

# **Performance Enhancement of Boiler, Heat Exchanger and Evaporator Pilot-Plants**

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# **Chapter 1**

# **Introduction**

## **1.1 Introduction**

A pilot plant is a small industrial system which is operated to generate information about the behavior of the system for use in design of larger facilities. The pilot plant can be used for training personnel for a full-scale plant. The main objective is to enthuse students to conduct experiments by arousing their curiosity. This would help them in learning basic and advanced concepts through remote experimentation. To share costly equipment and resources, which are otherwise available to limited number of users due to constraints on time and geographical distances we are communicating our plant around the world through virtual labs. Virtual Labs would cater to students at the undergraduate level, post graduate level as well as to research scholars.

Pilot plants are available to control from variety of controllers like Programmable Logic Controllers, Distributed Control Systems and simulation tools and test control strategies. Comparative studies can be done not only in class of control strategies but also in class of different controllers.

The main aim of this work is to make this pilot-plants run continuously and efficiently from local as well as remote domain

## **1.2 Problem Statement**

Focus on enhancing the performance of Boiler Heat Exchanger and Evaporator Pilot Plants for running the Pilot Plants continuously and efficiently

## **1.3 Objective**

The objective of this project as follows :

1. Putting the Pilot-Plant back in service & Recommissioning.
2. Recommissioning of Boiler, Heat Exchanger & Evaporator Pilot Plant with
  - Local PLC (Micrologix 1400)
  - Remote PLC (RXLogix 5000)
  - DCS (Emerson DeltaV)
  - Virtual PLC
  - Virtual DCS

3. Development of SCADA for Boiler,Heat Exchanger & Evaporator Pilot Plant.
4. Networking of different Pilot Plants
5. Make both the pilot plants fully functional.

**Part I**

**Boiler And Heat Exchanger**

# Chapter 2

## Literature Survey

### 2.1 Functional definition

#### 1. Boiler

A boiler is an enclosed vessel that provides a means for combustion heat to be transferred into water until it becomes heated water or steam. The hot water or steam under pressure is then usable for transferring the heat to a process. Water is a useful and cheap medium for transferring heat to a process. When water is boiled into steam its volume increases about 1,600 times, producing a force that is almost as explosive as gunpowder. This causes the boiler to be extremely dangerous equipment that must be treated with utmost care.[1].

The process of heating a liquid until it reaches its gaseous state is called evaporation. Heat is transferred from one body to another by means of (1) radiation, which is the transfer of heat from a hot body to a cold body without a conveying medium, (2) convection, the transfer of heat by a conveying medium, such as air or water and (3) conduction, transfer of heat by actual physical contact, molecule to molecule.

Boiler Make & Year	:	Non IBR Boiler & 2012
MCR(Maximum Continuous Rating)	:	30Kg/hr
Rated Working Pressure	:	3.5 Bar
Type of Boiler	:	Drum Boiler

Table 2.1: Boiler Specification

#### 2. Boiler Specification

The heating surface is any part of the boiler metal that has hot gases of combustion on one side and water on the other. Any part of the boiler metal that actually contributes to making steam is heating surface. The amount of heating surface of a boiler is expressed in square meters.

#### 3. Indian Boiler Regulation

The Indian Boilers Act was enacted to consolidate and amend the law relating to steam boilers. Indian Boilers Regulation (IBR) was created in exercise of the powers conferred by section 28 & 29 of the Indian Boilers Act.

**IBR Steam Boilers** means any closed vessel exceeding 22.75 liters in capacity and which is used expressively for generating steam under pressure and includes any mounting or other fitting attached to such vessel, which is wholly, or partly under pressure when the steam is shut off.

**IBR Steam Pipe** means any pipe through which steam passes from a boiler to a prime mover or other user or both, if pressure at which steam passes through such pipes exceeds 3.5 kg/cm<sup>2</sup> above atmospheric pressure or such pipe exceeds 254 mm in internal diameter and includes in either case any connected fitting of a steam pipe.

#### 4. Boiler Blowdown

When water is boiled and steam is generated, any dissolved solids contained in the water remain in the boiler. If more solids are put in with the feed water, they will concentrate and may eventually reach a level where their solubility in the water is exceeded and they deposit from the solution. Above a certain level of concentration, these solids encourage foaming and cause carryover of water into the steam. The deposits also lead to scale formation inside the boiler, resulting in localized overheating and finally causing boiler tube failure.

It is, therefore, necessary to control the level of concentration of the solids and this is achieved by the process of blowing down', where a certain volume of water is blown off and is automatically replaced by feed water thus maintaining the optimum level of total dissolved solids (TDS) in the boiler water. Blow down is necessary to protect the surfaces of the heat exchanger in the boiler. However, blow down can be a significant source of heat loss, if improperly carried out.

#### 5. Shrink and swell effect in Boiler

For the Boilers working at very high pressures and large evaporation rates,a phenomenon called swelling and shrinking of drum level makes such simple control strategies inadequate.

When steam demand increases pressure decreases, this results in formation of bubbles which indicates level high. This phenomenon is called as shrink. This absurd increase in the level will cause decrease in feed flow rate. Because of high drum pressure, bubbles formation increases. This phenomenon is called swell which causes further decrease in level.

#### 6. Heat Exchanger

A heat exchanger is a piece of equipment built for efficient heat transfer from one medium to another. The media may be separated by a solid wall, so that they never mix, or they may be in direct contact. They are widely used in space heating, refrigeration, air conditioning, power plants, chemical plants, petrochemical plants, petroleum refineries, natural gas processing, and sewage treatment. There are two primary classifications of heat exchangers according to their flow arrangement. In parallel-flow heat exchangers, the two fluids enter the exchanger at the same end, and travel in parallel to one another to the other side. In counter-flow heat exchangers the fluids enter the exchanger from opposite ends.

A double-pipe heat exchanger is the simplest type of heat exchanger and can operate with co-current or counter-current flow. The design consists of a single small pipe (tube-side) inside of a larger one (shellside). A co-current heat exchanger is most commonly

used when you want the exiting streams to leave the exchanger at the same temperature. A counter-current heat exchanger is used more often than co-current because they allow for a more efficient transfer of energy.

#### 7. **Fouling in Heat Exchanger**

Fouling is the accumulation of unwanted material on solid surfaces which can contain living organisms (biofouling) or nonliving material. Fouling includes deposit formation, encrustation, crudding, deposition, scaling, scale formation, slagging, and sludge formation

## 2.2 Expected Outcome

1. Both the pilot plant will be fully functional.
2. User will able to control the plant by Local PLC, Remote PLC, Remote DCS, Virtual PLC & Virtual DCS.
3. User will able to monitor the plant by SCADA and will get alarm if something goes wrong.
4. Interconnection of various plants so as to run them simultaneously and in interaction
5. As an outcome we are expecting the pilot plants should run continuously and efficiently

## Chapter 3

# Insight of Boiler And Heat Exchanger Pilot-plants

### 3.1 Process Description

We have a pilot plant of Electrical Boiler and Pipe in pipe type Heat Exchanger as shown in below picture.



Figure 3.1: Boiler and Heat Exchanger Pilot plant Pilot Plant

The boiler drum made up SS304 contains water which is electrically heated with a PWM controller and generates steam at 4 bar and 144C. The water for heating is pumped from

a boiler feed water tank using a positive displacement pump. The steam generated flows towards the heat exchanger through an equal percentage globe valve which controls the steam flow.

The heat exchanger being of tubular counter flow type, water to be heated is pumped from a cold water tank from the other end using a centrifugal pump. The condensate formed in the heat exchanger during heat transfer is collected in a separate condensate tank. The hot water is collected in hot water tank which also be either mixed in the cold water tank or can be added partially/fully to the feed to the boiler to change the feed water temperature.

The boiler pilot plant is providing steam to other pilot plants such as evaporator, bio-reactor and batch process. The heat exchanger pilot plant is giving hot water for sterilization process of bio-reactor pilot plant and is able to provide hot water to batch process for CIP

### 3.2 Variables Measured

Following process variables are measured (Parenthesis content represents tag of variables):

1. Level of water in the boiler drum (LT-1)
2. Drum pressure (PT-1)
3. Steam temperature (TT-1)
4. Boiler feed water temperature (TT-5)
5. Boiler feed water flow ((FT-2))
6. Temperature from water from hot water tank for mixing with boiler feed water (TT-4)
7. Steam flow (FT-3)
8. Heat exchanger steam inlet temperature (TT-2)
9. Heat exchanger water inlet temperature (TT-4)
10. Heat exchanger water outlet temperature (TT-3)
11. Heat exchanger water flow (FT-1)

### 3.3 Function of important components

The instrumentation components in the boiler and heat exchanger plant can be divided in the following groups:

1. Sensors and transmitters

The transducer measures a process variable while the transmitter transmits the data to the controller as a 4-20 mA current signal.(List with tag name are mentioned in index-A)

2. Final control elements

The final control element adjusts the amount of energy/mass that goes into or out from process as commanded by the controller. Following are the final control elements used in the plant:

a. Positive displacement pump for feeding boiler feed water : The speed of the motor and in turn feed flow is changed using variable frequency drive.

b. Centrifugal pump for feeding cold water to heat exchanger: The speed of the motor

- and in turn feed flow is changed using variable frequency drive.
- c. Equal percentage globe control valve for manipulating steam flow : Current signal from controller is converted to pneumatic signal using an I/P converter which decides the valve opening.
  - d. Solenoid valve which has 2 positions (open or close): Opening of the valve allows mixing of hot water with the cold water feed for heat exchanger as well as changing the boiler feed water temperature.

