

**Degree of BEng/MEng in Chemical Engineering**

**CP203 Thermodynamics and Chemical Principles**

**Date: Monday 9<sup>th</sup> May 2016**

**Time: 09:30-12:30  
Duration: 3 hours**

**Answer All Questions**

**Answer each section in a separate booklet**

**There are 200 marks available in each section of the paper**

**Calculators must not be used to store text and/or formulae nor be capable of communication. Invigilators may require calculators to be re-set.**

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## Section A: Answer All Questions

- QA1.** An ideal gas is expanded isothermally in a closed and frictionless piston/cylinder apparatus to 2.5 times its initial volume, producing in the process  $2.4 \text{ kJ mol}^{-1}$  of work. Calculate the temperature of the gas inside the cylinder. [10 marks]
- QA2.** 7 moles of methane are initially at a pressure of 2 bar and a temperature of 290 K. Calculate the enthalpy change of a process after which the gas has a pressure of 6 bar and a temperature of 420 K. You can make use of the fact that the enthalpy is a function of state to define a convenient path for the process. You can also assume that under these conditions methane behaves ideally and has heat capacities of  $c_P = 35.7 \text{ J mol}^{-1} \text{ K}^{-1}$  and  $c_V = 27.4 \text{ J mol}^{-1} \text{ K}^{-1}$ . [20 marks]
- QA3.** 42 moles of pure hydrogen gas and 17 moles of pure oxygen gas are first mixed at a constant temperature of  $60^\circ\text{C}$  and a constant pressure of 2 bar. The mixture is then cooled isobarically to a temperature of  $25^\circ\text{C}$ . Calculate the total entropy change for the process of mixing and cooling.  
You can assume ideal mixture behaviour. Heat capacities for the gases are  $c_P(\text{H}_2) = 29.2 \text{ J mol}^{-1} \text{ K}^{-1}$  and  $c_P(\text{O}_2) = 29.7 \text{ J mol}^{-1} \text{ K}^{-1}$ . [25 marks]
- QA4.** Derive an expression for the change in molar enthalpy with molar volume at constant temperature of a gas described by the van der Waals equation of state. [20 marks]
- QA5.** A heat pump uses an ideal gas to keep an exam venue warm (at  $25^\circ\text{C}$ ) during a typical Scottish summer (outside temperature of  $0^\circ\text{C}$ ). The following facts are known about the four-step cycle of operation of the heat pump:
- i) The first and third steps are adiabatic and involve gas expansion and gas compression, respectively;
  - ii) During the second step, involving isothermal expansion, the entropy of the gas increases by  $50 \text{ J K}^{-1}$ ;
  - iii) The fourth step involves isothermal gas compression, and consumes 20 kJ of work.
- Calculate the coefficient of performance of the heat pump and compare it to the corresponding coefficient of performance for a Carnot heat pump operating between the same two temperatures. [30 marks]

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- QA6.** A liquid mixture of acetone (component 1) and acetonitrile (component 2) is in equilibrium with its vapour in a closed vessel at 60°C. If the mole fraction of acetone in the vapour is 0.35, calculate the composition of the liquid phase, assuming that the mixture behaves ideally.

Pure component equilibrium for each of the two species is given by the following Antoine equations, where pressure is in kPa and temperature is in °C:

$$\ln(P_1^{sat}) = 14.5463 - \frac{2940.46}{T + 237.22}$$

$$\ln(P_2^{sat}) = 14.2724 - \frac{2945.47}{T + 224.00}$$

[20 marks]

- QA7.** Integrate the Clapeyron equation for vapour-liquid equilibrium assuming that the liquid molar volume is negligible compared to the vapour molar volume, and that the vapour is well described by the virial expansion below, with coefficient  $B = -0.045 \text{ bar}^{-1}$ :

$$Z = 1 + BP$$

Use the expression you obtained to estimate the boiling temperature of water at 7 bar, making use of the fact that water boils at  $T = 99.6^\circ\text{C}$  at  $P = 1 \text{ bar}$ . The enthalpy of vapourisation of water over the relevant range of conditions can be considered constant and equal to  $38.9 \text{ kJ mol}^{-1}$ .

