

We first represent the system by 1 dof : ψ . We need to write every rotational speed as a function of $\dot{\psi}$:

$$\omega_H = \tau_1 \omega_T ; \omega_T = \omega_D ; \omega_D = \tau_2 \omega_w ; \omega_w = \frac{V}{R} \Rightarrow \omega_T = \omega_D = \tau_2 \frac{V}{R} ; \omega_H = \tau_1 \tau_2 \frac{V}{R}$$

We then can compute the Lagrange equation for $\psi = \dot{\psi}$ in order to find the EoM:

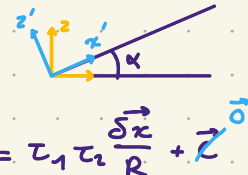
$$\frac{d}{dt} \left(\frac{\partial E_c}{\partial \dot{\psi}} \right) - \frac{\partial E_c}{\partial \psi} + \frac{\partial D}{\partial \dot{\psi}} + \frac{\partial V}{\partial \psi} = Q = \frac{\delta W}{\delta \psi}$$

$$E_c = \frac{1}{2} J_H \omega_H^2 + 2 J_w \omega_w^2 + \frac{1}{2} M V^2 + \frac{1}{2} J_T \omega_T^2 = \frac{1}{2} (J_H (\tau_1 \tau_2 \frac{V}{R})^2 + 4 J_w (\frac{V}{R})^2 + M V^2)$$

$$= \frac{1}{2} \underbrace{(J_H (\frac{\tau_1 \tau_2}{R})^2 + 4 \frac{J_w}{R^2} + M)}_{m^*} V^2 = \frac{1}{2} m^* \dot{\psi}^2$$

$$D = \frac{1}{2} (r_1 + r_2) \dot{\theta}^2 = \frac{1}{2} (r_1 + r_2) \left(\frac{\tau_2}{R} \right)^2 \dot{\psi}^2 = \frac{1}{2} r^* \dot{\psi}^2$$

$$V_R = 0$$



$$\delta W = \vec{T}_H \cdot \delta \vec{\theta}_H + \vec{F}_{DRAG} \cdot \delta \vec{x}' + \vec{F}_{ROLL} \cdot \delta \vec{x}' - M g \sin(\alpha) \vec{z}' \cdot \delta \vec{z}'$$

$$\text{and } \delta \vec{\theta}_H = \tau_1 \tau_2 \frac{\delta \psi}{R} + \vec{z}'$$

$$\Rightarrow Q = \frac{\delta W}{\delta \psi} = T_H \frac{\tau_1 \tau_2}{R} - F_D - F_R - M g \sin(\alpha)$$

$$\Rightarrow \frac{d}{dt} \left(\frac{\partial E_c}{\partial \dot{\psi}} \right) = \frac{d}{dt} (m^* \dot{\psi}) = m^* \ddot{\psi} ; \frac{\partial E_c}{\partial \psi} = 0 ; \frac{\partial D}{\partial \dot{\psi}} = r^* \dot{\psi} ; \frac{\partial V}{\partial \psi} = 0$$

$$\Rightarrow \text{EoM: } m^* \ddot{\psi} + r^* \dot{\psi} = T_H \frac{\tau_1 \tau_2}{R} - F_D - F_R - M g \sin(\alpha)$$

$$F_R = C_{RR} M g (1 + K_{RR} V)$$

$$F_D = \frac{1}{2} \rho_a C_x A v_{rel}^2 ; v_{rel}^2 = (V - V_{wind})^2 \Rightarrow F_D(V, V_w) = \frac{1}{2} \rho_a C_x A (V - V_w)^2$$

we consider that wind is horizontal

$$\rightarrow \text{linearization: } F_D(V, V_w) \approx F_D(V_0, V_{w0}) + \left. \frac{\partial F_D}{\partial V} \right|_{V_0, V_{w0}} (V - V_0) + \left. \frac{\partial F_D}{\partial V_w} \right|_{V_0, V_{w0}} (V_w - V_{w0})$$

$$\text{By writing } V = V_0 + \delta V ; V_w = V_{w0} + \delta V_w \rightarrow \dot{\psi} = \delta \dot{V} :$$

$$F_D(\delta V, \delta V_w) \approx \frac{1}{2} \rho_a C_x A ((V_0 - V_{w0})^2 + 2(V_0 - V_{w0})(\delta V - \delta V_w))$$

$$\Rightarrow m^* \delta \dot{V} + r^* (V_0 + \delta V) = (T_{H0} + T_C) \frac{\tau_1 \tau_2}{R} - \frac{1}{2} \rho_a C_x A ((V_0 - V_{w0})^2 + 2(V_0 - V_{w0})(\delta V - \delta V_w)) - C_{RR} M g (1 + K_{RR}(V_0 + \delta V)) - M g \sin \alpha$$

$$\Leftrightarrow m^* \delta \dot{V} + \delta V (r^* + C_{RR} K_{RR} M g + \rho_a C_x A (V_0 - V_{w0})) = (T_{H0} + T_C) \frac{\tau_1 \tau_2}{R} - \frac{1}{2} \rho_a C_x A ((V_0 - V_{w0})^2 - 2(V_0 - V_{w0}) \delta V_w) - C_{RR} M g (1 + K_{RR} V_0) - M g \sin \alpha - r^* V_0$$

We can compute the steady-state torque T_{H0} by having $\delta V = 0$ and $\delta V_w = 0$:

$$T_{H0} \frac{\tau_1 \tau_2}{R} - \frac{1}{2} \rho_a C_x A (V_0 - V_{w0})^2 - C_{RR} M g (1 + K_{RR} V_0) - M g \sin \alpha - r^* V_0 = 0$$

$$\Leftrightarrow T_{H0} = \frac{R}{\tau_1 \tau_2} \left(\frac{1}{2} \rho_a C_x A (V_0 - V_{w0})^2 + M g (C_{RR} (1 + K_{RR} V_0) + \sin \alpha) + r^* V_0 \right)$$

We can then compute numerically this torque for $V_0 = 15 \text{ m.s}^{-1}$ and $V_{w0} = 3,5 \text{ m.s}^{-1}$:

$$T_{H0} = 173,2237 \text{ or } 183,1278 \text{ N.m depending on the direction of the wind.}$$

$$m^* \delta \dot{V} + \delta V (r^* + C_{RR} K_{RR} M g + \rho_a C_x A (V_0 - V_{w0})) = T_C \frac{\tau_1 \tau_2}{R} + \rho_a C_x A (V_0 - V_{w0}) \delta V_w$$

$$G = \frac{1}{m^* \delta^2 + r^* \delta} \frac{\tau_1 \tau_2}{R} \quad ??$$