

Mechanical Engineering Project

Report

# STUDY OF LINEAR AND NON-LINEAR DYNAMIC VIBRATION ABSORBER

*Submitted in partial fulfillment of  
the requirements for the award of the degree of*

**Bachelor of Technology**  
**in**  
**Mechanical Engineering**

Submitted by

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May 2017

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## *Declaration*

The dissertation entitled ‘**Study of Linear and Non-linear Dynamic Vibration Absorber**’ is our own work carried out under the guidance of Prof. A. Chatterjee, Professor, Department of Mechanical Engineering, VNIT, Nagpur.

This work in the same form or in any other form is not submitted for the award of any degree/diploma to any other institute/university.

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## *Certificate*

This is to certify that the dissertation  
**“Study of Linear and Non-linear Dynamic Vibration Absorber”**  
has been successfully completed in the session 2016-2017 in a satisfactory  
manner as a fulfilment of the requirement for the degree of “Bachelor of  
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# ACKNOWLEDGEMENT

Success is never a single man's entity. This dissertation would not have been a real fulfilment without the backing and cooperation from various individuals through various mean. It is our pleasure to thank all those who made this thesis possible.

In the first place we would like to record our deepest appreciation and gratitude to our project guide Prof. A. Chatterjee, Professor, Department of Mechanical Engineering, VNIT, Nagpur, for his invaluable guidance and support throughout the project work. The present form of the work is all about his expertise in a vast domain and sincere desire to bring out the best of the students capabilities. Without his guidance and persistence help this dissertation would have not been possible. We are indebted to him more than he knows.

We are also thankful to our fellow B.Tech students, well-wishers and all those who directly or indirectly contributed to the successful realization of this dissertation, and express my apology to not being mentioned personally all of them.

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## CHAPTER 1

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### Introduction

## 1.1 Introduction

The dynamic vibration absorber (DVA) or tuned-mass damper (TMD) is a widely used passive vibration control device. Dynamic Vibration Absorbers (DVA) are based on the concept of attaching a secondary mass to a primary vibrating system such that the secondary mass dissipates the energy and thus reduce the amplitude of vibration of the primary system. A simple DVA consists of a mass and a spring. When a mass spring system or a primary system is excited by a harmonic force, its vibration can be suppressed by attaching a DVA as shown in Fig.1.1.

However, adding a DVA to a one-degree-of-freedom (dof) system results in a new 2-dof system. If the exciting frequency coincides with one of the two natural frequencies of the new system, the system will be at resonance. To overcome this problem, a damper is added to DVA. Figure 1.1 shows a primary system attached by a damped DVA.

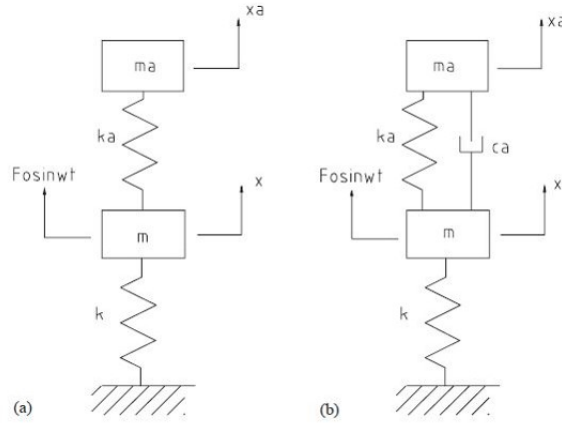


Figure 1.1: A simple dynamic vibration absorber

Equations of motion of the system are given as:

$$m_1 \ddot{x}_1 + k_1 x_1 + c_1 \dot{x}_1 + k_2(x_1 - x_2) + c_2(\dot{x}_1 - \dot{x}_2) = F_0 \sin(\omega * t) \quad (1.1)$$

$$m_2 \ddot{x}_2 + k_2(x_2 - x_1) + c_2(\dot{x}_2 - \dot{x}_1) = 0 \quad (1.2)$$

However, adding a Dynamic Vibration Absorber (DVA) to a one-degree-of-freedom (dof) system results in a new two-degree-of-freedom system. If the exciting frequency coincides one of the two natural frequencies of the new system, the system will be at resonance.

The vibration response of a single DOF system is compared with a system having a DVA without a damper, as shown in Fig 1.2 and a graph showing the effect of mass ratio(absorber mass by main mass) on the creation of two new

natural frequencies is shown in Fig 1.3. It can be seen that as mass ratio increases the two new frequencies are pushed further apart.

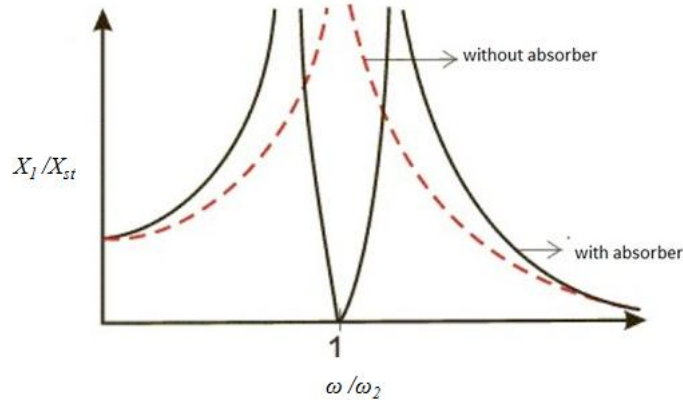


Figure 1.2: Change in response on addition of DVA without a damper

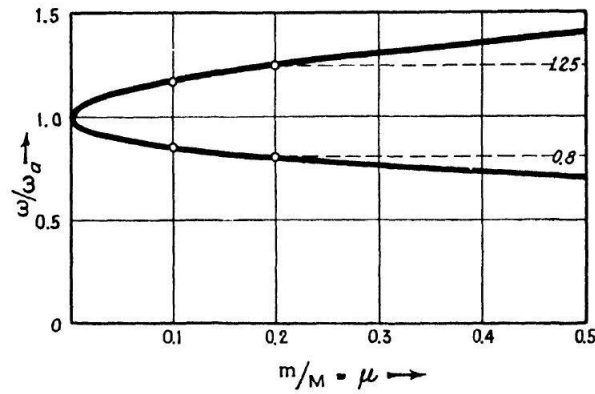


Figure 1.3: Effect of mass ratio on natural frequencies

## 1.2 Applications:

Tuned mass dampers are largely used in vibration control of crankshafts, hand-held devices and transmission cables.

### 1.2.1 Damping of hand-held devices

Hair clipper, dry shavers, and hand-held devices alike use electromagnetic motors to power themselves. Usually, the motor operates at a fixed frequency such as 60Hz. The figure 1.4 shows a typical electric hair clipper. In such hair-clippers, an electro-magnet is used to develop vibrating force for cutting. However, this also generates an unpleasant vibration of the housing. This vibration is neutralized

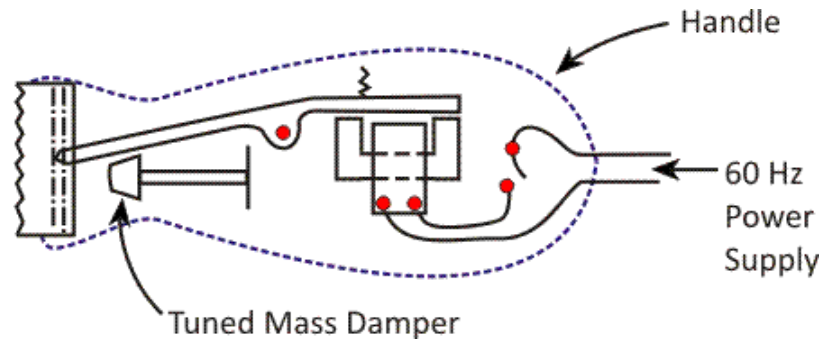


Figure 1.4: A typical electrical hair clipper

by the application of a pair of mass dampers fixed to the housing at two different points.

### 1.2.2 Floor vibration control

Wide column spans along with the use of high strength material (less of which would provide the needed structural integrity) tend to make modern composite floors flexible and oscillatory. Human activities (walking, running, dancing, etc.) and operating machines can induce high levels of vibration in such floors.

Floor vibration in a building are considered harmful due to several reasons:

1. Impair the operation of sensitive instruments
2. Affect human psychology for acceleration level even greater than  $0.005g$
3. Motion having peak amplitude greater than 1 mm is not desirable in active environments

Traditional methods for improving the environment include:

1. Adding extra columns
2. Adding extra thickness to the floors and
3. Increasing structural stiffening

Reactive damping, provided by attaching tuned mass dampers (TMDs) to the floor, is commonly used for treating vibrating floors. Negligible weight penalty, low cost, and ease of installation make TMDs the most practical, cost-effective, and least disruptive floor vibration control solution for both new and existing floor systems.



Figure 1.5: Two tuned mass dampers installed underneath a floor

### 1.2.3 Houdaille damper

A tuned viscous torsional damper referred to as the Houdaille damper or viscous Lanchester damper can be used to reduce the torsional oscillations of the crankshaft. A Houdaille damper can be used to reduce the vibration in rotating

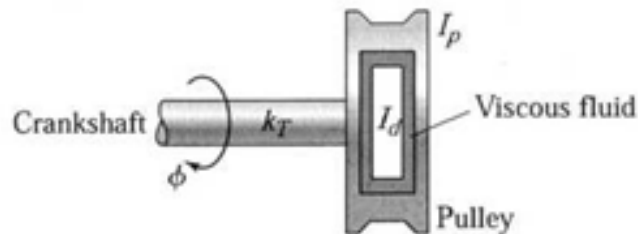


Figure 1.6: Figure showing Houdaille damper

systems, such as in engine installations where the operation speed may vary over a wide range. As shown in figure 1.6, the damper consists of a disk. The disk is free to rotate inside a housing which is attached to the rotating shaft, and the housing and the rotating shaft are assumed to have equivalent mass moment of inertia. The space between the housing and the disk is filled with viscous fluid. In most cases, the fluid is a silicon oil whose viscosity is of similar magnitude to oil but which does not change significantly when the temperature changes. The damping effect is produced by the viscosity of the oil and is proportional to the relative angular velocity between the housing and the disk.

### 1.2.4 Vibration control of structures

Mass damper is a device mounted on structures such as buildings or bridges to reduce the amplitude of the structures due to the vibrational motions induced by periodic or non-periodic dynamic loading. It operates effectively to prevent internal discomfort and damage as well as the outright structural failures. The installed mass damper moves in opposition to the resonance frequency oscillations of the structure by means of pendulum, spring or fluid. Mass damper that counter-reacts the movement of building guarantees the safety of buildings when subjected to strong wind blow or light seismic wave. These passive vibration control systems

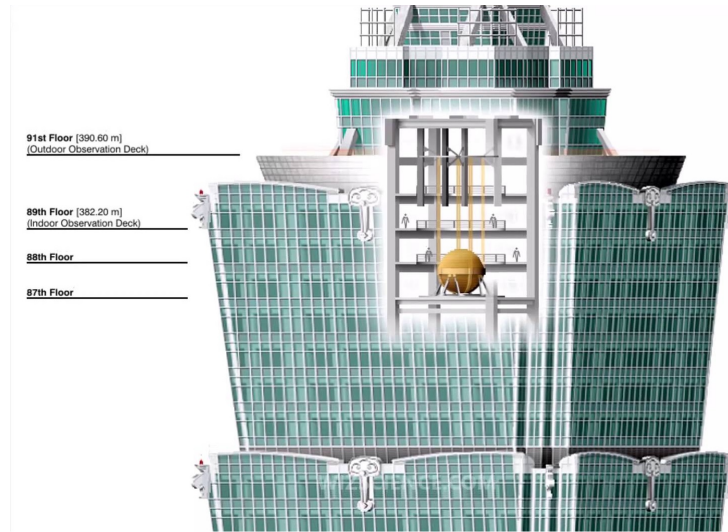


Figure 1.7: Tuned mass damper atop Taipei 101

have been widely utilized in many high-rise building structures particularly those located at seismically active zone. These include Taipei 101 at Taiwan and One Rincon Hill at U.S.A.

### 1.2.5 Wind turbines

A standard tuned mass damper for wind turbines consists of an auxiliary mass which is attached to the main structure by means of springs and dashpot elements. The natural frequency of the tuned mass damper is basically defined by its spring constant and the damping ratio determined by the dashpot. The tuned parameter of the tuned mass damper enables the auxiliary mass to oscillate with a phase shift with respect to the motion of the structure. In a typical configuration an auxiliary mass hung below the nacelle of a wind turbine supported by dampers or friction plates.

### 1.2.6 Optical Disk Drives

Demands for higher read/write speeds of optical disk drives (ODDs) have resulted in an increase in the rotational speed of the drive, which has led to greater vibration from the spindle motor. This, in turn, requires a higher servo gain of the pickup actuator, which leads to write failures in CDs and DVDs. The increased vibration also produces an unpleasant sensation for users of mobile equipment with integrated ODDs. Thus, additional mechanisms, such as dynamic vibration absorber (DVA), mass balancer, or auto-ball balancer, are required to decrease the vibration. The DVA is the most popular of these because of its low price and its effectiveness in reducing vibration.

## 1.3 Thesis Outline

There are four design variables involved while designing a DVA, objective being to minimize the vibration amplitude of the main mass over the operating frequency. The four design variables involved are the mass ratio( $\mu$ ), stiffness of the spring( $k_2$ ), the damping between primary mass and the absorber mass( $\zeta_2$ ) and the damping in the primary mass( $\zeta_1$ ) which is usually independent and is specified over which designer doesn't have much control over.

The basic outline of this thesis is:

- i) In chapter 2 we have discussed the effect in the absence of damper in the primary system, the optimum design parameters for the DVA. We have explored the two-point theory proposed by Den Hartog for closed form solution, Den Hartog's derivation is based on a very peculiar observation that for different values of secondary mass damping the curve always passes through 2 fixed points. In second case when DVA is present in both primary and absorber mass, a search for optimal parameters is done. But in this case a closed form solution cannot be obtained, hence numerical methods are adapted for selection of optimized parameters.
- ii) In the Chapter 3 we have considered the addition of coulomb damper between the primary mass and the absorber mass. A numerical search was done to find the optimum frictional force and the FRF generated in this case was compared with the FRF of optimum viscous damper
- iii) In Chapter 4 we had added cubic non-linearity in both primary mass and



secondary mass and obtained the parameters for obtaining an optimum FRF and compared it with the linear case. We had also tabulated effects of various parameters on the response of primary system.

- iv) In Chapter 5 we have used an analytical method called the Harmonic Balance Method for solving non linear differential equations present before us when non linearity is present in the system.

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## CHAPTER 2

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### Literature Review

## 2.1 Linear Dynamic Vibration Absorber

i) Randall and Taylor (1981)

- Randall and Taylor in this paper proposed a numerical search of optimal parameters when primary mass damping is present.
- The maximum amplitude response is a function of frequency and four design parameters  $f(\zeta_1, \zeta_2, \mu, f)$ ,  $\zeta_1$  is an independent parameter specified by the primary system.
- Of the three remaining parameters  $(\zeta_2, \mu, f)$  the mass ratio is the most probable to be specified in a design and will therefore is considered as a second independent parameter and search for optimal  $\zeta_2$  and  $f$  is carried out.

