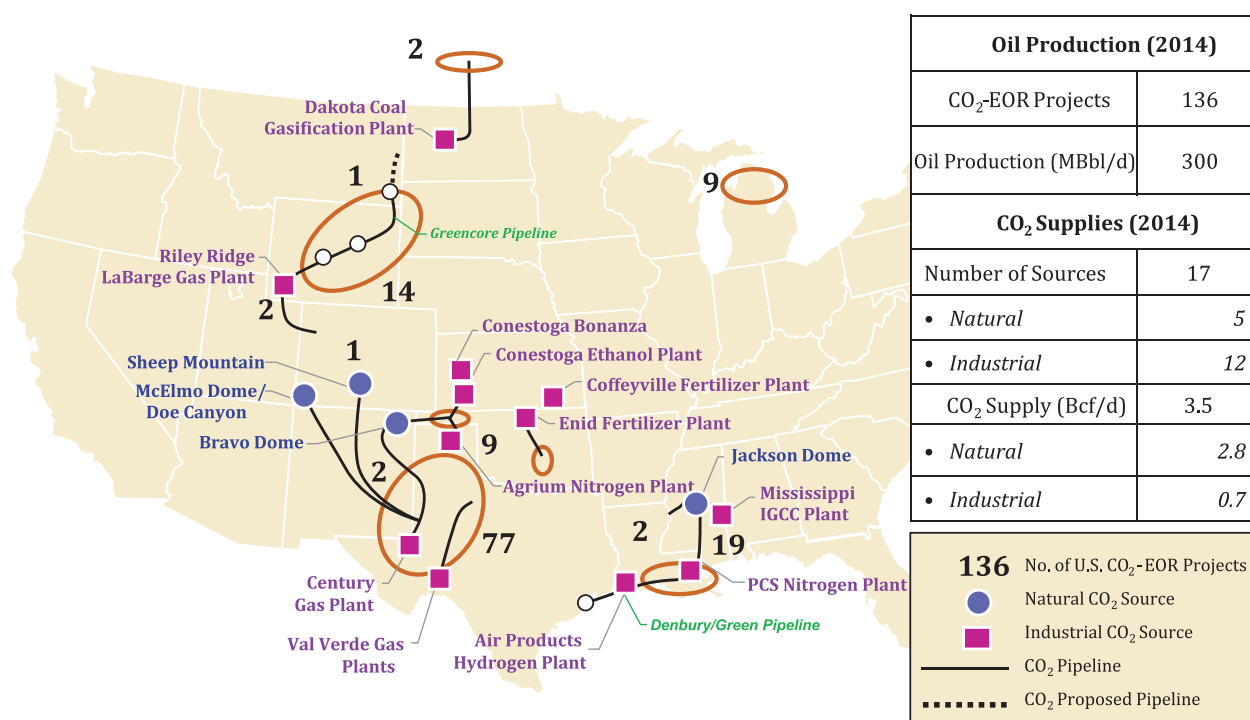
A.2 CO₂-EOR overview

CO₂-EOR is a mature technology. The first documented field trials of CO₂ for EOR were in Oklahoma (U.S.) during 1958. The first successful field CO₂ injection for the purposes of EOR took place beginning in 1964 at the Mead Strawn Field near Abilene, Texas (U.S.) (Holm and O'Brien, 1971). The commercial CO₂ industry began with the first successful large-scale CO₂ flooding in 1972 at the Budafa field (Hungary) and SACROC field in west Texas (US), the latter of which continues today. Initially, the SACROC project was supplied with CO₂ produced from CO₂ native to natural gas fields that was separated and captured from the raw production stream at several southern Permian Basin natural gas plants and transported via pipeline, totalling approximately 300 miles in length, and built specifically for CO₂ transport. Prior to this project, large quantities of CO₂ were being extracted from the natural gas production at these fields and vented to the atmosphere (Holtz, Nance and Finley, 1999). Since this time, CO₂-EOR has seen growth and expansion. It is estimated that by 2012, approximately 600 Mt (million metric tonnes) of CO₂ net of recycle had been injected for CO₂-EOR in the Permian Basin of west Texas. By 2015, an estimated one billion metric tonnes (1 Gt) net of recycle have been injected in the United States (Hill, Hovorka, and Melzer 2012). Approximately 75 to 80 percent of this quantity has come from naturally-occurring sources while the remainder has been captured from anthropogenic sources.

In 2014 (Kuuskraa and Wallace, 2014), there were 136 U.S. CO₂-EOR projects with approximately 7,100 CO₂ injection wells and 10,500 producing wells (see [Figure A.1](#)). Serving these projects are approximately 5,000 miles of CO₂ pipelines. See "Annual Report Mileage" from U.S. Department of Transportation, Pipeline and Hazardous Materials Safety Administration (2015 data). According to a 2011 report of the U.S. National Petroleum Council, approximately 3 BCF (billion cubic feet) per day of CO₂ (57 Mt/y) were injected in the United States for CO₂-EOR, producing about 300,000 bbls of oil per day (over 100 million bbls per year). Since the 1970s, the number of CO₂-EOR projects in the world has continued to grow, nearly doubling in each of the first three decades. In the U.S., the Permian Basin of west Texas has been the most active CO₂-EOR region, with 77 projects producing 200,000 bbl/d in 2014. Following the Permian Basin in that year were the Gulf of Mexico coastal states (50,000 bbls/d), the Rocky Mountains (39,000 bbls/d), and the Midcontinent (including Oklahoma, in particular) (10,000 bbls/d). Other U.S. regions, such as the Michigan Basin, have shown growth as well.

Additionally, there are several CO₂-EOR projects underway in other parts of the world (Kuuskraa and Wallace, 2014). Second to the U.S. in CO₂-EOR is Canada (e.g. Weyburn project, one of the world's largest CO₂-EOR projects is planning CO₂-EOR operations that will result in the associated storage of over 32 Mt of anthropogenic CO₂). There are also projects in China (Jilin, Daqing, Shengli, Jingbian, and others), Brazil (Bahia Oil and Lula oil fields), Saudi Arabia (Ghawar field), Turkey (Bati Raman) and Trinidad (Forest Reserve and Oropuche fields). Significant potential for CO₂-EOR has been reported for many parts of the world.

See [Table A.1](#).



Source: Advanced Resources International, Inc., based on Oil and Gas Journal, 2014 and other sources.

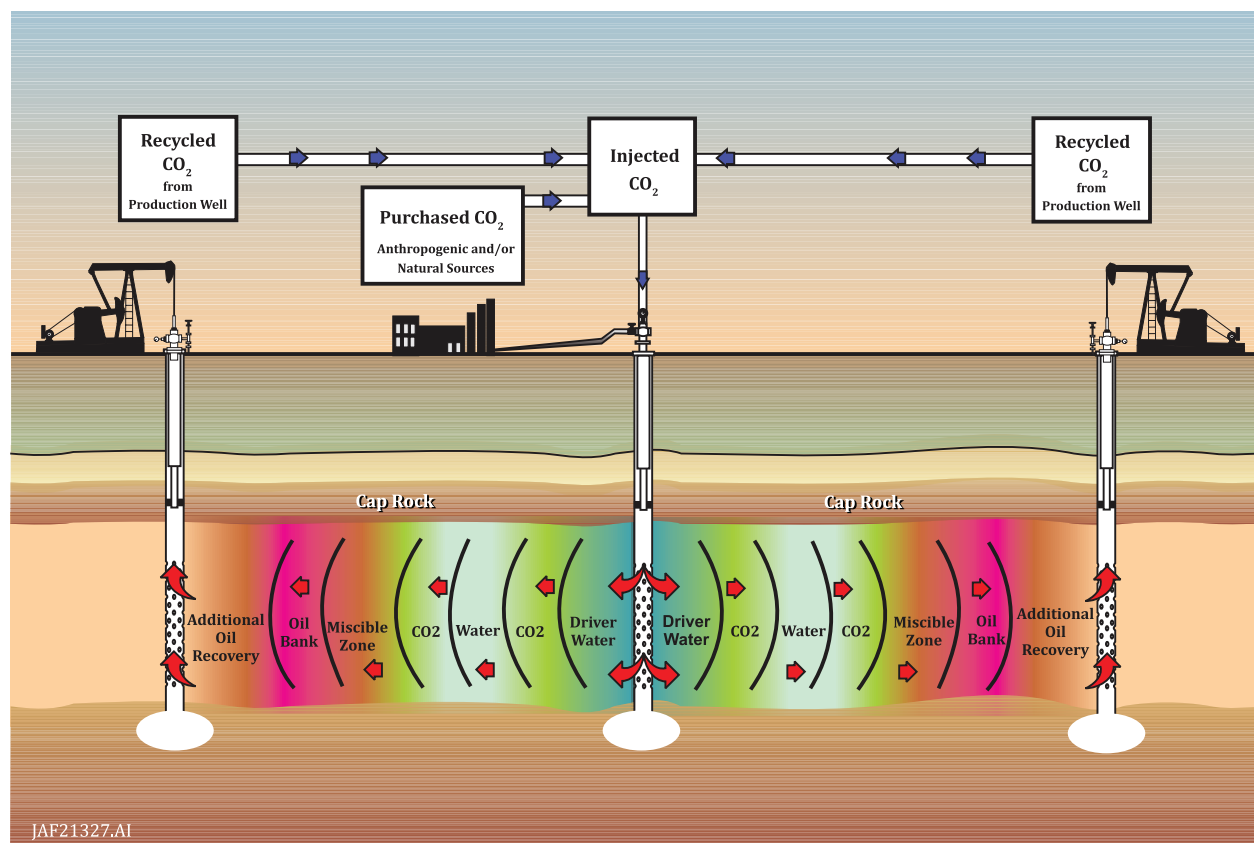
Figure A.1 — CO₂-EOR Operations and CO₂ sources in the U.S. (Kuuskraa and Wallace, 2014)

Table A.1 — International potential for CO₂-EOR and associated CO₂ storage (ARI, 2009)

Region name	CO ₂ -EOR oil recovery (MMBO)	Miscible basin count	CO ₂ /oil ratio (tonnes/bbl)	Potential CO ₂ stored (giga-tonnes)
Asia Pacific	18,376	6	0.27	5.0
Central and South America	31,697	6	0.32	10.1
Europe	16,312	2	0.29	4.7
Former Soviet Union	78,715	6	0.27	21.6
Middle East and North Africa	230,640	11	0.30	70.1
North America (non-US)	18,080	3	0.33	5.9
North America (United States)	60,204	14	0.29	17.2
South Asia	0	0	N/A	0
Sub-Saharan Africa and Antarctica	14,500	2	0.30	4.4
TOTAL	468,524	50	0.30 (weighted average)	139.0

Sources: IEA Greenhouse Gas R&D Programme, *CO₂ Storage in Depleted Oilfields: Global Application Criteria for Carbon Dioxide Enhanced Oil Recovery*, Report IEA/CON/08/155. Prepared by Advanced Resources International, Inc. and Melzer Consulting (August 31, 2009).

The ratio of CO₂ volume injected per barrel of oil produced (and hence the potential demand for CO₂ by CO₂-EOR operations) varies widely over the life of a particular CO₂-EOR project and among such projects. See, e.g. Kuuskraa and Wallace (2014); Bachu (2016) and Azzolina, *et al* (2015).



NOTE Other fields use continuous injection of CO₂. Note that CO₂-EOR is a closed-loop process and the recycling does not allow CO₂ to be released into the atmosphere.

Figure A.2 — Schematic of CO₂-EOR using WAG method (water alternating gas)

A.3 How CO₂-EOR works

In the process of CO₂ flooding (see [Figure A.2](#)), CO₂ is acquired from a CO₂ source and delivered to the oil field, typically by pipeline, and injected into the reservoir. Once injected, the CO₂ contacts and swells the oil in the reservoir. At certain pressure and temperature conditions, the CO₂ becomes miscible (mixing in all phases) with the oil, creating a more mobile oil that is more easily displaced through the reservoir. Oil, CO₂, and brine are then produced to the surface at production wells. This mixture of produced fluids is delivered to a separation plant in which pressure is dropped, and oil, water, and CO₂ and other gases are separated from one another. [Figure A.3](#) illustrates existing facilities in operation in Texas (U.S.). In most operations, the produced CO₂ is dehydrated, compressed, and reinjected within the same oilfield or transported to another nearby oilfield. Oil is sent to market and brine is reinjected for flooding as part of the operation or injected in permitted disposal wells.



Figure A.3 — CO₂ injection well and segment of CO₂ recycle facility

CO₂-EOR is typically developed in phases across a field, with areas of the field organized into sets of injection and production wells known as patterns. CO₂-EOR is usually designed in a closed loop so that atmospheric release of CO₂ is limited (as detailed below in [A.4](#)). In the U.S., for example, any releases of CO₂ (whether natural or anthropogenic) to the atmosphere from the surface facilities are reported to the Environmental Protection Agency (EPA) under the greenhouse gas reporting regulations (40 CFR Part 98 Subpart W). Also, in Canada, where the world's largest depleted oil field CO₂ storage and joint

CO₂-EOR project is located, under Saskatchewan's Oil & Gas Conservation Act, all injected and produced or released volumes of CO₂ are reported to the provincial government.

Injection of CO₂ for EOR is sometimes combined with injection of other fluids. A very common example of this is the "WAG" (water alternating gas) method, where recycled produced brine (or other water) is injected in alternation with CO₂ (see [Figure A.2](#)). This process could improve the vertical distribution of the injected CO₂ in the subsurface (referred to in the industry as "conformance") and/or manage pressure. The net quantity of CO₂ used to produce a barrel of oil is highly project specific, depending on the geology and the CO₂ injection practice used (e.g. WAG versus continuous CO₂ injection). In addition, the ratio varies immensely as a CO₂ flooding project proceeds, since CO₂ injections sometimes proceed for a year or even longer prior to the initial barrel of incremental oil production resulting in a very high initial ratio, diminishing sharply over time as a relatively constant level of CO₂ injection allows for an increase in oil production. Azzolina, et al. (2015), a study of actual experience at a number of projects in the U.S., calculated that the net quantity of CO₂ required per barrel of oil production varied by more than an order of magnitude, with average utilization in the range of 4.8 Mcf to 10.5 Mcf (0.25 tonnes to 0.5 tonnes) of CO₂ per barrel of oil production. Projects using continuous CO₂ injection use roughly twice as much CO₂ per barrel of oil produced as WAG projects.

Operating a CO₂-EOR flood requires both a robust, model-driven plan and considerable monitoring and operational adjustment during the flood. The basic planning and management system is guided by the injection-withdrawal ratio, which also serves to maintain control of the subsurface pressures. At the beginning of the flood, injection operations dominate the pressure behaviour; however, fluid withdrawal is generally brought into balance so that reservoir pressure is maintained at the designed and permitted optimum pressure at the injection wells and across the flood patterns. The ratio during a defined period of the volume of fluid and gas injections to the volume of fluids and gases produced from the reservoir is known as the "injection withdrawal ratio" (IWR).

The production response to CO₂ injection is monitored by periodic production sampling of the fluids at test facilities, where oil, water, and gas are separated and measured. Generally, testing at production facilities is conducted at a rate of one well per day and is rotated among wells so that, at many fields, each production well is tested monthly. Produced CO₂ quantities are monitored to allow the field operator to make adjustments to the flood, particularly in the case of WAG CO₂-EOR floods, to optimize the use of the CO₂ and maximize the oil production, while minimizing cost of handling excessive volumes of produced CO₂. This intensive field observation means that a substantial quantity of data is collected and used to update the operational plan and provide knowledge of the subsurface CO₂ movement for monitoring, verification and accounting (MVA) purposes and/or reporting purposes.

A.4 Associated storage of CO₂ in CO₂-EOR operations

The purpose of CO₂-EOR operations is to recover oil, and this purpose dominates the operation, including (in the U.S.) permitting, and mineral and property leasing.