### 3. Safety components

These components ensure process safety which generally refers to the prevention of unintentional releases of chemicals, energy, or other potentially dangerous materials (including steam) during the course of process that can have a serious effect to the plant and environment. Process safety involves, for example, the prevention of leaks, spills, equipment malfunction, over-pressures, over-temperatures, corrosion, metal fatigue and other similar conditions. Following instruments are included to keep process variables under safe limit as well as provide alarms interlocks to automatically take necessary action:

- a. Pressure switch and temperature switch : Shuts off the boiler if drum pressure/temperature exceeds 4 bar/144 deg C .
- b. Low level switches: For the boiler drum this switch, shuts off the heater if there is no water in the drum. For other tanks these switches are used to avoid dry running of pumps if there is nothing to pump in the tanks.
- c. High level switches :Provided to the cold water and hot water tanks to avoid overflow of liquid.

## 3.4 Plant Control

Plant can be controlled in various ways mentioned as follows,

- Local controllers
- Matlab
- Remote Triggering (VPLC/VDCS)
- Contrologix PLC (Central PLC)
- Deltav DCS

To achieve these many ways of control, we communicate a local plant PLC (Micrologix 1400-1766 L32BWA) with a analog and 5 digital cards woth respective controller.We divide plant control methodologies in two ways as Local and Remote, where local way includes local controllers like 3 element controller from yokogawa (US3000) and Invensys temperature controller(3200 Series PID Temperature controllers) with on-off switches for pumps and heater as well as MATLAB.In remote way, includes Remote Triggering (VPLC/VDCS),Contrologix PLC (Central PLC), Deltav DCS.For a selection of controller, a hard switch on panel has given.



Figure 3.2: Local Panel for Boiler and Heat Exchanger

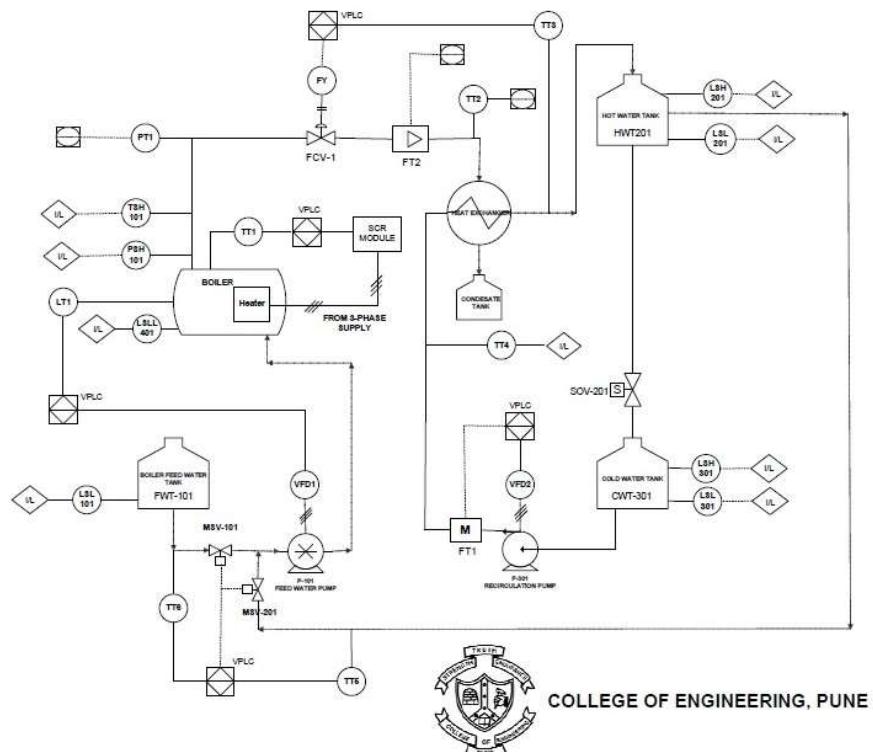


Figure 3.3: Piping and Instrument Drawing of Boiler and Heat Exchanger

### 3.5 Piping and Instrument Drawing of Boiler and Heat Exchanger

### 3.6 modeling equations of Boiler and Heat Exchanger

1. Boiler

Much of the behavior of the system can be captured by global mass and energy balances. Let the inputs to the system be the heat  $Q$ , the feed water mass flow rate  $q_f$ , and the steam mass flow rate  $q_s$ . Furthermore, let the outputs of the system be drum pressure  $p$ , and drum water level,  $l$ . This way of characterizing the system is convenient for modeling. To write the equations, let  $V$  denote volume,  $\rho$  denotes specific density,  $u$  specific internal energy,  $h$  specific enthalpy,  $t$  temperature and  $q$  flow rate. Furthermore, let subscripts s, w, f and m refer to steam, water, feed water, and metal, respectively. The total mass of drum is  $m_t$  and the specific heat of the metal is  $C_p$ . Mass balance and energy balance equation will be as following,

$$\frac{d}{dt} \{\rho_s V_{st} + \rho_w V_{wt}\} = q_f - q_s \quad (3.1)$$

$$\frac{d}{dt} \{\rho_s u_s V_{st} + \rho_w u_w V_{wt} + m_t C_p t_m\} = Q + q_f h_f + q_w h_w \quad (3.2)$$

Modifying mass balance equation,

$$\begin{aligned} \frac{d}{dt} \{\rho_s V_{st} + \rho_w V_{wt}\} &= q_f - q_s \\ V_{st} \frac{d\rho_s}{dt} + \rho_s \frac{dV_{st}}{dt} + \rho_w \frac{dV_{wt}}{dt} &= q_s - q_s \end{aligned} \quad (3.3)$$

As  $\rho_w = constant$ ; its derivative becomes zero.

Substituting in equation(4);

$$V_{st} = V_d - V_{wt} \quad (3.4)$$

$$(V_d - V_{wt}) \frac{d\rho_s}{dt} + \rho_s \frac{(V_d - V_{wt})}{dt} + \rho_w \frac{dV_{wt}}{dt} = q_s - q_s \quad (3.5)$$

$$(V_d - V_{wt}) \frac{d\rho_s}{dp} \frac{dp}{dt} + \rho_s \frac{d(V_{wt})}{dt} + \rho_w \frac{d(V_{wt})}{dt} = q_s - q_s \quad (3.6)$$

$$(V_d - Ah) \frac{d\rho_s}{dp} \frac{dp}{dt} + A(\rho_w - \rho_s) \frac{dh}{dt} = q_s - q_s \quad (3.7)$$

Modifying energy balance equation,

$$\frac{d}{dt} \{\rho_s u_s V_{st} + \rho_w u_w V_{wt} + m_t C_p t_m\} = Q + q_f h_f + q_w h_w$$

Since internal energy is  $(u = h - p/\rho)$ , by substituting this relation in energy balance equation with equation(5);

$$\begin{aligned} \frac{d}{dt} \{\rho_s h_s V_{st} - pV_{st} + \rho_w h_w V_{wt} - pV_{wt} + m_t C_p t_m\} &= Q + q_f h_f + q_w h_w \\ \frac{d}{dt} \{\rho_s h_s (V_d - V_{wt}) - pV_d + \rho_w h_w V_{wt} + m_t C_p t_m\} &= Q + q_f h_f + q_w h_w \\ h_s (V_d - V_{wt}) \frac{d\rho_s}{dt} + \rho_s (V_d - V_{wt}) \frac{dh_s}{dt} + \rho_s h_s \frac{d(V_d - V_{wt})}{dt} \\ - \frac{dpV_d}{dt} + \rho_w V_{wt} \frac{dh_w}{dt} + \rho_w h_w \frac{dV_{wt}}{dt} + m_t C_p \frac{dt_m}{dt} &= Q + q_f h_f + q_w h_w \\ h_s (V_d - V_{wt}) \frac{d\rho_s}{dt} + \rho_s (V_d - V_{wt}) \frac{dh_s}{dt} + \end{aligned} \quad (3.8)$$

We can write equation(4) and (12) in of state space form;

$$m_{11} \frac{dV_{wt}}{dt} + m_{12} \frac{dp}{dt} = q_s - q_s \quad (3.9)$$

$$m_{21} \frac{dV_{wt}}{dt} + m_{22} \frac{dp}{dt} = Q + q_f h_f + q_w h_w \quad (3.10)$$

where;

$$\begin{aligned}
 m_{11} &= (\rho_w - \rho_s) \\
 m_{12} &= (V_d - V_{wt}) \frac{d\rho_s}{dp} + V_{wt} \frac{d\rho_s}{dp} \\
 m_{21} &= (\rho_w h_w - \rho_s h_s) \\
 m_{22} &= (V_d - V_{wt}) \left( \rho_s \frac{dh_s}{dp} + h_s \frac{d\rho_s}{dp} \right) + \rho_w V_w \frac{dh_s}{dp}
 \end{aligned} \tag{3.11}$$

When we solve equation (11) and (12) simultaneously for  $(\frac{dV_{wt}}{dt})$  and  $(\frac{dp}{dt})$  we will get result as following,

$$\frac{dV_{wt}}{dt} = \frac{Qm_{12} + \rho_w q_w (h_f m_{12} - m_{22}) - \rho_s q_s (h_s m_{12} - m_{22})}{(m_{12} m_{21} - m_{11} m_{22})} \tag{3.12}$$

$$\frac{dp}{dt} = \frac{\rho_w q_w - \rho_s q_s - m_{11} \frac{dV_{wt}}{dt}}{m_{12}} \tag{3.13}$$

## 2. Heat Exchanger

As we discussed in previous chapter, we have counter-current pipe in pipe type heat exchanger setup with all necessary sensors and actuators installed.

Since heat exchangers are so widely used in industry, it is necessary for a chemical engineer to be able to optimize and control the system and know how independent variables will affect the outputs from system. To do this, a dynamic model is developed and utilized.

A dynamic model of a heat exchanger may be used, for example, to predict how a change in the fluid flow rates or the addition of an insulating jacket will affect the outlet temperature of the product stream. The model uses ordinary differential equations (ODEs) to describe the process and gives plots of the variables vs. time for the entire process. There are many independent variables in a heat exchanger, which can cause modeling to be very complex since multiple ODEs are required to define all of the process variables.