As shown below in fig 2.1, Randall and Taylor did a 3-dimensional search for optimal values and the results are shown below-

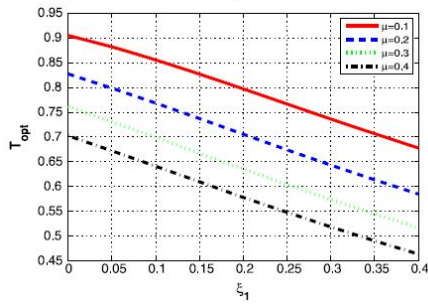


Figure 2.1: optimal  $f$  and  $\zeta_1$  as a function of  $\mu$

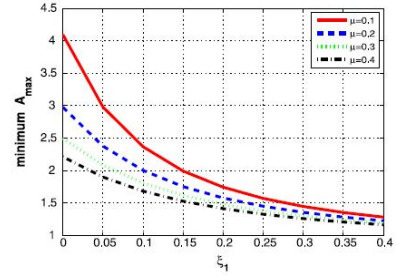


Figure 2.2: Maximum vibrational amplitude for optimum  $\zeta_1$

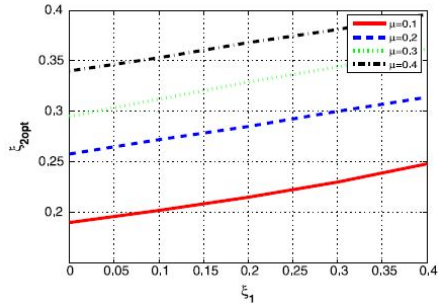


Figure 2.3: optimal  $\zeta_2$  and  $\zeta_1$  as a function of  $\mu$

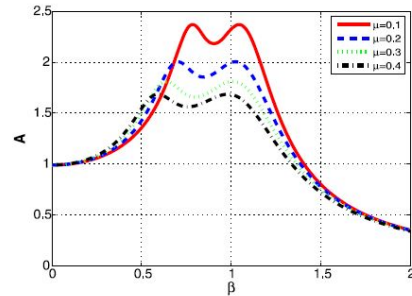


Figure 2.4: FRF

ii) Rana and Soong(**1998**)

This paper takes into account both primary and secondary mass damping. They studied the effects of detuning of some of the optimal DVA parameters on the performance of the vibration absorber.

Some of the conclusions are:

- The detuning effect of natural frequency of absorber is more pronounced than that of absorber damping.
- With increasing damping of the main mass, the effect of detuning becomes less severe.
- With increasing mass ratio also, the effect of detuning becomes less severe.

iii) R.L. Mayes And N. A. Mowbray (**1974**)

Paper takes a combination of Coulomb friction and viscous damping and equates the work done per cycle of coulomb friction to equivalent viscous damper, this is the method that we had adapted while working with Coulomb damper.

Some of the conclusions are:

- This paper gives us a method to determine the fraction of viscous and coulomb damping present in the structure and compares the effect of taking equivalent viscous damping.
- The effect on response of structure by combined damping is 10-48 percent higher than the result obtained through equivalent damping.

iv) Kifu Liu and Jie Liu(**2004**)

Studies in the field of DVA has tried to reduce the vibration of primary system, that is by looking for possibilities such as changing the type of damping or spring that is used. Benchmark being the optimum solution for FRF as suggested by Den Hartog without primary mass damping, which was later extended to system with primary mass damping, as discussed in earlier sections.

In 2004 Kifu Liu and Jie Liu came up with an optimum FRF for a system that was better than the Optimum FRF as suggested by Den Hartog. They worked on the two configuration of damper, instead of introducing a damper between the primary mass and the secondary mass, they attached the damper between ground and the secondary mass as shown in 2.5. This configuration of attachment is called as skyhook damper and groundhook damper based on the inertial frame where the other end of the damper is attached.

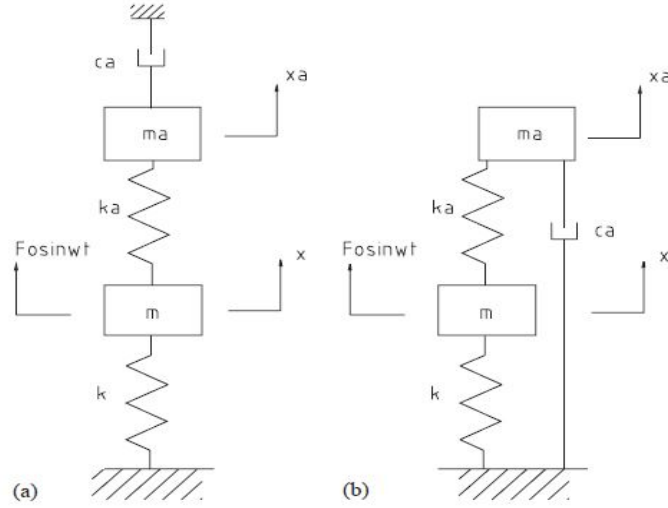


Figure 2.5: Configuration of skyhook and ground hook damper

They studied the groundhook and skyhook damper and compared the optimal value for vibration suppression with the Den Hartog optimal value for a simple DVA. They used the same concept of fixed point theory for deriving analytical solution. It was found out that, overall by changing the configuration, the results were better as shown in 2.6 In this thesis our work follows along the same

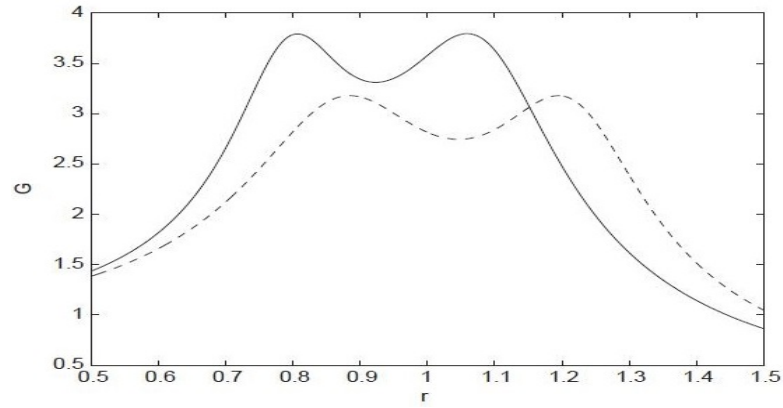


Figure 2.6: Comparison of FRF's

line, we have explored the effect that coulomb damper has on the vibration of primary mass and compared the optimum FRF's of coulomb and viscous dampers, then we had introduced cubic non-linear spring in both primary and secondary system, obtained their optimum FRF's. We have explored the various parameters that a designer can exploit to suppress vibration as much as possible.

## 2.2 Non-linearity in the System

- i) J.C. Ji, N.Zhang(2009) - Journal of Sound and Vibration

The paper presented found that the primary resonance response of a nonlinear oscillator can be suppressed by a linear vibration absorber which consists of a relatively light mass attached to the nonlinear oscillator by a linear damper and a linear spring. The small attachment of light mass can absorb vibrational energy without significantly modifying the nonlinear oscillator and adversely affecting its performance. The stiffness of the linked spring is much lower than the linear stiffness of the nonlinear oscillator itself. The contributions of the absorber stiffness and damping to the linear stiffness and damping of the nonlinear primary system can be considered as a perturbation. Thus the linearised natural frequencies of the nonlinear primary oscillator before and after addition of vibration absorber change only slightly.

The effects of the parameters of the massspringdamper absorber on the vibration suppression of the nonlinear oscillator have been studied. It has been found that a larger coupling damping results in a larger reduction of primary resonance vibrations.

- ii) R.A. Borges, V.Steffen (2007) - 19th International Congress of Mechanical Engineering, Brasilia

In this work, a damped nonlinear dynamic vibration absorber is studied. The nonlinear effect is introduced in the system by nonlinear springs. Then, the main purpose is to verify the nonlinear effects, intended to increase the efficiency of the DVA into the frequency band of interest. Equation of motion of the nonlinear DVA are presented. The steady state response of the system is determined using Krylov-Bogoliubov method, which yields four nonlinear equations that are solved to obtain the solution. The effect of adding nonlinear dynamic vibration absorber with hardening and softening spring is illustrated. The effect of changing non-dimensional coefficient of nonlinearity ( $\epsilon_1$  and  $\epsilon_2$ ) is shown in figure 2.7. In the end some numerical examples are presented to evaluate the performance of the optimal nonlinear DVA.

- iii) Yung-Sheng Hsu, Neil S Ferguson (2013) The aforementioned paper investigates the physical behaviour and effectiveness of a nonlinear dynamic vibration absorber(NLDVA). The nonlinear absorber considered involves a nonlinear hardening spring which was designed and attached to a cantilever beam excited by a shaker. The cantilever beam can be considered at low frequen-

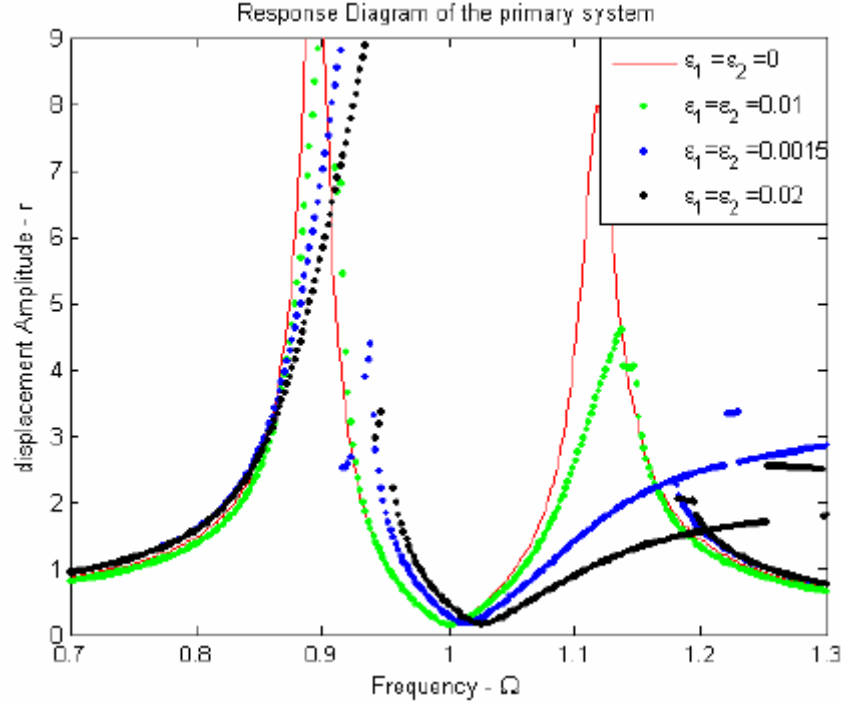


Figure 2.7: Effect of  $\zeta_1$  and  $\zeta_2$  on the system response

cies as a linear single degree-of-freedom system. The nonlinear attachment is designed to behave as a hardening Duffing oscillator. It investigated the potential for vibration reduction of the system. Analytical and numerical results are presented and compared. From the measured results it was observed that the NLDVA (Non-linear Dynamic Vibration Absorber) had a much wider effective bandwidth compared to a linear absorber. The frequency response curve of the NLDVA has the effect of moving the second resonant peak to a higher frequency away from the tuned frequency so that the device is robust to detuning. Experimental results have been presented to compare with the model derived.

iv) S. Natsiavas (**1992**)

The paper presents an analysis for determining the steady state response of dynamic vibration absorbers, for which both the machine and the absorber are assumed to possess a non-linear, Duffing type, stiffness. The harmonic steady state response is first determined by assuming weakly non-linear conditions and applying the method of averaging. The analysis is applied and numerical results are obtained for several combinations of the system parameters, in an effort to gain a better understanding of the effect of these parameters on the system response. Utilizing information from the amplitude of the solutions

obtained, as well as their stability characteristics, it is shown that proper selection of the system parameters results in substantial improvements of the technical performance of non-linear absorbers and avoids dangerous effects that are possible to occur due to the presence of the non-linearities. It is shown that absorbers with hardening/softening springs may result in considerable reduction of the vibration amplitudes in frequency ranges greater/less than the original resonance. The present study is useful in trying to eliminate instability effects systematically, without losing the advantages brought about by the non-linearities, by properly adjusting the parameters of the system.

In this thesis we have concentrated on the effects of non-linearity on the system. Most of the work in this field has either tried analytical, genetic algorithm or neural network to obtain the response of primary system in presence of non-linearity. We have tried to use an alternate approach of solving the non-linear coupled equations using 4th order Runge Kutta method. We have explored the possibility of obtaining an optimum FRF using when cubic non-linear hardening spring is present. We were able to show that when a small amount of non-linearity is present in the spring of primary mass, the optimum design parameters changes and the Frequency Response Function that is obtained is having lower peaks than the optimum Frequency Response Function in case of linear spring. Most of the work has also tried to counteract the non-linearity in the primary mass with a non-linear dynamic vibration absorber. A part of our work also concentrates on the possibility of using a linear dynamic vibration absorber along with non-linear stiffness in the primary mass.



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## CHAPTER 3

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# Linear Dynamic Vibration Absorber

### 3.1 Dynamic vibration absorber without primary mass damping

The first mathematical theory on the damped DVA was presented by Ormondroyd and Den Hartog. The mathematical model of a primary mass system attached with a damped DVA is given by-

$$m_1\ddot{x}_1 + k_1x_1 + c_1\dot{x}_1 + k_2(x_1 - x_2) + c_2(\dot{x}_1 - \dot{x}_2) = F_0\sin(\omega * t) \quad (3.1)$$

$$m_2\ddot{x}_2 + k_2(x_2 - x_1) + c_2(\dot{x}_2 - \dot{x}_1) = 0 \quad (3.2)$$

Den Hartog derived closed form expressions for optimum damper parameters. He assumed no damping to be present in the main mass to facilitate the derivations. Den Hartog's derivation is based on a very peculiar observation that for different values of secondary mass damping the curve always passes through 2 fixed points as can be seen from 3.1. Firstly, the closed form solution for the vibration

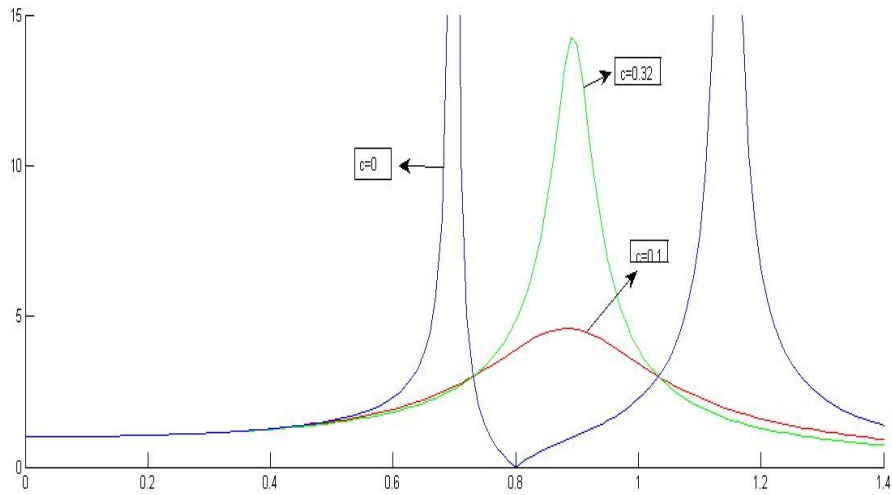


Figure 3.1: For three values of  $C_2$  it can be shown that FRF's pass through 2 fixed points

response of primary system was derived and this was later used to obtain closed form optimal solution.