However, as a natural part of CO₂-EOR operations, as well as by commercial necessity and regulation, CO₂ is effectively stored in the subsurface and securely isolated from the atmosphere, underground sources of drinking water, and other subsurface resources. This retention of CO₂ in the reservoir has been termed an "intrinsic part" of a CO₂-EOR operation (Whittaker and Perkins 2013) in which CO₂ is "inherently stored" (Carbon Sequestration Leadership Forum, Task Force on Technical Challenges in the Conversion of CO₂-EOR Projects to CO₂ Storage Projects, September 2013). This *associated storage* (sometimes termed in the literature "incidental storage") serves a valuable function in offtake agreements with sources that capture and want to confirm associated storage of CO₂. This "associated" storage of CO₂ that occurs during CO₂-EOR operations has been recognized by expert studies from around the world (Carbon Sequestration Leadership Forum, 2013; Whittaker and Perkins, 2013; Kuuskraa, et. al., 2012; and Melzer, 2012).

While CO₂ separation from the oil in the production stream is a necessary part of oil production, the process of CO₂ recycling is a very important, but not mandatory, part of a CO₂-EOR project. Recycling of the separated CO₂ is done to minimize the cost of additional CO₂ purchases. Discussion of this element has created confusion between CO₂-EOR project designers, CO₂-EOR carbon offset protocols, and geologic storage accounting systems. It is important to note that recycle is a closed loop system

in which essentially all the CO₂ produced is separated and reinjected a short time later. Inventory of the recycle system could be conducted using the same approaches used for other industrial processes, with quantification of and accounting for fugitive emissions and venting or flaring. In a GHG accounting system, energy connected to other operations related to extraction, separation, and injection such as pumping, heating, and compression could also need to be included.

It is important to correctly account for recycle, and confusion has occurred because the description of recycle depends on the purpose of the description. In a GHG accounting framework, the difference between mass extracted and mass reinjected could be inferred to equal emissions to the atmosphere. In contrast, from the oil production standpoint, where most previous work has been focused, the most important metric is the total mass of CO₂ injected (newly acquired CO₂ plus recycle), in terms of how much of the pore volume of the rock is contacted per unit of time to contact and mobilize oil. In this case, the ability to re-inject large volumes of CO₂ that have previously been injected, produced and captured could be an advantage. Additional quantities of “make up” CO₂ will need to be acquired to operate a mature field because a significant fraction of injected CO₂ becomes trapped in place and is physically unrecoverable. Modelling and core plug studies illuminate the trapping that occurs; it includes CO₂ trapped by capillary processes and in dead end pores, dissolved in immobile oil, dissolved in brine, or moved into “attic” areas and outside of the active flow paths. Some discussions of CO₂-EOR operations characterize only this non-recyclable CO₂ as “stored” (e.g., Whittaker and Perkins, 2013). However others follow the same approach as is used in accounting for saline formation storage projects, where all forms of effective trapping in the reservoir are counted as stored (including CO₂ trapped as a mobile phase beneath the confining system).

In accounting for the associated stored CO₂: (1) recycled and reinjected volumes are counted a single time, which is to say that no matter how many times the same molecule is injected and produced, it is counted as only one molecule stored; and (2) recycled CO₂ retained within a closed loop is not mistakenly counted as a loss from storage. Quantification of recycled CO₂ could be difficult if mixed gasses (CO₂ plus light hydrocarbons and other gases) are metered. The volume-to-mass conversions are complex for mixed gasses and could lead to measurement errors. Since repeated measurement of the large volumes extracted, separated and reinjected during the recycle process could lead to an accumulation of potentially large errors, the direct measurement of losses from the system would be more accurate.

Losses from venting and fugitive emissions have been published in a few cases and amount to a few percent or less of the originally injected CO₂ (i.e. net of recycle). For example, an assessment by Kinder Morgan of its large volume CO₂-EOR operation at the SACROC oilfield indicates that vented and fugitive emissions were less than 0,875 percent of the total CO₂ injected (net of recycle) (Fox, 2009). Occidental Petroleum has stated that experience at its Denver Unit (a very large field) indicates that about 0.3 percent of the original purchased volume is lost from fugitive and operating emissions (Docket Number 08-AFC-8A). This is consistent with the operator’s desire to conserve and re-use as much of the CO₂ commodity as possible.

A.5 Potential advantages of associated storage of CO₂ in EOR operations

In general, CO₂-EOR is undertaken in pre-existing mature oilfields (sometimes referred to as brownfields), in communities that are already accustomed to oil and gas drilling and production operations. As a result of the prior oil production via primary and/or water injection, CO₂-EOR sites also provide a known geologic reservoir, with known injectivity and capacity, a demonstrated seal and could include pre-existing roads, well pads, and other access infrastructure, and oil and water handling infrastructure. The storage potential for oil fields is further indicated as the hydrocarbons have been securely trapped within the producing reservoirs, indicating that the primary seal is likely to be effective. The trapping potential is also demonstrated by in-situ retention of the CO₂. Existing reservoir production and surveillance knowledge contributes to improved geologic understanding.

Pressure management is a routine component of CO₂-EOR. CO₂ management is also a routine part of every CO₂-EOR operation with injection and production, and many recycle CO₂ in a closed loop system. Development of monitoring, reporting and verification (MRV) will be easier because of the monitoring and management already conducted, but it will be more difficult to observe CO₂ fluid behaviour because

of the presence of hydrocarbon gases. The subsurface is well characterized because of the presence of many existing wells, but the number of wells also poses a challenge because some of the wells could be in unacceptable condition. It could be expensive to remedy the wells; operators will need to identify and re-enter wells to plug or repair them prior to CO₂-EOR operations. The areal extent necessary to contain a given quantity of CO₂ is relatively small (due to more efficient use of pore space including CO₂ replacing produced fluids). (See, e.g. [Figure A.4](#)). The existing legal framework under oil and gas law and regulation will simplify ownership issues in some locations, yet leases held by oil production typically expire at the end of oil recovery operations. Oil and gas production provide revenues that could serve to offset CO₂ capture costs.

[Table A.2](#) provides a comparison of some aspects of CO₂-EOR operations and geologic storage of carbon dioxide in saline formations.

Table A.2 — Comparison of CO₂-EOR and saline storage
(adapted from Hill, Hovorka, and Melzer 2012)

Type	Storage only — Saline formations	Storage only — Non-producing depleted oil or gas fields	CO ₂ -EOR with associated storage
Land	Greenfield	Brownfield — already impacted by oil industry operations	Brownfield — already impacted by oil industry operations
CO₂ management	CO ₂ injection	CO ₂ injection	CO ₂ injection, production, many have recycle in closed loop system
Geographic availability (i.e. relative proximity to CO₂ sources)	Relatively widely distributed geographically with relative- ly high proximity to major CO ₂ sources	Relatively limited due to geo- graphic distribution of hydro- carbon-bearing formations	Significantly limited to the subset of hydrocar- bon-bearing formations that are technically and commercially amenable to CO ₂ -EOR operations
Worldwide CO₂ storage potential	Very great (individual coun- try estimates range from tens to hundreds to >1,000's of gigatonnes of potential storage capacity) (Consoli et Wildgust 2016)	Medium (perhaps as much as 1,000 gigatonnes (IEAGHG 2000))	Modest (roughly on the order of ~120 gigatonnes to 140 gigatonnes or more) (IEAGHG 2009)
Pressure build-up risk	Potential for pressure increase; pressure manage- ment may be needed	Often depleted; pressure management may not be needed but phase behaviour may need management	Pressure management is routine component of CO ₂ - EOR
CO₂ trapping	Trapping demonstrated in pilot projects	Demonstrated mechanisms	Demonstrated trapping by in-situ retention of the CO ₂
Density of poten- tial leakage path- ways from existing wellbores	Low density of existing wellbores, since tend to be “greenfield” development sites	High density of existing well- bores due to prior hydrocar- bon recovery operations	High density of existing wellbores due to both prior hydrocarbon recovery operations and newly con- structed injection wells
Solubility of CO₂ in formation fluid	CO ₂ weakly soluble in forma- tion brine	CO ₂ weakly soluble in for- mation brine and residual hydrocarbon phases	High solubility of CO ₂ in oil if miscible, particularly under higher pressures; weakly soluble in formation brine
Subsurface infor- mation density	Few wells: if any, sparse information	Subsurface well character- ized	Many wells: subsurface well known and characterized in detail

Table A.2 (continued)

Type	Storage only — Saline formations	Storage only — Non-producing depleted oil or gas fields	CO ₂ -EOR with associated storage
Mechanical integrity/risk of well failure	Few wells, recently drilled, cased and cemented; may have legacy wells from other subsurface activities, some of which might require careful assessment and remediation	More wells anticipated, may need work to convert to CO ₂ injectors; some older wells may be in unacceptable condition	Many existing wells, including older wells some of which may be in unacceptable condition. Expense to remedy: identify, and re-enter to plug/repair prior to CO ₂ -EOR operations. Easier to show containment.
Access to surface and subsurface (including pore space)	Variable by jurisdiction; evolving	Variable by jurisdiction; evolving	Existing legal framework defined under oil and gas law and regulation; leases held by oil production and expire at the end of oil recovery operations
Revenues to offset CO₂ capture cost	Variable by jurisdiction; evolving	Variable by jurisdiction, evolving	Yes
Monitoring, reporting and verification, (MRV)	MRV is based on comprehensive geologic study and may cover large area	MRV is based on comprehensive geologic study and may cover large area	Existing reservoir production and monitoring knowledge contributes to improved geologic understanding and development of MRV; integrity of existing wells in the field a principal leakage concern; difficult to observe CO ₂ fluid behaviour; pressure maintenance reduces MRV 'footprint'
Public acceptance	On-shore has had some challenges in areas without oil and gas production, off-shore likely to be good (positive public response to existing storage operations)	Likely to be good. Public generally familiar/comfortable with oil production	Likely to be good. Public generally familiar/comfortable with oil production; communities benefit from royalty payments; severance taxes; income from oil sales, etc. Siting or policy concerns in some areas
Areal extent required to contain a given quantity of CO₂	Depending on storage management strategy. If no pressure maintenance planned area may be relatively large.	The area is comparable to original HC extent: may be comparable to CO ₂ -EOR operations.	Relatively small (due to more efficient use of pore space including CO ₂ replacing produced fluids). (See, e.g. Figure A.4.)

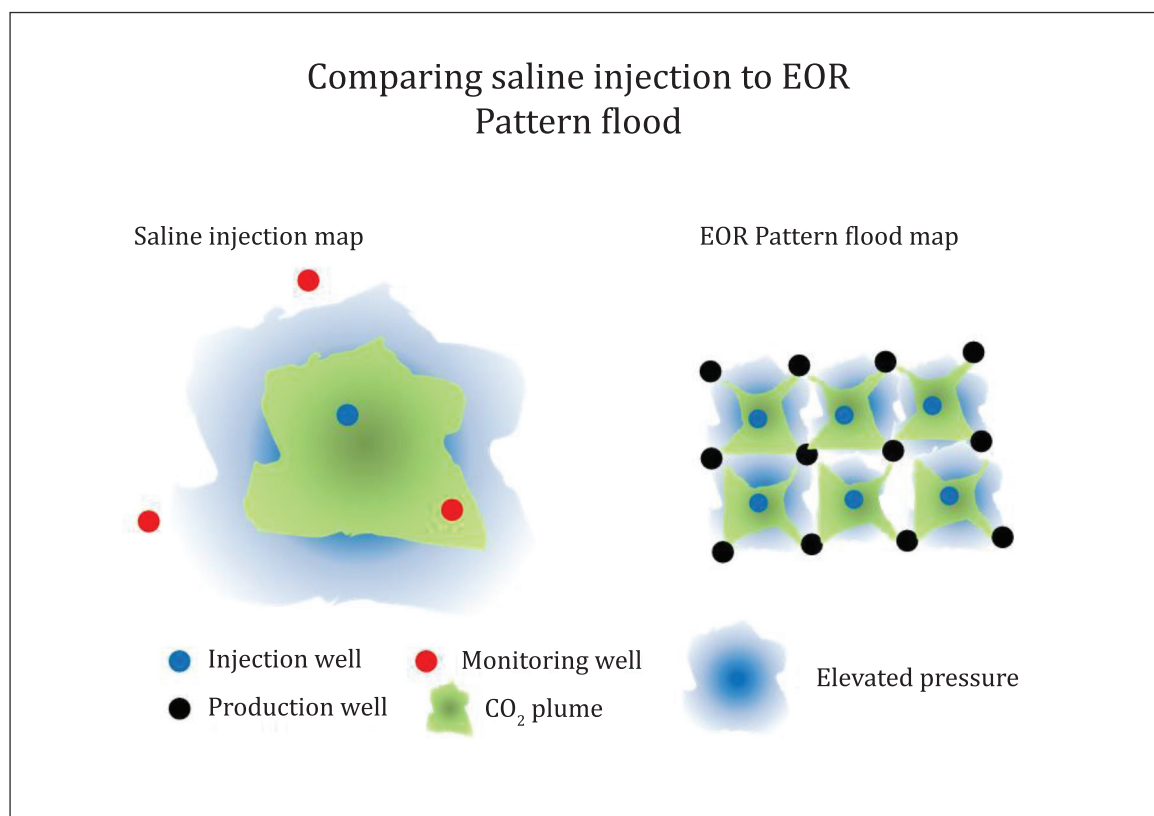


Figure A.4 — In CO₂-EOR, the CO₂ (green) is carefully controlled by production wells during injection and production operations

A.6 Possible challenges for associated storage during CO₂-EOR operations

There are also several aspects of CO₂-EOR operations to be considered with respect to providing assurance that CO₂ will be retained in the injection zone.

A.6.1 Inventory and assessment of existing wells

Poorly plugged or damaged wells penetrating targeted formations could become pathways for injected CO₂ to leak into other formations (including overlying formations that could contain underground sources of drinking water) or into the soil or to the atmosphere. CO₂-EOR operations are typically conducted in previously producing oil fields which could contain large numbers of pre-existing wells, which could have been drilled many decades before. Some of these older wells could not have been identified in the relevant records; others could have been improperly plugged or suffered damage. Some of these existing wells could develop well integrity flaws or could have been degraded during prior primary or secondary production operations. Flaws in well construction could lead to micro-annuli or damage to the cement seal during past production operations. The objective is to identify all wells penetrating the reservoir seal and, if necessary, to remediate them prior to CO₂ injection activities. Although rare, wellbore leakage is an issue of concern for injection projects, both in oilfield and waste disposal context. A considerable body of academic research in recent years has examined CO₂ leakage through well cements (e.g., Bachu and Bennion, 2009; Huerta, 2009; Carey and others, 2010) as well as U.S. State experience with older wells (including orphaned well programs). Management of the risk could be conducted in three steps: characterization, pre-injection remediation, and during EOR and possibly post-injection operations. CO₂-EOR projects also make substantive investments in well monitoring and maintenance. Corrosion-management programs such as the introduction of corrosion-inhibiting chemicals or cathodic protection are common. Field technicians make regular rounds to inspect well and pipeline infrastructure, and monitoring results are being increasingly reported to supervisory

control and data acquisition (SCADA) systems, which allow the whole system to be monitored from a central location.

A.6.2 Review of sealing formations

Sites are reviewed for possible geomechanical damage to the sealing formation during strong pressure depletion or water injection if significantly above the initial pressure. The mechanical integrity of the reservoir seal is assessed for damage during injection as a part of selection of robust CO₂ storage sites.

A.6.3 CO₂ movement out of CO₂-EOR project acreage

CO₂ containment is inherently demonstrable. It is important for operators to plan for the CO₂-EOR project to encompass the entire surface and subsurface area under which the injected CO₂ could move beyond the EOR complex. Significant commercial and legal issues would arise in certain jurisdictions if injected gas or fluids move outside of the owned, leased, or permitted if publicly owned acreage and interfere with adjacent mineral owners, and CO₂ is not exempt from these concerns. For example, natural gas storage operators ensure that natural gas injected for storage remains in the storage formation — and does not migrate under adjacent land where it could be produced through a well on that property and sold. Similarly, operators injecting water in waterflood operations seek to ensure that the injected water does not interfere with or damage oil or gas recovery operations from adjacent property. Over the last century, oil and gas regulators and courts (and legislatures) have developed a vast body of law, regulation and precedent that addresses a host of variations on these types of issues. Hence, CO₂-EOR operators are keenly aware of this concern and plan and design operations to avoid incurring these costs as well as the loss of a valuable CO₂ commodity.