(a) Shell side (Outer Pipe)

- i. Fluid
- ii. Flow rate
- iii. Temperature

(b) Tube side (Inner Pipe)

- i. Fluid
- ii. Flow rate
- iii. Temperature

(c) Flow Configuration

*As there is no mass accumulation so mass balance will not apply in Heat Exchanger*

## 3. Fouling in Heat Exchanger

Fouling is the accumulation of unwanted material on solid surfaces which can contain living organisms (biofouling) or nonliving material. Fouling includes deposit formation, encrustation, crudding, deposition, scaling, scale formation, slagging, and sludge formation. Mathematical perspective of fouling is explained in this section with its effect

on heat exchanger and ways to remove it.

Fouling is a deposit of extraneous material that appears upon the heat transfer surface during lifetime of heat exchanger. This deposit adds heat resistance to heat transfer and operational capability of heat exchanger gets reduced. If deposit is in heavy content, then it causes significant change in flow rate and pressure is dropped which can be given mathematically as follows, For both smooth and rough tubes, estimate of pressure drop can be given as follows,

$$\frac{\Delta p}{\Delta L} = \xi \frac{\rho u^2}{2d_i} \quad (3.14)$$

where;

$\xi$ = friction factor for smooth tubes,  $\xi = 0.0056 + 0.5R_e^{-0.32}$

For rough tubes,  $\xi = 0.0014 + 1.056R_e^{-0.42}$

$\Delta p$ =pressure drop

$\Delta L$ =change in length

$u$ =flow velocity

$\rho$ =density

$d_i$ =inner diameter

Fouling parameters are as follows,

- (a) fouling thickness ( $d_f$ )
- (b) fouling resistance ( $R_f$ )
- (c) heat transfer coefficient ( $U_f$ )

We can derive above parameters in two ways; theoretically and experimentally. Necessary mathematical relation is explained as below,

$$R_f = \frac{d_i}{2\lambda_d} \ln \frac{d_i}{d_f} \quad (3.15)$$

$$d_f = d_i \exp \left( \frac{2\lambda_d R_f}{d_i} \right) \quad (3.16)$$

where  $\lambda_d$  is thermal conductivity.

Total heat transfer rate can be given as (Subscript  $f$  denotes fouled condition),

$$\dot{Q} = UA\Delta T_m \quad (3.17)$$

$$\frac{1}{U_f} = \frac{1}{U_{clean}} + R_f \quad (3.18)$$

$$\dot{Q}_f = U_f A_f \Delta T_{mf} \quad (3.19)$$

where  $U$  denotes temperature coefficient,  $A$  is effective area of heat transfer and  $\Delta T_m$  denotes logarithmic temperature difference.

For plate type Heat Exchanger, coefficient of heat transfer ( $U_f$ ) can be estimated theoretically using following relation,

$$U_f = \frac{1}{\left( \frac{A_o}{A_i h_i} \right) + \left( \frac{A_o R_f}{A_i} \right) + \left( \frac{A_o \ln \frac{d_o}{d_i}}{2\lambda_d L} \right)} \quad (3.20)$$

We can evaluate  $U_{actual}$  experimentally from equation, where we know  $\Delta T_m$ ,  $A$  and  $\dot{Q}$ , we calculate  $R_f$  from  $U_{clean}$  using following relations,

$$\dot{Q} = U_{actual} A \Delta T_m \quad (3.21)$$

$$R_f = \frac{1}{U_{clean}} - \frac{1}{U_{actual}} \quad (3.22)$$

For pipe in pipe type heat exchanger, thickness of fouling can be calculated as,

$$d_f = \frac{(R^2 + 1)^{0.5} \ln \left( \frac{1-S}{1-RS} \right)}{(R-1) \ln \left[ \frac{2-S(R+1-(R^2+1)^{0.5})}{2-S(R+1-(R^2+1)^{0.5})} \right]} \quad (3.23)$$

$$R = \frac{T_1 - T_2}{t_2 - t_1} \quad S = \frac{1}{R} \quad (3.24)$$

Thus we can evaluate fouling parameters for plate type as well as for tubular type heat exchanger. We can classify the methods to remove fouling in two ways as offline and online. In offline technique, heat exchangers are cleaned by mechanical and chemical means. In online mechanical cleaning, citric acid is used for where process fluid is water. In some systems, filters, cyclones (inlet), brushes, vibrating springs and scrubbing devices, grit blasting are used. In some systems, hydro-steam cleaning technique is used by high pressure jet washing with or without chemical. Sometimes, abrasive bullets are forced through tubes by compressed air. These bullets have advantage of being able to negotiate tube bends, unlike other mechanical terms.

Thus fouling causes low heat transfer and pressure drop which eventually causes loss in energy and product quality and quantity for which heat exchangers should be cleaned regularly.

# Chapter 4

## Control Strategies

This chapter focuses on control schemes for our plant. Each sections of this chapter tell us the scope of control strategies and there implementation in various domains such as local and remote. It focuses on Boiler Drum level control and introduces MPC in Delta V DCS.

### 4.1 Local Domain

Boiler and heat exchanger plant has got some extra features when compared with the other pilot plants. It has got a dedicated three element controller from Yokogawa for boiler drum level control and a dedicated temperature controller from Eurotherm for heat exchanger temperature control. So the local PLC is not controlling the boiler level and temperature of heat exchanger. Local PLC role is to take care of the interlocks and transferring inputs and outputs to the remote domains such as DCS, Contrologix PLC and so on.

#### 4.1.1 Yokogawa Three Element Controller US1000

The US1000-11 Dual Loop Digital Indicating Controller can easily be implemented as a three element boiler drum level/feed water controller. Steam drum level control is necessary to add makeup water as steam is delivered into the header pipe. The level measurement and feed water flow input are the process variables (PV) for a cascade control strategy. A steam flow signal is applied to the feed forward input of the US1000 allowing it to anticipate changes in the steam demand and adjust the feed water flow rate accordingly.

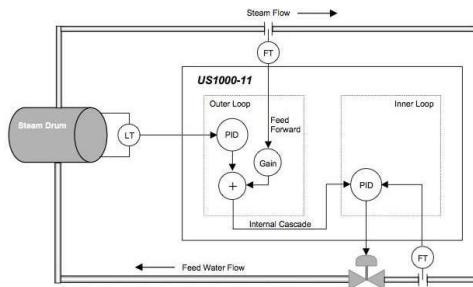


Figure 4.1: US1000 Three element control scheme

Multiple inputs allow the three element configuration for boilers with varying steam demands and feed water pressure. The digital communication option allows connectivity to a PC, providing an operator interface. US1000 is the right choice in digital control.

## Inputs/Outputs

- The three analog inputs are pre-assigned for 1-5VDC. Square root extraction can be applied to the flow inputs if differential pressure transmitters are used. Input filters can be used for noisy flow signals.
- The control output is assigned as a 4-20mA signal. The level input can be retransmitted as an isolated 1-5VDC signal to a recorder or other receiving device. The US1000-11 has two isolated 24VDC supplies to power two field transmitters.
- Five discrete inputs are pre-assigned and functionality may be changed while configuring the US1000. DI1 allows the output to the feed water valve to be forced to a pre-set output value, e.g., fully open. If the contact input is made. DI2 allows the inner (feed water) control loop to be forced to AUTO, bypassing the CASCADE (remote) set point input from the outer level controller. DI3-5 permit switching from CASCADE/AUTO or AUTO/MANUAL.
- Four discrete outputs are available for alarming. The default functions are high and low alarms for both control loops. During configuration, the functions can be changed for specific requirements.



Figure 4.2: US1000 Three element controller from Yokogawa

#### 4.1.2 Temperature controller form Eurotherm

1/4 DIN Model Number 3204 Eurotherm from Schneider Electric is the temperature controller which takes temperature Transmitter (TT-3) as Process variable and manipulate FCV opening to regulate the hot water temperature.



Figure 4.3: 3204 Eurotherm temperature controller

### 4.2 Controlling from ControlLogix system 1756-L61

The ControlLogix system of series 1756-L61 is chassis-based and provides the option to configure a control system that uses sequential, process, motion, and drive control in addition to communication and I/O capabilities.

RSLogix 5000 is a programming software of ControlLogix which offers an easy-to-use IEC61131-3 compliant interface. It provides ladder logic, structured text, function block diagram and sequential function chart editors for program development as well as support for the S88 equipment phase state model for batch and machine control applications. We also used RSView32 works to develop SCADA and to log data. RSView32 is an integrated, component-based HMI for monitoring and controlling automation machines and processes. It also integrates Microsoft's popular Visual Basic for Applications (VBA) as a built-in programming language and supports OPC standards as both a server and a client for fast, reliable communications with a wide variety of hardware devices.

Ladder programming for boiler and heat exchanger plant is done in ControlLogix system and developed SCADA for the same. The implemented controllers are explained in detail in this section. We consider variables as shown in Table (4.1).

### 4.3 Boiler Drum Level control

#### 4.3.1 Overview

Proper operation of Drum Level Measurement and Control circuit is very crucial for uninterrupted operation of Boiler. Principle of measurement and three-element control of Boiler

Sr.No.	Controlled Variable	Manipulated Variable
1	Boiler Level	Feed Pump Speed Or Steam flow rate
2	Boiler Temperature	SCR
3	Heat Exchanger Outlet Temperature	Cold water pump speed Or Control Valve

Table 4.1: List of controlled and corresponding manipulated variable

Drum Level is explained here. Steam drum level control is necessary to add makeup water as steam is delivered into the header and to the associated process equipment. The system should control the drum level at a specific set point while compensating for varying steam demands and drum pressures. For a given volume of steam and blowdown leaving the steam drum, an equal amount of water should replace that inventory. Discussions here include the primary sensing devices and the various strategies used to control steam drum level and feed water rate

#### 4.3.2 Level Measurement

The drum level is measured using a differential pressure transmitter. The output of the instrument increases as the differential pressure decreases. A condensing reservoir is installed to allow the high side of the D/P to measure the steam pressure plus the hydraulic pressure in the reference leg. The low pressure side senses the boiler drum pressure, the weight of the water above the low pressure tap and the weight of a column of saturated steam from the high pressure tap to the water level. Being a differential pressure device, the boiler drum pressure is canceled out of the measurement, leaving only the water column pressure difference. The level measurement is accurate only at a single drum pressure. If needed, a pressure measurement can compensate for varying drum pressures by applying a gain and bias to the drum level signal.

