Siringability

$$\Delta P = \frac{Q \cdot 8 \cdot \eta \cdot l}{\pi \cdot R^4}$$

$$Q = 0, 2 \frac{ml}{s} = 2 \cdot 10^{-7} \frac{m^3}{s}$$

$$L_{motor} = \tau \cdot \vartheta$$

$$L_{worm} = F_{worm} \bullet \Delta x_{worm} = P \cdot A \cdot pitch \cdot n^\circ threads \cdot n^\circ motor RPM$$

$$pitch = 2mm$$

$$n^\circ threads = 4$$

$$n^\circ motor RPM = \frac{\vartheta}{2\pi}$$

To assess whether the torque delivered by the motor is suitable to deliver the drug, we consider the following condition:

$$\begin{split} L_{motor} & \geq L_{worm} \\ L_{motor} & = L_{worm} \rightarrow \tau \cdot \vartheta = P \cdot A \cdot pitch \cdot n^{\circ} \ threads \cdot \frac{\vartheta}{2\pi} \\ & \rightarrow \tau = P \cdot A \cdot pitch \cdot n^{\circ} \ threads \cdot \frac{1}{2\pi} \cdot dissipative \ effect \\ A & = \pi \cdot R^2 = \pi \cdot \left(6.5 \cdot 10^{-3} \ m\right)^2 = 1,327 \cdot 10^{-4} \ m^2 \\ P & = \Delta P + P_{vene} \\ P_{vene} & = 20 \ mmHg = 2666,45 \ Pa \\ \Delta P & = \Delta P_{syringe} + \Delta P_{catheter} + \Delta P_{needle} \end{split}$$

We consider water delivery:

$$\eta = 8.9 * 10^{-4} Pa * s$$

1) Syringe Pressure:

$$R_{syringe} = 6,5 mm = 6,5\cdot10^{-3} m$$

$$l_{syringe} = 37.67 mm = 37.67\cdot10^{-3} m$$

$$\Delta P_{syringe} = \frac{Q\cdot8\cdot\eta\cdot l}{\pi\cdot R^4} = \frac{2\cdot10^{-7}\frac{m^3}{s}\cdot8\cdot8,9*10^{-4}Pa^*s\cdot37.67\cdot10^{-3}m}{\pi\cdot(6.5\cdot10^{-3}m)^4} = 9,57\cdot10^{-3} Pa$$

2) Catheter Pressure:

$$R_{catheter} = 5 mm = 5.10^{-3} m$$

$$l_{catheter} = 1,5 m$$

$$\Delta P_{catheter} = \frac{Q \cdot 8 \cdot \eta \cdot l}{\pi \cdot R^4} = \frac{2 \cdot 10^{-7} \frac{m^3}{s} \cdot 8 \cdot 8,9 \cdot 10^{-4} Pa^* s \cdot 1,5 m}{\pi \cdot \left(5 \cdot 10^{-3} m\right)^4} = 1,088 Pa$$

3) Needle (22GG) Pressure:

$$R_{needle} = 0.7 mm = 0.7 \cdot 10^{-3} m$$

$$l_{needle} = 32 mm = 32 \cdot 10^{-3} m$$

$$\Delta P_{needle} = \frac{Q \cdot 8 \cdot \eta \cdot l}{\pi \cdot R^4} = \frac{2 \cdot 10^{-7} \frac{m^3}{s} \cdot 8 \cdot 8.9 \cdot 10^{-4} Pa^* s \cdot 32 \cdot 10^{-3} m}{\pi \cdot (0.7 \cdot 10^{-3} m)^4} = 60,411 Pa$$

$$\Delta P = \Delta P_{syringe} + \Delta P_{catheter} + \Delta P_{needle} = 9,57 \cdot 10^{-3} Pa + 1,088 Pa + 60,411 Pa = 61,51 Pa$$