The closed form solution was obtained in the non-dimensional parameters as it helped in understanding how the vibrational response depended on various parameters, for example-the effect on  $x_1$  if  $F_0$  is doubled and also by introducing

non-dimensional parameters, the number of variables can be reduced.

$$\frac{x_1}{x_{st}} = \sqrt{\frac{(2\frac{c}{c_c}g)^2 + (g^2 - f^2)^2}{(2\frac{c}{c_c}g)^2(g^2 - 1 + \mu g^2)^2 + [\mu f^2 g^2 - (g^2 - 1)(g^2 - f^2)]^2}} \quad (3.3)$$

where  $\mu = m/M = \text{absorber mass} / \text{main mass}$

$w_a = k/m = \text{natural frequency of absorber}$

$\Omega_n^2 = K/M = \text{natural frequency of main system}$

$f = w_a/\Omega_n = \text{frequency ratio (natural frequency)}$

$g = w/\Omega_n = \text{forced frequency ratio}$

$x_{st} = P_0/K = \text{static deflection system}$

$c_c = 2m\Omega_n = \text{"critical" damping}$

That is the amplitude ratio  $\frac{x_1}{x_{st}}$  of the main mass is a function of four variables  $\mu, f, g$  and  $\frac{c}{c_c}$ . It is interesting to follow what happens for increasing damping. When the damping becomes infinite, the two masses are virtually clamped together and we have a single-degree-of-freedom system. In adding the absorber to the system, the objective is to bring the resonant peak of the amplitude down to its lowest possible value. With  $c_2 = 0$ , the peak is infinite at the resonant frequency ( $g=1$ ); with  $c = \infty$  it is again infinite. Somewhere in between there must be a value of  $c$  for which the peak becomes a minimum. As can be seen from 3.1, irrespective of damping the FRF always pass through two points and this is no accident. If we can calculate their location, our problem is practically solved, because the most favourable curve is the one which passes with a horizontal tangent through the highest of the two fixed points P or Q. The best obtainable "resonant amplitude" (at optimum damping) is the ordinate of that point. Even this is not all that can be done. By changing the relative tuning  $f = \frac{\omega_a}{\omega_n}$  of the damper with respect to the main system, the two fixed points P and Q can be shifted up and down the curve for  $c = 0$ . By changing  $f$ , one point goes up and the other down. Clearly the most favourable case is such that first by a proper choice of  $f$  the two fixed points are adjusted to equal heights, and second by a proper choice of  $\frac{c}{c_c}$  the curve is adjusted to pass with a horizontal tangent through one of them. By adapting the above said procedure, the frequency ratio, damping co-efficient and amplitude ratio is given by:

$$f = \frac{1}{1 + \mu} \quad (3.4)$$

$$\frac{x_1}{x_{st}} = \sqrt{\frac{2}{1 + \mu}} \quad (3.5)$$

### 3.2 Dynamic vibration absorber with primary mass damping

When we add a viscous damper in the primary system, alongside the viscous damper in DVA, the response of the system changes. The resultant system is shown in Fig

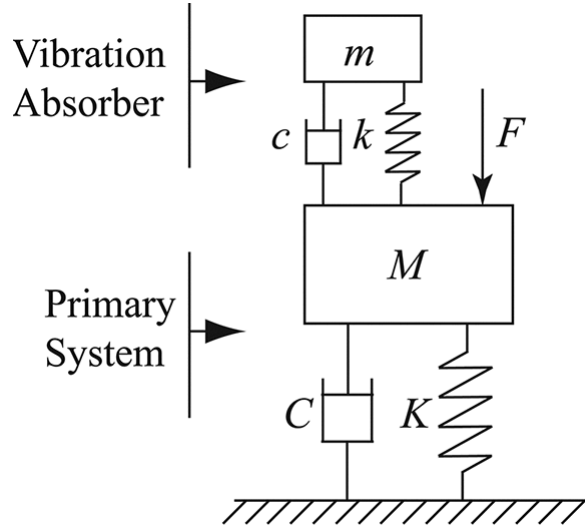


Figure 3.2: The main mass and the DVA, both are damped

The governing equations yield the solution:

$$\frac{X_1}{X_{st}} = \frac{\sqrt{(1 - r_{f2}^2)^2 + 4(\zeta_2 r_{f2})^2}}{\Delta} \quad (3.6)$$

$$\frac{X_2}{X_{st}} = \frac{\sqrt{1 + 4(\zeta_2 r_{f2})^2}}{\Delta} \quad (3.7)$$

$$\text{where } \Delta = \{[r_{f1}^2 r_{f2}^2 - (r_{f2}^2 + r_{f1}^2(1 + \mu) + 4\zeta_1 \zeta_2 r_{f1} r_{f2}) + 1]^2 + 4[\zeta_1 r_{f1} + \zeta_1 r_{f1} - (\zeta_1 r_{f1} r_{f2}^2 + \zeta_2 r_{f2} r_{f1}^2(1 + \mu))]^2\}^{\frac{1}{2}} \quad (3.8)$$

$$r_{f_1} = \frac{\omega}{\sqrt{K_1/m_1}} \quad (3.9)$$

$$r_{f_2} = \frac{\omega}{\sqrt{K_2/m_2}} \quad (3.10)$$

$$\mu = \frac{m_2}{m_1} \quad (3.11)$$

$$\zeta_1 = \frac{c_1}{2\sqrt{K_1/m_1}} \quad (3.12)$$

$$\zeta_2 = \frac{c_2}{2\sqrt{K_2/m_2}} \quad (3.13)$$

As we can expect the addition of viscous damping in main mass bring additional terms involving main mass damping ( $\zeta_1$ ) in the solution. If we set these terms to zero ( $\zeta_1 = 0$ ), we obtain the previously mentioned analytical solution when primary mass damping is zero.

Using the analytical solution obtained above, Frequency Response Function (FRF) is plotted which is shown in Fig. 3.3

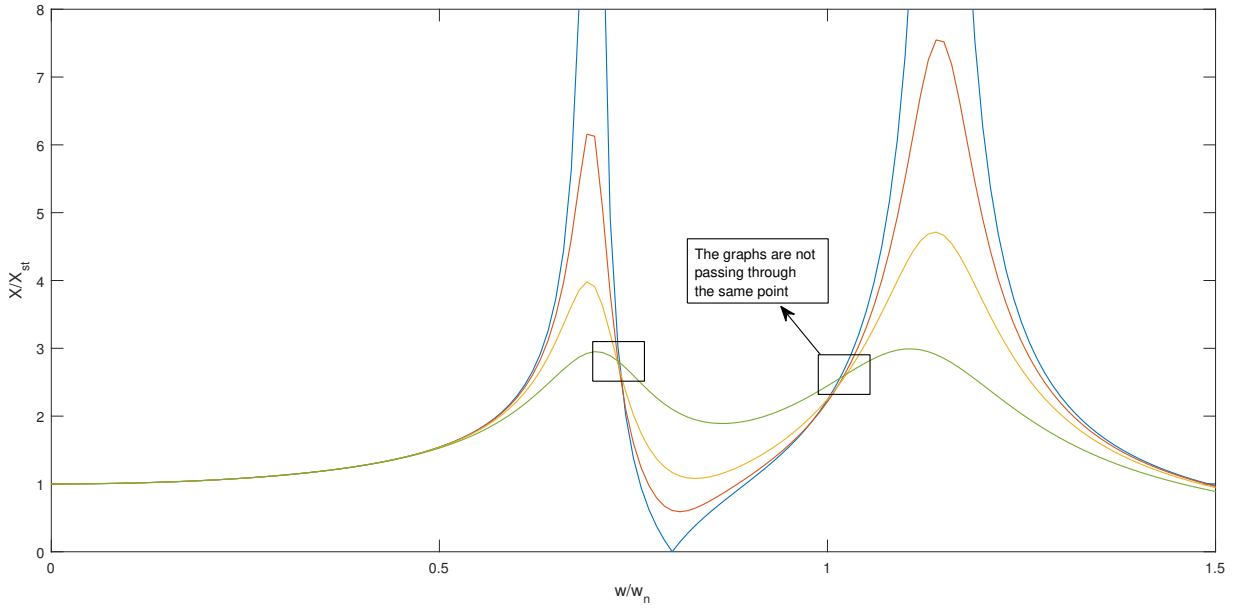


Figure 3.3: The graphs are not passing through a fixed point

The most important observation from the plot is that: the graphs are not passing through a fixed point. Hence, we cannot use ‘fixed point theory’ for finding analytically, the optimal parameters to the system, as we had done earlier for the case with damping present only in DVA.

In absence of an analytical solution, a numerical approach is adopted. The basic premise of the numerical technique is to evaluate the response of the system over a range of frequency ratio ( $f$ ) and secondary mass damping( $\zeta_2$ ). The primary mass damping ( $\zeta_1$ ) is kept constant because real life systems do not provide control

over their damping. Hence, we have to work with whatever damping is present in the primary system. Mass ratio is also kept constant.

The numerical search is visually shown through the surface generated as shown in Fig. 3.4. The lowest point on the surface represents optimal solution for the given system whose parameters are given in Table 3.2, along with optimum values of  $f$  and  $\zeta_2$  obtained from numerical search.

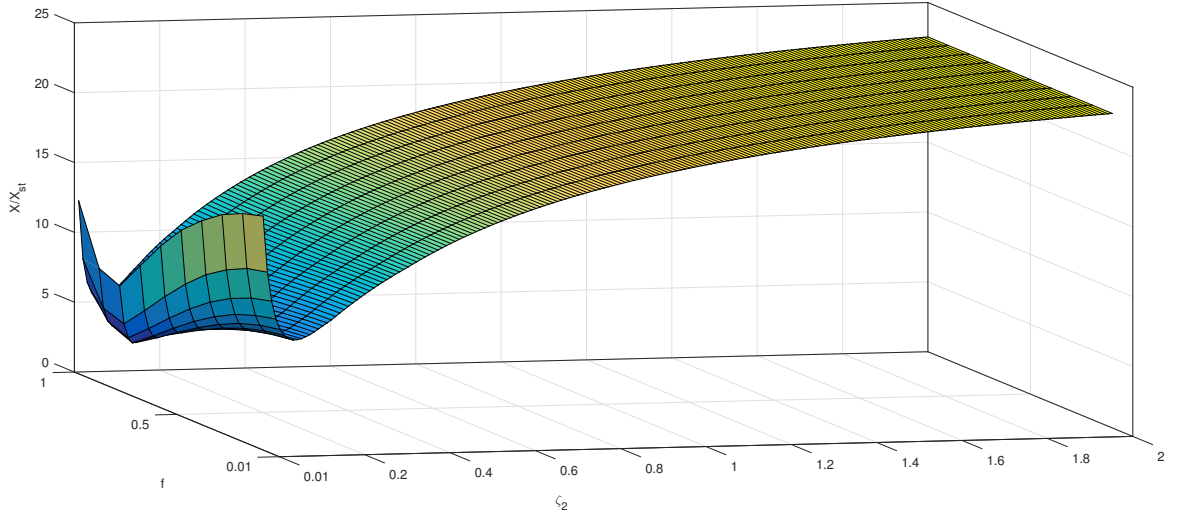


Figure 3.4: Numerical search. Lowest point on the surface represents optimal solution

Table 3.1: System parameters with optimum values from numerical search

PARAMETER	VALUE
Main Mass	1 kg
Mass of Absorber	0.25kg
Stiffness in main mass	$10^3 N/m$
Optimum frequency ratio( $f_{opt}$ )	0.8
Optimum secondary mass damping( $\zeta_2$ )	0.04

The optimum frequency response function obtained has the following characteristics:

- The two maximum amplitudes obtained in the FRF are approximately equal. Table 3.2 shows the forcing frequency ratio at which the maximum amplitudes occur.

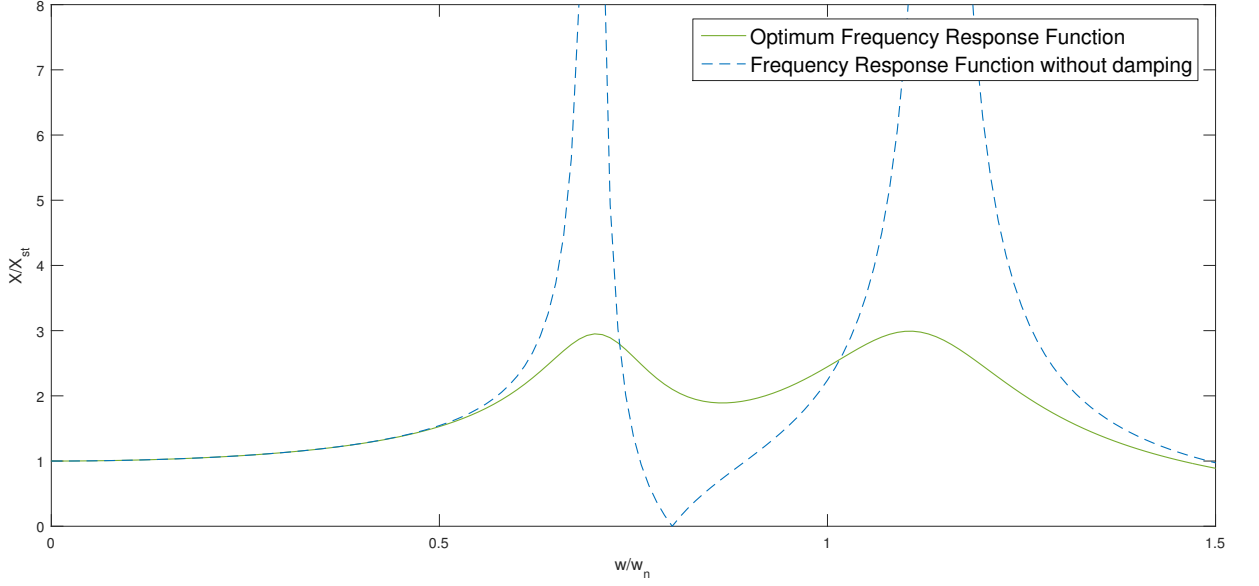


Figure 3.5: Frequency Response Function for optimum values found by numerical search

Table 3.2: Maximum amplitude of the Frequency Response Function

Forcing Frequency ratio	Amplitude
0.7	2.951
1.11	2.991

### 3.3 Coulomb Damping

Friction is difficult to model in multi-degree of freedom mechanical systems. Experimental studies of damping in vibrating mechanical systems typically use modal damping factors to represent the damping. Energy lost by friction is included in these factors. One of the drawbacks is that Friction between contacting surfaces can dissipate energy and cause damage by wear in many engineering systems. The purpose of the present study is to explore the possibility of equivalent friction modal damping for a dynamic vibration absorber and to compare its performance with the viscous damping. The equation of motion when coulomb damping is present is given by-

$$m_1\ddot{x}_1 + k_1x_1 + k_2(x_1 - x_2) + c_1(\dot{x}_1) = F_0\sin(\omega * t) \quad (3.14)$$

$$m_2\ddot{x}_2 + k_2(x_2 - x_1) + del * \text{signum}(\dot{x}_2 - \dot{x}_1) = 0 \quad (3.15)$$

where  $del$  is the frictional force acting on the absorber mass.

In figure 3.6 as frictional force is varied between 0 to 200 N, it can be seen that the FRF retains some of the essential characteristics of a viscous damper, for 2-DOF system and for a smaller frictional force there are 2 local peaks and as in case

of viscous damping if it is increased after a certain point, one of the peaks dies out. FRF's would be smoother if the resolution of  $\omega$  used is smaller for numerical solution.