[30 marks]

- QA8.** A stream of pure carbon dioxide gas initially at  $T = 300 \text{ K}$  and  $P = 8 \text{ bar}$  is throttled adiabatically through a valve, such that its pressure drops by 6 bar. Calculate the temperature of the stream after passing the valve, assuming that there is no work done in the throttling process and that the molar volume is inversely proportional to the pressure with constant  $a = 2500 \text{ J mol}^{-1}$ :

$$v = \frac{a}{P}$$

Within the relevant range of pressure and temperature, you may assume that  $c_P = 37.5 \text{ J/molK}$  and  $\alpha = 0.0035 \text{ K}^{-1}$  are constants. [25 marks]

- QA9.** A reversible adiabatic turbine accepts steam at 5 bar and  $280^\circ\text{C}$ . The steam leaves the turbine at 3.5 bar. Using the steam tables provided, calculate the molar work produced by the turbine and the outlet temperature of the steam. You may ignore kinetic and potential energy changes during the process.

[20 marks]

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## NUMERICAL SOLUTIONS

**QA1.** 315 K

**QA2.** 32.5 kJ

**QA3.** 102.4 J/K

**QA4.**  $\left(\frac{\partial h}{\partial v}\right)_T = \frac{2a}{v^2} - \frac{RTb}{(v-b)^2}$

**QA5.**  $\beta = 3.15$ ;  $\beta_{ID} = 11.93$

**QA6.**  $x_1 = 0.202$

**QA7.** 430.2 K

**QA8.** 296 K

**QA9.** -1.55 kJ/mol; 236 °C

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## Thermodynamics Equation Sheet

All symbols have the meaning as given in class materials.

First Law (general)

$$\Delta U = Q + W - \Delta\left(\frac{1}{2}mv^2\right) - \Delta(mgz)$$

Gibbs phase rule

$$F = 2 - \pi + N$$

Thermal expansion coefficient

$$\alpha = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

Isothermal compressibility

$$\beta = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

Heat capacities

$$C_V = \left( \frac{\partial U}{\partial T} \right)_V = T \left( \frac{\partial S}{\partial T} \right)_V$$

$$C_P = \left( \frac{\partial H}{\partial T} \right)_P = T \left( \frac{\partial S}{\partial T} \right)_P$$

$$C_P - C_V = T \left( \frac{\partial V}{\partial T} \right)_P \left( \frac{\partial P}{\partial T} \right)_V$$

Van der Waals equation of state

$$P = \frac{RT}{v-b} - \frac{a}{v^2}$$

Virial equation of state

$$Z = 1 + \frac{B}{v} + \frac{C}{v^2} + \frac{D}{v^3} + \dots$$

Thermodynamic potentials

$$H = U + PV$$

$$A = U - TS$$

$$G = H - TS$$

Fundamental thermodynamic relations

$$dU = TdS - PdV$$

$$dH = TdS + VdP$$

$$dA = -SdT - PdV$$

$$dG = -SdT + VdP$$

Maxwell equations

$$\left( \frac{\partial T}{\partial V} \right)_S = - \left( \frac{\partial P}{\partial S} \right)_V$$

$$\left( \frac{\partial T}{\partial P} \right)_S = \left( \frac{\partial V}{\partial S} \right)_P$$

$$\left( \frac{\partial S}{\partial P} \right)_T = - \left( \frac{\partial V}{\partial T} \right)_P$$

$$\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial P}{\partial T} \right)_V$$

Internal energy and enthalpy

$$\left( \frac{\partial U}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V - P$$

$$\left( \frac{\partial U}{\partial P} \right)_T = -T \left( \frac{\partial V}{\partial T} \right)_P - P \left( \frac{\partial V}{\partial P} \right)_T$$

$$\left( \frac{\partial H}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V + V \left( \frac{\partial P}{\partial V} \right)_T$$

$$\left( \frac{\partial H}{\partial P} \right)_T = -T \left( \frac{\partial V}{\partial T} \right)_P + V$$