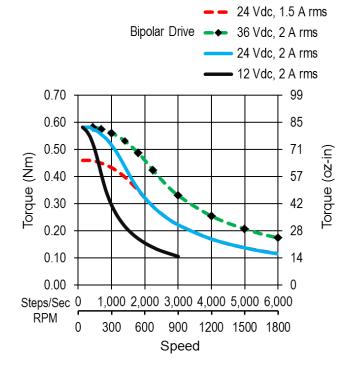
$$P = \Delta P + P_{vene} = 61,51 Pa + 2666,45 Pa = 2727,96 Pa$$

$$\tau = P \cdot A \cdot step \cdot n^{\circ} threads \cdot \frac{1}{2\pi} = 2727,96 Pa \cdot 1,327 \cdot 10^{-4} m^{2} \cdot 2 \cdot 10^{-3} m \cdot 4 \cdot \frac{1}{2\pi} = 4,6 \cdot 10^{-4} Nm$$

$$v_{motore} = micro_stepping \ number \cdot \frac{Q}{A} = 2 \cdot \frac{2 \cdot \frac{10^{-7} m^{3}}{s}}{\pi^{*} (6,5 \cdot 10^{-3} m)^{2}} = 3.014 \cdot 10^{-3} \frac{m}{s} = 3.014 \cdot \frac{mm}{s}$$

$$v_{motore_RPM} = v_{motore} \bullet \frac{30}{\pi} \bullet \frac{1}{R_{worm}} = 3.014 \cdot 10^{-3} \frac{m}{s} \bullet \frac{30}{\pi} \bullet \frac{1}{4 \cdot 10^{-3} m} = 7,2 \text{ rpm} = 0.12 \text{ rps}$$

$$= 48 \text{ pps}$$



For a velocity of 7,2 rpm, from the graph we can observe a torque approximately equal to the maximum torque (0.59 Nm). The torque obtained for our application (4, $6\cdot10^{-4}$ Nm) is less than the maximum torque that can be delivered by the motor at this speed.

This demonstration can be applied to any drug that has the same rheological properties as water.

We calculate the torque that the motor must generate to allow the drug to be injected into the vein, considering increasing flows:



Two types of needles are evaluated in detail:

Needle 18G

• Needle radius: 1.2 mm

• Needle length: 38 mm

$$P_{needle1} = \frac{\frac{Q \cdot 8 \cdot \eta \cdot l_{ago1}}{\pi \cdot (R_{ago1})^4}}{\frac{1}{\pi \cdot (R_{ago1})^4}}$$

Needle 22G

• Needle radius: 0.7 mm

• Needle length: 32 mm

$$P_{needle2} = \frac{\frac{Q \cdot 8 \cdot \eta \cdot l_{ago2}}{\pi \cdot (R_{ago2})^4}$$

Working conditions:

$$\tau_{motor} < \tau_{motor_{max}} = 0.59 \, Nm$$

$$\tau = P \cdot A \cdot step \cdot n^{\circ} threads \cdot \frac{1}{2\pi} < \tau_{motor_{max}}$$

$$P < \frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads}$$

$$P = \Delta P + P_{veins}$$

$$\Delta P + P_{veins} < \frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads}$$

$$\Delta P < \frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads} - P_{veins}$$

$$\Delta P = \Delta P_{syringe} + \Delta P_{catheter} + \Delta P_{needle}$$

We determine a relationship to determine the size of the needle to be used in our application:

$$\begin{split} \Delta P_{needle} < \frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads} - P_{veins} - \Delta P_{syringe} - \Delta P_{catheter} \\ \Delta P_{needle} = \frac{Q \cdot 8 \cdot \eta \cdot l}{\pi \cdot R^4} \\ \frac{l}{e^4} < \frac{\pi \cdot (\frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads} - P_{veins} - \Delta P_{syringe} - \Delta P_{catheter})}{O \cdot 8 \cdot n} \end{split}$$

We determine a relationship to establish the allowable viscosity value:

$$\Delta P = \eta \left(\frac{Q \cdot 8 \cdot l_{s}}{\pi \cdot R_{s}^{4}} + \frac{Q \cdot 8 \cdot l_{c}}{\pi \cdot R_{s}^{4}} + \frac{Q \cdot 8 \cdot l_{n}}{\pi \cdot R_{n}^{4}} \right) < \frac{\tau_{motor_{max}} \cdot 2\pi}{A \cdot step \cdot n^{\circ} threads} - P_{veins}$$

$$\eta < \frac{\frac{\tau_{motor_{max}}^{\bullet 2\pi} - P_{veins}}{A \cdot stepn's threads} - P_{veins}}{\left(\frac{Q \cdot 8 \cdot l_s}{\pi \cdot R_s^4 + \pi \cdot R_c^4 + \frac{Q \cdot 8 \cdot l_n}{\pi \cdot R_n^4}}\right)}$$