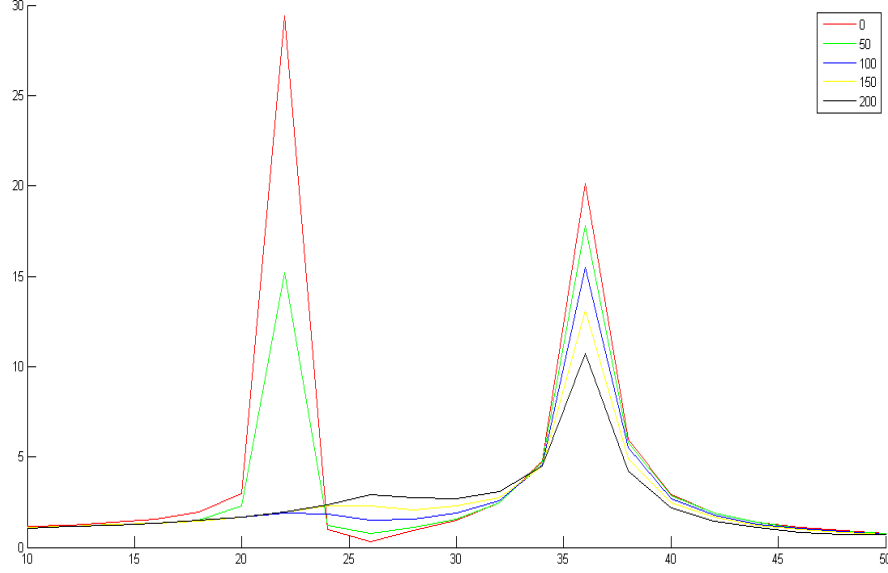


Figure 3.6: FRF in case of coulomb damping.

We would be varying the frictional force to obtain an optimum solution that minimizes the vibration of the main mass. For this the following steps are done-

- FRF is obtained by first evaluating steady state value from time history at a given friction force and forcing frequency.
- the maximum amplitude from this particular FRF is stored.
- The above 2 steps are repeated by varying Frictional force over the range from 0-500 N and 0-200 N.

The results are as shown in figure 3.7. Now the FRF when the frictional force is 390 N, the FRF obtained is compared with the optimal viscous FRF. Important observations:

- It was observed that the optimum value of friction force is close to 400 N (390 N to be precise, and this is valid for a particular excitation force (500 N)).
- Over certain range of frequency that is lower band ( $\frac{\omega}{\omega_n} < 0.77$ ) and higher band ( $\frac{\omega}{\omega_n} > 1.19$ ), coulomb damping is slightly better than viscous damping.



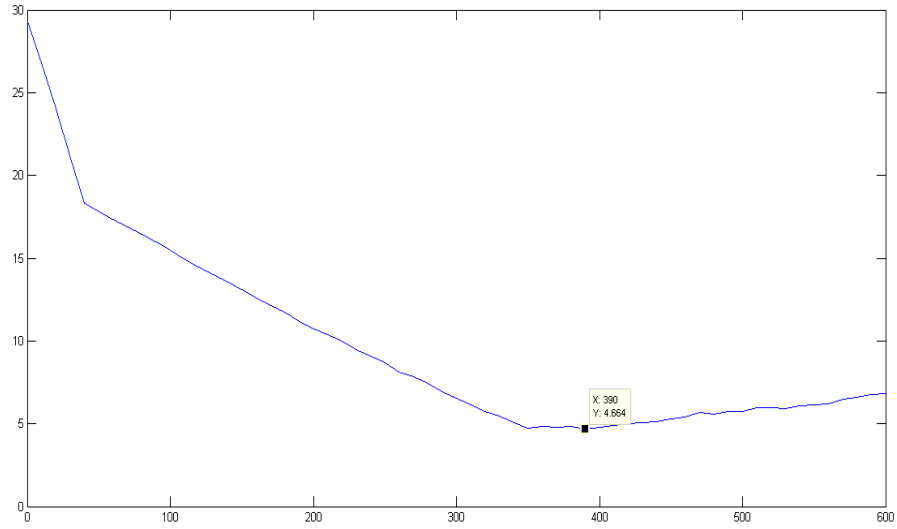


Figure 3.7: Search for best possible coulomb damping.

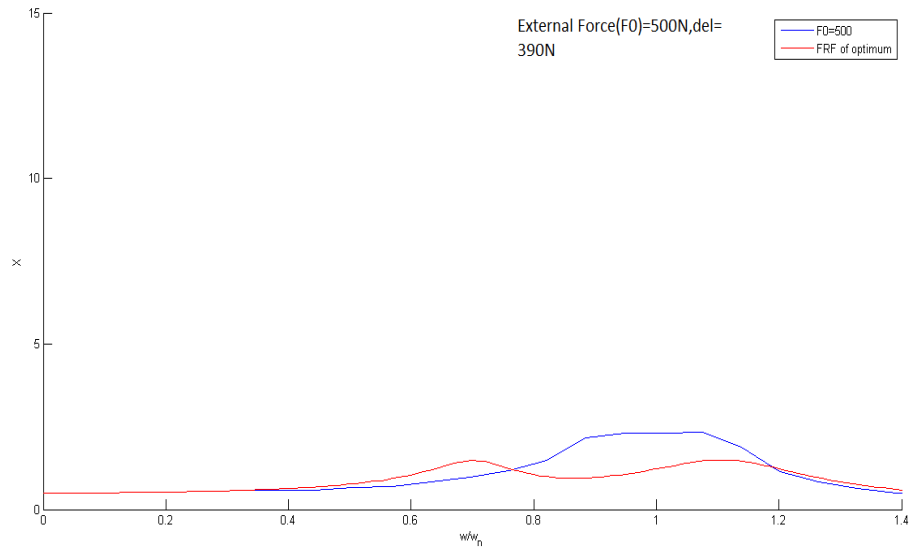


Figure 3.8: Comparison of Optimum viscous with the best FRF in case of coulomb damping .

- For  $(0.77 < \frac{\omega}{\omega_n} < 1.19)$ , viscous damping is found to be more suitable.
- The above observations are by keeping optimal parameters in case of viscous damping. Further improvement may be possible by changing frequency ratio(f).

Important Note: Coulomb damping doesn't offer much benefit over viscous damping, but it is also responsible for wear and tear of mechanical system. Also it

can be seen that Search for the best coulomb damping is difficult as no analytical solutions are available, and performing numerical search has its limitations because in case of coulomb damping the response is a function of external force  $F_0$  and the frictional force  $del$ . Also as shown in figure 3.7, addition of coulomb damping becomes beneficial only for somewhat large frictional force, which in addition to causing wear and tear, from a practical perspective it can become difficult to add such an high frictional force.

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## CHAPTER 4

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### Vibration Absorber with Non-linearity

## 4.1 Background

The characteristics of the non linear primary system attached by the linear absorber change only slightly in terms of the values of its new linearised natural frequency, damping coefficient and frequency interval for primary resonance, because the vibration absorber is a small attachment and does not contribute significantly to the change of these parameters (linear stiffness and damping coefficient). Two ratios, namely attenuation ratio and desensitisation ratio, will be defined to indicate the effectiveness of the linear absorber in Suppressing the primary resonance vibrations. The attenuation ratio will be defined by the ratio of the maximum Amplitude of vibrations of the non linear primary system after and before adding the linear vibration absorber under a given value of the amplitude of excitation. The desensitisation ratio will be given by the ratio of the critical values of the amplitude of external excitations presented in the non linear primary system after and before the linear vibration absorber is attached. The critical value of the excitation amplitude refers to here as a certain value of external excitation that results in the occurrence of saddle-node bifurcations and jump phenomena in the frequencyresponse curve. Below this critical value, the frequencyresponse curve of the primary resonance vibrations does not show saddle-node bifurcations (and jump phenomena) and will exhibit saddle-node bifurcations and jump phenomena if the amplitude of excitation exceeds the critical value.

The forced oscillations of a two degree-of-freedom non linear system having cubic non linearities have been studied by many researchers The attention of these studies has focused on the case of internal resonances when  $\omega_1 = \omega_2$  or  $\omega_3 = \omega_1$ . Specifically, Nayfeh and Mook considered the forced oscillations of cubically non linear systems without linear coupling terms under internal resonances  $\omega_2 = 3\omega_1$ . Natsiavas studied the steady-state oscillations and stability of the non linear system having cubic non linearities under one-to-one internal resonances  $\omega_1 = \omega_2$ . It was shown that the presence of one-to one internal resonances in the nonlinear system of dynamic vibration absorber may result in instability of the periodic response and quasi-periodic oscillations with much higher amplitudes. The non-linear system considered is as shown in figure Below we included the figures of FRF when a hardening spring(cubic stiffness is positive) is included in the system. In figure 4.3 the FRF's are drawn without absorber and then to this system a cubic hardening spring is included without the absorber (green line), it is seen that FRF shifts towards right, it is seen that as non-linearity increases more the shift occurs.

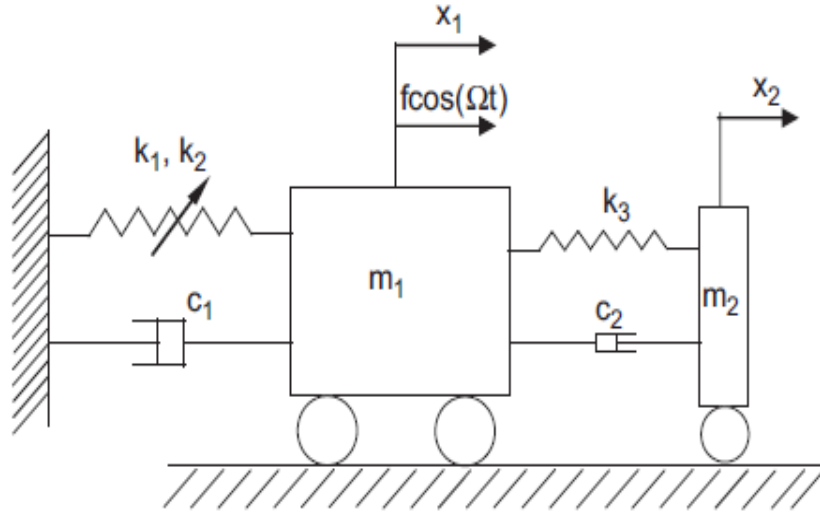


Figure 4.1: Non-linearity added in the primary system.

Similar effects are seen when the non-linearity is introduced in the absorber system, in this case also the graphs lean to right at both first and second peak and with increase in non-linearity same leaning effect is seen.

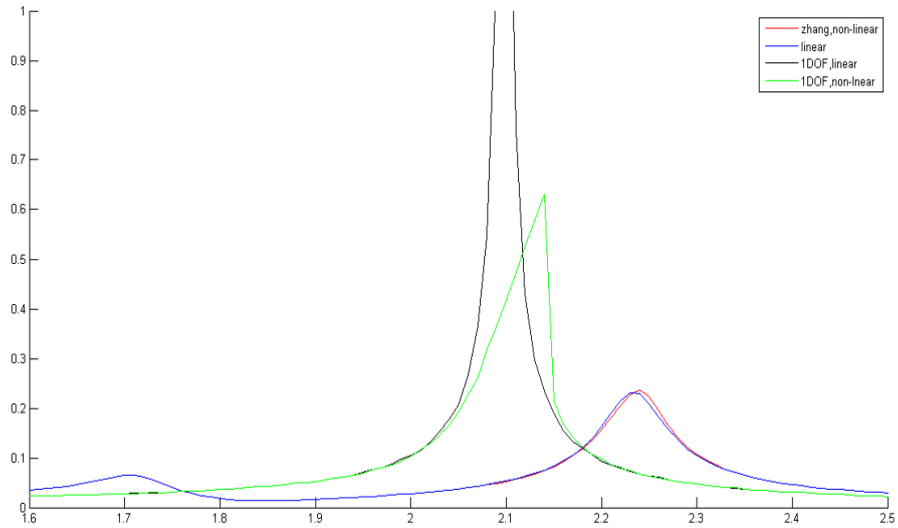


Figure 4.2: non-linearity is added in secondary system.

Given the fairly limited literature concerning the nonlinear dynamic vibration absorber (NDVA), the specific objectives of the study were as follows: To develop a complete analytical expression and verify the numerical solutions that describe the performance of the particular NDVA under harmonic excitation. Subsequently,

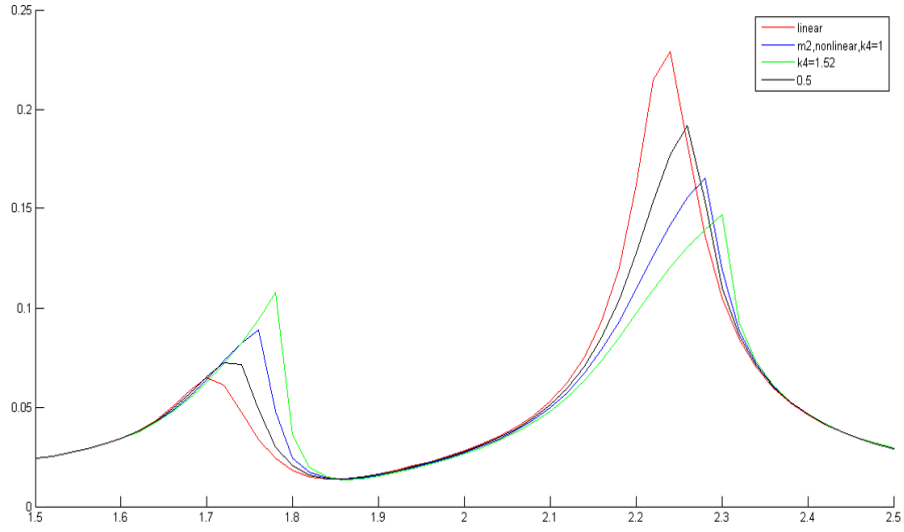


Figure 4.3: 2-DOF non linear system.

investigate the response and its sensitivity to the various physical parameters of the absorber namely the absorber mass, damping and stiffness. The latter possesses restoring force contributions which are both linear and nonlinear cubic powers of the displacement.

## 4.2 Non-linear spring in primary system: Optimum solution

### 4.2.1 Effect of varying stiffness of spring of the absorber

Initially an FRF for the linear parameters

$$m_1 = 10 \text{ kg} \quad m_2 = 0.6 \text{ kg} \quad k_1 = 44 \text{ N/m} \quad c_1 = 0.1 \text{ Ns/m}$$

is drawn. In this case it can be seen that the two peaks are equal. Now a non-linearity is added in the primary system by addition of a cubic spring with  $k_{1n} = 44 \text{ N/m}^3$ . After the addition of a cubic spring, the effect of change in the stiffness of the spring of absorber on the two peaks in the FRF and the bandwidth is to be studied.

The equation of motion when a non-linear spring is added in the primary system is given by-

$$m_1 \ddot{x}_1 + k_1 x_1 + k_{1n} x_1^3 + c_1 \dot{x}_1 + k_2 (x_1 - x_2) + c_2 (\dot{x}_1 - \dot{x}_2) = F_0 \sin(\omega * t) \quad (4.1)$$

$$m_2 \ddot{x}_2 + k_2 (x_2 - x_1) + c_2 (\dot{x}_2 - \dot{x}_1) = 0 \quad (4.2)$$

When  $K_{1N}$  is the cubic non-linear stiffness in the primary system and all the other terms have the usual meaning that we had used in earlier chapters.