#### 4.3.3 Swell and Shrink

Increase in steam flow rate is associated with the phenomenon of swelling. Steam and water mixture from water wall enters drum. Steam bubbles continuously leave bulk water from the interface between steam and water in drum. At steady state conditions, Drum Pressure is stable. Bubbles do not coalesce. Whenever the steam flow increases, there is a drop in drum pressure. This causes increased rate at which steam bubbles come out of bulk water causing large number of bubbles rising from the bulk water and coalescing at the inter phase surface. This apparent increase in level will cause reduction in feed water flow and lesser quantity of water will enter drum. As soon as drum pressure stabilizes, the rate of steam bubbles coming out from bulk water reduces, and level starts shrinking at a very fast rate. Reduced feed flow further aggravates the situation and level starts dropping at very rapid rate. The feed control circuit many times is unable to cope with the situation leading to level dropping to tripping values.

Inversely, as the steam load decreases, the steam bubbles in the steam/water mixture decrease in size and volume. This causes a decrease in drum level, although the mass of water and steam has not changed. This phenomenon is called shrink.

#### 4.3.4 Blowdown

When water is boiled and steam is generated, any dissolved solids contained in the water remain in the boiler. If more solids are put in with the feed water, they will concentrate and may eventually reach a level where their solubility in the water is exceeded and they deposit from the solution. Above a certain level of concentration, these solids encourage foaming and cause carryover of water into the steam. The deposits also lead to scale formation inside the boiler, resulting in localized overheating and finally causing boiler tube failure.

It is, therefore, necessary to control the level of concentration of the solids and this is achieved by the process of blowing down, where a certain volume of water is blown off and is automatically replaced by feed water thus maintaining the optimum level of total dissolved solids (TDS) in the boiler water.



Figure 4.4: A damaged heater coil because of improper level maintenance and lack of blow down

#### 4.3.5 Single element control

In this scheme called single element control, signals of measured level and set point are fed to the controller, output of which goes to the Variable Frequency drive(VFD).Depending upon the deviation of measured level from set point, controller output manipulates the VFD thus regulating the Feed Water flow rate to Drum.This scheme thus controls the mass of feed water going to drum.If Drum level drops below the set value, controller output causes increased VFD output and feed flow rate increases.In low operating pressure boilers with low evaporation rates, this type of single element control gives reasonable automatic level control.

Reasons for failure of single element drum level control are :

- When steam flow rate increases, due to swelling in level, feed flow rate decreases, which lead to depletion of mass of water in drum.
- When drum pressure reaches stability, coalesced bubbles collapse and drum level shrinks very fast.
- Due to already depleted quantity of water in drum and shrinking, level drop is rapid Inherent time lag in the process can not make up the water quantity in drum at the required rate.

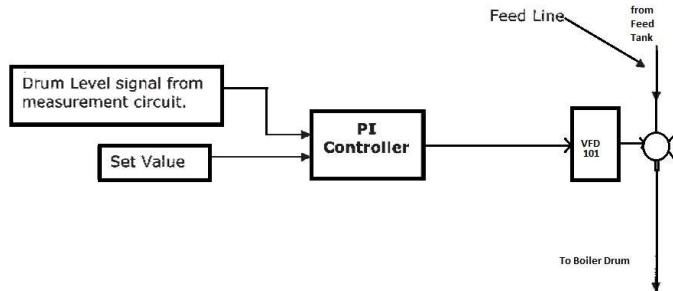


Figure 4.5: Single Element Drum level Control

Single element control is in one subroutine and it will be controlling boiler level at start up to when the boiler level is more than 86 % and temperature is more than 110 degree Celsius.

#### 4.3.6 Two Element Drum Level Control

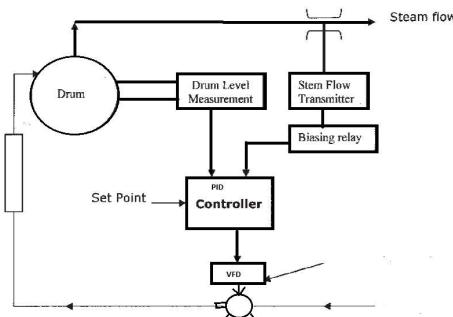


Figure 4.6: Two Element Drum level Control

The problem of reduced feed flow in case of increased steam flow encountered in single element control circuit is taken care of in two element control circuit by measuring the steam flow rate and using it as another input to the controller. In this type of control, tuning of Controller and Biasing relay is so arranged that feed flow rate shall always be equal to steam flow rate. VFD output is not dependent on level alone. This control philosophy prevents reduction in Feed Flow rate even if level swells. This avoids depletion of quantity of water present in drum. When level starts shrinking, feed flow increases and thus sudden at rapid fall in level is prevented. But feed flow may not match with steam flow in many operating conditions, leading to instability of the control.

#### 4.3.7 Three Element Drum Level Control

In this control, Feed Flow transmitter measures feed flow and its output is connected to the computing relay to which is connected steam flow signal. Difference between steam flow and feed flow is then fed to drum Level control, to which drum level signal is also connected. Since actual measurement of feed flow is carried out, this control circuit gives very stable and high quality performance.

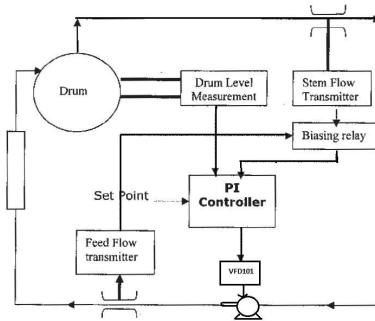


Figure 4.7: Three Element Drum level Control

Three Element control strategy is implemented in Contrologix 1756-L61. For start up single element control strategy is been used and once the level is reached above 86% and boiler temperature is above 110 degree Celsius three element control strategy is been activated.

### 4.4 Controlling from Delta V DCS

This section Deals with the programming and development of SCADA for boiler and heat exchanger pilot plant. It also elaborates the implementation of MPC in Delta V DCS.

#### 4.4.1 About DeltaV

- Control Module

Control strategies in the DeltaV system are configured in modules. A module, which is the smallest logical control entity in the system, contains algorithms, conditions, alarms, displays, historical information, and other characteristics that define the process equipment. Function blocks are building blocks for creating the continuous and discrete algorithms that perform the control or monitoring for the process. The DeltaV Library contains function block templates for analog control (bias/gain, lead/lag, PID, etc.), Logical, I/O (analog and discrete input/output), and other basic functions. Each function block contains parameters that can be modified to customize the algorithm. Algorithms range from simple input conversions to complex control strategies. Function blocks can be combined into composite function blocks to build complex algorithms.

- Collecting Displaying Data

The DeltaV system supports the collection of user-specified parameter field values and alarms and events for long-term storage, retrieval, and presentation. There are three main aspects of continuous data collection and presentation:

- Detection by defining history collection in the modules and nodes
- Storage by the Continuous Historian subsystem
- Presentation through the Process History View application

The DeltaV system also lets you export data to the Microsoft Excel spreadsheet software so that you can use that application's extensive analysis and reporting features.

- Operator Picture

Delta V Operate in configure mode to create an operator picture for the process system. It is important to understand the operating environment for a Delta V process system before we start creating pictures to be used in that environment. The Delta V Operate application functions in two modes

1. Configure mode used to create pictures
2. Run mode used to run pictures in the Delta V Operate application

#### 4.4.2 Auto tuning using Delta V insight

Once a control loop is designed and configured to govern a process it must be tuned. Making the necessary adjustments to provide for stable and responsive operation is referred as loop tuning. If a loop is tuned for responses that are too slow, the process is stable but not responsive. If the loop is tuned for responses that are too fast, it can be very responsive, but it might overshoot and cycle around the set point. The Objective is to achieve a reasonably responsive and stable control loop.

For auto tuning with Delta V insight one has to select the PID controller right and open with tune with insight as shown below. Before starting the tuning process in tune with

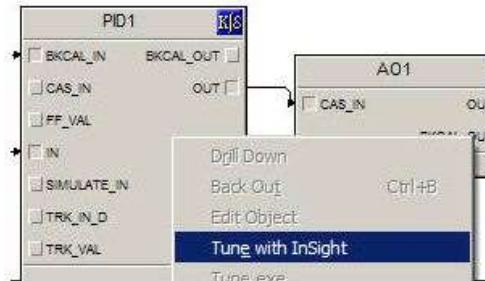


Figure 4.8: Opening Insight from Control Studio

insight, make sure that the loop is reasonably stabilized at the SP. If the PV is not close to the SP, begin the tuning from manual mode. When tuning a loop, the SP and output

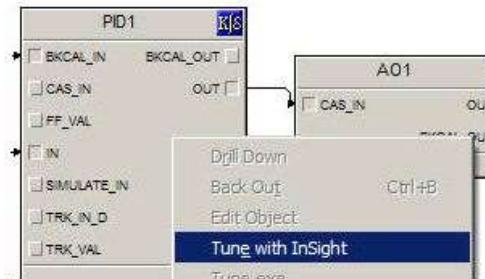


Figure 4.9: Opening Insight from Control Studio

should not be at either end of their respective ranges. The output must be no lower than 10 percent of the range and no higher than 90 percent of the range or the oscillations will be affected. The PV of the loop should be close to the SP when tuning is started. Insight check the value of SP and PV before tuning the loop. If the deviation is large this indicate that the loop is not stable. The tuner waits until the SP-PV values is with in the required limit.