Carnot relationship

$$\left| \frac{Q_1}{Q_2} \right| = \frac{T_1}{T_2}$$

Entropy

$$\Delta S = \int_1^2 \frac{dQ_{\text{rev}}}{T}$$

$$dS = \frac{C_P}{T} dT - \left( \frac{\partial V}{\partial T} \right)_P dP$$

$$\Delta S_{\text{IG}} = C_P \ln \frac{T_2}{T_1} - nR \ln \frac{P_2}{P_1}$$

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## Thermodynamics Equation Sheet

Joule-Thomson coefficient

$$\left(\frac{\partial T}{\partial P}\right)_H = \frac{V}{C_P}(\alpha T - 1)$$

Phase equilibrium

$$\frac{dP^{sat}}{dT_b} = \frac{\Delta h}{T_b \Delta v}$$

$$\frac{dP^{sat}}{dT_b} = \frac{\Delta h P^{sat}}{RT_b^2}$$

$$\ln P^{sat} = A - \frac{B}{T_b + C}$$

Multi-component systems ( $m$  or  $M$  stand for any extensive property)

$$dU = TdS - PdV + \sum_{i=1} \mu_i dn_i$$

$$\mu_i = \left(\frac{\partial G}{\partial n_i}\right)_{T,P,n_j}$$

$$m = \sum_i x_i \bar{m}_i$$

$$\Delta M_{\text{Mix}} = \sum_i n_i \bar{m}_i - \sum_i n_i m_i^0$$

$$\sum_i x_i d\bar{m}_i = 0$$

Ideal mixture

$$\mu_i = \mu_i^0 + RT \ln x_i$$

$$U = \sum_i n_i u_i^0$$

$$H = \sum_i n_i h_i^0$$

$$V = \sum_i n_i v_i^0$$

$$S = \sum_i n_i s_i^0 - nR \sum_i x_i \ln x_i$$

$$G = \sum_i n_i \mu_i^0 + nRT \sum_i x_i \ln x_i$$

$$Py_i = P_i^{sat} x_i$$

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# Thermodynamics Steam Tables