A.6.4 Re-use of injected CO₂ in other portions of a field or other EOR projects

Another issue that has been of concern to stakeholders is the potential for subsequent withdrawal of CO₂ that had previously been injected. For example, the infrastructure such as production wells and pipelines would allow transfer of CO₂ from one part of the reservoir to another. Increasing injection in some patterns could be accomplished by increasing withdrawal in less productive patterns. Pressure could also be decreased. Alternatively, when a WAG flood is employed, the ratio could be changed to all water resulting in more CO₂ being removed than injected. The same processes could theoretically be used to transfer CO₂ that was injected into one field by placing it back in the pipeline and sending it to another field, in effect in another part of the CO₂-EOR closed loop system. Such between-field recycling will, however, require attention to accounting to avoid double-counting any such transfers.

A.7 “In-situ” or “native” CO₂

There are many oil and gas fields that contain CO₂ that is found in-situ (also referred to as “native” CO₂), that is, contained within the hydrocarbon reservoir at discovery. This type of occurrence is common in the Southwest U.S., in Southeast Asia, and in the Middle East. As such fields are developed through primary production and then by applying secondary production techniques (e.g. waterflooding), any native CO₂ that is produced is typically vented to the atmosphere through routine production and separation processes. However, in oil projects where CO₂-EOR techniques are applied and CO₂ recycling is introduced, this native CO₂ will be captured rather than vented, as would otherwise occur. The portion of the captured CO₂ that was initially native to the reservoir becomes anthropogenic in such a case because absent the intervention of the man-made and installed capture equipment, the CO₂ would have been emitted to the atmosphere. As an analogue, it is noted that capture of CO₂ inherently existing within natural gas fields occurs at Sleipner, Snøvit, Molve, Penon, Gorgon, and Shute Creek Fields. The CO₂ that is captured at these fields is anthropogenic CO₂ since it is co-produced and would otherwise be vented to the atmosphere. The CO₂ content of separator gas at pre-CO₂ injection oil fields varies but is generally in the range of 0 % to 30 %. CO₂ re-cycling facilities have been built to capture these native CO₂ molecules which would otherwise be emitted to the atmosphere.

An example calculation of how the quantification of native CO₂ may be carried out is presented in [Annex B](#) (see [B.4.1](#)). The method utilizes the content of “native CO₂” volume per volume of oil produced, which would be determined by the operator and if necessary be agreed to by the authority. This content

could take into account the native CO₂ content at the initial condition and modified appropriately if the reservoir pressure has fallen below the bubble point. Various approaches, including numerical simulation, could be utilized to derive the appropriate content value.

A.8 Offshore CO₂-EOR

Use of CO₂ in offshore, sub-seafloor reservoirs for EOR is widely thought to be technically feasible (e.g., Alekemode, 1995; Tzimas and others, 2005; Holloway and others, 2006; Manrique and others, 2010). Despite nearly a half century of technological maturity onshore, only a few offshore projects have tested or employed CO₂-EOR. While the production mechanisms are principally the same in both settings, offshore CO₂-EOR poses additional challenges since the operations are conducted from a platform, creating both technical and financial hurdles. A list of the advantages and disadvantages of offshore CO₂-EOR is shown in [Table A.3](#).

Table A.3 — Advantages and disadvantages of offshore CO₂-EOR

Advantages	Disadvantages
Federal/State owned leases make production and CO ₂ storage less complex (in the U.S. avoids unitization of private mineral rights)	High capital cost (long pipelines, separation facilities, drilling wells)
Large fields have higher upside	Well placement challenges & subsea completions; Wide well spacing, wells expensive to drill
New fields could be designed for future EOR more cost effectively	O&M more costly
	High conventional recoveries means smaller EOR targets
	Retrofitting wells & facilities with corrosion resistant materials

A.9 Residual oil zones could be produced by CO₂-EOR methods

An oil-bearing zone where natural processes have resulted in water displacement and/or the opening of a spill point to greatly reduce the oil in place (typically 20 % to 40 % of original pore volume) is known as a residual oil zone (ROZ). Often, these saturations are too low to allow oil production under primary depletion methods or by waterflood. ROZs are commonly recognized as largely unexploited oil accumulations that could exist below the original oil-water contact as well as in areas that were completely swept to a residual hydrocarbon saturation and would have no primary production potential (see [Figure A.5](#)). A ROZ could exist if certain tectonic or deformation occurs after a hydrocarbon trap develops. ROZs are distinct from capillary transition zones found below many oil reservoirs because they deviate from the imbibition profile and are economically important because they could be relatively thick. ROZs were initially described in the Texas Permian Basin but are now being found and described in other regions of the world. Recognition of ROZ potential adds to the traditional post-waterflood pay horizons targets for CO₂-EOR. The significance of these ROZs for CO₂-EOR and for the associated storage of CO₂ is that they have the potential to boost CO₂ demand significantly beyond current volumes of CO₂ supply and thereby offer an additional geologic storage option for anthropogenic CO₂ that is captured for emissions reduction purposes.

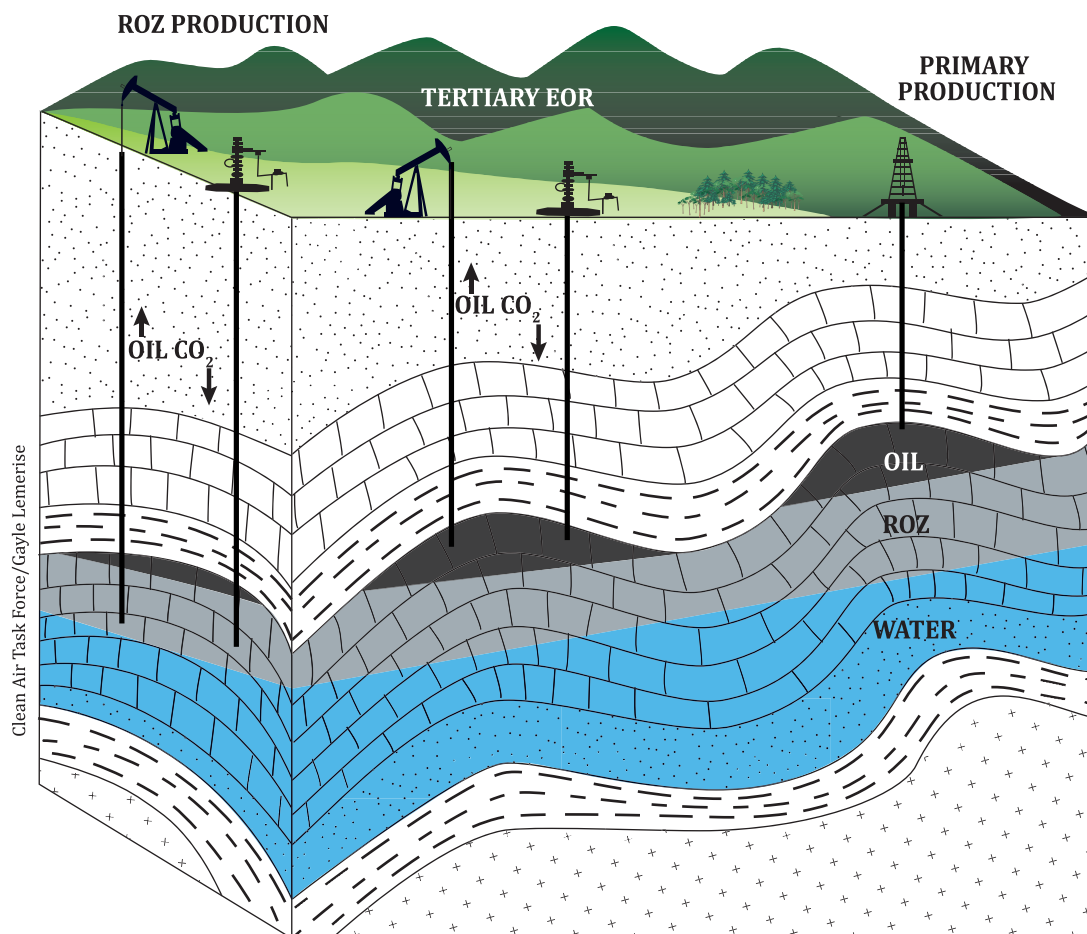


Figure A.5 — ROZ Schematic. Where present, the residual oil zone is a naturally waterflooded zone below the main pay zone that could be produced by miscible CO₂-EOR methods (Hill, Hovorka, Melzer, 2013)

A.10 Adaptation of existing CO₂-EOR subsurface characterization, planning and monitoring activities for associated storage during CO₂-EOR

A number of operational characteristics for CO₂-EOR are different from those of a saline formation storage project (see [Table A.2](#)). Therefore, the spectrum of monitoring activities selected to document associated storage during CO₂-EOR will not be the same as in a non-EOR context. In particular, the data from CO₂-EOR monitoring for commercial purposes would be available as well as data and information describing the geology, characterizing the reservoir and seal, and depicting the historical reservoir and well performance during active oil injection/production. The same objectives are met with this CO₂-EOR data as those initially required or recommended for saline sites.

Documenting associated storage during EOR operations will rely on

- a) data relevant to containment that is extracted from proprietary data to justify the purchase volume of CO₂, design of flood, and for CO₂-EOR operations optimization, and
- b) additional data collection targeted to the areas where uncertainties exist.

Data generated during the commercial design of the CO₂-EOR flood provides much of the same information developed during characterization and initial operation of a saline storage project, and this data is valuable for documenting associated storage. There are numerous CO₂-EOR operations that include additional monitoring to test methods for documenting associated storage in the U.S. and Canada, as summarized in [Table A.4](#). A principal advantage of CO₂-EOR is the wealth of existing

information and data that could be mined to demonstrate knowledge of the subsurface and the CO₂ movement/containment. This means that MVA programs designed to work within the context of the specific field are intrinsically different than for a saline site. When techniques for confirming associated storage are considered alongside data collection used for field development and operational activities, a high standard of assurance, possibly at relatively low additional costs, is expected at a CO₂-EOR site compared to a saline storage-only site. Moreover, any additional monitoring could lead to increased oil recovery and improved CO₂ utilization.

Some limitation in monitoring could be more common or severe in hydrocarbon fields where CO₂-EOR is deployable. For example, seismic surveys would be of more limited utility in areas where natural gas remains in the reservoir or overburden. Similarly, biodegradation of natural or man-made hydrocarbon in near surface geologic formations could lead to false indication of CO₂ beyond containment or completely “mask” the presence of CO₂ out of containment. Pressure and fluid chemistry perturbations could induce long-lived transients, rendering some monitoring tools of limited use.

Table A.4 — CO₂-EOR fields with monitoring programs designed to provide additional information about storage (Hill, Hovorka, and Melzer 2012)

Field name	Location	Operator	Monitoring lead	Flood start date	Web resource
Weyburn	Saskatchewan, Canada	Cenovus, Apache	Petroleum Technology Research Centre	2000	http://ptrc.ca/+pub/document/Summary_Report_2000_2004.pdf
SACROC	Scurry County, Texas	Kinder Morgan	Bureau of Economic Geology, Southwest RCSP	1972	http://www.netl.doe.gov/.../10-SWP_SACROC_EOR_Sequestration_Oil.pdf
Zama	Alberta, Canada	Apache Canada	Energy & Environmental Research Center, PCOR RCSP	2006	http://www.netl.doe.gov/.../7-PCOR_Zama_Field_Validation.Oil.pdf
Cranfield	Adams County, Mississippi	Denbury Onshore LLC	Bureau of Economic Geology, SECARB RCSP	2008	http://www.secarbon.org/files/early-test.pdf
Hastings	Alvin, Texas	Denbury Onshore LLC	Bureau of Economic Geology, Denbury	2001	Hovorka; unpublished
Farnsworth	Farnsworth, Texas,	Tabula Rasa Energy LLC	Southwest Regional Partnership on Carbon Sequestration	2010	https://www.southwestcarbonpartnership.org/
Bell Creek	Montana	Denbury Onshore LLC	Energy & Environmental Research Center, PCOR RCSP	2012	https://www.undeerc.org/pcor/CO2sequestrationprojects/BellCreekDemonstration.aspx

References on monitoring tools and practices are found in Bibliography.

A.11 What information is needed to demonstrate the safe and long-term containment of anthropogenic CO₂ stored in association with a CO₂-EOR operation?

During CO₂-EOR operations, virtually all of the delivered and injected CO₂ will ultimately be trapped in the reservoir as an inherent part of the oil recovery operation even though the purpose of the CO₂ injection is to enhance oil recovery, not to store CO₂. The process of documenting the quantity of associated storage is essentially a two-step process. It consists of

- a) determining throughout the EOR operation the net quantity of CO₂ that is injected, net of recycle, re-use, and any surface emissions, and then
- b) demonstrating that this net quantity will be contained in the EOR complex long term.

A.12 Determining the quantity of CO₂ from a commingled stream that is to be quantified for associated storage

In order to determine the quantity of CO₂ to be quantified for associated storage in a CO₂-EOR operation, the operator needs first to know the portion of the total CO₂ stream delivered to the site that is to be so quantified. If the EOR operator receives CO₂ exclusively from suppliers that seek quantification of the associated storage, this is straightforward since the relevant portion would be 100 percent of the CO₂ delivered to the site. The current (and likely future) reality is more complex, however, since in the United States, for example, supplies of various sources of CO₂ are commingled in the pipeline such that the pipeline delivers a “system average” CO₂ stream, only a portion of which may represent CO₂ for which quantification as associated storage during EOR is sought. The percentage of such CO₂ may vary with changes in the operational levels at the power plant or other industrial source facility supplying the CO₂ to be quantified, as well the needs of the EOR project for total CO₂.

The contractual agreement between a CO₂ capture facility and a receiving pipeline may address the measurement of the quantity of total CO₂ supplied (information required for both billing and for operational purposes). Knowing the quantity received from each supply source and any contractual allocation to particular delivery points, the pipeline operator can then determine the relative portion of CO₂ in the commingled stream delivered to each delivery point (including each CO₂-EOR site) that is attributable to each relevant source of supply. Similarly, CO₂ to be quantified as associated storage may be delivered to the CO₂-EOR site separately from a supplying pipeline and commingled with the pipeline supply on site for injection into the reservoir.

Once the EOR operator knows the quantity of the total CO₂ stream delivered at the site and the percentage that is to be quantified as associated storage in that operation, the operator can then measure and account the quantity of CO₂ injected at the CO₂-EOR site to be used as part of a CO₂ injection input calculation and then carry forward the relevant percentages in accounting during recycle operations. The operator can also measure and account for any off-site dispositions, removals or emissions of CO₂, such as transfer of CO₂ (including previously injected CO₂) off-site for use in another EOR operation, venting/flaring during maintenance operations or due to equipment failure, repairs, etc.

This kind of framework may thus serve as the basis for identifying and accounting for the portion of the total CO₂ received at a CO₂-EOR site that is to be injected and (assuming appropriate accounting, monitoring and documentation) ultimately recognized as associated storage.

A.13 Demonstrating the net quantity of CO₂ that is safely contained long-term in the EOR complex

In the normal course of developing a project, obtaining permits from the regulator, and conducting operations, including maintaining and verifying the mechanical integrity of wells that penetrate the formation and actively managing subsurface fluid flow to confine the injected fluids in the intended formations, the operator of the project undertakes the key steps required for ensuring that injected CO₂ stays safely contained in the EOR complex and will not interfere with other uses of the subsurface

or endanger underground sources of drinking water. Here, the principal objectives with site evaluation and selection are to ensure that injection formations are properly overlain with non-permeable rock formations and do not communicate with either drinking water sources, permeable formations, leakage pathways, or with nearby wells outside of the EOR complex that could allow injected CO₂ to move to the surface; maintaining and verifying the mechanical integrity of wells that penetrate the formation; and actively managing subsurface fluid flow to confine the injected fluids in the intended formations.