If the tuning proceeds properly , the state changes to an active state and the control block actual mode changes to LO(local override). The time between each change in the block output depends on the process response time. for example , a change in the process input might not be immediately affected because of process delay in the controlled parameter. Watch the trend display area during tuning process. If loop trend traces are not typical or tuning does not start, restore initial loop conditions by clicking abort button. On rare occasions , Insight may not detect a response and test becomes stuck in LO mode with no PV movement,click abort button and repeat the procedure. while testing is active status is shown as testing process in test process panel. The progression of testing indicated by a bar graph showing percent completion.

A yellow circle icon appears next to the control block to indicate the test is active . The obtained results are shown here in this section. The recommended settings after the test can be updated to the controller by clicking update button.

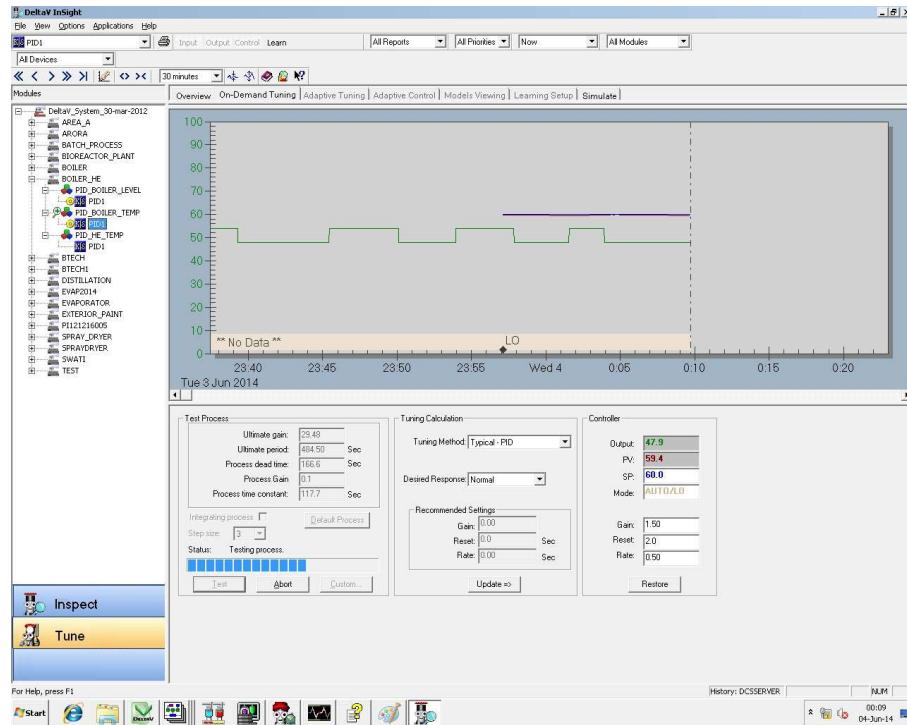


Figure 4.10: Tuning in progress, Delta V Insight

#### 4.4.3 Model Predictive Control in Delta V DCS

##### Model Predictive Control (MPC) Function Block

The MPC function block is the basis of implementing multivariable control in a DeltaV system. This function block replaces standard PID control that utilizes feedforward, decoupling

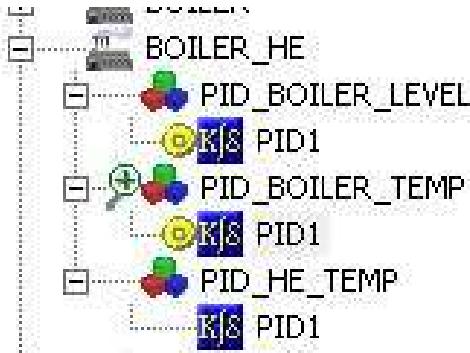


Figure 4.11: Tuning in progress, indicated by yellow circle

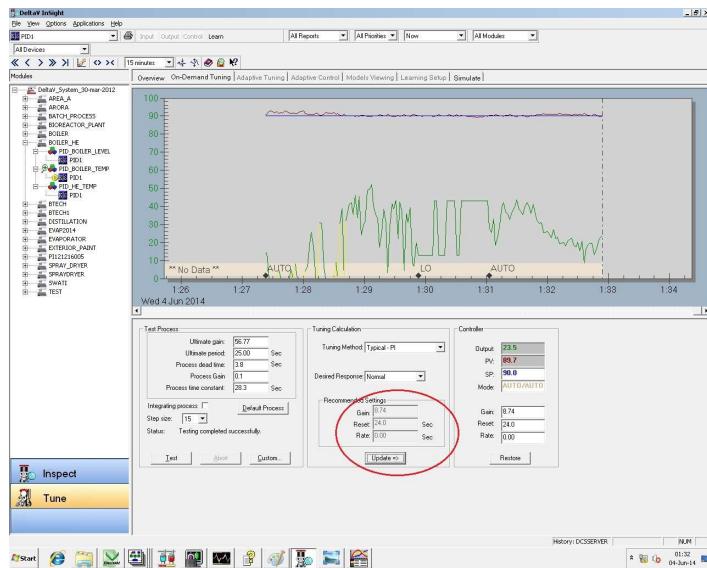


Figure 4.12: Tuning completed recommended values by insight is shown in circle

networks, and override for multivariable control. All parameters (manipulated, disturbance, constraint, and controlled) can be defined in the MPC function block for the desired process using Control Studio. The DeltaV Predict application can be launched from Control Studio.

The DeltaV Predict application is used to commission the MPC function block. When a module that contains the MPC block is downloaded, all inputs and outputs are assigned to the Continuous Historian.

Through the Predict application, we can change the manipulated inputs to the process so that we can collect historical data that reflects the process response to these changes. Using this historical data, the Predict application can identify the process step response to changes in the manipulated or disturbance inputs to the process. Also, the control definition used by the MPC function block can be generated from the model that is identified.

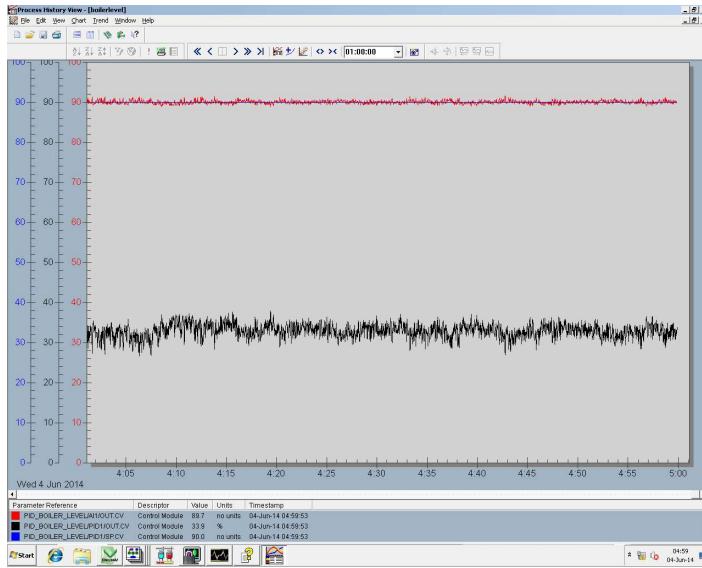


Figure 4.13: Boiler level maintained at 90% after autotuning with Delta V insight

## MPC Configuration

Since the MPC block is an extensible function block, we can select the number of controlled, constraint, and disturbance parameters that are required to meet your process control needs. The number of manipulated and back calculation input parameters are set to equal the number of controlled parameters that you specify. The default is for the MPC block to have two controlled parameters. we can right-click the MPC function block and select Extensible Parameters. The maximum number of controlled, manipulated, disturbance , constraints is limited to four in our case. After specifying the number of inputs to meet application needs, select OK. The dialog closes, and the MPC block resizes to reflect the specified number of inputs (and outputs).

Once the number of inputs to the MPC block is defined, we can configure the parameters associated with this function block. To enter configuration information, right-click the MPC function block and then select Properties. We can specify the configurable parameters associated with the controlled, manipulated, disturbance, and constraint parameters. Click an input or output listed in this dialog and select the Modify button. Then, we can change the configurable values associated with this parameter.

For a controlled parameter, the following configuration dialog appears Provide the following configuration information.

- Description The parameter name that you want to appear in the Predict application and the MPC Operate view.
- Optimization The impact of the Control parameter on plant cost or profit. The selections are:
  - None - Not considered in the objective function. There is no cost or profit associated with this parameter
  - Maximize - the working setpoint of this Controlled Variable will increase until the setpoint is reached or decrease by as much as required to prevent constraint variables from violating their limits.

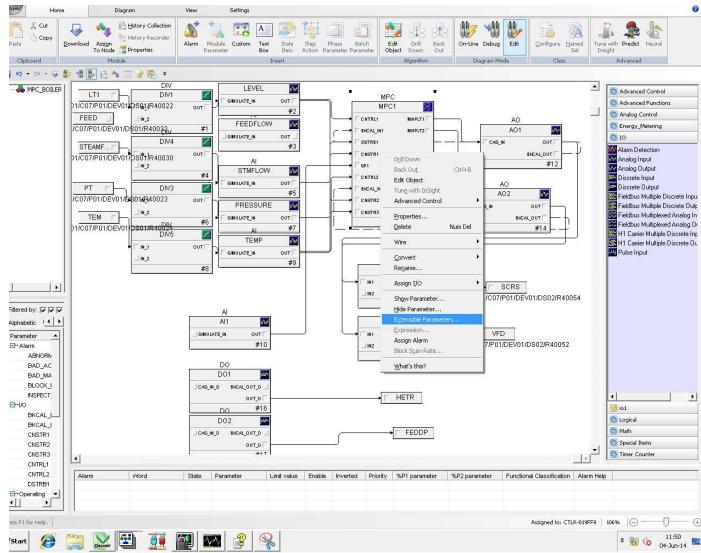


Figure 4.14: MPC in Control studio for Boiler Pilot plant

- Minimize - the working setpoint of this Controlled Variable will decrease until the setpoint is reached or increase by as much as required to prevent constraint variables from violating their limits.
- Observe Limit - the working setpoint of this Controlled Variable will drive towards the setpoint or move away from it by as much as required to prevent constraint variables from violating their limits.