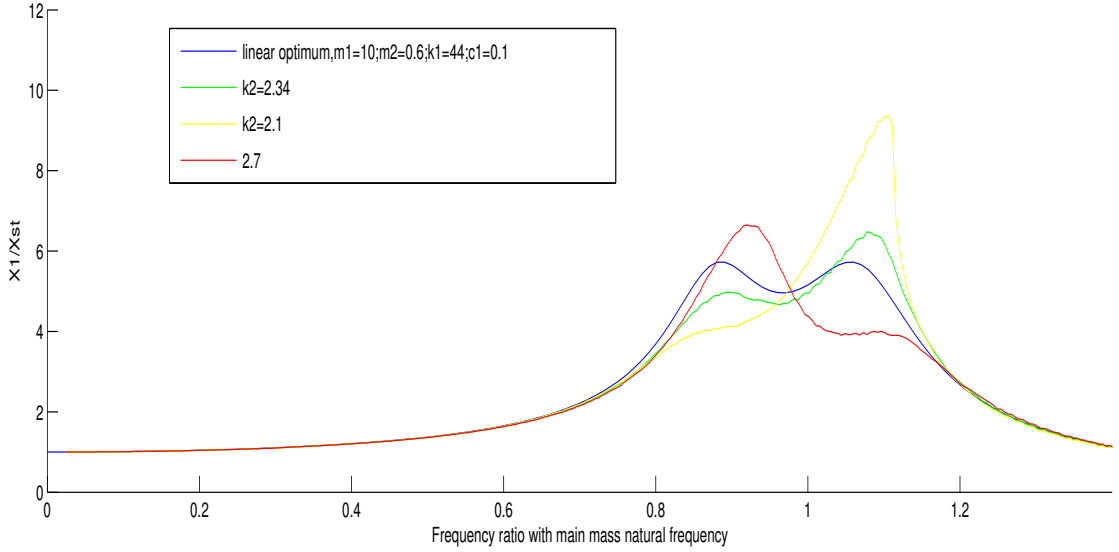


Figure 4.4: Effect of varying stiffness of absorber.

From the Figure 4.4 it can be seen that on increasing the stiffness of absorber spring, the 1st peak increases whereas the 2nd goes on decreasing as  $k_2$  is increased. It is difficult to conclusively predict the effect on bandwidth that is the distance between two peaks, as both the peaks are shifted towards right. The optimum solution by varying  $k_2$ , would have both left and right peaks as equal, also it can be seen that if  $k_2$  goes on decreasing the second peak almost disappears and only peak 1 becomes prominent.

By conducting mini-max search the optimal solution was found to be  $k_2 = 2.43$ . It can be seen that when a non-linear spring is added the optimal solution changes, in this case only  $k_2$  is varied, but in the sections that follow we have explored the effect that secondary damping has on the peaks and the combined effects of secondary stiffness and damping to provide a best case scenario.

It is to be noted that the optimum case of non-linearity is obtained in this case by varying only the stiffness of spring attached to the secondary mass. We were able to obtain an FRF that was as good as the FRF for optimized linear case and as stated earlier there is not much change in the bandwidth.

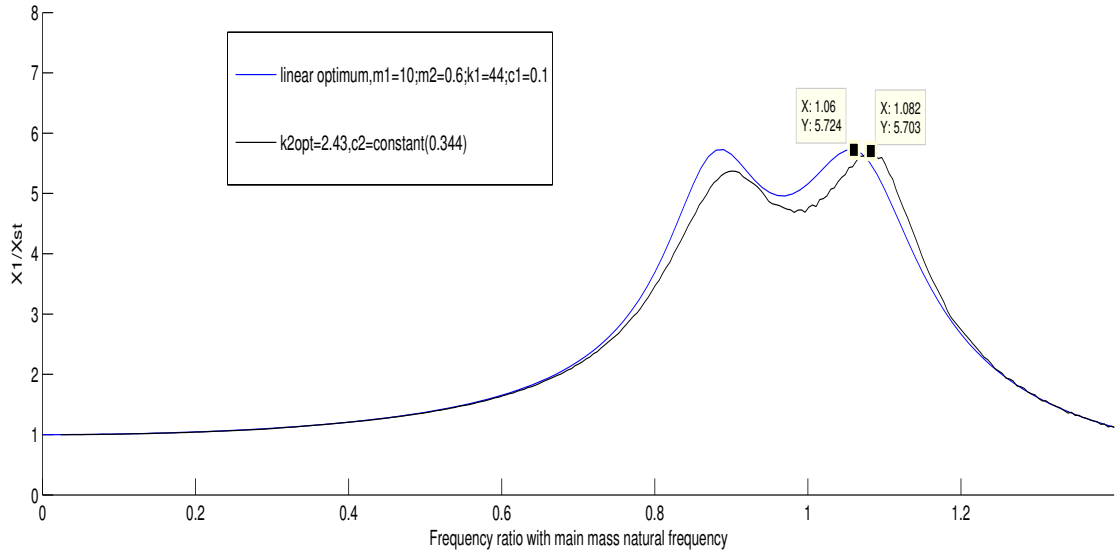


Figure 4.5: Comparison of optimum FRF of linear and non-linear spring .

#### 4.2.2 Effect of varying damping of the absorber

The initial system is having all its components to be linear. When the linear system is designed having optimum parameters, its Frequency Response Characteristic is as shown in Figure 4.6.

The two peaks have almost same value and they are at the minimum possible

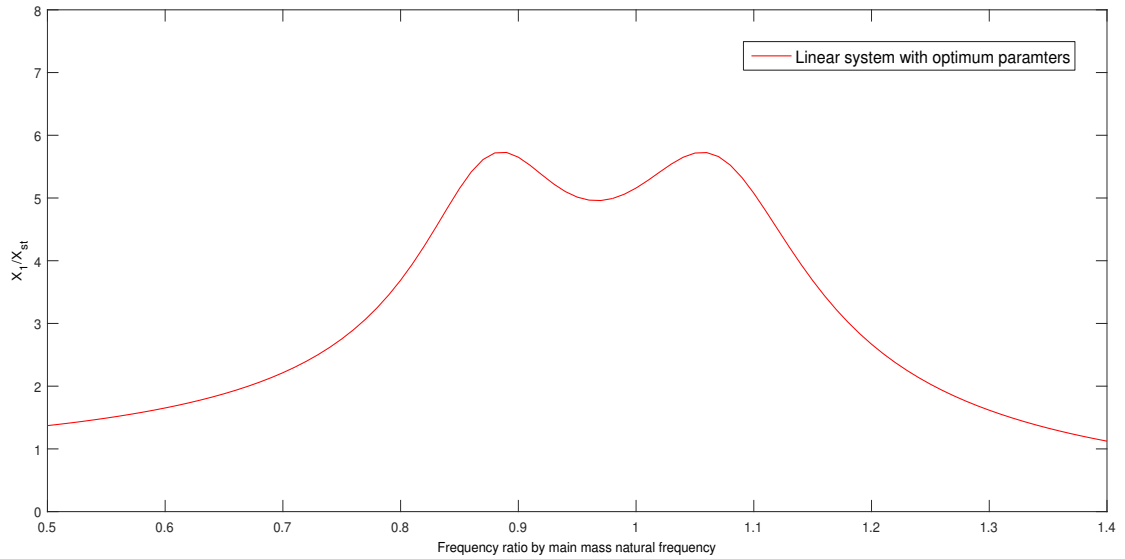


Figure 4.6: FRF of linear system with optimum parameters

value. Hence, the system as a whole is said to have the best or optimum response over a range of frequency.

If now we add a non-linearity in the primary mass, the FRF changes with a



Table 4.1: Comparing maximum values of linear and non-linear FRF

	Linear	Non-Linear	Difference
Peak 1	5.726	5.004	-0.722
Peak 2	5.724	6.412	0.688

reduction in maximum value of left peak and with increase in amplitude of the right peak.

$$m_1 = 10 \text{ kg} \quad m_2 = 0.6 \text{ kg} \quad (4.3)$$

$$k_1 = 44 \text{ N/m} \quad k_{1N} = 1000 \text{ N/m}^3 \quad k_2 = 2.347 \text{ N/m} \quad (4.4)$$

$$c_1 = 0.1 \text{ N} \cdot \text{s/m} \quad c_2 = 0.344 \text{ N} \cdot \text{s/m} \quad (4.5)$$

Once it is established that addition of non-linearity to the primary mass disturbs the linear system under optimal conditions, we studied the effect of changing the secondary mass damping, on the system.

The graph in Figure 4.7 is plotted with varying values of secondary mass damping ( $\zeta_2$ ). The linear plot is retained for comparison purpose. Since we are concerned with getting the best response from the system, we need to minimize its maximum amplitude over the whole range. This is achieved when both the peaks have approximately the same maximum value.

From Figure 4.7, the following points are to be noted:

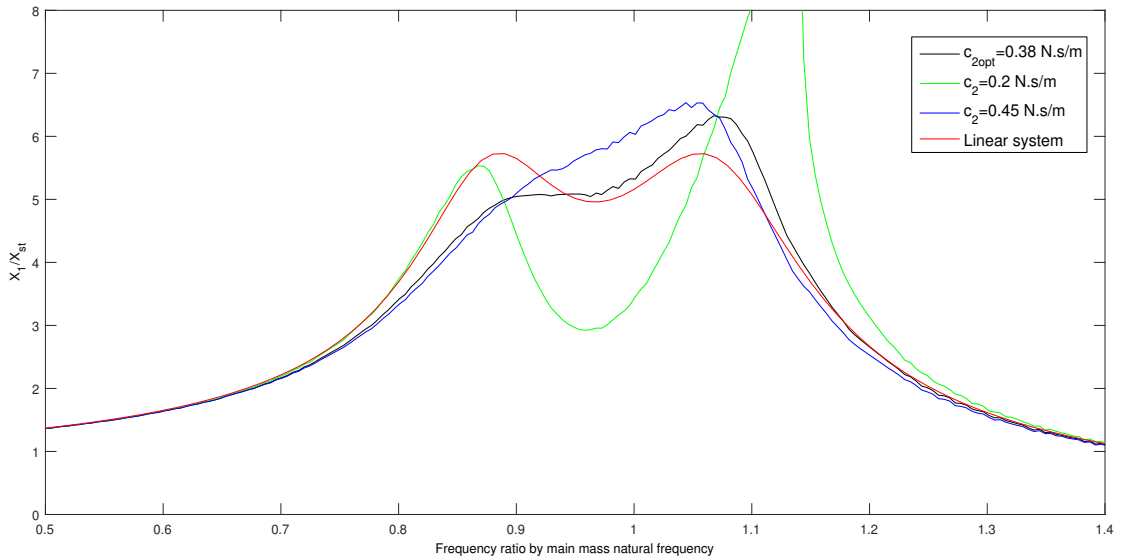


Figure 4.7: FRF with changing damping of the absorber

- If non-linearity is decreased, the right peak increases whereas the left peak comes down and vice-versa when non-linearity is increased.
- The value of  $c_2 = 0.38N \cdot s/m$  gives the best case scenario when we are changing the secondary mass damping. It is certainly not the best case, if we were also allowed to vary other system parameters. However, the maximum of the two peaks are close to each other.
- The value  $c_2 = 0.38N \cdot s/m$  is not too offset from the linear system's optimal secondary mass damping value  $c_2 = 0.344N \cdot s/m$ . In the non-linear case, however, the response is better near the first peak and worse off near the second peak, as compared to the linear system.

### 4.2.3 Optimum Frequency Response Function for Nonlinear spring in Primary system

In this section the combined effects of variation secondary mass spring stiffness and damping co-efficient is used to obtain the best possible solution and is used to compare with the optimal linear solution, to see if there is a reduction in the maximum amplitude of vibration of the primary mass system and how the bandwidth between peak 1 and 2 of the optimal linear and non-linear FRF differs. It

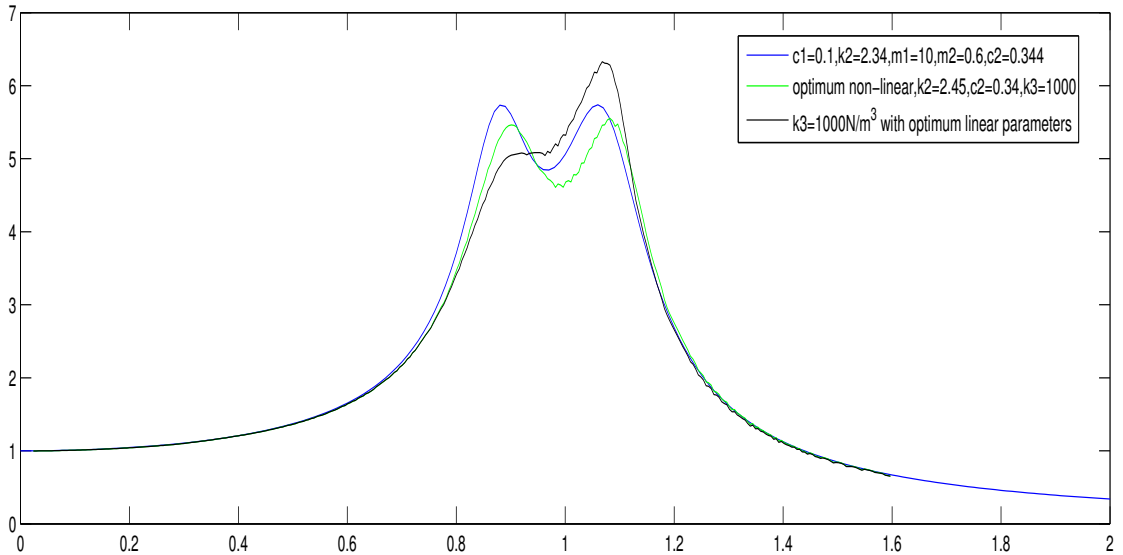


Figure 4.8: Comparison of optimum FRF's for linear and cubic spring.

is observed that after performing mini-max search by varying both stiffness and damping co-efficient, the non-linear FRF obtained as can be seen from figure 4.8 is better than the optimum linear FRF, both left and right peaks can be brought

down. So if non-linearity is already present in the primary system, designers have an opportunity to bring down the maximum amplitude of vibration further down. Also as seen from figure 4.8 the vibration response at the resonant frequency ( $\omega = 1$ ) is also brought down as hardening spring has an effect of shifting the FRF towards right.

As such it is difficult to conclusively predict the difference in bandwidth between peaks of linear and non-linear optimum solution.