		TEMPERATURE: $t$ °C (TEMPERATURE: $T$ kelvins)									
$P$ /kPa ( $t^{\text{sat}}$ /°C)		sat. liq.	sat. vap.	75 (348.15)	100 (373.15)	125 (398.15)	150 (423.15)	175 (448.15)	200 (473.15)	225 (498.15)	250 (523.15)
1 (6.98)	$V$	1.000	129200.	160640.	172180.	183720.	195270.	206810.	218350.	229890.	241430.
	$U$	29.334	2385.2	2480.8	2516.4	2552.3	2588.5	2624.9	2661.7	2698.8	2736.3
	$H$	29.335	2514.4	2641.5	2688.6	2736.0	2783.7	2831.7	2880.1	2928.7	2977.7
	$S$	0.1060	8.9767	9.3828	9.5136	9.6365	9.7527	9.8629	9.9679	10.0681	10.1641
10 (45.83)	$V$	1.010	14670.	16030.	17190.	18350.	19510.	20660.	21820.	22980.	24130.
	$U$	191.822	2438.0	2479.7	2515.6	2551.6	2588.0	2624.5	2661.4	2698.6	2736.1
	$H$	191.832	2584.8	2640.0	2687.5	2735.2	2783.1	2831.2	2879.6	2928.4	2977.4
	$S$	0.6493	8.1511	8.3168	8.4486	8.5722	8.6888	8.7994	8.9045	9.0049	9.1010
20 (60.09)	$V$	1.017	7649.8	8000.0	8584.7	9167.1	9748.0	10320.	10900.	11480.	12060.
	$U$	251.432	2456.9	2478.4	2514.6	2550.9	2587.4	2624.1	2661.0	2698.3	2735.8
	$H$	251.453	2609.9	2638.4	2686.3	2734.2	2782.3	2830.6	2879.2	2928.0	2977.1
	$S$	0.8321	7.9094	7.9933	8.1261	8.2504	8.3676	8.4785	8.5839	8.6844	8.7806
30 (69.12)	$V$	1.022	5229.3	5322.0	5714.4	6104.6	6493.2	6880.8	7267.5	7653.8	8039.7
	$U$	289.271	2468.6	2477.1	2513.6	2550.2	2586.8	2623.6	2660.7	2698.0	2735.6
	$H$	289.302	2625.4	2636.8	2685.1	2733.3	2781.6	2830.0	2878.7	2927.6	2976.8
	$S$	0.9441	7.7695	7.8024	7.9363	8.0614	8.1791	8.2903	8.3960	8.4967	8.5930
40 (75.89)	$V$	1.027	3993.4	.....	4279.2	4573.3	4865.8	5157.2	5447.8	5738.0	6027.7
	$U$	317.609	2477.1	.....	2512.6	2549.4	2586.2	2623.2	2660.3	2697.7	2735.4
	$H$	317.650	2636.9	.....	2683.8	2732.3	2780.9	2829.5	2878.2	2927.2	2976.5
	$S$	1.0261	7.6709	.....	7.8009	7.9268	8.0450	8.1566	8.2624	8.3633	8.4598
50 (81.35)	$V$	1.030	3240.2	.....	3418.1	3654.5	3889.3	4123.0	4356.0	4588.5	4820.5
	$U$	340.513	2484.0	.....	2511.7	2548.6	2585.6	2622.7	2659.9	2697.4	2735.1
	$H$	340.564	2646.0	.....	2682.6	2731.4	2780.1	2828.9	2877.7	2926.8	2976.1
	$S$	1.0912	7.5947	.....	7.6953	7.8219	7.9406	8.0526	8.1587	8.2598	8.3564
75 (91.79)	$V$	1.037	2216.9	.....	2269.8	2429.4	2587.3	2744.2	2900.2	3055.8	3210.9
	$U$	384.374	2496.7	.....	2509.2	2546.7	2584.2	2621.6	2659.0	2696.7	2734.5
	$H$	384.451	2663.0	.....	2679.4	2728.9	2778.2	2827.4	2876.6	2925.8	2975.3
	$S$	1.2131	7.4570	.....	7.5014	7.6300	7.7500	7.8629	7.9697	8.0712	8.1681
100 (99.63)	$V$	1.043	1693.7	.....	1695.5	1816.7	1936.3	2054.7	2172.3	2289.4	2406.1
	$U$	417.406	2506.1	.....	2506.6	2544.8	2582.7	2620.4	2658.1	2695.9	2733.9
	$H$	417.511	2675.4	.....	2676.2	2726.5	2776.3	2825.9	2875.4	2924.9	2974.5
	$S$	1.3027	7.3598	.....	7.3618	7.4923	7.6137	7.7275	7.8349	7.9369	8.0342