The MPC function block provided by DeltaV Predict may be used to address multi variable control requirements. Predict application can be used to create process models and control definitions from process data. The automated test feature of the Predict application allows the step response of controlled or constraint outputs to be determined based on changes in the manipulated inputs. This capability can meet multi variable control requirements in all process industries. In many cases, the MPC function block can replace control techniques that have traditionally been used to address the control requirements of multi variable processes. Multi variable control is defined as control that uses multiple process measurements to produce one or more outputs.

#### 4.4.4 DeltaV Predict

DeltaV Predict implements multi variable, model predictive control in DeltaV environments. It allows us to control interactive processes within measurable operating constraints while automatically accounting for process interaction and measurable disturbances. It also allows you to easily address the numerous small and medium-sized multi variable processes.

Predict allows those with moderate process control knowledge to apply MPC control strategies. It also makes applying such strategies easier and faster than it would be using a PID controller and traditional techniques to address process disturbances, operating constraints, and loop interaction through the application of feed forward, override control or decoupling networks. DeltaV Predict consists of the following set of tools:

- Model Predictive Control (MPC) function block - allows you to implement multivariable control strategies

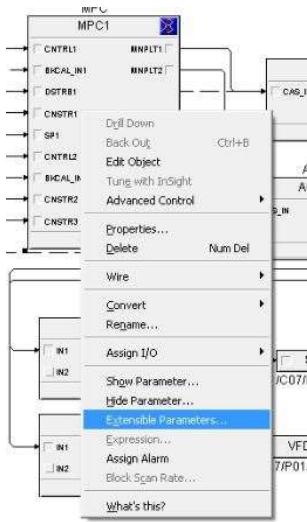


Figure 4.15: MPC block extensible parameter selection

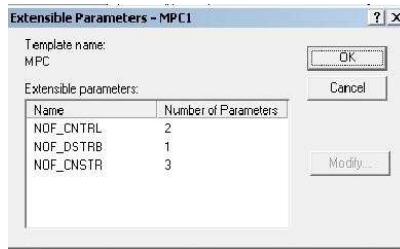


Figure 4.16: MPC block extensible parameter configuration window

- MPC Simulation function block - allows you to create multivariable training systems
- Predict application - allows you to commission the MPC function block and create process models to use with the MPC Process Simulator function block
- MPC Operate application and advanced control dynamos - enable operator to view and interact with control implemented with the MPC function block

#### 4.4.5 Commissioning MPC

After downloading an MPC function block to a DeltaV controller, verify that the transmitters and valves that provide the inputs and utilize the outputs of the MPC function block are working correctly. Also, make sure the Continuous Historian is enabled and the area containing the module has been assigned to the Continuous Historian. Once you have verified all I/Os to the MPC function block, you can use the Predict application to commission the MPC control. You can select the Predict application by right-clicking the MPC function block when the module is online. Otherwise download the module and then right click and launch the predict application. In response, the Predict application is launched and the following interface appears.

The control (CNTRL) parameters are trended automatically. Up to six of the MPC inputs and outputs can be trended at one time. For good data values, trends appear in the

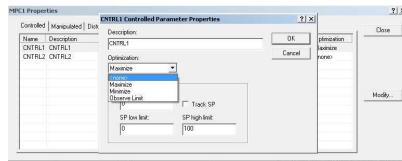


Figure 4.17: MPC block controlled parameter configuration window

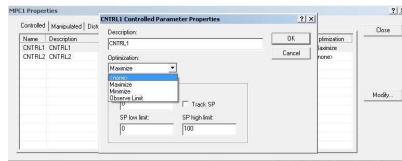


Figure 4.18: MPC block controlled parameter configuration window

colors indicated in the parameter data area. The color varies to indicate questionable status (yellow for uncertain or limited values, red for bad values). To add or delete a parameter from the trend, double-click the parameter in the Operate Trend pane. When right-click a selected parameter, options are provided that allow us to modify the trend view (that is, change the trend range). we can use the toolbar controls or the slider bar to adjust the time window that is shown on the trend.

Once the PV and SP are almost same we can launch test process. The predict application will automatically generate PRBS signal for manipulated variable and estimate the process model.

While testing is active, the actual mode of the MPC function block changes to LO. During testing, a manipulated parameter can be changed using the Operate Trend panel. The portion of testing that is complete is indicated by a progression bar. The estimated time remaining to complete the test is shown below the progression bar.

Upon completion of the test, a green area automatically covers portions of the trend associated with the time that testing was active. You can adjust the time covered by the green area either by dragging the start and end divider bars or positioning the bars by right-clicking the chart.

The area of test data that reflects normal process operating conditions is indicated by dragging the green area over the data on the trend window. You can exclude data within the green bar that does not represent normal operation by right-clicking within that area and stretching the resulting red bar over the bad data. After you select the test data, indicate if the control or constraint parameters are integrating and then choose Autogenerate to create a step response model for the process and the associated control.

Any disturbances included in the control should be closely examined. The associated step response might be inaccurate if an input did not change significantly in the data used for autogenerate. If this occurs, a warning message will be displayed when the model is generated. In addition, this will be indicated in some cases by the step response that is shown as a straight line (that is, no response). One means of determining if the step response is accurate is to compare the ARX model to the FIR response. This can be done by identifying yourself as an expert by selecting Options — Expert and choosing the FIR check box. Both responses will be displayed, as shown in the following figure. In some cases, the ARX and FIR responses might not agree. In such a case, we might need to use other data that includes times when the input changed. Then, you will need to regenerate the model and the controller. Alternatively, if one is familiar with the process dynamics, he can identify himself as an expert by selecting Options — Expert and then modify the step response to

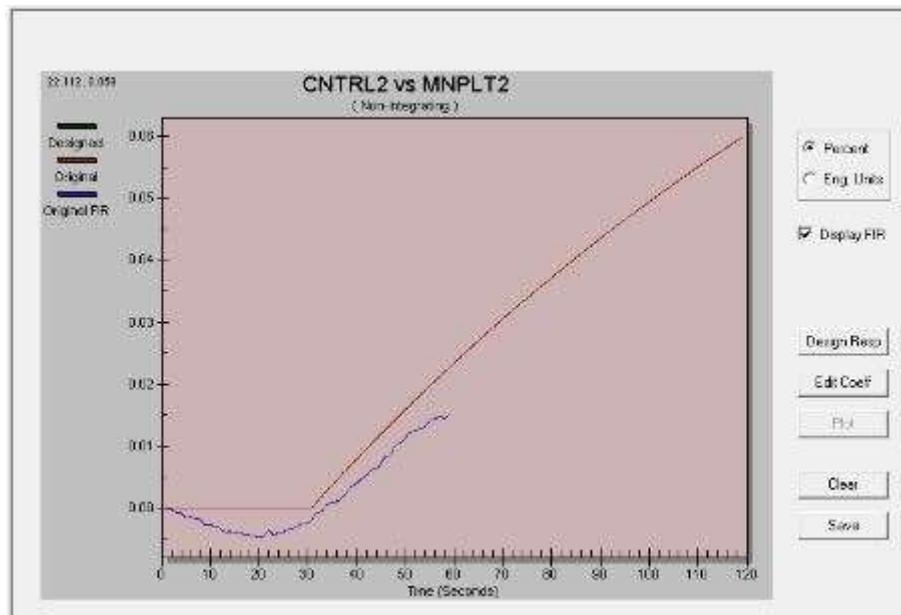


Figure 4.19: FIR and ARX response for controller with manipulated variable

reflect his knowledge of the process. Once done with the testing we can check the accuracy of model by selecting verify from model overview.

We can examine the accuracy of the model by selecting Verify from the model overview. In response, we can examine the calculated output based on the model (as opposed to the actual process output) either for the time frame defined by the green area of the trend plot or for the original data used in generating the model. If the model is accurate the result will be similar to the following figure.

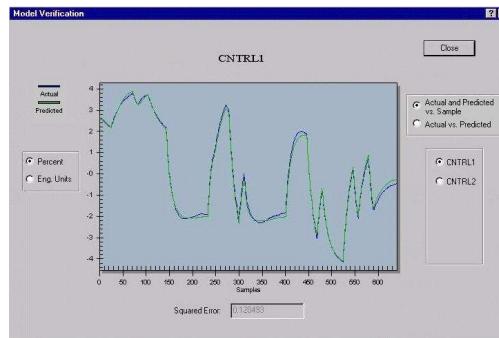


Figure 4.20: Model verification result reference

Once you are satisfied that the model accurately reflects the process dynamics, select Generate Control to update the MPC configuration for the new model. When the control is generated from a selected model, control parameters used to generate the control are displayed. In most cases, it is recommended by Delta V to leave the control generation parameters at their default values and select Start (in the Controller Generation window) to generate the control.