Below is the comparison of the parameters:

Table 4.2: Maximum amplitude and bandwidth of linear and non-linear FRF

Case	$\left(\frac{X_1}{X_{stat}}\right)_{max}$	Bandwidth
Linear optimum FRF	5.733	0.18
Non-Linear optimum FRF	5.452	0.1857

#### 4.2.4 Cases for verification

##### Case A

Mass of primary system,  $m_1 = 20\text{kg}$

Mass of secondary system,  $m_2 = 1.6\text{kg}$

Mass ratio,  $\mu = 0.08$

Primary mass stiffness  $k_1 = 8000\text{ N/m}$

Primary mass damping ratio  $\zeta_1 = 0.02$

Optimum Frequency ratio,  $f_{opt} = 0.914$

Optimum secondary mass damping,  $\zeta_{2opt} = 0.013$

Stiffness of secondary mass spring,  $k_2 = 534.65\text{ N/m}$

Stiffness of non-linear spring,  $k_{1n} = 10420\text{ N/m}^3$

Optimum stiffness of secondary mass spring with added non-linearity =  $566\text{ N/m}$

Table 4.3: Comparing maximum values of linear and non-linear FRF : Case A

	Linear	Non-Linear	Difference
Peak 1	4.075	3.838	-0.237
Peak 2	4.076	3.827	-0.249

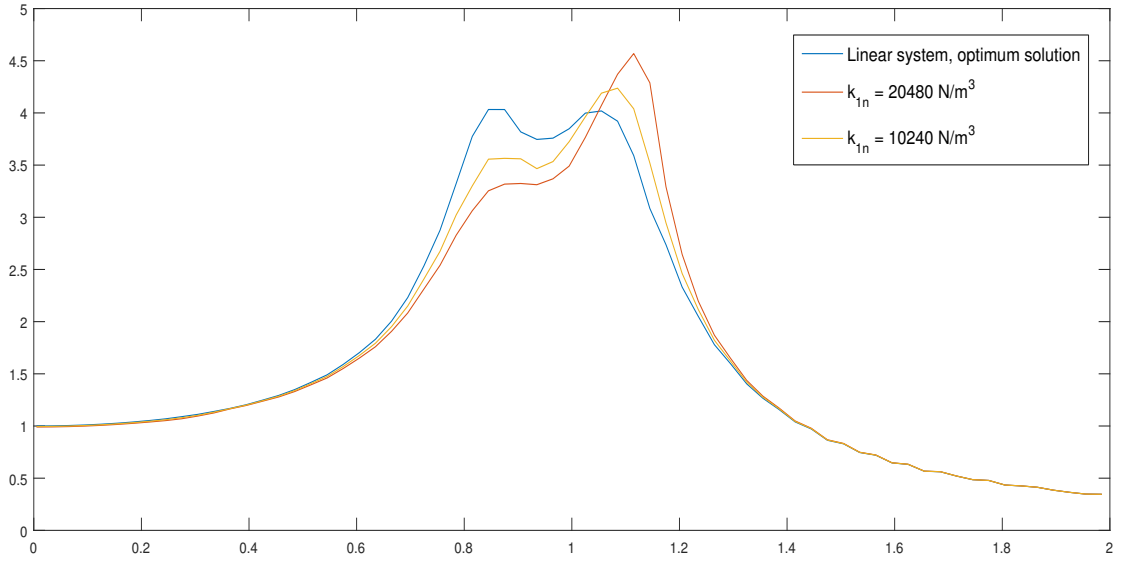


Figure 4.9: Effect of adding non-linearity in the primary system

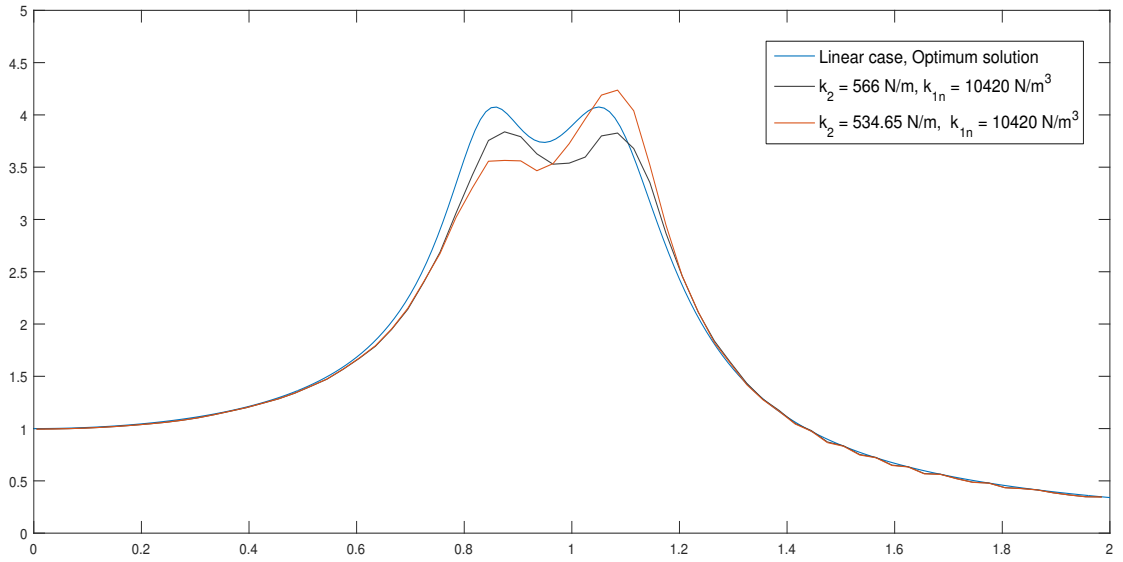


Figure 4.10: Effect of changing stiffness of absorber

## Case B

Mass of primary system,  $m_1 = 50\text{kg}$

Mass of secondary system,  $m_2 = 5\text{kg}$

Mass ratio,  $\mu = 0.1$

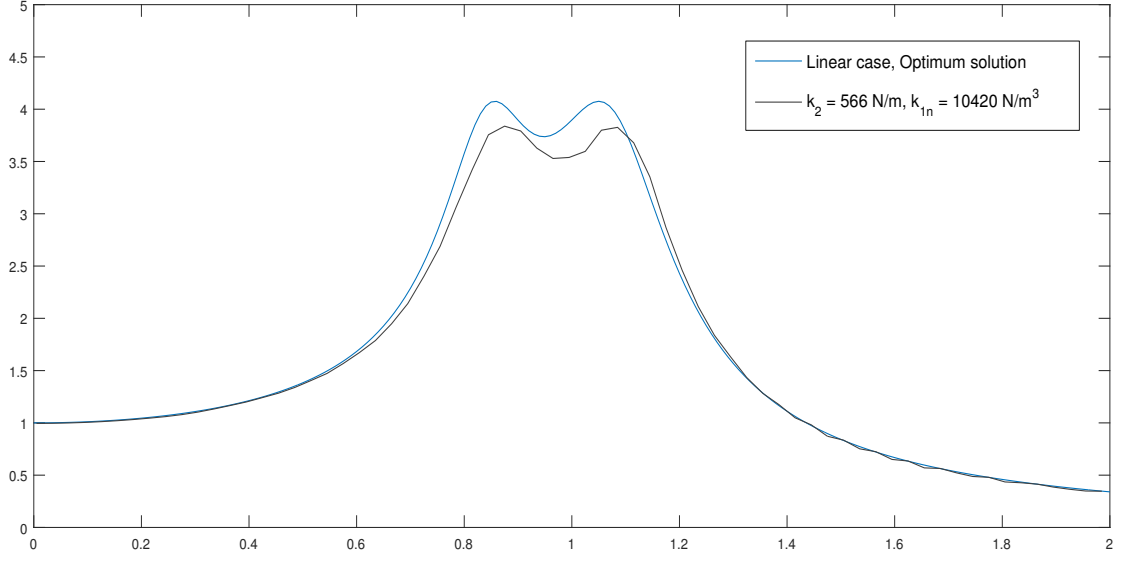


Figure 4.11: Comparison of non-linear and linear optimal solution

Table 4.4: Maximum amplitude and bandwidth of linear and non-linear FRF: Case A

Case	$\left(\frac{X_1}{X_{stat}}\right)_{max}$	Bandwidth
Linear optimum FRF	4.075	0.21
Non-Linear optimum FRF	3.838	0.22

Primary mass stiffness  $k_1 = 11250$  N/m

Primary mass damping ratio  $\zeta_1 = 0.02$

Optimum Frequency ratio,  $f_{opt} = 0.914$

Optimum secondary mass damping,  $\zeta_{2opt} = 0.017$

Stiffness of secondary mass spring,  $k_2 = 913.27$  N/m

Stiffness of non-linear spring,  $k_{1n} = 14238$  N/m<sup>3</sup>

Optimum stiffness of secondary mass spring with added non-linearity = 1010 N/m

Table 4.5: Comparing maximum values of linear and non-linear case FRF: Case B

	Linear	Non-Linear	Difference
Peak 1	3.993	3.636	-0.357
Peak 2	3.989	3.634	-0.355

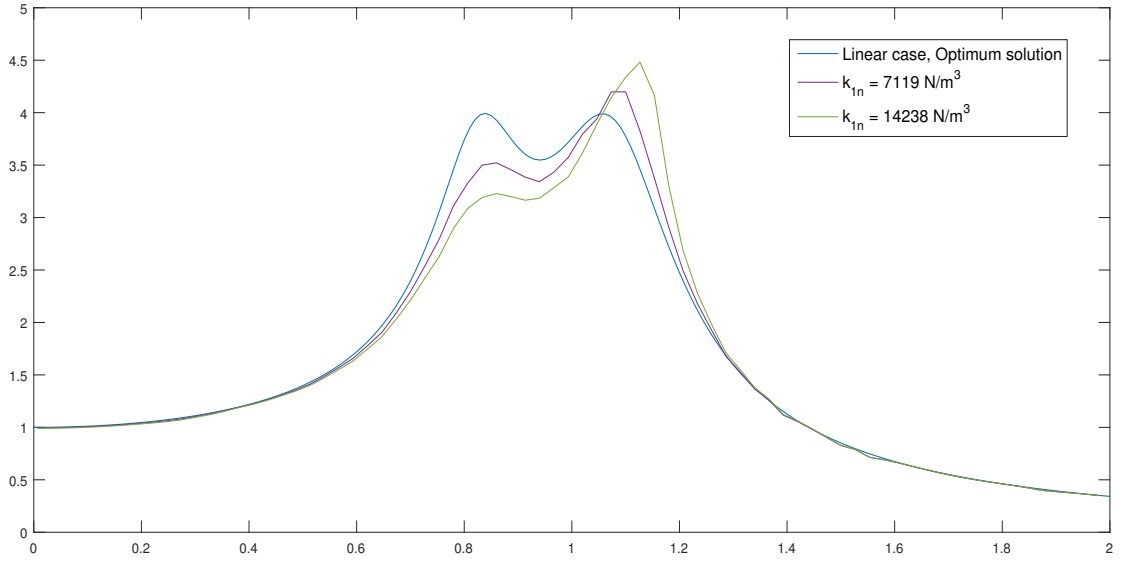


Figure 4.12: Effect of adding non-linearity in the primary system

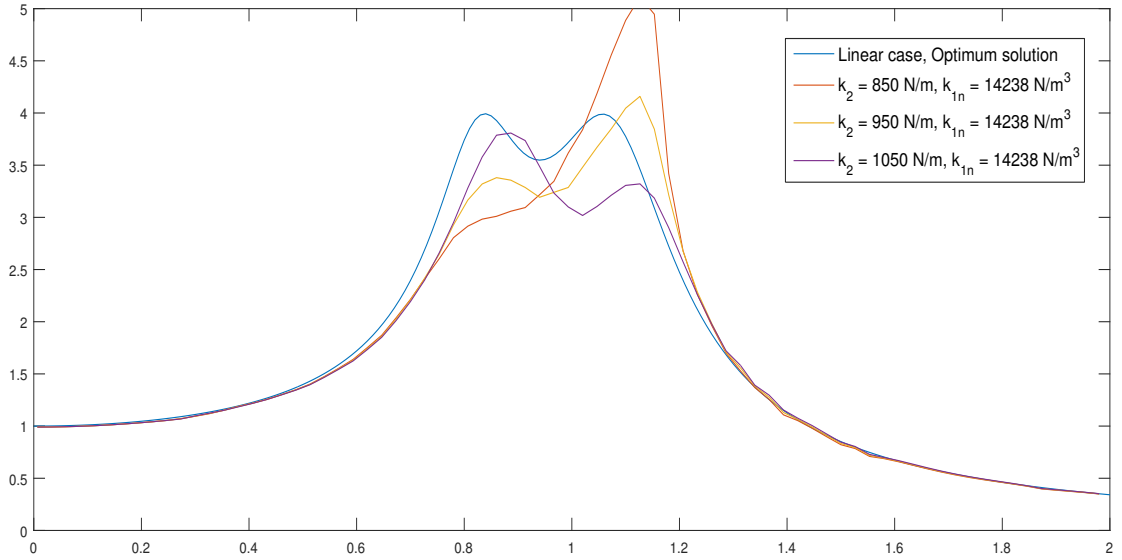


Figure 4.13: Effect of changing stiffness of absorber

Table 4.6: Maximum amplitude and bandwidth of linear and non-linear FRF:  
Case B

Case	$\left(\frac{X_1}{X_{stat}}\right)_{max}$	Bandwidth
Linear optimum FRF	3.993	0.22
Non-Linear optimum FRF	3.636	0.267

### 4.3 Non-linear spring in the Secondary system: Optimum solution

#### 4.3.1 Effect of varying stiffness of spring of the absorber

In the sections below, we would analyse and tabulate the effects of varying stiff-

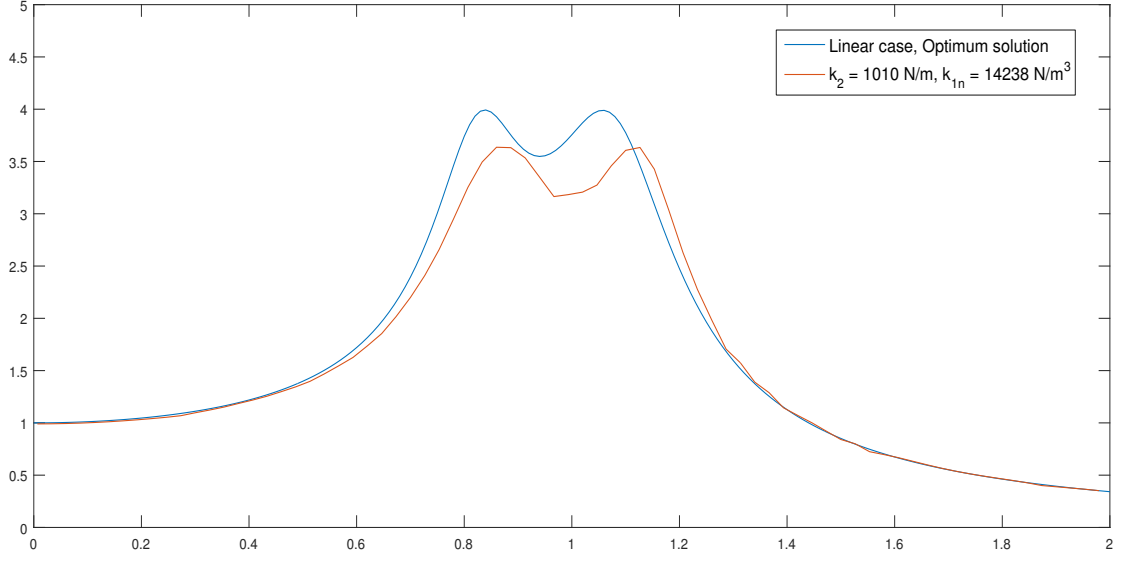


Figure 4.14: Comparison of non-linear and linear optimal solution

in between the main mass and the absorber mass. The procedure adapted in this section is similar to previous sections, qualitative results are presented on varying the independent parameters.