101.325 (100.00)	$V$	1.044	1673.0	.....	1673.0	1792.7	1910.7	2027.7	2143.8	2259.3	2374.5
	$U$	418.959	2506.5	.....	2506.5	2544.7	2582.6	2620.4	2658.1	2695.9	2733.9
	$H$	419.064	2676.0	.....	2676.0	2726.4	2776.2	2825.8	2875.3	2924.8	2974.5
	$S$	1.3069	7.3554	.....	7.3554	7.4860	7.6075	7.7213	7.8288	7.9308	8.0280
125 (105.99)	$V$	1.049	1374.6	.....	.....	1449.1	1545.6	1641.0	1735.6	1829.6	1923.2
	$U$	444.224	2513.4	.....	.....	2542.9	2581.2	2619.3	2657.2	2695.2	2733.3
	$H$	444.356	2685.2	.....	.....	2724.0	2774.4	2824.4	2874.2	2923.9	2973.7
	$S$	1.3740	7.2847	.....	.....	7.3844	7.5072	7.6219	7.7300	7.8324	7.9300
150 (111.37)	$V$	1.053	1159.0	.....	.....	1204.0	1285.2	1365.2	1444.4	1523.0	1601.3
	$U$	466.968	2519.5	.....	.....	2540.9	2579.7	2618.1	2656.3	2694.4	2732.7
	$H$	467.126	2693.4	.....	.....	2721.5	2772.5	2822.9	2872.9	2922.9	2972.9
	$S$	1.4336	7.2234	.....	.....	7.2953	7.4194	7.5352	7.6439	7.7468	7.8447
175 (116.06)	$V$	1.057	1003.34	.....	.....	1028.8	1099.1	1168.2	1236.4	1304.1	1371.3
	$U$	486.815	2524.7	.....	.....	2538.9	2578.2	2616.9	2655.3	2693.7	2732.1
	$H$	487.000	2700.3	.....	.....	2719.0	2770.5	2821.3	2871.7	2921.9	2972.0
	$S$	1.4849	7.1716	.....	.....	7.2191	7.3447	7.4614	7.5708	7.6741	7.7724
200 (120.23)	$V$	1.061	885.44	.....	.....	897.47	959.54	1020.4	1080.4	1139.8	1198.9
	$U$	504.489	2529.2	.....	.....	2536.9	2576.6	2615.7	2654.4	2692.9	2731.4
	$H$	504.701	2706.3	.....	.....	2716.4	2768.5	2819.8	2870.5	2920.9	2971.2
	$S$	1.5301	7.1268	.....	.....	7.1523	7.2794	7.3971	7.5072	7.6110	7.7096
225 (123.99)	$V$	1.064	792.97	.....	.....	795.25	850.97	905.44	959.06	1012.1	1064.7
	$U$	520.465	2533.2	.....	.....	2534.8	2575.1	2614.5	2653.5	2692.2	2730.8
	$H$	520.705	2711.6	.....	.....	2713.8	2766.5	2818.2	2869.3	2919.9	2970.4
	$S$	1.5705	7.0873	.....	.....	7.0928	7.2213	7.3400	7.4508	7.5551	7.6540
250 (127.43)	$V$	1.068	718.44	.....	.....	.....	764.09	813.47	861.98	909.91	957.41
	$U$	535.077	2536.8	.....	.....	.....	2573.5	2613.3	2652.5	2691.4	2730.2
	$H$	535.343	2716.4	.....	.....	.....	2764.5	2816.7	2868.0	2918.9	2969.6
	$S$	1.6071	7.0520	.....	.....	.....	7.1689	7.2886	7.4001	7.5050	7.6042
275 (130.60)	$V$	1.071	657.04	.....	.....	.....	693.00	738.21	782.55	826.29	869.61
	$U$	548.564	2540.0	.....	.....	.....	2571.9	2612.1	2651.6	2690.7	2729.6
	$H$	548.858	2720.7	.....	.....	.....	2762.5	2815.1	2866.8	2917.9	2968.7
	$S$	1.6407	7.0201	.....	.....	.....	7.1211	7.2419	7.3541	7.4594	7.5590
300 (133.54)	$V$	1.073	605.56	.....	.....	.....	633.74	675.49	716.35	756.60	796.44
	$U$	561.107	2543.0	.....	.....	.....	2570.3	2610.8	2650.6	2689.9	2729.0
	$H$	561.429	2724.7	.....	.....	.....	2760.4	2813.5	2865.5	2916.9	2967.9
	$S$	1.6716	6.9909	.....	.....	.....	7.0771	7.1990	7.3119	7.4177	7.5176