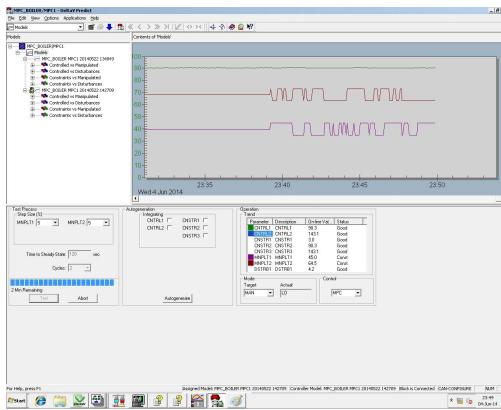


Figure 4.21: Delta V predict when testing is going on

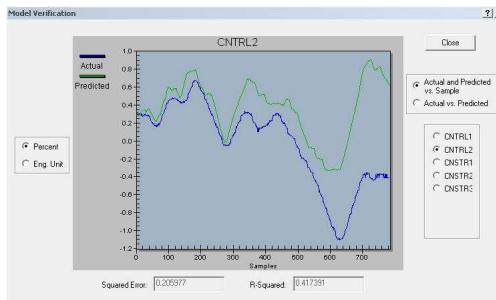


Figure 4.22: Model verification result obtained for CNTRL2

## 4.5 Controlling From Virtual Lab

### 4.5.1 Overview

Virtual Lab is a concept where College of Engineering Pune along with all IITS in the country provides a unique learning opportunity to all engineering aspirants around the world. In this concept they developed certain experiments where in which students can learn by them self the concepts of engineering ,utilizing the simulators online. One step ahead of this was a VTU concept which is Virtual Technical University where in which one has to enroll here as a faculty(Subject Master Expert) or student. This time instead of simulators there will be highly sophisticated and user friendly front end which on back end interacting with the real physical operating units.

Out of many such courses run by VTU, a few are PG Diploma in Industrial Automation,Process modeling and optimization and so on. For running this courses mere interaction with the simulators won't suffice. For example in case of tuning a PID controller the PV(Process Variable) is expected to change in accordance with the controller output to track the SP(Set Point). With the implementation of this concept the PID loop is interacting with real plant so that user or student who do not have such resources can learn all this from a remote distance just like a game, but a real game.

For virtual lab we developed programming and tested with the pilot plant. Testing PID tuning for non integrating process is mentioned in chapter 8.

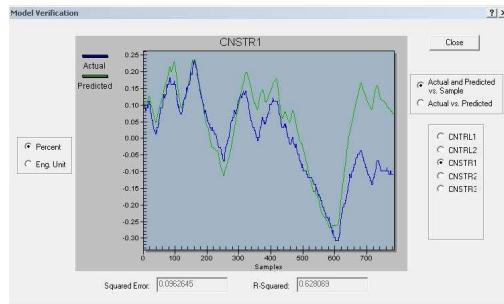


Figure 4.23: Model verification result obtained for CNSTR1

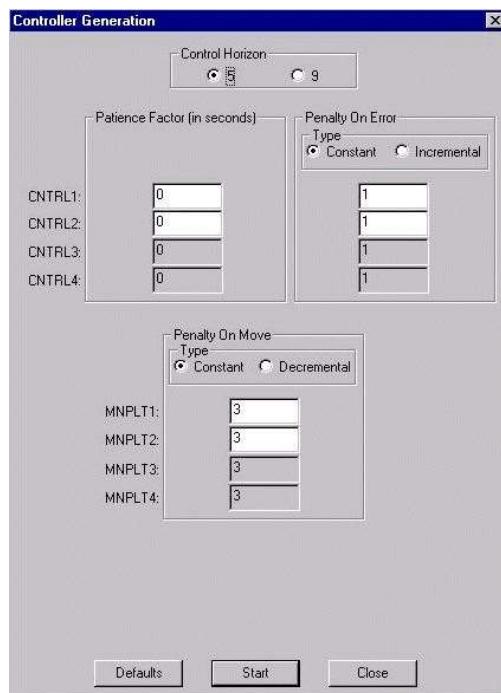


Figure 4.24: Controller generation window after test

Figure 4.25: Main page for student in VTU

Test Name	Slot Date	Camera Link
Evaporator Test11	Fri Jun 20 2014 00:00:00 GMT+0530 (India Standard Time)	No camera Available
Boiler and Heat Exchanger Test	Mon Jun 30 2014 00:00:00 GMT+0530 (India Standard Time)	<a href="#">Click Here to View Camera.</a>

Figure 4.26: Remote test view showing Plant link as well as camera view

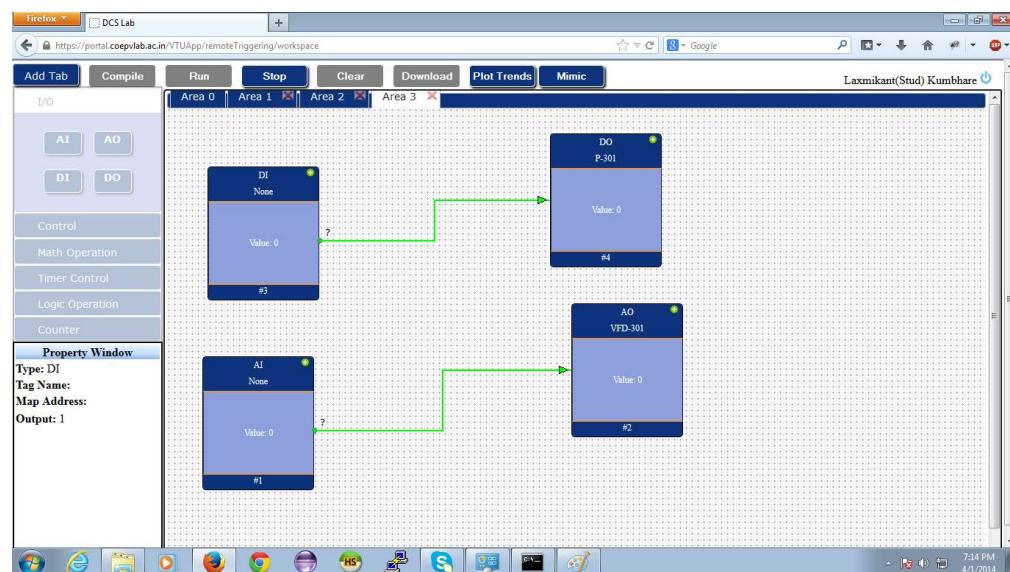


Figure 4.27: Remote test view showing Virtual DCS Blocks

## **Part II**

# **Evaporator Pilot Plant**

# Chapter 5

## Literature Survey

### 5.1 Forced Circulation Vacuum Evaporator

Forced circulation evaporators are used if boiling of the product on the heating surfaces is to be avoided due to the fouling characteristics of the product, or to avoid crystallization. The flow velocity in the tubes must be high, and high-capacity pumps are required.

The circulating product is heated when it flows through the heat exchanger and then partially evaporated when the pressure is reduced in the flash vessel (separator). The liquid product is typically heated only a few degrees for each pass through the heat exchanger. To maintain a good heat transfer within the heat exchanger it is necessary to have a high recirculation flow rate.

This type of evaporator is also used in crystallizing applications. Evaporation occurs as the liquid is flash evaporated in the flash vessel/sePARATOR. Since milk, due to the protein content, is a heat-sensitive product, evaporation (i.e. boiling) at 100°C will result in denaturation of these proteins to such an extent that the final product is considered unfit for consumption.

The boiling section is therefore operated under vacuum, which means that the boiling/evaporation takes place at a lower temperature than that corresponding to the normal atmospheric pressure. The vacuum is created by a vacuum pump prior to start-up of the evaporator and is maintained by condensing the vapor by means of cooling water. A vacuum pump is used to evacuate incondensable gases from the milk.

The steam is introduced through the jacket. The space between the tubes is thus forming the heating section. The inner side of the tubes is called the boiling section. Together they form the so-called calandria. The concentrated milk and vapors leaving top of the calandria and get separated by using a separator. The vapours produced are condensed by a condenser.

#### 5.1.1 Vacuum Evaporation

Vacuum evaporation is the process of causing the pressure in a liquid-filled container to be reduced below the vapor pressure of the liquid, causing the liquid to evaporate at a lower temperature than normal. Although the process can be applied to any type of liquid at any vapor pressure, it is generally used to describe the boiling of water by lowering the container's internal pressure below standard atmospheric pressure and causing the water to boil at room temperature.

#### 5.1.2 Need for evaporator before Spray Drying

The first part before spray drying involves milk being pumped to an evaporator where it is concentrated in a series of steps to around 40-50% total solids. Omitting evaporation of the

milk prior to drying is not economically feasible because the demand for energy would be severely increased. For example, the energy used in multiple effect evaporators with steam compression is about 10 times lower than in spray drying. Omission of evaporation would also result in an inferior quality milk powder because evaporation produces large powder particles that contain less occluded air, which results in an extended shelf-life.

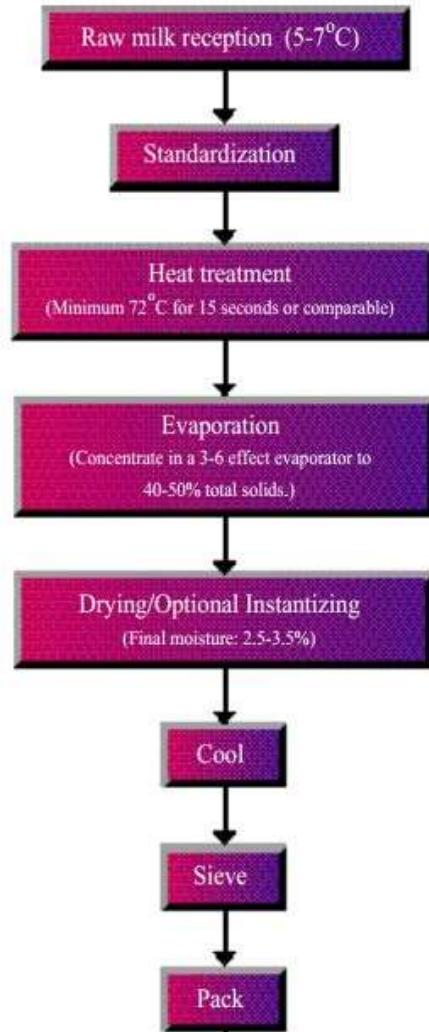


Figure 5.1: Milk Powder Production Steps

### 5.1.3 Difference between Boiling and Evaporation

- Occurs at any temperature.
- Occurs at the surface of liquid.
- No bubbles formed.