The equation of motion when non-linearity is introduced in the absorber system

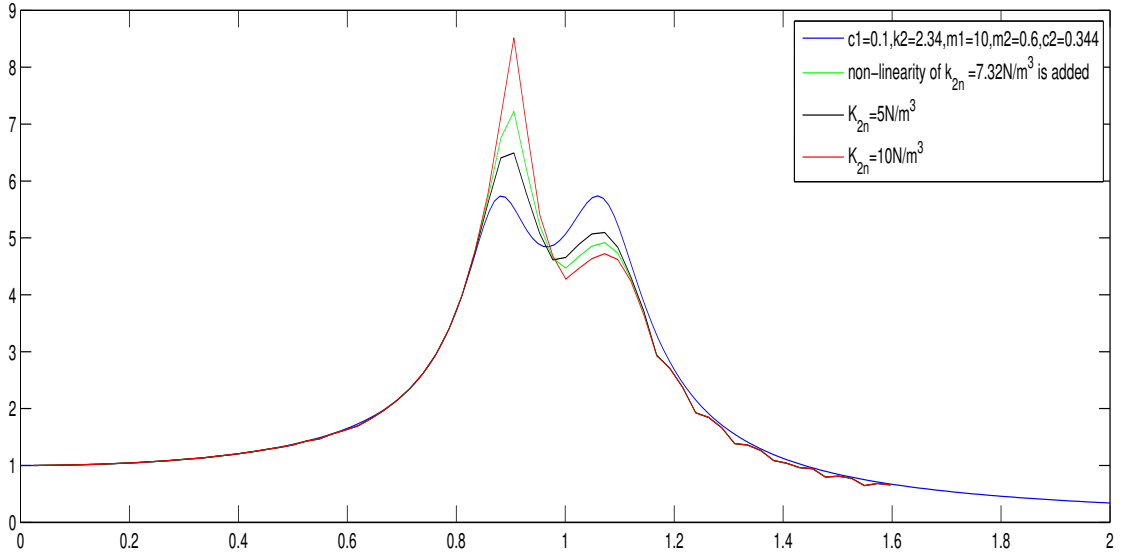


Figure 4.15: Effect of increasing non-linear stiffness of absorber.

is given by-

$$m_1 \ddot{x}_1 + k_1 x_1 + c_1 \dot{x}_1 + k_2 (x_1 - x_2) + k_{2N} (x_1 - x_2)^3 + c_2 (\dot{x}_1 - \dot{x}_2) = F_0 \sin(\omega * t) \quad (4.6)$$

$$m_2 \ddot{x}_2 + k_2 (x_2 - x_1) + k_{2N} (x_2 - x_1)^3 + c_2 (\dot{x}_2 - \dot{x}_1) = 0 \quad (4.7)$$

When  $K_{2N}$  is the cubic non-linear stiffness in between absorber and main mass and all the other terms have the usual meaning that we had used in earlier chapters.

It is to be noted that for secondary mass system, we have control over the amount of non-linearity that is to be introduced and the linear stiffness and damping. For a designer one more design variable is introduced. So we will start with the effect of non-linearity, from 4.15 it can be qualitatively seen that as the cubic non-linearity increases the first peak goes on increasing whereas the second peak decreases and both are shifted towards right.

Now for  $k_{2N} = 7.32 \text{ N/m}^3$  we would change the linear stiffness value of the secondary spring and note the effects.

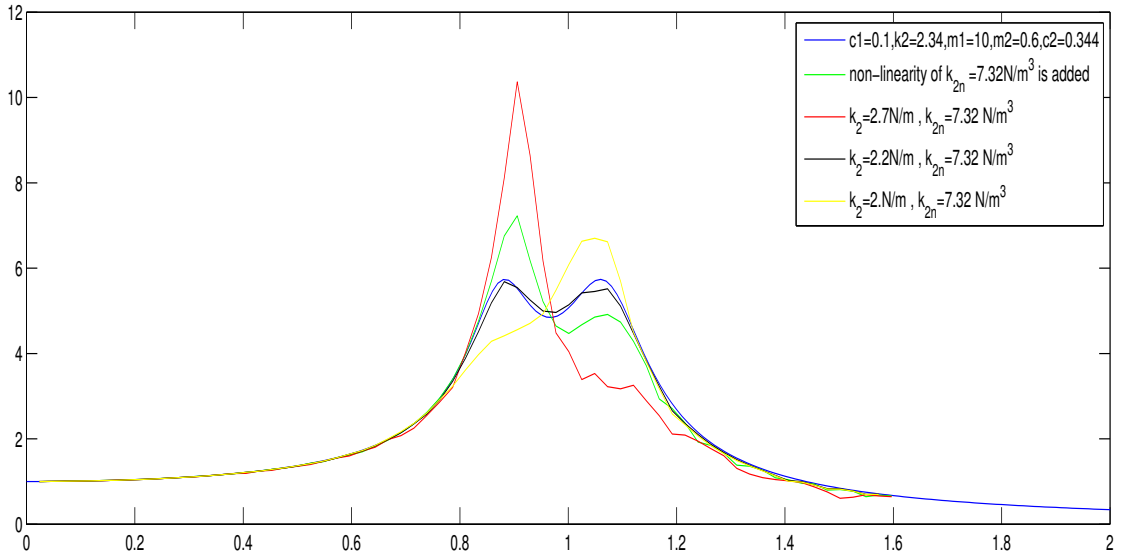


Figure 4.16: Effect of increasing linear stiffness if cubic non-linearity is present in absorber.

- On increasing the linear stiffness  $K_2$  peak 1 goes up whereas the second peak goes down.
- The effect is similar to the cubic stiffness, so increasing both linear and non-linear stiffness would have an adverse effect.
- Bandwidth between 2 peaks is essentially same as we vary linear stiffness.
- To obtain an optimum solution, the two peaks should be equal, so if we increase  $K_{2N}$ , we need to reduce the value of linear stiffness.



### 4.3.2 Effect of varying the damping of secondary system

We would be keeping  $K_{2N} = 7.34N/m^3$  and  $k_2 = 2.34N/m^3$  but we note the effects of varying the damping in the secondary system. The idea is to combine the effects that are noted for change in spring stiffness and the damping, to obtain an optimum solution in case when non-linearity is introduced in the secondary mass and compare it with the linear optimum solution, this exercise gives us an idea of whether we can further reduce the vibrational amplitude of primary mass. The observations made on varying the damping are:

- The variation damping has a major effect on the first peak.
- On increasing the damping peak 1 decreases
- Increase of damping decreases the second peak but the rate of decrease is much smaller, if damping is increase beyond certain level second peaks dies out.
- From the above two points, it is wrong to infer that more the damping lesser the vibration.
- As can be seen in figure 4.17 for  $C_2 = 0.6Ns/m$  only one peak remains but the maximum amplitude in FRF is greater than for  $C_2 = 0.4Ns/m$ . So after certain point, increasing damping would be counter productive.

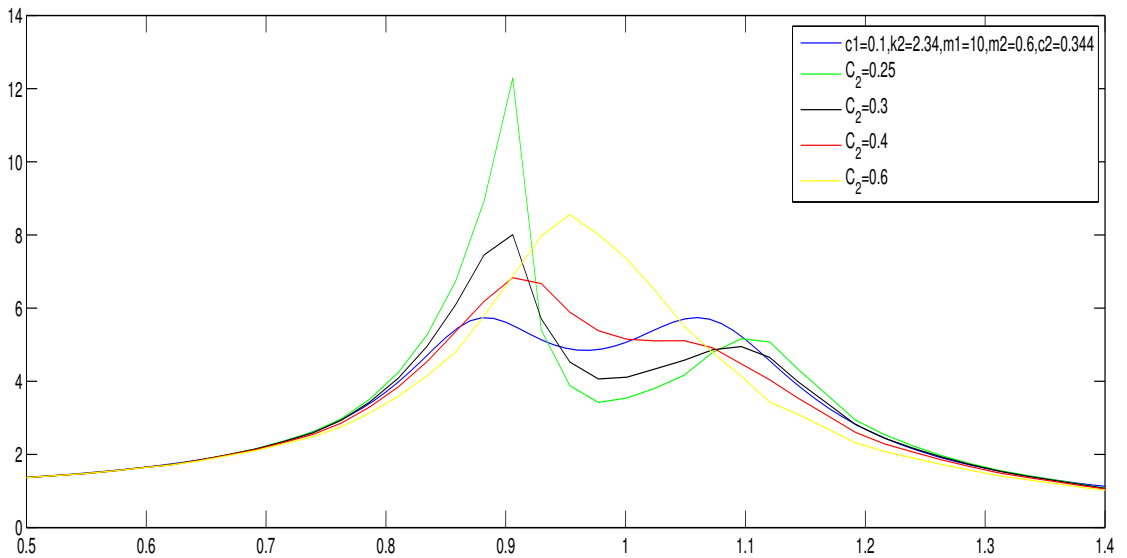
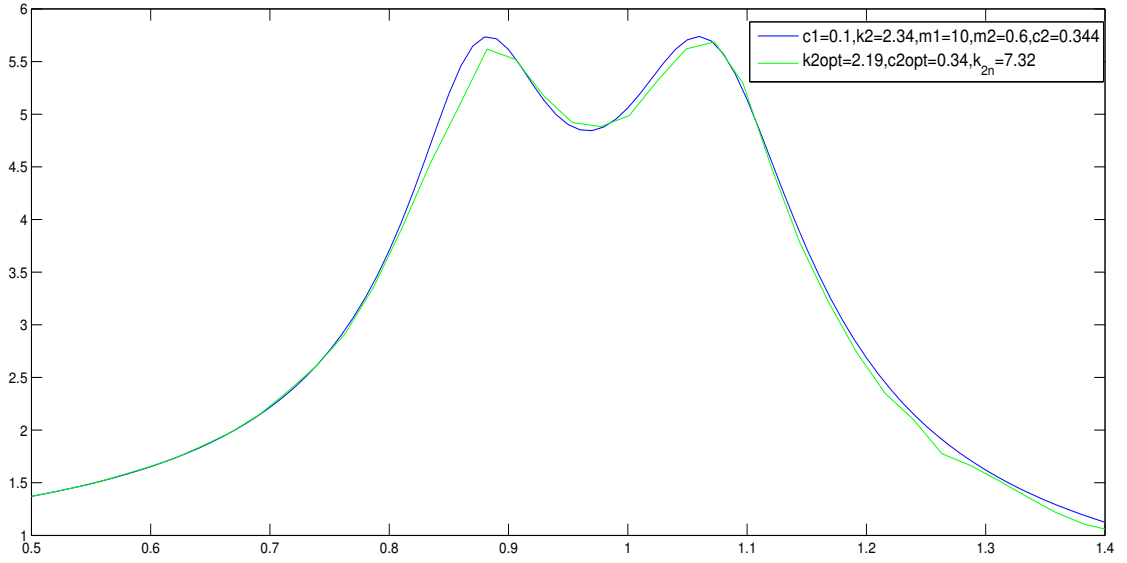


Figure 4.17: Effect of increasing damping if cubic non-linearity is present in absorber.

### 4.3.3 Comparison of optimum solution when non-linearity is introduced with the linear optimum solution

It is observed that after performing mini-max search by varying both stiffness and damping co-efficient, the non-linear FRF obtained is as shown in figure 4.8 and is almost similar to linear optimum FRF, this can be attributed to smaller value of cubic non-linear spring, but on introduction of non-linear spring the optimum value for linear stiffness changes but optimum damping almost remains same



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## CHAPTER 5

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Analytical study of non-linearity in single  
degree of freedom system:  
Harmonic Balance Method

Harmonic balance method is selected for analytical study because it is not restricted to weakly nonlinear problems and, for smooth systems the assumed harmonic solutions always converge to the exact solution. The mathematical analysis can be conducted relatively easily due to it not producing complicated mathematical expressions for higher order terms. However, the HBM has some limitations in accuracy. In the interpretation considered here, one chooses just to use the response at the excitation frequency, i.e., by assuming that sub and super harmonics are negligible compared to the fundamental harmonic and that the system is only under periodic excitation. In addition, the stability characteristics require a separate analysis. We will be considering the non-linear system governed by duffing equation. Here we will be considering the forced vibration of a single degree of freedom system with viscous damping, the equation of motion of such a system is given by

$$m\ddot{x} + \alpha x + c(\dot{x}) + \beta x^3 = F_0 \sin(\omega t) \quad (5.1)$$

We will be considering only forced vibration and neglecting the transient vibration which decays after a certain interval of time because of presence of damping in the system. The steady state forced vibrations will have harmonics corresponding to forcing frequency  $\omega$  and higher harmonics corresponding to odd multiples of  $\omega$ ,  $3\omega$ ,  $5\omega$  etc. The forced vibration will be dominant in first harmonic and decreases rapidly for higher harmonics. Here, for harmonic balance method, we would be restricting ourselves to the first harmonic.

$$\ddot{x} + p^2 x + 2\zeta p(\dot{x}) + p^2 \mu x^3 = F_0 \sin(\omega t) \quad (5.2)$$

$$p^2 = \alpha/m \quad (5.3)$$

$$\mu = \beta/\alpha \quad (5.4)$$

$$\zeta = c/2mp \quad (5.5)$$

$$\tau = pt \quad (5.6)$$

$$r = \omega/p \quad (5.7)$$

$$x = a \sin(r\tau) + b \cos(r\tau) \quad (5.8)$$

We use harmonic balance method in which each harmonic is balanced by separating out the terms in LHS and RHS. The third harmonic and higher order harmonics are neglected. Equating the co-efficients of  $\cos(r\tau)$  and  $\sin(r\tau)$  we get:

$$-ar^2 - 2\zeta br + a + 3/4\mu a^3 + 3/4\mu ab^2 = 0 \quad (5.9)$$

$$-br^2 - 2\zeta ar + b + 3/4\mu b^3 + 3/4\mu a^2 b = 0 \quad (5.10)$$

$$X^2 = a^2 + b^2 \quad (5.11)$$

rearranging the above equations-

$$9/16(\mu)^2 X^6 + 3/2\mu(1 - r^2)X^4 + (r^4 - 2r^2 + 1)X^2 - X_{st}^2 = 0 \quad (5.12)$$

For constant force excitation, FRF is plotted by varying  $r$  and for  $\mu = 9$ ,  $X_{st} = 10$ ,  $\zeta = 0.1$  A comparison of Linear and non-linear system-

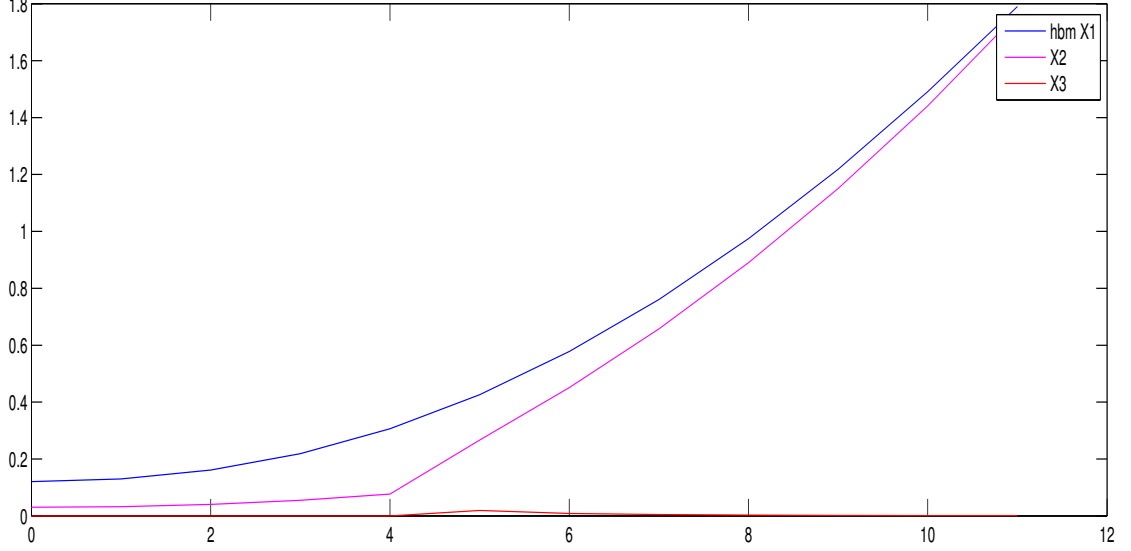


Figure 5.1: Response by harmonic balance method.