In a CO₂-EOR operation, the target reservoir is selected with care and intensive evaluation to make sure that it is a formation that lends itself to a CO₂-EOR flood. The hydrocarbon resource has itself been trapped in the target formation for many millions of years. This fact provides assurance that injected CO₂ will be similarly trapped.

The planned operation of the field is modelled to calculate the in-reservoir volume of fluids that will be injected (CO₂, water and other fluids) and the volume of fluids (hydrocarbon liquids and gases, CO₂, water and other fluids) that will be withdrawn by production to optimize the flood. Overall, the injection/withdrawal ratio (IWR) of all fluids is managed so that the CO₂ and the oil that it contacts are drawn toward producing wells and does not escape out of the planned reservoir. The IWR could be audited, monitored, and operationally managed to determine if the flood is performing as planned such that there is little or no loss of CO₂ outside of the project reservoir. There will be times where IWR is imbalanced, for example at the start of the flood where pressure is increased to achieve an optimized flood and periods where fluids (oil and CO₂) are preferentially extracted from some patterns to allow development of a new part of the field. An assessment of these imbalanced IWR periods could be conducted and monitored as a practice to ensure that there is little or no loss of CO₂ from the EOR complex.

The pattern of the injection and withdrawal wells could be important in providing assurance that the CO₂ is retained in the intended reservoir. For example, water injection could be used to create a “water pressure curtain” that keeps CO₂ within the reservoir. Alternatively, extraction wells could also be strategically placed to contain the fluids. This active fluid management is valuable in assuring that CO₂ does not move outside the EOR complex.

An operator tracking the fluid management via these mechanisms could provide assurance that the CO₂ has been retained in the EOR complex. Many kinds of monitoring are possible to provide additional assurance that this goal has been accomplished or account for any losses. Monitoring of pressure is commonly used; other methods including geophysics and geochemical techniques could also be used where applicable.

At the end of the CO₂-EOR operation (which could come years after the cessation of injections of anthropogenic CO₂), all the wells penetrating the formation will be plugged and abandoned in accordance with local and regional regulatory and permitting requirements. The stable configuration of the injected CO₂ could be relatively easily assessed, as it typically will mimic the original distribution of hydrocarbons in the reservoir. Well construction is important as well. Existing petroleum industry standards and regulatory requirements address well construction and provide that materials used be compatible with the fluids with which they come into contact and designed for the pressures at which they will operate. In this respect, while the particular materials or techniques used could vary, CO₂-EOR operations are no different than any other oil field operations involving subsurface injections (whether the fluids contain hydrogen sulfide, natural gas or natural gas liquids, brine, polymers or other substances). Occasionally well design fails to provide the intended isolation of the reservoir zone from other zones. Fluids, including CO₂, oil, gasses, and brine could move through the failed elements into shallower (or deeper) zones or to the surface. Oil and gas regulations require routine testing of well construction so that zonal isolation is maintained. If isolation is lost, the well is repaired and CO₂ losses could be estimated. Loss of fluids from the intended zone does not necessarily mean that they will escape to the surface or impact freshwater resources. However, long term assurance of CO₂ isolation from the atmosphere becomes uncertain and such losses could be quantified.

A.14 Addressing other issues

- a) *Matching CO₂ supply to demand.* Before a power plant or other industrial facility installs CO₂ capture equipment, it will of course make arrangements for the sale or disposition of the CO₂ expected to

be captured. Where the generator of the CO₂ contracts to send the CO₂ to markets for CO₂-EOR, it will need to contract with one or more EOR operators to take the contractually-agreed portion of the CO₂ output over the life of the facility. The agreement may address how the parties plan to deal with planned or unplanned variations in actual CO₂ quantities and compositions supplied or taken. In addition, a given CO₂ source may need multiple agreements timed to take the supply because the inherent nature of CO₂-EOR projects may require less new CO₂ in each successive year. Such matters are a routine part of business planning in any long-term contract. Potential suppliers and purchasers of anthropogenic CO₂ are thus no different than suppliers and purchasers of countless other goods in the world economy.

- b) *Ensuring that associated storage of anthropogenic CO₂ is not subsequently vented to the atmosphere or double-counted.* Upon termination of hydrocarbon recovery operations, the termination documentation should identify the EOR complex within which the anthropogenic CO₂ will remain stored, the mass of CO₂ stored, and describe how risks and uncertainties relating to the geologic storage of anthropogenic CO₂ were managed and reduced throughout the EOR project life.
- c) *Lateral location of injected CO₂.* CO₂-EOR projects are long-lived operations that normally occur after secondary recovery operations (e.g., waterflood). Studies conducted as part of the planning and development of earlier phases are valuable in the planning and development for CO₂-EOR. As a result, many of the geological characteristics of the CO₂-EOR operation will have been defined years before any CO₂ is ever injected. The operators will consider the movement of the injected water during the waterflood phase and may consider how waterflood operations may affect the subsequent tertiary recovery phase.

Since the purpose of injecting the CO₂ in an EOR flood is to bring the CO₂ into contact with as much of the remaining residual oil in the reservoir as is feasible, the operator needs to design the flood with this in mind. As a result, CO₂-EOR operators will monitor the behaviour of the injected CO₂ in the reservoir (including its lateral extent) as an integral part of prudent and economic operations. Various production monitoring techniques are used, including a number that involve modifying the subsurface pressures in order to guide the CO₂ — and the petroleum that it mobilizes — on the optimum flow path to the production wells. Thus active pressure monitoring and management are essential elements of successful and prudent CO₂-EOR operations. The operator may alter the development plan over the years in response to actual experience with injections in a given field. In North America, information regarding these operational changes is continually presented before the oil and gas regulator.

- d) *Vertical movement of the injected CO₂.* In CO₂-EOR operations the subsurface is a four-dimensional space. It involves the two lateral dimensions of length and width of the operation; the vertical dimension of the depth and thickness of the producing formation (which depth and thickness of course may vary greatly as one moves across the lateral dimensions of the reservoir); and time (e.g. initial CO₂ injections may be conducted for more than a year before production operations commence in order to achieve miscible pressure requirements). All four of these dimensions are managed in the flood. Because supercritical CO₂ is less dense than brine, there is a tendency for CO₂ to rise above the native reservoir fluids. Operators take this fact into account in designing and operating the flood in order to maximize the amount of oil that is contacted by the CO₂ and thus achieve the optimal value from the injections.
- e) *Providing notice to future potential users of existence of injected CO₂.* The documentation is supplied to the regulatory authority and will apply to the same surface unit area plat that was originally filed with the public records where the operation takes place, as approved by the regulatory agency. Thus, any person proposing to make any later use of that subsurface space would have notice of the prior injection and production history occurring in the relevant formations.

A.15 Cessation of CO₂ injection and hydrocarbon recovery: “coincident” and “non-coincident” cessation of CO₂ injections

Typically, the oil recovery operations will have begun years, or even many decades, prior to the commencement of CO₂ injection operations and may continue for years after CO₂ injections have ceased.

In all CO₂-EOR operations, both onshore and offshore, a significant portion of the hydrocarbon resource will remain in the formations even after hydrocarbon recovery operations become uneconomic and injection and production wells are plugged and abandoned. Published estimates of the percentage of the Original Oil in Place (OOIP) that will remain at the end of CO₂ injections in the project vary broadly, typically from 30 % to 50 %.

Because of the presence of the remaining hydrocarbon resource and the ever-changing economic and technical parameters of oil recovery operations, there are various possibilities for when and how CO₂ injections in a CO₂-EOR operation could come to an end.

- *“Non-coincident” cessation of CO₂ injections and oil recovery.* Injections of anthropogenic CO₂ in an oil recovery operation could be ended even as hydrocarbon recovery continues. This could result from a variety of different factors, including, for example, an interruption or failure of the CO₂ supply; a change in CO₂ source from anthropogenic to non-anthropogenic; an adverse change in economics or in the applicable regulatory rules affecting the CO₂ supply; or a change in the recovery technique applied in the oil recovery project. In this scenario, the hydrocarbon recovery operations continue (or are re-commenced at a future time) even though the anthropogenic CO₂ injection has come to an end. In such a case, oil recovery operations continue, perhaps for decades following the end of injections, and the various wells penetrating the hydrocarbon formations are not plugged and abandoned, but EOR complex monitoring might continue. Hence, in this scenario cessation of anthropogenic CO₂ injection operations are *non-coincident* with the cessation of oil recovery operations. Conceivably CO₂ injections could begin again at some future time as economic changes dictate or technical advances allow, moving this to a coincident cessation model.
- *“Coincident” cessation of CO₂ injections and oil recovery.* Anthropogenic CO₂ injections could, however, also be ended *coincident* with the oil recovery operation. While this scenario could apply to either an onshore or an offshore operation, it would be found most frequently in future offshore operations because of the higher capital cost of offshore operations, or the operational constraints imposed by platform-based operations. Measurement, reporting and documentation of the disposition of the produced CO₂ (e.g., if it is reinjected, shipped offsite or released) could continue until the project is terminated.

These differing operational scenarios suggest differing potential documentation periods for the quantity of CO₂ that is incidentally stored in association with a CO₂-EOR operation since a given documentation period could either “nest within” an ongoing oil recovery operation or come to an end coincident with the end of the oil recovery operation. However, since subsequent hydrocarbon production would continue to produce injected CO₂ long after the actual CO₂ injection has been terminated, periodic assurance of containment of the stored CO₂ would continue until the final plugging and abandonment of the project wells.

Annex B (informative)

Example quantification calculation

B.1 Introduction

[Annex B](#) provides guidance for how the quantification principles and documented values outlined in [Clause 8](#) could be utilized for the quantification of associated storage. First, the total associated storage of CO₂ is calculated using the approach set forth in [Clause 8](#). Second, the Annex supplements the initial quantification of total CO₂ associated storage by calculating the portion of associated storage that represents anthropogenic CO₂. This supplemental calculation would use mass or volumetric (at standard conditions) allocation ratios based on the fraction of the anthropogenic mass of CO₂ to the total mass of CO₂. The example identifies the variables used in, or derived from, the calculation procedures along with the applicable allocation ratio for each.

The example considers the quantification period of one year from the start of quantification; the likely first documentation period. Although quantification results normally would be converted into mass, this example for simplicity of demonstration uses standard oil and gas industry volumetric units (see [Annex C](#) for SI conversions) and converts the results to mass as a final step.

NOTE Please note that in the following example calculation, SI Units will use standard ISO Numerical Format ("Comma" will be used to denote decimal point and space will segregate every three digits) and Oil Field Units will utilize "Decimal Points" and using "Commas" to segregate every three digits.

In this example, the total CO₂ associated storage is calculated (see [B.3](#)) as a first step and then the second step calculation (see [B.4](#)) uses allocation ratios to show how the anthropogenic portion could be quantified. The calculations assume non-leap year (365 days) and use a four digit significant figure.

[Annex C](#) contains a table for converting the standard oil and gas industry units of the Society of Petroleum Engineers (SPE) used in this hypothetical example into International System of Units (SI) units.

In this example, operational loss [$m_{\text{loss operations}}$] is deemed to be composed of two variables defined by [Formula \(B.1\)](#):

$$m_{\text{loss operations}} = m_{\text{loss operations inlet}} + m_{\text{loss operations other}} \quad (\text{B.1})$$

- a) **$m_{\text{loss operations inlet}}$** ; the total mass of CO₂ loss occurring in operations between the custody transfer meter and the point where the CO₂ received at the custody meter is first combined with CO₂ recovered from production. This variable is composed of leakage from facilities (see [8.4.2](#)) and venting/flaring (see [8.4.3](#)) related to the inlet portion.
- b) **$m_{\text{loss operations other}}$** ; the total mass of CO₂ loss occurring in operations during injection into the EOR complex, and production and during processing of the produced fluids and CO₂, from all aspects of CO₂-EOR project excluding only the portion covered by $m_{\text{loss operations inlet}}$. This variable is composed of leakage from facilities (see [8.4.2](#)), venting/flaring from operations (see [8.4.3](#)), entrained CO₂ in products (see [8.4.4](#)) and transfer of CO₂ (see [8.4.5](#)).

In most cases, different allocation ratios would be utilized for the $m_{\text{loss operations inlet}}$ and $m_{\text{loss operations other}}$ because the proportion of anthropogenic CO₂ likely would be different for each of these variables (See [Figure B.1](#)).

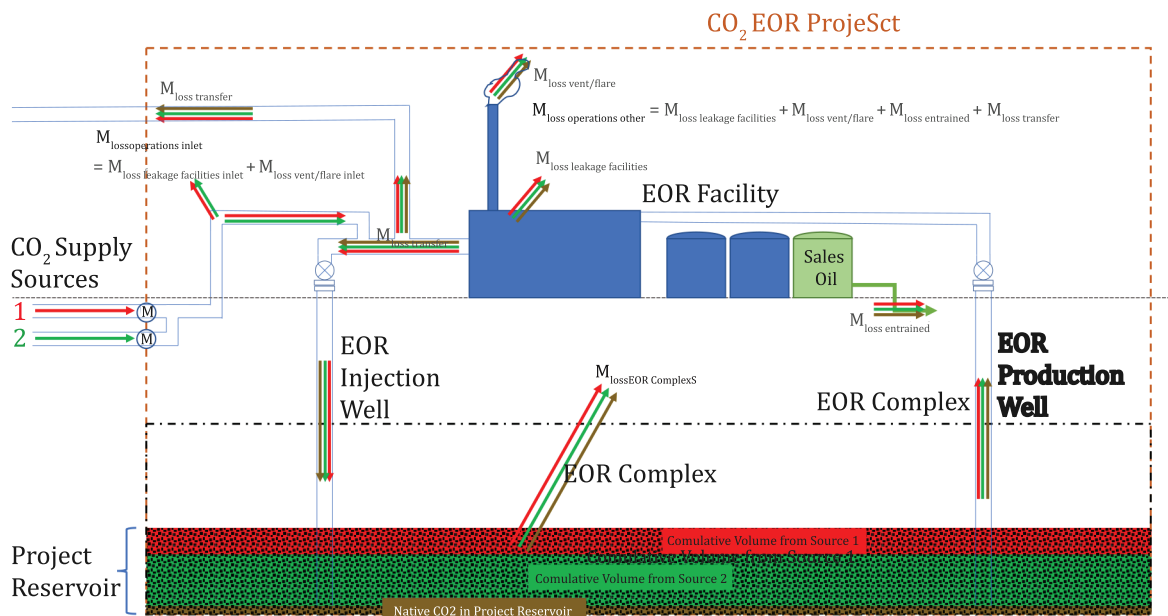


Figure B.1 — Illustration of CO₂ allocations and loss variables

B.2 Hypothetical project

For this illustration, a hypothetical CO₂-EOR project is provided as an example. To encompass various scenarios, a relatively small-scale CO₂-EOR project is presented as having ongoing CO₂-EOR operations using non-anthropogenic CO₂ (irrelevant of source) prior to receiving anthropogenic CO₂ for injection. Additionally, a small concentration of native CO₂ is also assumed to have existed in the project reservoir at the time of field discovery. Further, the CO₂ received is comprised of both non-anthropogenic CO₂ (irrelevant of source) and anthropogenic CO₂. It is assumed that the Project has recycling facilities. The parameters necessary for this quantification example are as follows.

B.2.1 Previously received and injected total and anthropogenic CO₂ within the EOR complex

In the project, the total volume of previously received and injected CO₂ (no anthropogenic portion is assumed) within the EOR complex at the start of the quantification period is known to be 6,000 MMscf (169 900 000 Sm³). This term is to be documented as part of the initial documentation [see 4.3 e) and 8.5]. If CO₂ meeting the definition of anthropogenic CO₂ had been received and injected during CO₂-EOR operations prior to the beginning of the quantification period, it would be treated as non-anthropogenic CO₂ for purposes of quantifying the anthropogenic portion of associated storage.

B.2.2 New CO₂ received and the percentage of anthropogenic CO₂

New CO₂ received during the first documentation period for this example will be 10.00 MMscf/D (283 200 Sm³/D), of which 40 percent is anthropogenic CO₂. This example would represent a CO₂-EOR project that might have a non-anthropogenic supply of CO₂ now being supplemented by a new source of anthropogenic CO₂.