$V$  = SPECIFIC VOLUME  $\text{cm}^3 \text{g}^{-1}$   
 $U$  = SPECIFIC INTERNAL ENERGY  $\text{kJ kg}^{-1}$   
 $H$  = SPECIFIC ENTHALPY  $\text{kJ kg}^{-1}$   
 $S$  = SPECIFIC ENTROPY  $\text{kJ kg}^{-1} \text{K}^{-1}$

# Thermodynamics Steam Tables

		TEMPERATURE: $t\text{ }^{\circ}\text{C}$ (TEMPERATURE: $T$ kelvins)									
$P/\text{kPa}$ ( $t^{\text{sat}}/^{\circ}\text{C}$ )		sat. liq.	sat. vap.	150 (423.15)	175 (448.15)	200 (473.15)	220 (493.15)	240 (513.15)	260 (533.15)	280 (553.15)	300 (573.15)
325 (136.29)	V	1.076	561.75	583.58	622.41	660.33	690.22	719.81	749.18	778.39	807.47
	U	572.847	2545.7	2568.7	2609.6	2649.6	2681.2	2712.7	2744.0	2775.3	2806.6
	H	573.197	2728.3	2758.4	2811.9	2864.2	2905.6	2946.6	2987.5	3028.2	3069.0
	S	1.7004	6.9640	7.0363	7.1592	7.2729	7.3585	7.4400	7.5181	7.5933	7.6657
350 (138.87)	V	1.079	524.00	540.58	576.90	612.31	640.18	667.75	695.09	722.27	749.33
	U	583.892	2548.2	2567.1	2608.3	2648.6	2680.4	2712.0	2743.4	2774.8	2806.2
	H	584.270	2731.6	2756.3	2810.3	2863.0	2904.5	2945.7	2986.7	3027.6	3068.4
	S	1.7273	6.9392	6.9982	7.1222	7.2366	7.3226	7.4045	7.4828	7.5581	7.6307
375 (141.31)	V	1.081	491.13	503.29	537.46	570.69	596.81	622.62	648.22	673.64	698.94
	U	594.332	2550.6	2565.4	2607.1	2647.7	2679.6	2711.3	2742.8	2774.3	2805.7
	H	594.737	2734.7	2754.1	2808.6	2861.7	2903.4	2944.8	2985.9	3026.9	3067.8
	S	1.7526	6.9160	6.9624	7.0875	7.2027	7.2891	7.3713	7.4499	7.5254	7.5981
400 (143.62)	V	1.084	462.22	470.66	502.93	534.26	558.85	583.14	607.20	631.09	654.85
	U	604.237	2552.7	2563.7	2605.8	2646.7	2678.8	2710.6	2742.2	2773.7	2805.3
	H	604.670	2737.6	2752.0	2807.0	2860.4	2902.3	2943.9	2985.1	3026.2	3067.2
	S	1.7764	6.8943	6.9285	7.0548	7.1708	7.2576	7.3402	7.4190	7.4947	7.5675
425 (145.82)	V	1.086	436.61	441.85	472.47	502.12	525.36	548.30	571.01	593.54	615.95
	U	613.667	2554.8	2562.0	2604.5	2645.7	2678.0	2709.9	2741.6	2773.2	2804.8
	H	614.128	2740.3	2749.8	2805.3	2859.1	2901.2	2942.9	2984.3	3025.5	3066.6
	S	1.7990	6.8739	6.8965	7.0239	7.1407	7.2280	7.3108	7.3899	7.4657	7.5388
450 (147.92)	V	1.088	413.75	416.24	445.38	473.55	495.59	517.33	538.83	560.17	581.37
	U	622.672	2556.7	2560.3	2603.2	2644.7	2677.1	2709.2	2741.0	2772.7	2804.4
	H	623.162	2742.9	2747.7	2803.7	2857.8	2900.2	2942.0	2983.5	3024.8	3066.0
	S	1.8204	6.8547	6.8660	6.9946	7.1121	7.1999	7.2831	7.3624	7.4384	7.5116
475 (149.92)	V	1.091	393.22	393.31	421.14	447.97	468.95	489.62	510.05	530.30	550.43
	U	631.294	2558.5	2558.6	2601.9	2643.7	2676.3	2708.5	2740.4	2772.2	2803.9
	H	631.812	2745.3	2745.5	2802.0	2856.5	2899.1	2941.1	2982.7	3024.1	3065.4
	S	1.8408	6.8365	6.8369	6.9667	7.0850	7.1732	7.2567	7.3363	7.4125	7.4858
500 (151.84)	V	1.093	374.68	.....	399.31	424.96	444.97	464.67	484.14	503.43	522.58
	U	639.569	2560.2	.....	2600.6	2642.7	2675.5	2707.8	2739.8	2771.7	2803.5