- In non-linear system frequency of free vibration depends on amplitude of vibration.
- For the linear system, the amplitude-frequency relationship for free vibration is a vertical line on the forced response diagram at the excitation frequency equal to the natural frequency. The forced vibration response occurs to the left and right of this vertical resonance line. For a nonlinear system this relationship for a hardening spring bends to the right and for a softening spring, it bends to the left. The forced response follows above and below the free vibration characteristic, giving rise to the jump phenomenon.
- The forced vibration response in a linear system with harmonic excitation force is also harmonic with the same frequency as the excitation frequency. In a nonlinear system with harmonic excitation, however, the response is non-harmonic but periodic with the first and higher harmonics of the fundamental period. For symmetric stiffness characteristics, only odd harmonics are present.
- For linear systems, the response is directly proportional to the magnitude of the excitation force at a given frequency of excitation. For nonlinear

systems, however a sudden upward jump in the amplitude takes place when the force is increased gradually and reaches a specific point. Similarly, if the magnitude of the force is decreased gradually, a sudden downward jump in amplitude of vibration takes place.

- In a linear system, the forced vibration response gradually increases until resonance and decreases gradually as the frequency is increased keeping the excitation force constant. The response is unique at all the frequencies of excitation, irrespective of the case whether the frequency is increasing or decreasing. However, in a nonlinear system, as the frequency of excitation is increased for a constant force, the response increases gradually and at a certain frequency sudden downward jump occurs and when the frequency is gradually decreased a sudden upward jump occurs at a particular frequency.
- Some solutions theoretically possible may not be realised for nonlinear systems in practice. Also, some solutions in nonlinear systems may be unstable.
- A linear system analysis is useful to predict the natural frequencies, where large amplitudes of vibration will occur. The designer can then avoid frequencies of excitation around the natural frequencies. Linear system analysis may therefore be of limited value, if large deformations are to be considered in a system.

From 5.3 it can be seen that there are three solutions to the given problem.

## 5.1 Harmonic balance method applied to a DVA

### 5.1.1 First order Harmonic balance

To investigate the dynamic behaviour of the primary system with the nonlinear spring and an absorber attached, the HBM is used, as this enables mathematical expressions to be derived and the analysis to be conducted relatively easily. The fundamental assumption in the HBM approach used for the first order solution is that the response of the primary system and the absorber is predominantly harmonic at the harmonic excitation frequency. Applying the HBM, it is assumed that a solution exists of the form:

$$x = A\sin(\omega t) + B\cos(\omega t) \quad (5.13)$$

$$z = C\sin(\omega t) + D\cos(\omega t) \quad (5.14)$$

where  $z = x - x_2$ , this two equations are substituted into equation of motion.

$$m_1 \ddot{x}_1 + k_1 x_1 + k_2 z + c_2(\dot{z}) + c_2(\dot{x}) + k_{1N} x^3 = F_0 \sin(\omega * t) \quad (5.15)$$

$$m_2 \ddot{z} + k_2 z + c_2 \dot{z} = m_2 \ddot{x} \quad (5.16)$$

By neglecting higher order harmonics and equating the co-efficient of cosine and sine in both the equations, we get 4 equations in 4 variables A,B,C,D as given below:

$$-m_2 * C * \omega^2 + k_2 * C - c_2 * D * \omega + m_2 * A * \omega^2 = 0 \quad (5.17)$$

$$-m_2 * D * \omega^2 + k_2 * D - c_2 * C * \omega + B * m_2 * \omega^2 = 0 \quad (5.18)$$

$$\begin{aligned} -A * m_1 * \omega^2 + k_1 * A + k_2 * C + 0.75 * k_{1N} * A^3 + 0.25 * k_{1N} * A * B^2 \\ - B * c_1 * \omega - D * c_2 * \omega = F_0 \end{aligned} \quad (5.19)$$

$$\begin{aligned} -B * m_1 * \omega^2 + k_1 * B + k_2 * D + 0.75 * k_{1N} * B^3 + 0.25 * k_{1N} * B * A^2 \\ + c_1 * A * \omega + c_2 * C * \omega = 0 \end{aligned} \quad (5.20)$$

The response of primary mass is given by:

$$\sqrt{A^2 + B^2}$$

### 5.1.2 Third order Harmonic balance

For the third order harmonic balance method the assumption is that the response of the primary system and the absorber predominantly has a response which is in the form as given below-

$$x = A \sin(\omega t) + B \cos(\omega t) + C \sin(3\omega t) + D \cos(3\omega t) \quad (5.21)$$

$$z = L \sin(\omega t) + M \cos(\omega t) + N \sin(3\omega t) + P \cos(3\omega t) \quad (5.22)$$

Similar to approach adapted in the previous section, on substituting the above equations in to governing differential equation, and by neglecting higher order harmonics and equating the co-efficient of first order and third order cosine and sine in both the governing equations, we get 8 equations in 8 variables A,B,C,D,L,M,N,P as given below:

$$\begin{aligned} -m_1 \omega^2 * A + k_1 * A + k_2 * L - B * c_1 * \omega + M * c_2 * \omega \\ + 0.75 * K_{1n} * A^3 + 0.25 * K_{1n} * A * B^2 + 0.75 * K_{1n} * (A^2 + B^2) * C - \\ 1.5 * K_{1n} * A * B * D + 1.5 * K_{1n} * A * (D^2 - C^2) = F_0 \end{aligned} \quad (5.23)$$

$$\begin{aligned}
& m1 * -\omega^2 * B + (k1 * B + k2 * M) + (A * c1 * \omega + L * c2 * \omega) + \\
& (0.75 * K_{1n} * B^3 + 0.25 * K_{1n} * B * A^2 + 0.75 * K_{1n} * (A^2 + B^2) * D \\
& - 1.5 * K_{1n} * A * B * C + 1.5 * K_{1n} * B * (D^2 - C^2)) = 0
\end{aligned} \tag{5.24}$$

$$\begin{aligned}
& - 9 * M * C * \omega^2 + k1 * C + k2 * N - 3 * D * c1 * \omega \\
& - 3 * P * c2 * \omega - 0.25 * K_{1n} * A^3 + 0.25 * K_{1n} * A * B^2 + 0.75 * K_{1n} * C^3 + \\
& 0.25 * K_{1n} * C * D^2 + 1.5 * K_{1n} * (B^2 - A^2) * C = 0
\end{aligned} \tag{5.25}$$

$$\begin{aligned}
& - 9 * M * D * \omega^2 + k1 * D + k2 * P + 3 * C * c1 * \omega - 3 * N * c2 * \omega \\
& + 0.25 * K_{1n} * B^3 - 0.25 * K_{1n} * B * A^2 + 0.75 * K_{1n} * D^3 + \\
& 0.25 * K_{1n} * D * C^2 + 1.5 * K_{1n} * (B^2 - A^2) * D = 0
\end{aligned} \tag{5.26}$$

$$k2 * L + A * m2 * \omega^2 - L * m2 * \omega^2 - c2 * M * \omega = 0 \tag{5.27}$$

$$k2 * M + B * m2 * \omega^2 - M * m2 * \omega^2 + c2 * L * \omega = 0 \tag{5.28}$$

$$k2 * N + 9 * C * m2 * \omega^2 - 9 * m2 * N * \omega^2 - 3 * c2 * P * \omega = 0 \tag{5.29}$$

$$k2 * P + 9 * D * m2 * \omega^2 - 9 * m2 * P * \omega^2 + 3 * c2 * N * \omega = 0 \tag{5.30}$$

Using these 8 equations, values of 8 variables is found using numerical solver(fsolve) in matlab,but the limitation of using numerical method is that an initial value of A,B,C,D,L,M,N,P has to be supplied,about which the solver tries to find the solution,so we would get only the local solution in these cases.

The vibration response or FRF is obtained by getting the maximum value of  $A \sin(\omega t) + B \cos(\omega t) + C \sin(3\omega t) + D \cos(3\omega t)$  at each frequency.

We had given the 2 initial values:

- 1) All the 8 variables A,B,C,D,L,M,N and P are given a zero initial value at all the frequency,In the graph that is shown below,we have compared this solution with the response obtained through RK-4.
- 2) The second initial condition that we had supplied was that for each frequency initial values of A,B,C,D,L,M,N and P was the solution of A,B,C,D,L,M,N and P obtained for the previous frequency.For example  $A_{initial}$  for  $\omega = 0.2$  rad/s is equal to A for  $\omega=0.1$ rad/s.The solution obtained in this case is as shown in figure 5.3.



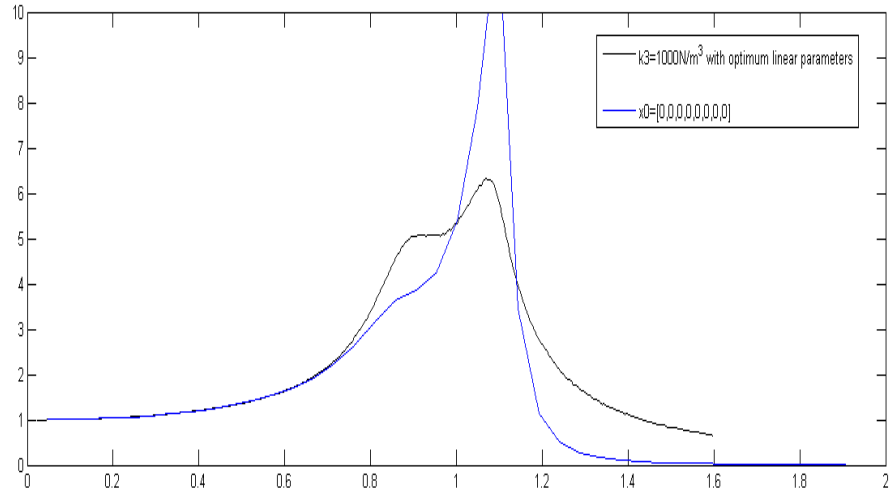


Figure 5.2: comparison of one of the solutions of third order HBM.

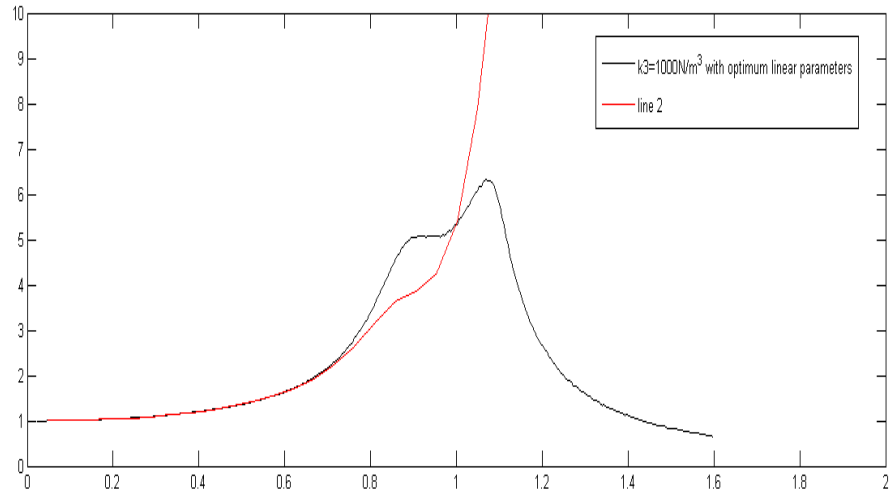


Figure 5.3: comparison of the second solutions obtained through third order HBM.

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## CHAPTER 6

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### Conclusion

## 6.1 Present work

Many researchers are interested in and have investigated the linear vibration absorber. This thesis has been concerned with the way in which other parameters such as coulomb damping, configuration or attachment of damping and nonlinearity produced by the nonlinear absorber stiffness can be put to good use in a vibration absorber. The reasons for the preference of this passive approach are to be found in the cost, simplicity, and reliability of this type of absorbers. The effect of the nonlinear vibration absorber parameters on the vibration response was investigated and the effects of such a change were noted and tabulated. The results of this research are summarized in the following.

- We started off with optimum solution proposed by Den-hartog using two point theory for a DVA without a primary mass damping. Then we had presented a max-min search when damping is introduced, as closed form solution becomes difficult to obtain, even though researchers such as Ghosh et al have extended the two point theory to this type of systems with limitations that it can be applied to low-moderate damping only.
- Most of the research in the field of DVA is concerned with the viscous damping, in this thesis we have evaluated the effects when the viscous damping is replaced with coulomb damping. It was found that only over a certain range of frequency (in the lower and upper band) coulomb damping offered a better vibration reduction than viscous damping. Overall the maximum vibration response of viscous damping is lower than the coulomb damping. Also, sometimes very high frictional force is required to achieve the required reduction, which in some cases is practically impossible to achieve and large frictional force leads to wear and tear of mechanical system.
- For a hardening stiffness nonlinear absorber design, the limitation on the value of the nonlinear stiffness parameter should be identified first. In order to produce an effective vibration bandwidth, the limitation on the value of the damping and the mass were determined. The larger the damping and the heavier the mass in the nonlinear absorber, a much wider effective vibration bandwidth will be produced compared to using a linear absorber with the same damping and mass levels.
- The nonlinear absorber has a much wider effective bandwidth compared to a conventional linear absorber. Compared to the linear absorber, the

nonlinearity has the effect of shifting the second resonance peak to a higher frequency away from the effective tuned frequency, improving the robustness of the device to mistune and on adding the cubic hardening spring in the primary system, the second peak goes up and first peak comes down and both these peaks shift towards right.

- The lower the damping in the nonlinear absorber, the effective bandwidth is slightly increased compared to the linear absorber with the same level of damping. However, larger damping in the nonlinear absorber generally produces a wider frequency vibration reduction bandwidth compared to the linear absorber. When damping in the nonlinear absorber is further increased above a certain value though, there appears to be no effective vibration bandwidth. In engineering applications, it is desirable to have a large vibration reduction bandwidth, so that the damping in the absorber needs to be quite small.
- It was seen that the parameters obtained for optimum linear system changes when we need to find an optimum FRF on introduction of non-linearity, especially  $k_2$  when a cubic non-linear spring is introduced but the damping  $c_2$  almost remains same.
- By introducing non-linearity, we can reduce the vibration of primary system. The optimum non-linear FRF lies below the linear FRF. But as said earlier the spring stiffness to obtain optimum FRF is different. Also the FRF as a whole shifts towards right.
- For a low nonlinear stiffness in the primary system, the absorber parameters can be chosen such that it produces an FRF that is better than linear optimum FRF case. But for high nonlinear stiffness, the nonlinear absorber would have higher mean square primary system displacement compared to a linear absorber. The use of a high stiffness nonlinearity does not improve the vibration reduction compared to the linear absorber case.

## 6.2 Future Work

- The numerical results for the vibration reduction bandwidth and effective tuned frequency have been obtained. However, the mathematical expressions for the vibration reduction bandwidth and effective tuned frequency have not been investigated. A recommendation is to determine the effect of

NVDA parameters on the vibration reduction bandwidth and effective tuned frequency with, if possible, analytical expressions.

- Analytical work, when a non-linearity is added to the system has tried to derive the mathematical expression for a vibration response at a particular frequency but more could be done to derive the optimum parameters for a non-linear system.

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