B.2.3 Native CO₂ content

The native CO₂ content is 100.0 scf/stb (17,81 Sm³/Sm³). It is assumed that the inclusion of captured native CO₂ as anthropogenic CO₂ has been approved by the authority.

B.2.4 Oil production

During year one, the oil production average from this project was 1,000 stb/D (159,0 Sm³/D).

B.2.5 Operational inlet loss [$m_{\text{loss operations inlet}}$]

The loss from facilities of the inlet portion (after custody transfer from CO₂ delivery and prior to the point where the CO₂ received at the custody meter is first combined with CO₂ recovered from production) is measured, calculated or estimated to be 2.000 Mscf/D (56,64 Sm³/D). This loss is the total CO₂ loss including both anthropogenic and non-anthropogenic CO₂ components.

B.2.6 EOR complex loss [$m_{\text{loss EOR complex}}$]

The loss from the EOR complex is measured, calculated or estimated to be 1.000 Mscf/D (28,32 Sm³/D). This loss is the total CO₂ loss including both anthropogenic and non-anthropogenic CO₂ (inclusive of previously injected non-qualifying volumes injected prior to the quantification period).

B.2.7 Other operational losses [$m_{\text{loss operations other}}$]

The total loss from all operations through production facilities, only excluding the inlet portion, is measured, calculated or estimated to be 15.00 Mscf/D (424,8 Sm³/D). This loss is the total CO₂ loss including both anthropogenic and non-anthropogenic CO₂ (inclusive of volumes injected prior to the quantification period). This loss is an aggregate of the following:

- Loss of CO₂ due to leakage from production, handling and recycling CO₂-EOR facilities (infrastructure including wellheads) [$m_{\text{loss leakage facilities}}$];
- Loss of CO₂ from venting/flaring from production operations [$m_{\text{loss vent/flare}}$];
- Loss of CO₂ due to entrainment within produced gas/oil/water when this CO₂ is not separated and reinjected. [$m_{\text{loss entrained}}$]; and
- Loss of CO₂ due to any transfer of CO₂ outside the CO₂-EOR project. [$m_{\text{loss transfer}}$].

Daily metering could be used to minimize calculation errors through this quantification process.

B.3 Calculation procedures for the first year (for the total CO₂)

The calculation of total CO₂ associated storage is shown as the first step. (see [B.3.1](#) to B.3.6).

B.3.1 Calculation of native CO₂ recovered

If the authority approval to include the native CO₂ is obtained, the following parameters are used to calculate the mass of native CO₂ included in m_{input} :

- Native CO₂ content is 100.0 scf/stb (17,81 Sm³/Sm³).
- Production rate is 1,000 stb/D (159,0 Sm³/D).

Calculation:

$$(1,000 \text{ stb/D} \times 365.0 \text{ D/Year}) \times (100.00 \text{ scf/stb}) / (1,000,000 \text{ scf/MMscf}) = 36.50 \text{ MMscf}$$

$$[(159,0 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year}) \times (17,81 \text{ Sm}^3/\text{Sm}^3)] = 1\,034\,000 \text{ Sm}^3 = 1\,931 \text{ t}$$

This value is the total native CO₂ recovered during the first year.

B.3.2 Total CO₂ input [m_{input}]

The daily quantity of CO₂ received by the project, if no native CO₂ is approved and received, is multiplied by 365 days to obtain the annual total m_{input} .

$$10.00 \text{ MMscf/D} \times 365.0 \text{ D/Year} = 3,650 \text{ MMscf}$$

$$[(283\,200 \text{ Sm}^3/\text{D} \times 365.0 \text{ D/Year}) = 103\,400\,000 \text{ Sm}^3 = 193\,100 \text{ t}]$$

If authority approval to include native CO₂ is obtained, then m_{input} includes the m_{native} volume (see B.3.1).

$$3,650 \text{ MMscf} + 36.50 \text{ MMscf} = 3,686.50 \text{ MMscf}$$

$$103\,400\,000 + 1\,034\,000 \text{ Sm}^3 = 104\,434\,000 \text{ Sm}^3 = 195,000 \text{ t}]$$

B.3.3 Operational loss [$m_{\text{loss operations}}$]

The daily loss from both injection and production facilities (see B.2.5 and B.2.7) is converted from Mscf to MMscf and is then multiplied by 365 days to obtain the annual $m_{\text{loss operations}}$, where:

$$m_{\text{loss operations}} = m_{\text{loss operations inlet}} + m_{\text{loss operations other}}$$

$$[(2.000 \text{ Mscf/D} + 15.00 \text{ Mscf/d}) / 1,000 (\text{Mscf/MMscf}) \times 365.0 \text{ D/Year}] = 6.205 \text{ MMscf}$$

$$[481.4 \text{ Sm}^3/\text{D} \times 365.0 \text{ D/Year} = 175\,770 \text{ Sm}^3 = 328.2 \text{ t}]$$

B.3.4 EOR complex loss [$m_{\text{loss EOR complex}}$]

The daily loss from the EOR complex (see B.2.6) is converted from Mscf to MMscf and is multiplied by 365 days to obtain the annual $m_{\text{loss EOR complex}}$.

$$(1.000 \text{ Mscf/D}) / 1000 (\text{Mscf/MMscf}) \times 365.0 \text{ D/Year} = 0.3650 \text{ MMscf}$$

$$[28.32 \text{ Sm}^3/\text{D} \times 365.0 \text{ D/Year} = 10\,340 \text{ Sm}^3 = 19.31 \text{ t}]$$

B.3.5 Associated storage calculation [m_{stored}]

The total CO₂ associated storage for the first year is calculated based on following formulas:

$$m_{\text{stored}} = m_{\text{input}} - m_{\text{loss operations}} - m_{\text{loss EOR complex}}$$

$$3,686.5 \text{ MMscf} - 6.205 \text{ MMscf} - 0.3650 \text{ MMscf} = 3,680 \text{ MMscf}$$

$$[104\,400\,000 \text{ Sm}^3 - 20\,670 \text{ Sm}^3 - 155\,100 \text{ Sm}^3 - 10\,340 \text{ Sm}^3 = 104\,213\,890 \text{ Sm}^3 = 194\,700 \text{ t}]$$

NOTE If the previously injected volume of 6,000 MMscf is included, then the total CO₂ within the EOR complex will be 9,680 MMscf (274 100 000 Sm³ = 512 100 t).

B.4 Calculation procedures for the first year for the anthropogenic portion of

m_{stored}

Calculation of the anthropogenic portion of CO₂ associated storage will follow the same approach, using the same formula (see 8.3), and using variables that have been adjusted to reflect the application of allocation ratios. Note that if there were no previously received and injected CO₂ at this hypothetical project (i.e. a new project) and the new CO₂ received was 100 % anthropogenic CO₂, the calculations below will reduce to simply losses subtracted from the amount of CO₂ received. The example provided herein is intended to address a relatively complex scenario, albeit in a simplified manner for ease of understanding.

B.4.1 Calculation of native CO₂ if included

If the authority approval to include the native CO₂ is obtained, the following parameters are used to calculate the mass of native CO₂ included in m_{input} :

- Native CO₂ content is 100.0 scf/stb (17,81 Sm³/Sm³)

b) Production Rate is 1,000 stb/D (159,0 Sm³/D)

Calculation:

$$(1,000 \text{ stb/D} \times 365.0 \text{ D/Year}) \times (100.0 \text{ scf/stb}) / (1,000,000 \text{ scf/MMscf}) = 36.50 \text{ MMscf}$$

$$[(159,0 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year}) \times (17,81 \text{ Sm}^3/\text{Sm}^3) = 1\,034\,000 \text{ Sm}^3 = 1\,931 \text{ t}]$$

This value is the total native CO₂ recovered during the first year.

B.4.2 Anthropogenic CO₂ m_{input} calculation using a ratio

To derive the volume of anthropogenic CO₂ received at the project, a three-step process is used. First, the total CO₂ received at the custody transfer meter for the project is calculated, and then it is reduced by the proportion of non-anthropogenic CO₂ within the total CO₂ stream. Finally, m_{native} is added to the anthropogenic stream, if approved by the authority. The following parameters are used:

a) New CO₂ received is 10.00 MMscf/D (283 200 Sm³/D), of which 40 % is defined as anthropogenic CO₂; and

b) First Year of anthropogenic native CO₂ is 36.50 MMscf (1 034 000 Sm³) (see [B.4.1](#)).

Calculation:

B.4.2.1 Total CO₂ m_{received} for the first year

$$(10.00 \text{ MMscf/D} \times 365.0 \text{ D/Year}) = 3,650 \text{ MMscf}$$

$$[(283\,200 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year}) = 103\,400\,000 \text{ Sm}^3 = 193\,200 \text{ t}]$$

The anthropogenic allocation ratio for m_{received} is deemed to be 40 % (0,400 0), and this allocation factor is to be utilized for calculating the anthropogenic CO₂ portion of $m_{\text{loss operations inlet}}$ (see [B.4.3](#)).

B.4.2.2 Total CO₂ m_{input} for the first year

$$m_{\text{input}} = m_{\text{received}} + m_{\text{native}}$$

$$(10.00 \text{ MMscf/D} \times 365.0 \text{ D/Year}) + 36.50 \text{ MMscf} = 3,687 \text{ MMscf}$$

$$[(283\,200 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year}) + 1\,034\,000 \text{ Sm}^3 = 104\,400\,000 \text{ Sm}^3 = 195\,000 \text{ t}]$$

B.4.2.3 Anthropogenic CO₂ m_{input} for the first year

The anthropogenic portion of m_{input} is calculated by applying the anthropogenic ratio (40 %) to m_{received} and adding m_{native} , all of which is anthropogenic.

$$(10.00 \text{ MMscf/D} \times 365.0 \text{ D/Year}) \times 0.400\,0 + 36.50 \text{ MMscf} = 1,497 \text{ MMscf}$$

$$[(283\,200 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year}) \times 0,400\,0 + 1\,034\,000 \text{ Sm}^3 = 42\,380\,000 \text{ Sm}^3 = 79\,170 \text{ t}]$$

B.4.2.4 First year anthropogenic ratio for m_{input}

The anthropogenic portion of m_{input} (see [B.4.3](#)) is divided by the total m_{input} (see [B.3.2](#)), including m_{native} (see [B.4.1](#)), when allowed by the authority.

$$1,497 \text{ MMscf} / (3,650 + 36.50) \text{ MMscf} = 0.406\,0$$

$$[42\,380\,000 \text{ Sm}^3 / 104\,400\,000 \text{ Sm}^3 = 0,406\,0]$$

B.4.3 Operational inlet loss [$m_{\text{loss operations inlet}}$] of anthropogenic CO₂

Because the anthropogenic ratios will vary across the system, this first calculation quantifies the anthropogenic CO₂ loss between the custody meter and the point where the CO₂ received at the custody transfer meter is first combined with CO₂ recovered from production and recycling for reinjection purposes. The following parameters are used:

- a) Operational inlet loss of 2.000 Mscf/D (56,64 Sm³/D) for the inlet CO₂ stream (see [B.2.5](#)).
- b) First year anthropogenic CO₂ received ratio of 0,400 0 (see [B.2.2](#)).

Calculation:

B.4.3.1 Total CO₂ operational inlet loss [$m_{\text{loss operations inlet}}$] for the first year

Operational inlet loss daily rate is converted from Mscf to MMscf, and then multiplied by 365 days to yield the total annual $m_{\text{loss operations inlet}}$.

$$(2.000 \text{ Mscf/D} / 1,000 (\text{Mscf/MMscf}) \times 365.0 \text{ D/Year}) = 0.7300 \text{ MMscf} = 38.62 \text{ t}$$

$$[56,64 \text{ Sm}^3/\text{D} / 28\,320 \text{ Sm}^3 / 28\,320 \text{ Sm}^3 \times 365,0 \text{ D/Year} = 20\,670 \text{ Sm}^3 = 38,62 \text{ t}]$$

B.4.3.2 Anthropogenic CO₂ operational inlet loss [$m_{\text{loss operations inlet}}$] for the first year

Multiplying the total annual $m_{\text{loss operations inlet}}$ by the anthropogenic ratio yields the annual anthropogenic $m_{\text{loss operations inlet}}$.

$$0.7300 \text{ MMscf} \times 0.4000 = 0.2920 \text{ MMscf} = 15.45 \text{ t}$$

$$[20\,674 \text{ Sm}^3 \times 0,400\,0 = 8\,270 \text{ Sm}^3 = 15,45 \text{ t}]$$

B.4.4 EOR complex anthropogenic CO₂ ratio

This ratio represents the proportion of anthropogenic CO₂ existing within the EOR complex at the end of the first year of the quantification period. It is utilized to calculate the quantity of anthropogenic CO₂ portion of operational loss production and loss from EOR complex. This ratio changes with time and could be calculated at shorter intervals (to tie in with monitoring and loss measurement events) to improve accuracy. The following parameters are used:

- a) Previously injected CO₂ within the EOR complex at the start of the quantification period (see [B.2.1](#)) of 6,000 MMscf (169 900 00 Sm³);
- b) Total CO₂ received for the first year is 3,687 MMscf (104 400 00 Sm³), including native CO₂ (see [B.3.2](#) and [B.4.1](#));
- c) Total first year anthropogenic CO₂ received is 1,497 MMscf (42 395 000 Sm³) (see [B.4.2.2](#));
- d) First year total CO₂ operational inlet loss is 0,730 0 MMscf (20 670 Sm³) (see [B.4.3.1](#)); and
- e) First year anthropogenic CO₂ operational inlet loss is 0,292 0 MMscf (8 270 Sm³) (see [B.4.3.2](#)).

Calculation:

The anthropogenic ratio for $m_{\text{loss EOR complex}}$ and $m_{\text{loss operations other}}$ is derived by taking the anthropogenic portion of m_{input} (including m_{native}) minus the anthropogenic portion of $m_{\text{loss operations inlet}}$ and dividing that result by the total of ($m_{\text{previous injection}} + m_{\text{input}} - m_{\text{loss operations inlet}}$). The resultant formulation is:

$$(1,497 \text{ MMscf} - 0.2920 \text{ MMscf}) / (6,000 \text{ MMscf} + 3,687 \text{ MMscf} - 0.7300 \text{ MMscf}) = 0.154\,5$$

$$[(42\,395\,000 \text{ Sm}^3 - 8\,270 \text{ Sm}^3) / (169\,900\,000 \text{ Sm}^3 + 104\,400\,000 \text{ Sm}^3 - 20\,670 \text{ Sm}^3) = 0,154\,5]$$

B.4.5 Anthropogenic CO₂ portion of operational other loss [$m_{\text{loss operations other}}$] and EOR complex loss [$m_{\text{loss EOR complex}}$]

This calculation derives the anthropogenic portion of the operational other loss and EOR complex loss by applying the anthropogenic ratio derived in [B.4.4](#) to total operational other loss and total EOR complex loss.

Parameters used:

- a) EOR complex anthropogenic CO₂ ratio is 0,154 5 (see [B.4.4](#));
- b) EOR complex loss is 1.000 Mscf/D (28,32 Sm³/D); and
- c) Operational other loss is 15.00 Mscf/D (424,8 Sm³/D).