	H	640.116	2747.5	.....	2800.3	2855.1	2898.0	2940.1	2981.9	3023.4	3064.8
	S	1.8604	6.8192	.....	6.9400	7.0592	7.1478	7.2317	7.3115	7.3879	7.4614
525 (153.69)	V	1.095	357.84	.....	379.56	404.13	423.28	442.11	460.70	479.11	497.38
	U	647.528	2561.8	.....	2599.3	2641.6	2674.6	2707.1	2739.2	2771.2	2803.0
	H	648.103	2749.7	.....	2798.6	2853.8	2896.8	2939.2	2981.1	3022.7	3064.1
	S	1.8790	6.8027	.....	6.9145	7.0345	7.1236	7.2078	7.2879	7.3645	7.4381
550 (155.47)	V	1.097	342.48	.....	361.60	385.19	403.55	421.59	439.38	457.00	474.48
	U	655.199	2563.3	.....	2598.0	2640.6	2673.8	2706.4	2738.6	2770.6	2802.6
	H	655.802	2751.7	.....	2796.8	2852.5	2895.7	2938.3	2980.3	3022.0	3063.5
	S	1.8970	6.7870	.....	6.8900	7.0108	7.1004	7.1849	7.2653	7.3421	7.4158
575 (157.18)	V	1.099	328.41	.....	345.20	367.90	385.54	402.85	419.92	436.81	453.56
	U	662.603	2564.8	.....	2596.6	2639.6	2672.9	2705.7	2738.0	2770.1	2802.1
	H	663.235	2753.6	.....	2795.1	2851.1	2894.6	2937.3	2979.5	3021.3	3062.9
	S	1.9142	6.7720	.....	6.8664	6.9880	7.0781	7.1630	7.2436	7.3206	7.3945
600 (158.84)	V	1.101	315.47	.....	330.16	352.04	369.03	385.68	402.08	418.31	434.39
	U	669.762	2566.2	.....	2595.3	2638.5	2672.1	2705.0	2737.4	2769.6	2801.6
	H	670.423	2755.5	.....	2793.3	2849.7	2893.5	2936.4	2978.7	3020.6	3062.3
	S	1.9308	6.7575	.....	6.8437	6.9662	7.0567	7.1419	7.2228	7.3000	7.3740
625 (160.44)	V	1.103	303.54	.....	316.31	337.45	353.83	369.87	385.67	401.28	416.75
	U	676.695	2567.5	.....	2593.9	2637.5	2671.2	2704.2	2736.8	2769.1	2801.2
	H	677.384	2757.2	.....	2791.6	2848.4	2892.3	2935.4	2977.8	3019.9	3061.7
	S	1.9469	6.7437	.....	6.8217	6.9451	7.0361	7.1217	7.2028	7.2802	7.3544
650 (161.99)	V	1.105	292.49	.....	303.53	323.98	339.80	355.29	370.52	385.56	400.47
	U	683.417	2568.7	.....	2592.5	2636.4	2670.3	2703.5	2736.2	2768.5	2800.7
	H	684.135	2758.9	.....	2789.8	2847.0	2891.2	2934.4	2977.0	3019.2	3061.0
	S	1.9623	6.7304	.....	6.8004	6.9247	7.0162	7.1021	7.1835	7.2611	7.3355
675 (163.49)	V	1.106	282.23	.....	291.69	311.51	326.81	341.78	356.49	371.01	385.39
	U	689.943	2570.0	.....	2591.1	2635.4	2669.5	2702.8	2735.6	2768.0	2800.3
	H	690.689	2760.5	.....	2788.0	2845.6	2890.1	2933.5	2976.2	3018.5	3060.4
	S	1.9773	6.7176	.....	6.7798	6.9050	6.9970	7.0833	7.1650	7.2428	7.3173
700 (164.96)	V	1.108	272.68	.....	280.69	299.92	314.75	329.23	343.46	357.50	371.39
	U	696.285	2571.1	.....	2589.7	2634.3	2668.6	2702.1	2735.0	2767.5	2799.8
	H	697.061	2762.0	.....	2786.2	2844.2	2888.9	2932.5	2975.4	3017.7	3059.8
	S	1.9918	6.7052	.....	6.7598	6.8859	6.9784	7.0651	7.1470	7.2250	7.2997
725 (166.38)	V	1.110	263.77	.....	270.45	289.13	303.51	317.55	331.33	344.92	358.36
	U	702.457	2572.2	.....	2588.3	2633.2	2667.7	2701.3	2734.3	2767.0	2799.3
	H	703.261	2763.4	.....	2784.4	2842.8	2887.7	2931.5	2974.6	3017.0	3059.1
	S	2.0059	6.6932	.....	6.7404	6.8673	6.9604	7.0474	7.1296	7.2078	7.2827