Calculation:

B.4.5.1 Total CO₂ operational other loss [$m_{\text{loss operations other}}$]

Other loss daily rate is converted from Mscf to MMscf, multiplied by 365 days to yield the annual total $m_{\text{loss operations other}}$.

$$(15.00 \text{ Mscf/D}) / (1,000 \text{ Mscf/MMscf}) \times 365.0 \text{ D/Year} = 5.475 \text{ MMscf}$$

$$[424,8 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year} = 155\,100 \text{ Sm}^3 = 289,6 \text{ t}]$$

B.4.5.2 Total CO₂ EOR complex loss [$m_{\text{loss EOR complex}}$]

Total CO₂ EOR complex loss daily rate is converted from Mscf to MMscf, multiplied by 365 days to yield the annual total $m_{\text{loss EOR complex}}$.

$$(1.000 \text{ Mscf/D}) / (1,000 \text{ Mscf/MMscf}) \times 365.0 \text{ D/Year} = 0.3650 \text{ MMscf}$$

$$[28,30 \text{ Sm}^3/\text{D} \times 365,0 \text{ D/Year} = 10\,340 \text{ Sm}^3 = 19,31 \text{ t}]$$

B.4.5.3 Anthropogenic CO₂ operational other loss [$m_{\text{loss operations other}}$]

Total CO₂ operational other loss is multiplied by the anthropogenic ratio derived in [B.4.4](#) to obtain the anthropogenic portion of annual $m_{\text{loss operations other}}$.

$$(5.475 \text{ MMscf}) \times 0.1545 = 0.8459 \text{ MMscf}$$

$$[155\,100 \text{ Sm}^3 \times 0,154\,5 = 23\,960 \text{ Sm}^3 = 44,75 \text{ t}]$$

B.4.5.4 Anthropogenic CO₂ EOR complex loss [$m_{\text{loss EOR complex}}$]

Total CO₂ EOR complex loss is multiplied by the anthropogenic ratio derived in [B.4.4](#) to obtain the anthropogenic portion of annual $m_{\text{loss EOR complex}}$.

$$(0.3650 \text{ MMscf}) \times 0.1545 = 0.05639 \text{ MMscf}$$

$$[10\,340 \text{ Sm}^3 \times 0,154\,5 = 1\,598 \text{ Sm}^3 = 2,980 \text{ t}]$$

B.4.6 Quantification of anthropogenic CO₂ stored in association with EOR operations

Parameters used:

- a) Anthropogenic CO₂ operational inlet loss: 0.2920 MMscf (8 270 Sm³) (see [B.4.3.2](#));
- b) Anthropogenic CO₂ operational other loss: 0.8459 MMscf (23 960 Sm³) (see [B.4.5.3](#));
- c) Anthropogenic CO₂ EOR complex loss: 0.05639 MMscf (1 598 Sm³) (see [B.4.5.4](#));

- d) New CO₂ received and the percentage of anthropogenic CO₂: 10.00 MMscf/D (283 200 Sm³/D) (40 % anthropogenic); and
- e) Native CO₂ received: 36.50 MMscf (1 034 000 Sm³) (see [B.4.1](#)).

Calculation

To quantify the portion of anthropogenic CO₂ stored for the first year, the calculation also considers m_{native} , which is included in the m_{input} portion of the calculation, and is calculated based on the anthropogenic CO₂ inputs to the following formula:

$$m_{\text{stored}} = m_{\text{input}} - m_{\text{loss operations}} - m_{\text{loss EOR complex}}$$

$$m_{\text{stored}} = (m_{\text{received}} + m_{\text{native}}) - (m_{\text{loss operations inlet}} + m_{\text{loss operations other}}) - m_{\text{loss EOR complex}}$$

$$[(10.00 \text{ MMscf/D} \times 0.400 \text{ 0} \times 365.0 \text{ D/Year}) + 36.50 \text{ MMscf}] - (0.2920 \text{ MMscf} + 0.8459 \text{ MMscf}) - 0.05639 \text{ MMscf} = 1,495.3 \text{ MMscf}$$

$$[(283 \text{ 200 Sm}^3/\text{D} \times 0,400 \text{ 0} \times 365,0 \text{ D/Year}) + 1 \text{ 034 000 Sm}^3] - (8 \text{ 270 Sm}^3 + 23 \text{ 960 Sm}^3) - 1 \text{ 598 Sm}^3 = 42 \text{ 347 000 Sm}^3 = 79 \text{ 110 t}$$

Table B.1 — Example table documenting the variables and allocation ratios calculated for the anthropogenic CO₂ case

Variable	For Total CO ₂ (in MMscf)	Anthropogenic Ratio	For Anthropogen- ic CO ₂ (in MMscf)
m_{input}	3 687	0,406 0	1497
m_{native} (CO ₂ per unit of oil = 100.0 scf/stb)	36.50	1,000	36.50
$m_{\text{previous injection}}$	6 000	0,000 0	0.000
$m_{\text{loss operations inlet}}$	0.7300	0,400 0	0.2920
$m_{\text{loss operations other}}$	5.475	0,154 5	0.8459
$m_{\text{loss EOR complex}}$	0.3650	0,154 5	0.05639
m_{stored}	3 643		1 495

Annex C (informative)

Unit conversion

Standard oil and gas industry units

barrel(s) of oil	stb
barrels of oil per day	stb/D
million standard cubic feet	MMscf
million standard cubic feet per day	MMscf/D
standard cubic foot	scf
standard cubic feet per barrel	scf/stb
standard cubic feet per day	scf/D
thousand standard cubic feet	Mscf
thousand standard cubic feet per day	Mscf/D

International system of units (SI) metric conversion factors

1 barrel = 0,158 9 Sm³

1 M = 1 000

1 MM = 1 000 000

1 t = 1 000 kg

International system of units (SI) metric conversion factors at 60 °F (15,555 6 °C), 1 atm¹⁾

	Volume m ³	Mass kg	Volume scf	Mass lb
Volume (m ³)	1,000	1,868	35.31	4.118
Mass (kg)	0,535 3	1,000	18.90	2.204
Volume (scf)	0,028 32	0,052 90	1.000	0.116 6
Mass (lb)	0,242 8	0,453 6	8.575	1.000
NOTE In this table, for columns (m ³) and (kg), comma (",") is used to denote decimal point (".").				

SOURCE: NIST Chemistry WebBook, SRD 69 Thermodynamic properties of carbon dioxide.

1) Conversion is valid for pure CO₂ only.

Bibliography

Annex A references:

- [1] FIGURE A. 2, Joyce Frank, CO₂-EOR Schematic, graphic art
- [2] FIGURE A. 3, Bruce Hill, Whiting North Ward Estes Field, Permian Basin, photograph
- [3] Figure A.4, Susan Hovorka, Comparing Saline Injection to EOR Pattern Flood, graphic art
- [4] ALEKEMODE P.L.C. CO₂ Miscible Displacement Enhanced Oil Recovery in Dutch North Sea. Proceedings of the Fifth (1995) International Offshore and Polar Engineering Conference. The Hague, The Netherlands. Vol. ISBN 1-880653-16-8 (Set); ISBN 1-880653-17-6 (Vol 1). 1995
- [5] ARI. Global technology roadmap for CCS in industry. Sectoral assessment CO₂ enhanced oil recovery. 2009. Available at: https://www.unido.org/fileadmin/user_media/Services/Energy_and_Climate_Change/Energy_Efficiency/CCS/EOR.pdf
- [6] ARI. Improving domestic energy security and lowering CO₂ emissions with next-generation CO₂ enhanced oil recovery (CO₂-EOR). NETL (2011). NOE/NETL 2011/1504/. Available at: <http://www.netl.doe.gov/File%20Library/Research/Energy%20Analysis/Publications/DOE-NETL-2011-1504-StoringCO2-wEOR-Final.pdf>
- [7] AZZOLINA N., NAKLES D., GORECKI C., PECK W., AYASH S., MELZER S. CO₂ storage associated with CO₂ enhanced oil recovery: A statistical analysis of historical operations, *International Journal of Greenhouse Gas Control*, V. 37, pp. 384–397 (June 2015). Available at: <http://www.sciencedirect.com/science/article/pii/S1750583615001413>
- [8] BACHU S., & BENNION D.B. Experimental assessment of brine and/or CO₂ leakage through well cements at reservoir conditions, *Int. J. Greenhouse Gas Control*, 3, 494–501. 2009
- [9] BACHU S. Identification of Oil Reservoirs Suitable for CO₂-EOR and CO₂ Storage (CCUS) Using Reserves Databases, with Application to Alberta, Canada, *International Journal of Greenhouse Gas Control*. 44 (2016). 152–165
- [10] CARBON SEQUESTRATION LEADERSHIP FORUM. *Final Report by the CSLF Task Force on Technical Challenges in the Conversion of CO₂-EOR Projects to CO₂ Storage Projects* (September 2013) (Bachu, *et al.*). Available at: https://www.cslforum.org/cslf/sites/default/files/documents/CO2-EORtoCCS_FinalReport.pdf
- [11] CONSOLI C., & WILDGUST N. Current status of global storage resources. *Energy Procedia* v. 114, 4623-4628. 2016. Available at: <https://www.sciencedirect.com/science/article/pii/S1876610217320684>
- [12] DIPIETRO P., BALACH P., WALLACE M. A note on sources of CO₂ supply for enhanced oil recovery operations. SPE 0412. 2012. Available at: <http://www.co2conference.net/2012/12/a-note-on-sources-of-co2supply-for-enhanced-oil-recovery-operations/>
- [13] Docket Number (08-AFC-8A), Amended Application for Certification, Hydrogen Energy California Power Plant Licensing Case, Amended Application for Certification. Available at: http://www.energy.ca.gov/sitingcases/hydrogen_energy/ and http://www.energy.ca.gov/sitingcases/hydrogen_energy/documents/others/2012-06-20_OEHI_Project_Overview_workshop_presentation.pdf
- [14] Fox C. CO₂ EOR Carbon balance. Presentation, CO₂ Conference, Houston. 2013. Available at: <http://www.CO2conference.net/wp-content/uploads/2013/05/Fox-KM-Presentation-SACROC.pdf>
- [15] Halliburton. Supergiant Lula Brings CO₂-EOR Advances: <http://halliburtonblog.com/supergiant-lula-brings-CO2-eor-advances/>. 2012

- [16] HILL B., HOVORKA S., MELZER S. Geologic carbon storage through enhanced oil recovery. *Energy Procedia* v. 37, 6808-6830. 2012. Available at <http://www.sciencedirect.com/science/article/pii/S1876610213008576>
- [17] HOLLOWAY S., VINCENT C.J., BENTHAM M. S., KIRK K.L. Top-down and bottom-up estimates of CO₂ storage capacity in the UK sector of the Southern North Sea Basin. *Environmental Geoscience* Vol. 13: 74-81. 2006
- [18] HOLM L., & O'BRIEN L. *Carbon Dioxide Test at the Mead-Strawn Field*, Journal of Petroleum Technology, vol. 23, issue 4 (April 1971) Society of Petroleum Engineers publication SPE-3103-PA. Available at <https://doi.org/10.2118/3103-PA>
- [19] HOLTZ M., NANCE P., FINLEY R. *Reduction of Greenhouse Gas Emissions through Underground CO₂ Sequestration in Texas Oil and Gas Reservoirs*; EPRI, Palo Alto, CA: 1999 (Finley, R., Principal Investigator)
- [20] HOVORKA S. EOR as Sequestration — Geoscience Perspective. White paper for symposium on role of EOR in accelerating deployment of CCS. An MIT Energy Initiative and Bureau of Economic Geology at UT Austin Symposium on role of EOR in accelerative deployment of CCS (2010). Available at: <https://energy.mit.edu/wp-content/uploads/2010/07/MITEI-RP-2010-003.pdf>
- [21] HOVORKA S. 2013). Managing storage resources-role of enhanced oil recovery (EOR). Available from Gulf Coast Carbon Center, University of Austin, TX
- [22] HUERTA N.J., BRYANT S.L., STRAZISAR B.R., KUTCHKO B.G., CONRAD L.C. The influence of confining stress and chemical alteration on conductive pathways within wellbore cement, *Energy Procedia* 1, 3571-3578. 2009
- [23] JX Nippon Oil and Gas Exploration (2011). PetroVietnam, JVPC and JOGMEC announce success of CO₂-EOR Pilot Test in Rang Dong Oil Field, Block 15-2 Offshore Vietnam: http://www.nexjx-group.co.jp/english/newsrelease/2011/20120229_01.html
- [24] KUUSKRAA V., GODEC M., DIPIETRO P. CO₂ Utilization from “Next Generation” CO₂ Enhanced Oil Recovery Technology, *Energy Procedia*, 37 (2013) (6854–6866)
- [25] KUUSKRAA V. Using the Economic value of CO₂-EOR to accelerate the deployment of CO₂ capture, utilization and storage. Presentation, CCUS, EPRI Cost Workshop, Palo Alto, CA, April 25-26, 2012
- [26] KUUSKRAA V., & WALLACE M. CO₂-EOR set for growth as new CO₂ supplies emerge. *Oil and Gas Journal*. April 7, 2014
- [27] LAKE L.W. *Enhanced oil recovery*. ISBN 978132816014, Prentice Hall, Englewood Cliffs, NJ. 1989
- [28] MANRIQUE E., THOMAS C., RAVIKIRAN R., IZADI M., LANTZ M., ROMERO J. EOR: Current status and opportunities. SPE Improved Oil Recovery Symposium. Tulsa, Oklahoma, USA. Vol. 130113-MS. 24–28 April 2010
- [29] MARSTON P., MOORE P., SCHNACKE G. Carbon Dioxide Infrastructure: Pipeline Transport Issues and Regulatory Concerns — Past, Present and Future. 52 Rocky Mtn. Mineral Law Foundation Journal 275 (2015)
- [30] MARSTON P. Pressure profiles for CO₂-EOR and CCS: Implications for regulatory frameworks. *Greenhouse Gas Sci Technol*. V. 3, P. 165-168. 2013. (<http://onlinelibrary.wiley.com/doi/10.1002/ghg.1348/full>)
- [31] MARSTON P. Bridging the Gap: An Analysis and Comparison of Legal and Regulatory Frameworks for CO₂-EOR and CO₂-CCS, report to the Global Carbon Capture and Storage Institute (2013): <http://www.globalccsinstitute.com/sites/default/files/publications/118951/eor-report-2013-4-nov.pdf>
- [32] MELZER L. Stephen, “Carbon Dioxide Enhanced Oil Recovery (CO₂ EOR): Factors Involved in Adding Carbon Capture, Utilization and Storage (CCUS) to Enhanced Oil Recovery” (February

2012) (report prepared for the National Enhanced Oil Recovery Initiative, Center for Climate and Energy Solutions). Available at: http://carboncapturecoalition.org/wp-content/uploads/2018/01/Melzer_CO2EOR_CCUS_Feb2012.pdf

- [33] National Petroleum Council. 2011). Conventional Onshore Oil Including Enhanced Oil Recovery
- [34] FINAL REPORT RPSEA *Commercial exploitation and the origin of residual oil zones: Developing a case history in the Permian Basin of New Mexico and West Texas*, Research Partnership to Secure Energy for America. 2012
- [35] TZIMAS E. "CO₂ Storage Potential in the North Sea via Enhanced Oil Recovery". EU Commission DG-Joint Research Centre, Institute for Energy, Petten, The Netherlands. Paper 03-20-09 presented at Eighth International Conference on GHG Technologies, Trondheim, Norway. 2006.
- [36] WHITTAKER S. Ph.D and PERKINS E Ph.D., "*Technical Aspects of CO₂-Enhanced Oil Recovery and Associated Carbon Storage*" (Report to Global CCS Institute) (October 2013)
- [37] WOLAVER B., HOVORKA S., SMYTH R. Greensites and brownsites: Implications for CO₂ sequestration, characterization, risk assessment and monitoring. *International Journal of Greenhouse Gas Control*. V. 19, p. 49-62. 2013

American Society of Mechanical Engineers (ASME) and International Organization for Standardization (ISO) Pipeline Related Standards

- [38] ASME B31.4, *Pipeline Transportation Systems for Liquid Hydrocarbons and Other Liquids*
- [39] ISO 3183, *Petroleum and natural gas industries — Steel pipe for pipeline transportation systems*
- [40] ISO 12490, *Petroleum and natural gas industries — Mechanical integrity and sizing of actuators and mounting kits for pipeline valves*
- [41] ISO 12736, *Petroleum and natural gas industries — Wet thermal insulation coatings for pipelines, flow lines, equipment and subsea structures*
- [42] ISO/TS 12747, *Petroleum and natural gas industries — Pipeline transportation systems — Recommended practice for pipeline life extension*
- [43] ISO 13623, *Petroleum and natural gas industries — Pipeline transportation systems*
- [44] ISO 13847, *Petroleum and natural gas industries — Pipeline transportation systems — Welding of pipelines*
- [45] ISO 14313, *Pipeline valves*
- [46] ISO 14723, *Petroleum and natural gas industries — Pipeline transportation systems — Subsea pipeline valves*
- [47] ISO 15589-1, *Petroleum, petrochemical and natural gas industries — Cathodic protection of pipeline systems — Part 1: On-land pipelines*
- [48] ISO 15589-2, *Petroleum, petrochemical and natural gas industries — Cathodic protection of pipeline transportation systems — Part 2: Offshore pipelines*
- [49] ISO 15590-1, *Pipeline induction bends*
- [50] ISO 15590-2, *Petroleum and natural gas industries — Induction bends, fittings and flanges for pipeline transportation systems — Part 2: Fittings*
- [51] ISO 15590-3, *Petroleum and natural gas industries — Induction bends, fittings and flanges for pipeline transportation systems — Part 3: Flanges*
- [52] ISO 16440, *Petroleum and natural gas industries — Pipeline transportation systems — Design, construction and maintenance of steel cased pipelines*

- [53] ISO 16708, *Petroleum and natural gas industries — Pipeline transportation systems — Reliability-based limit state methods*
- [54] ISO 21329, *Petroleum and natural gas industries — Pipeline transportation systems — Test procedures for mechanical connectors*
- [55] ISO 21809-1, *Polyolefin coatings (3-layer PE and 3-layer PP)*
- [56] ISO 21809-2, *Petroleum and natural gas industries — External coatings for buried or submerged pipelines used in pipeline transportation systems — Part 2: Single layer fusion-bonded epoxy coatings*
- [57] ISO 21809-3, *Petroleum and natural gas industries — External coatings for buried or submerged pipelines used in pipeline transportation systems — Part 3: Field joint coatings*
- [58] ISO 21809-4, *Petroleum and natural gas industries — External coatings for buried or submerged pipelines used in pipeline transportation systems — Part 4: Polyethylene coatings (2-layer PE)*
- [59] ISO 21809-5, *Petroleum and natural gas industries — External coatings for buried or submerged pipelines used in pipeline transportation systems — Part 5: External concrete coatings*

American Petroleum Institute (API) and NACE International Standards and recommended practices

- [60] Spec 5/CT ISO 11960, *Specifications for Casing and Tubing*
- [61] API 10D/Spec 1 — *TR4 Centralizers*
- [62] API Std 53, *Blowout Prevention Equipment Systems for Drilling Wells, Fourth Edition, (Includes Addendum 1)*
- [63] Bull 5C2: *Performance Properties of Casing Tubing and Drill Pipe*
- [64] Spec 5L: *Specification for Line Pipe*
- [65] Spec 5LD: *CRA or Lined Steel Pipe*
- [66] Spec 6A: *Specifications for Wellhead and Christmas Tree Equipment*
- [67] Spec 6D/ISO 14313: *Specifications for Pipeline Vales*
- [68] Bull 6J: *Testing of Oilfield Elastomers*
- [69] RP 10B-2 through 5: *Testing Well Cements*
- [70] Spec 10A/ISO 10426-1: *Specifications for Cements and Materials for Well Cementing*
- [71] TR 10TR1: *Cement Sheath Evaluation*
- [72] API STANDARD 65—PART 2 *Isolating Potential Flow Zones During Well Construction (2d ed. Dec) 2010)*
- [73] Spec 11D/ISO 14310: *Petroleum and Natural Gas Industries — Downhole Equipment — Packers and Bridge Plugs*
- [74] Spec 15HR: *High Pressure Fiberglass Line Pipe*
- [75] Spec 15LR: *Low Pressure Fiberglass Line Pipe*
- [76] API. RP51R (R2013), *Environmental sound practices to promote protection of the environment in domestic onshore oil and gas production*
- [77] API. API Environmental Guidance Document: *Onshore Solid Waste Management in Exploration and Production Operations*

- [78] API. *Guidelines for Commercial Exploration and Production Waste Management Facilities*
- [79] BULLETIN A.P.I. E2, *Bulletin on Management of Naturally Occurring Radioactive Materials (NORM) in Oil and Gas Production*
- [80] BULLETIN A.P.I. E3, *Environmental Guidance Document: Well Abandonment and Inactive Well Practices for U.S. Exploration and Production Operations*
- [81] API Specification 7B-11C, *Specification for Internal-Combustion Reciprocating Engines for Oil-Field Service*
- [82] API Recommended Practice 7C-11F, *Recommended Practice for Installation, Maintenance, and Operation of Internal-Combustion Engines*
- [83] API Recommended Practice 11ER, *Recommended Practice for Guarding of Pumping Units*
- [84] BULLETIN API 11K, *Data Sheet for the Design of Air Exchange Coolers*
- [85] API Specification 11N, *Specification for Lease Automatic Custody Transfer (LACT) Equipment*
- [86] API Specification 12B, *Specification for Bolted Tanks for Storage of Production Liquids*
- [87] API Specification 12D, *Specification for Field Welded Tanks for Storage of Production Liquids*
- [88] API Specification 12F, *Specification for Shop Welded Tanks for Storage of Production Liquids*
- [89] API Specification 12J, *Specification for Oil and Gas Separators*
- [90] API Specification 12K, *Specification for Indirect Type Oilfield Heaters*
- [91] API Specification 12L, *Specification for Vertical and Horizontal Emulsion Treaters*
- [92] API Recommended Practice 12N, *Recommended Practice for the Operation, Maintenance and Testing of Firebox Flame Arresters*
- [93] API Specification 12P, *Specification for Fiberglass Reinforced Plastic Tanks*
- [94] API Recommended Practice 12R1, *Recommended Practice for Setting, Maintenance, Inspection, Operation, and Repair of Tanks in Production Service*
- [95] API Recommended Practice 49, *Recommended Practice for Drilling and Well Servicing Operations Involving Hydrogen Sulfide*
- [96] API Recommended Practice 53, *Recommended Practices for Blowout Prevention Equipment Systems for Drilling Wells*
- [97] API Recommended Practice 55, *Recommended Practices for Oil and Gas Producing and Gas Processing Plant Operations Involving Hydrogen Sulfide*
- [98] API Bulletin 75L, *Guidance Document for the Development of a Safety and Environmental Management System for Onshore Oil and Natural Gas Production Operations and Associated Activities*
- [99] API Recommended Practice 580, *Risk-Based Inspection, Third Edition*
- [100] API Recommended Practice 581, *Risk-Based Inspection Technology, Third Edition*
- [101] API Recommended Practice 2350, *Overfill Protection for Storage Tanks in Petroleum Facilities API Publication 4663, Remediation of Salt-Affected Soils at Oil and Gas Production Facilities*
- [102] NACE International. NACE RP 0475, *Selection of Metallic Materials to be used in All Phases of Water Handling for Injection into Oil-Bearing Formations*

- [103] NACE International. NACE Standard MR 0175, *Petroleum and Natural Gas Industries—Materials for Use in H₂S-containing Environments in Oil and Gas Production—Parts 1, 2 and 3*
- [104] International Organization for Standardization (ISO) Standards and Guides.
- [105] ISO 12039:2001, *Stationary source emissions — Determination of carbon monoxide, carbon dioxide and oxygen — Performance characteristics and calibration of automated measuring systems*
- [106] ISO 15649:2001, *Petroleum and natural gas industries — Piping*
- [107] ISO 10439:2002, *Petroleum, chemical and gas service industries — Centrifugal compressors*
- [108] ISO 13631:2002, *Petroleum and natural gas industries — Packaged reciprocating gas compressors*
- [109] ISO 21457:2010, *Petroleum, petrochemical and natural gas industries — Materials selection and corrosion control for oil and gas production systems*
- [110] ISO 10418, *Basic surface safety systems*
- [111] ISO 10423, *Petroleum and natural gas industries — Drilling and production equipment — Wellhead and christmas tree equipment*
- [112] ISO/TR 12489, *Petroleum, petrochemical and natural gas industries — Reliability modelling and calculation of safety systems*
- [113] ISO 13354, *Petroleum and natural gas industries — Drilling and production equipment — Shallow gas diverter equipment*
- [114] ISO 13533, *Petroleum and natural gas industries — Drilling and production equipment — Drill-through equipment*
- [115] ISO 13534, *Petroleum and natural gas industries — Drilling and production equipment — Inspection, maintenance, repair and remanufacture of hoisting equipment*
- [116] ISO 13535, *Petroleum and natural gas industries — Drilling and production equipment — Hoisting equipment*
- [117] ISO 13626, *Petroleum and natural gas industries — Drilling and production equipment — Drilling and well-servicing structures*
- [118] ISO 13702, *Petroleum and natural gas industries — Control and mitigation of fires and explosions on offshore production installations — Requirements and guidelines*
- [119] ISO 13703, *Petroleum and natural gas industries — Design and installation of piping systems on offshore production platforms*
- [120] ISO 14224, *Petroleum, petrochemical and natural gas industries — Collection and exchange of reliability and maintenance data for equipment*
- [121] ISO 14692 (all parts), *Petroleum and natural gas industries — Glass-reinforced plastics (GRP) piping*
- [122] ISO 14693, *Petroleum and natural gas industries — Drilling and well-servicing equipment*
- [123] ISO 15156-1, *Petroleum and natural gas industries — Materials for use in H₂S-containing environments in oil and gas production — Part 1: General principles for selection of cracking-resistant materials*
- [124] ISO 15156-2, *Petroleum and natural gas industries — Materials for use in H₂S-containing environments in oil and gas production — Part 2: Cracking-resistant carbon and low-alloy steels, and the use of cast irons*

- [125] ISO 15156-3, *Petroleum and natural gas industries — Materials for use in H₂S-containing environments in oil and gas production — Part 3: Cracking-resistant CRAs (corrosion-resistant alloys) and other alloys*
- [126] ISO 15138, *Petroleum and natural gas industries — Offshore production installations — Heating, ventilation and air-conditioning*
- [127] ISO 15544, *Petroleum and natural gas industries — Offshore production installations — Requirements and guidelines for emergency response*
- [128] ISO 15663, *Petroleum and natural gas industries — Life-cycle costing*
- [129] ISO 17776:2016, *Petroleum and natural gas industries — Offshore production installations — Major accident hazard management during the design of new installations*
- [130] ISO/TS 17969, *Petroleum, petrochemical and natural gas industries — Guidelines on competency management for well operations personnel*
- [131] ISO 20815, *Production assurance and reliability management*
- [132] ISO 23936-1, *Petroleum, petrochemical and natural gas industries — Non-metallic materials in contact with media related to oil and gas production — Part 1: Thermoplastics*
- [133] ISO 23936-2, *Petroleum, petrochemical and natural gas industries — Non-metallic materials in contact with media related to oil and gas production — Part 2: Elastomers*
- [134] ISO/TS 27469, *Petroleum, petrochemical and natural gas industries - Method of test for fire dampers*
- [135] ISO/TS 29001, *Petroleum, petrochemical and natural gas industries — Sector-specific quality management systems — Requirements for product and service supply organizations*
- [136] ISO 13624-1, *Petroleum and natural gas industries — Drilling and production equipment — Part 1: Design and operation of marine drilling riser equipment*
- [137] ISO/TR 13624-2, *Petroleum and natural gas industries — Drilling and production equipment — Part 2: Deepwater drilling riser methodologies, operations, and integrity technical report*
- [138] ISO 13625, *Petroleum and natural gas industries — Drilling and production equipment — Marine drilling riser couplings*
- [139] ISO 19901-7, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 7: Stationkeeping systems for floating offshore structures and mobile offshore units*
- [140] ISO 19904-1, *Floating offshore structures*
- [141] ISO 13628-1, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 1: General requirements and recommendations*
- [142] ISO 13628-2, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 2: Unbonded flexible pipe systems for subsea and marine applications*
- [143] ISO 13628-3, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 3: Through flowline (TFL) systems*
- [144] ISO 13628-4, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 4: Subsea wellhead and tree equipment*
- [145] ISO 13628-5, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 5: Subsea umbilicals*
- [146] ISO 13628-6, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 6: Subsea production control systems*

- [147] ISO 13628-7, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 7: Completion/workover riser systems*
- [148] ISO 13628-8, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 8: Remotely Operated Vehicle (ROV) interfaces on subsea production systems*
- [149] ISO 13628-9, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 9: Remotely Operated Tool (ROT) intervention systems*
- [150] ISO 13628-10, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 10: Specification for bonded flexible pipe*
- [151] ISO 13628-11, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 11: Flexible pipe systems for subsea and marine applications*
- [152] ISO 13628-15, *Petroleum and natural gas industries — Design and operation of subsea production systems — Part 15: Subsea structures and manifolds*
- [153] ISO 19900, *General requirements for offshore structures*
- [154] ISO 19901-1, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 1: Metocean design and operating considerations*
- [155] ISO 19901-2, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 2: Seismic design procedures and criteria*
- [156] ISO 19901-3, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 3: Topsides structure*
- [157] ISO 19901-4, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 4: Geotechnical and foundation design considerations*
- [158] ISO 19901-5, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 5: Weight control during engineering and construction*
- [159] ISO 19901-6, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 6: Marine operations*
- [160] ISO 19901-8, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 8: Marine soil investigations*
- [161] ISO 19902, *Amd 1 Fixed steel offshore structures (Amd)*
- [162] ISO 19903, *Fixed concrete offshore structures*
- [163] ISO 19905-1, *Petroleum and natural gas industries — Site-specific assessment of mobile offshore units — Part 1: Jack-ups*
- [164] ISO/TR 19905-2, *Petroleum and natural gas industries — Site-specific assessment of mobile offshore units — Part 2: Jack-ups commentary and detailed sample calculation*
- [165] ISO 19906, *Arctic offshore structures*
- [166] ISO/TR 10400, *Calculations for OCTG performance properties*
- [167] ISO 10405, *Petroleum and natural gas industries — Care and use of casing and tubing*
- [168] ISO 10407-1, *Drill stem design*
- [169] ISO 10407-2, *Petroleum and natural gas industries — Rotary drilling equipment — Part 2: Inspection and classification of used drill stem elements*

- [170] ISO 10414-1, *Petroleum and natural gas industries — Field testing of drilling fluids — Part 1: Water-based fluids*
- [171] ISO 10414-2, *Petroleum and natural gas industries — Field testing of drilling fluids — Part 2: Oil-based fluids*
- [172] ISO 10416, *Petroleum and natural gas industries — Drilling fluids — Laboratory testing*
- [173] ISO 10417, *Petroleum and natural gas industries — Subsurface safety valve systems — Design, installation, operation and redress*
- [174] ISO 10424-1, *Petroleum and natural gas industries — Rotary drilling equipment — Part 1: Rotary drill stem elements*
- [175] ISO 10424-2, *Petroleum and natural gas industries — Rotary drilling equipment — Part 2: Threading and gauging of rotary shouldered thread connections*
- [176] ISO 10426-1, *Petroleum and natural gas industries — Cements and materials for well cementing — Part 1: Specification*
- [177] ISO 10426-2, *Petroleum and natural gas industries — Cements and materials for well cementing — Part 2: Testing of well cements*
- [178] ISO 10426-3, *Testing of deepwater well cement*
- [179] ISO 10426-4, *Preparation and testing of atmospheric foamed cement slurries*
- [180] ISO 10426-5, *Petroleum and natural gas industries — Cements and materials for well cementing — Part 5: Determination of shrinkage and expansion of well cement formulations at atmospheric pressure*
- [181] ISO 10426-6, *Petroleum and natural gas industries — Cements and materials for well cementing — Part 6: Methods for determining the static gel strength of cement formulations*
- [182] ISO 10427-1, *Petroleum and natural gas industries — Equipment for well cementing — Part 1: Casing bow-spring centralizers*
- [183] ISO 10427-2, *Petroleum and natural gas industries — Equipment for well cementing — Part 2: Centralizer placement and stop-collar testing*
- [184] ISO 10427-3, *Petroleum and natural gas industries — Equipment for well cementing — Part 3: Performance testing of cementing float equipment*
- [185] ISO 10432, *Petroleum and natural gas industries — Downhole equipment — Subsurface safety valve equipment*
- [186] ISO 11960, *Casing and tubing for wells*
- [187] ISO 11961, *Drill pipe*
- [188] ISO 12835, *Qualification of casing connections for thermal wells*
- [189] ISO 13085, *Petroleum and natural gas industries — Aluminium alloy pipe for use as tubing for wells*
- [190] ISO 13500, *Petroleum and natural gas industries — Drilling fluid materials — Specifications and tests*
- [191] ISO 13501, *Petroleum and natural gas industries — Drilling fluids — Processing equipment evaluation*
- [192] ISO 13503-1, *Petroleum and natural gas industries — Completion fluids and materials — Part 1: Measurement of viscous properties of completion fluids*

- [193] ISO 13503-2, *Petroleum and natural gas industries — Completion fluids and materials — Part 2: Measurement of properties of proppants used in hydraulic fracturing and gravel-packing operations*
- [194] ISO 13503-3, *Petroleum and natural gas industries — Completion fluids and materials — Part 3: Testing of heavy brines*
- [195] ISO 13503-4, *Petroleum and natural gas industries — Completion fluids and materials — Part 4: Procedure for measuring stimulation and gravel-pack fluid leakoff under static conditions*
- [196] ISO 13503-5, *Petroleum and natural gas industries — Completion fluids and materials — Part 5: Procedures for measuring the long-term conductivity of proppants*
- [197] ISO 13503-6, *Petroleum and natural gas industries — Completion fluids and materials — Part 6: Procedure for measuring leakoff of completion fluids under dynamic conditions*
- [198] ISO 13678, *Petroleum and natural gas industries — Evaluation and testing of thread compounds for use with casing, tubing, line pipe and drill stem elements*
- [199] ISO 13679, *Casing and tubing connections testing*
- [200] ISO 13680, *Petroleum and natural gas industries — Corrosion-resistant alloy seamless tubes for use as casing, tubing and coupling stock — Technical delivery conditions*
- [201] ISO 14310, *Petroleum and natural gas industries — Downhole equipment — Packers and bridge plugs*
- [202] ISO 14998, *Petroleum and natural gas industries — Downhole equipment — Completion accessories*
- [203] ISO 15136-1, *Petroleum and natural gas industries — Progressing cavity pump systems for artificial lift — Part 1: Pumps*
- [204] ISO 15136-2, *Petroleum and natural gas industries — Progressing cavity pump systems for artificial lift — Part 2: Surface-drive systems*
- [205] ISO 15463, *Petroleum and natural gas industries — Field inspection of new casing, tubing and plain-end drill pipe*
- [206] ISO 15464, *Gauging and inspection of threads*
- [207] ISO 15546, *Petroleum and natural gas industries — Aluminium alloy drill pipe*
- [208] ISO 16070, *Petroleum and natural gas industries — Downhole equipment — Lock mandrels and landing nipples*
- [209] ISO/TS 16530-2, *Well integrity operational phase*
- [210] ISO 17078-1, *Petroleum and natural gas industries — Drilling and production equipment — Part 1: Side-pocket mandrels*
- [211] ISO 17078-2, *Petroleum and natural gas industries — Drilling and production equipment — Part 2: Flow-control devices for side-pocket mandrels*
- [212] ISO 17078-3, *Petroleum and natural gas industries — Drilling and production equipment — Part 3: Running tools, pulling tools and kick-over tools and latches for side-pocket mandrels*
- [213] ISO 17078-4, *Petroleum and natural gas industries — Drilling and production equipment — Part 4: Practices for side-pocket mandrels and related equipment*
- [214] ISO 17824, *Petroleum and natural gas industries — Downhole equipment — Sand screens*
- [215] ISO 20312, *Petroleum and natural gas industries — Design and operating limits of drill strings with aluminium alloy components*

- [216] ISO 27627, *Petroleum and natural gas industries — Aluminium alloy drill pipe thread connection gauging*
- [217] ISO 28781, *Petroleum and natural gas industries — Drilling and production equipment --Subsurface barrier valves and related equipment*
- [218] ISO 15551-1:2015, *Petroleum and natural gas industries — Drilling and production equipment — Part 1: Electric submersible pump systems for artificial lift*
- [219] ISO 16904:2016, *Petroleum and natural gas industries — Design and testing of LNG marine transfer arms for conventional onshore terminals*
- [220] ISO 17348:2016, *Petroleum and natural gas industries — Materials selection for high content CO₂ for casing, tubing and downhole equipment*
- [221] ISO 17349:2016, *Petroleum and natural gas industries — Offshore platforms handling streams with high content of CO₂ at high pressures*
- [222] ISO 17945:2015, *Petroleum, petrochemical and natural gas industries — Metallic materials resistant to sulfide stress cracking in corrosive petroleum refining environments*
- [223] ISO 18797-1:2016, *Petroleum, petrochemical and natural gas industries — External corrosion protection of risers by coatings and linings — Part 1: Elastomeric coating systems-polychloroprene or EPDM*
- [224] ISO Guide to the Expression of Uncertainty in Measurement. (JCGM 100:2008), EN ISO/IEC 17025, EN 14181, Stationary source emissions, EN 15259, Air quality, EN ISO/IEC 17025

Additional reference publications

- [225] ISO/TR 27912:2016, *Carbon dioxide capture — Carbon dioxide capture systems, technologies and processes*
- [226] ISO 27913:2016, *Carbon dioxide capture, transportation and geological storage — Pipeline transportation systems*
- [227] ISO 27914:2017, *Carbon dioxide capture, transportation and geological storage — Geological storage*
- [228] ISO/TR 27915:2017, *Carbon dioxide capture, transportation and geological storage — Quantification and verification*
- [229] ISO 27920²⁾, *Carbon dioxide capture, transportation and geological storage — Quantification and Verification*
- [230] ISO/TR 27918, *Lifecycle risk management for integrated CCS projects*
- [231] ISO 27917, *Carbon dioxide capture, transportation and geological storage — Vocabulary, cross cutting terms*
- [232] ISO 14064-1, *Greenhouse gases — Part 1: Specification with guidance at the organization level for quantification and reporting of greenhouse gas emissions and removals*
- [233] ISO 14064-2, *Greenhouse gases — Part 2: Specification with guidance at the project level for quantification, monitoring and reporting of greenhouse gas emission reductions or removal enhancements*
- [234] ISO 14064-3, *Greenhouse gases — Part 3: Specification with guidance for the validation and verification of greenhouse gas assertions*

Examples of relevant regulatory frameworks

2) Under preparation. Stage at the time of publication ISO/CD 27920:2018.

- [235] ENERGY A. 2007. Quantification Protocol for Enhanced Oil Recovery: <http://open.alberta.ca/publications/9780778572336> (undergoing review as of January 2018)
- [236] ALBERTA ENERGY. 2013. Carbon capture & storage: Summary Report of the Regulatory Framework Assessment: <http://www.energy.alberta.ca/CCS/pdfs/CCSrfaNoAppD.pdf>
- [237] European Union, EU CCS DIRECTIVE 2009/31/EC OF THE EUROPEAN PARLIAMENT AND OF THE COUNCIL of 23 April 2009, amendment to Council Directive 85/337/EEC and European Parliament and 1719 Council Directives 2000/60/EC, 2001/80/EC, 2004/35/EC, 2006/12/EC, 2008/1/EC, and Regulation (EC) No 1720 1013/2006, 2009. <http://eur-lex.europa.eu/LexUriServ/LexUriServ.do?uri=OJ:L:2009:140:0114:0135:EN:PDF>
- [238] European Union, 2009. Implementation of Directive 2009/31/EC: Geological Storage of Carbon Dioxide: http://ec.europa.eu/clima/policies/lowcarbon/ccs/implementation/documentation_en.htm
- Guidance Document 1: CO₂ Storage Life Cycle Risk Management Framework
- Guidance Document 2: Characterisation of the Storage Complex, CO₂ Stream Composition, Monitoring and Corrective Measures
- Guidance Document 3: Criteria for Transfer of Responsibility to the Competent Authority
- Guidance Document 4: Financial Security (Art. 19) and Financial Mechanism (Art. 20)
- [239] European Union, Directive 2003/87/EC of the European Parliament and of the Council of 13 October 2003 establishing a scheme for greenhouse gas emission allowance trading within the Community and amending Council Directive 96/61/EC (Text with EEA relevance)
- [240] European Union, Commission Regulation (EU) No. 601/2012 of 21 June 2012 on the monitoring and reporting of greenhouse gas emissions pursuant to Directive 2003/87/EC of the European Parliament and of the Council Text with EEA relevance
- [241] European Union, Directive 2010/75/EU of the European Parliament and of the Council of 24 November 2010 on industrial emissions (integrated pollution prevention and control) Text with EEA relevance
- [242] European Union, Commission Regulation (EU) No. 1193/2011 of 18 November 2011 establishing a Union Registry for the trading period commencing on 1 January 2013, and subsequent trading periods, of the Union emissions trading scheme pursuant to Directive 2003/87/EC of the European Parliament and of the Council and Decision No 280/2004/EC of the European Parliament and of the Council and amending Commission Regulations (EC) No 2216/2004 and (EU) No 920/2010 Text with EEA relevance
- [243] European Union, Commission Regulation (EC) No. 166/ 2006 of the European Parliament and of the Council concerning the establishment of a European Pollutant Release and Transfer Register and amending Council Directives 91/689/EEC and 96/61/EC
- [244] European Union, Commission Regulation (EU) No. 600/2012 on the verification of greenhouse gas emission reports and tonne-kilometre reports and the accreditation of verifiers pursuant to Directive 2003/87/EC of the European Parliament and of the Council
- [245] CALIFORNIA CARBON CAPTURE AND STORAGE REVIEW PANEL. 2010. Technical Advisory Committee Report, Enhanced Oil Recovery as Carbon Dioxide Sequestration, August 10, 2010: http://www.climatechange.ca.gov/carbon_capture_review_panel/meetings/2010-08-18/white_papers/Enhanced_Oil_Recovery_as_Carbon_Dioxide_Sequestration.pdf
- [246] CENTER FOR CLIMATE AND ENERGY SOLUTIONS. 2012. Greenhouse Gas Accounting Framework for Carbon Capture and Storage Projects: <http://www.c2es.org/publications/greenhouse-gas-accounting-framework-carbon-capture-and-storage-projects>

- [247] INTERNATIONAL ENERGY AGENCY. 2010. Carbon Capture and Storage: Model Regulatory Framework: <http://www.iea.org/topics/ccs/ccslegalandregulatoryissues/ccsmodelregulatoryframework/>
- [248] INTERSTATE OIL AND GAS COMPACT COMMISSION. 2010. A Policy, Legal, and Regulatory Evaluation of the Feasibility of a National Pipeline Infrastructure for the Transport and Storage of Carbon Dioxide: <http://www.sseb.org/wp-content/uploads/2010/05/pipeline.pdf>
- [249] Oklahoma Corporation Commission. 2016, Oil and Gas Conservation: *Oklahoma Register*, v. 33, no. 23, p. 569-1138
- [250] State of Mississippi, 2013. Mississippi Geologic Sequestration of Carbon Dioxide Act, Miss. Code Ann) § 53-11-1
- [251] State of Texas. 2011. Title 16, Texas Administrative Code, Part 1, Chapter 5. Carbon Dioxide (CO₂), Subchapter C. Certification Of Geologic Storage Of Anthropogenic Carbon Dioxide (CO₂) Incidental to Enhanced Recovery Of Oil, Gas, Or Geothermal Resources, 16 TAC §§5.301-5.308. See also: 36 Texas Register 4397-4402 (July 8, 2011)
- [252] U.S. ENVIRONMENTAL PROTECTION AGENCY. 2015. 40 CFR Part 146, Subpart C — Criteria and Standards Applicable to Class II Wells: <https://www.gpo.gov/fdsys/pkg/CFR-2015-title40-vol23/pdf/CFR-2015-title40-vol23-part146-subpartC.pdf>
- [253] WYOMING OIL AND GAS CONSERVATION COMMISSION. (2015-Current): <http://wogcc.state.wy.us/wogcchelp/commission.html>

Additional recommended reading:

- [254] AKBARABADI M., & PIRI M. in-press. Co-sequestration of SO₂ with supercritical CO₂ in Carbonates: An experimental study of capillary trapping, relative permeability, and capillary pressure, *Advances in Water Resources*:
- [255] AKBARABADI M., & PIRI M. Relative permeability hysteresis and capillary trapping characteristics of supercritical CO₂/brine systems: An experimental study at reservoir conditions. *Advances in Water Resources*, Volume 52, Pages 190–206. 2013
- [256] BENSON S.M., & COLE D.R. CO₂ Sequestration in Deep Sedimentary Formations, *ELEMENTS*, Vol. 4, pp. 325-331. 2008. DOI:10.2113/gselements.4.5.325
- [257] GILFILLAN STUART MV. Solubility trapping in formation water as dominant CO₂ sink in natural gas fields." *Nature* 458.7238: 614-618. 2009
- [258] IEAGHG. Quantification Techniques for CO₂ Leakage, 2012/02 (January, 2012)
- [259] INTERNATIONAL ASSOCIATION OF OIL & GAS PRODUCERS. 2014. Standards Bulletin No. 15: <http://www.iogp.org/bookstore/product/standards-bulletin-15/>
- [260] IEA Greenhouse Gas R&D Programme (Prepared by Advanced Resources International, Inc. and Melzer Consulting), 2009. CO₂ Storage in Depleted Oilfields: Global Application Criteria for Carbon Dioxide Enhanced Oil Recovery, Report IEA/CON/08/155 <http://www.CO2storage.org/Reports/2009-12.pdf>
- [261] INTERGOVERNMENTAL PANEL ON CLIMATE CHANGE. Special Report: Carbon Dioxide Capture and Storage, (ed. Metz, et al.) (2005): <https://www.ipcc.ch/report/carbon-dioxide-capture-and-storage/>
- [262] INTERGOVERNMENTAL PANEL ON CLIMATE CHANGE. 2006 IPCC Guidelines for National Greenhouse Gas Inventories. (ed. Eggleston, et al.) (2006): <http://www.ipcc-nggip.iges.or.jp/public/2006gl/>
- [263] MIT Energy Initiative and Bureau of Economic Geology at UT Austin Symposium, 2012. The Role of Enhanced Oil Recovery in Accelerating the Deployment of Carbon Capture and Sequestration: <https://energy.mit.edu/wp-content/uploads/2010/07/MITEI-RP-2010-003.pdf>

- [264] PENTLAND C.H., EL-MAGHRABY R., IGLAUER S., BLUNT M.J. Measurements of the capillary trapping of supercritical carbon dioxide in Berea sandstone. *Geophys Res Letters*, **38**, p.L06401. 2011
- [265] U.K. DEPARTMENT OF ENERGY & CLIMATE CHANGE (DECC). Office of Carbon Capture & Storage (prepared by Advanced Resources International, Inc. and Melzer Consulting), 2010. Optimization of CO₂ Storage in CO₂ Enhanced Oil Recovery Projects: <https://www.gov.uk/government/publications/optimization-of-co2-storage-in-co2-enhanced-oil-recovery-projects>
- [266] U.S. Department of Energy/National Energy Technology Laboratory. Best Practices for Monitoring, [Verification, and Accounting of CO₂ Stored in Deep Geologic Formations — 2012 Update, DOE/NETL- 2012/ 1568 (October 2012) (2d ed.)
- [267] U.S. DEPARTMENT OF ENERGY/NATIONAL ENERGY TECHNOLOGY LABORATORY. (prepared by Advanced Resources International), 2011. Improving Domestic Energy Security and Lowering CO₂ Emissions with “Next Generation” CO₂-Enhanced Oil Recovery (CO₂-EOR), report DOE/NETL-2011/1504: http://www.netl.doe.gov/energy-analyses/pubs/NextGen_CO2_EOR_06142011.pdf
- [268] U.S. ENVIRONMENTAL PROTECTION AGENCY. Key Principles in EPA's Underground Injection Control Program Class VI Rule Related to Transition of Class II Enhanced Oil or Gas Recovery Wells to Class VI (April 23, 2015): https://www.epa.gov/sites/production/files/2015-07/documents/class2eorclass6memo_1.pdf