## Boiling

- Occurs at definite temperature-at Boiling Point.
- Occurs within Liquid.
- Bubbles appear.

### 5.1.4 Heat transfer coefficient in Evaporators

A practical presentation of the fundamental heat transfer principles underlying basic evaporation method and equipment has been given by Badger and Banchero (1955). The general equation describing heat transferred from the heating steam through the metal wall to the product being evaporated is

$$Q = V_0 \lambda_s = UA(T_s - T) = UA\Delta T \quad (5.1)$$

where Q = rate of heat transfer,

$V_0$  = condensed steam rate,

$\lambda_s$  = the latent heat of vaporization of steam at condensing temperature,

U = overall heat transfer coefficient,

A = heating surface area,

$T_s$  = condensing steam temperature,

T = product evaporating temperature,

T =  $T_s$  T, temperature drop.

The overall heat transfer coefficient for condensing steam through a heating surface to liquid foods may be written as

$$\frac{1}{UA} = \frac{1}{h_s A_s} + \frac{X}{k A_m} + \frac{1}{h_f A_f} \quad (5.2)$$

where  $A_m$  = the mean area for the steam and product sides of the heat exchange surface,  
 $A_s$  = steam-side heat transfer area,

$h_s$  = steam-side heat transfer coefficient,

k = thermal conductivity of the wall material,

x = thickness of the wall,

$h_f$  = liquid-side heat transfer coefficient,

and  $A_f$  = liquid-side heat transfer area

for tubular evaporators the equation becomes

$$\frac{1}{U_0} = \frac{1}{h_s} + \frac{d_o}{2k \ln(\frac{d_o}{d_i})} + \frac{d_o}{h_f d_f} \quad (5.3)$$

where,

$d_o$  = outside heat transfer tube diameter

$d_i$  = inside heat transfer tube diameter.

Local heat transfer coefficients are generally expressed as dimensionless parameters,  $h^* = h_d/k$ , usually in function of the Reynolds ( $R_e$ ) and Prandtl ( $P_r$ ) numbers,

$$h^* = aRe^bPr^c \quad (5.4)$$

Where, a,b,c are experimental constants

Forced circulation evaporators (Coulson and Richardson, 1978)

$$h^* = 0.023R_e^{0.8}P_r^{0.4} \quad (5.5)$$

## Chapter 6

# Insight of Evaporator Pilot-Plants

This chapter introduces Industrial Evaporators and Provide a brief overview of their function and operation. Forced circulation Evaporator is discussed particularly. The Final section of chapter introduces the Department of Instrumentation and Control's Evaporator Pilot Plant. The Evaporator is Forced Circulation Evaporator and its design, operation and instrumentation is described.

### 6.0.5 Function of important components

The instrumentation components in the evaporator plant can be divided in the following groups:

1. Sensors and transmitters
2. Final control elements
3. Safety components

#### Sensors and transmitters

The transducer measures a process variable in the plant while the transmitter produces an output signal, often in the form of a 420 mA electrical current signal.

#### Final control elements

Final control element is a physical device whose activation or movement causes a change in dynamic process as commanded by the controller. Following are the final control elements used in the plant:

- a. Positive displacement pump for feed: The speed of the motor and in turn feed flow is changed using variable frequency drive depending on the level in the separator.
- b. Centrifugal pump for recirculation: The speed of the motor and in turn feed flow is changed using variable frequency drive depending on the product concentration.
- c. Equal percentage globe valve for manipulating steam flow: Takes proper action in terms of valve opening depending on the current signal from controller.



Figure 6.1: Evaporator Pilot Plant

### Safety components

These components ensure process safety which generally refers to the prevention of unintentional releases of chemicals, energy, or other potentially dangerous materials (including steam) during the course of process that can have a serious effect to the plant and envi-

ronment. Process safety involves, for example, the prevention of leaks, spills, equipment malfunction, over-pressures, over-temperatures, corrosion, metal fatigue and other similar conditions. Following instruments are included to keep process variables under safe limit as well as provide alarms interlocks to automatically take necessary action:

- a. Pressure switch: Pressure switch on evaporator shuts off the steam if evaporator pressure/temperature exceeds operating limits.
- b. Temperature switch: This switch shuts off the vapors from separator if in case the feed temperature exceeds the set point.
- c. Low level switches: For the separator, shuts off the feed pump if level in the separator goes below the expected. For feed tank switch is provided so as to avoid dry running of pumps if there is nothing to pump in the tank.
- d. High level switches: Provided for the separator and product tanks to avoid overflow of liquid.

## 6.1 Overview of Evaporator Pilot Plant

### 6.1.1 Functional definition

Evaporation is a special case of the unit operation called heat transfer. The aim of evaporation is to concentrate a solution consisting of a volatile solvent and a non-volatile solute. Steam is often used as a heating source. This unit operation is achieved by vaporizing part of the solvent to produce a concentrated solution. Most evaporation operations used by industry use water as the solvent. Evaporators are commonly found in the inorganic, organic, paper and sugar industries. Typical applications include the concentration of sodium hydroxide, brine, organic colloids and fruit juices

### 6.1.2 Process description

The evaporator used is of forced circulation type. Here, feed coming from feed tank is mixed with a high volumetric flow rate of recirculating liquor and is pumped in to a vertical heat exchanger, in which heat is exchanged with 3.5 bar steam coming from boiler which condenses on the outside of the tube walls. The liquor which passes up the inside of the tubes, boils and then passes to a separation vessel. In this vessel, liquid and vapor are separated. The liquid (now more concentrated than when it entered the evaporator) is recirculated and drawn as product when desired concentration is reached. The concentrated solution withdrawn from the evaporator is known as the thick liquor or process liquid which is collected in a product tank. This process liquid is further given as a feed to dryer plant.

Variable	Description
F1	Feed flow rate(kg/min)
F2	Product flow rate(kg/min)
F3	Circulating flow rate(kg/min)
F4	Vapor flow rate (kg/min)
F5	Condensate flow rate(kg/min)
X1	Feed composition(Percent)
X2	Product composition(Percent)
T1	Feed temperature(deg C)
T2	Product temperature(deg C)
T3	Vapor temperature(deg C)
L2	Separator level(meters)
P2	Operating pressure(kPa)
F100	Steam flow rate(kg/min)
T100	Steam temperature(deg C)
P100	Steam pressure(kPa)
F200	Cooling water flow rate(kg/min)
T200	Cooling water inlet temperature(deg C)
T201	Cooling water outlet temperature(deg C)
Q200	Condenser duty(kW)

Table 6.1: Evaporator Variables

## 6.2 List of Instruments

Sensors	Type	Range	Quantities
Temperature	Pt-100	0-200 °C	7
Flow	Vortex Flow Meter	0-40 kg/hr	1
	magnetic flowmeter	0-10000 lph	1
Pressure		0-2.5 bar	1
		0-5 bar	1
Level	Differential Pressure Type	0-500mm H <sub>2</sub> O	1
Density	Inline	0-1.5 gm/ cm <sup>3</sup>	1

Table 6.2: List of Sensors Evaporator Pilot Plant

The main aim of most evaporator control systems is to regulate conditions within the evaporator so that the product stream meets a particular specification. This requires that the control system minimizes fluctuations in the product composition arising from disturbances in the input stream or in the plant itself. The nature of the fluid, the operating conditions, the equipment design, and the manner of association with other plant, all influence the detailed nature of the control scheme. That is why the plant and its associated control equipment should be considered together at the design stage. In particular where the process is associated with other processes in a plant with little or no storage capacity to act as a buffer between processes, care must be taken to guard against interaction between control loops. Even in the course of this work involving only a single process, certain control schemes showed pronounced interaction between control loops.

## 6.3 Operation

The liquid is circulated through the calandria by means of a circulation pump, where it is superheated at an elevated pressure, higher than its normal boiling pressure. Upon entering the separator, the pressure in the liquid is rapidly reduced resulting in some of the liquid being flashed, or rapidly boiled off. Since liquid circulation is maintained, the flow velocity in the tubes and the liquid temperature can be controlled to suit the product requirements independently of the pre-selected temperature difference

The often used evaporator, known as a forced circulation evaporator. In this evaporator, feed is mixed with a high volumetric flow rate of recirculation liquor and is pumped in to a vertical heat exchanger, in which heat is exchanged with steam which condenses on the outside of the tube walls. The liquor which passes up the inside of the tubes, boils and then passes to a separation vessel. In this vessel, liquid and vapor are separated. The liquid (now more concentrated than when it entered the evaporator) is re-circulated and drawn as product when desired concentration is reached. The concentrated solution withdrawn from the evaporator is known as the thick liquor or process liquid.

### 6.3.1 Standard Operating Procedure:

Referring to the P&ID of the process given in the indices, follow the procedures for start-up, Normal operation and shut down.

#### Start up Procedure

1. Fill the separator with feed from feed tank using feed pump
2. Check All Valves Status ,Keep it to Required Condition
3. Start the Vacuum Pump to Get Required Vacuum in the Separator
4. Start the Sealing Water supply for Circulation Pump, Vacuum Pump and Surface Condenser
5. Shut the feed supply and start circulating the feed in vertical heat exchanger
6. Adjust the steam supply to heat exchanger and circulation flow rate to get the required product concentration
7. The thin solution vapors generated due to heat exchange and flashing in Separator is passed through condenser and collected in condensate tank
8. Flashing of solution occurs at Separator as the operating pressure is reduced by using vacuum pump
9. In line density measurement is carried out using density meter
10. When the required product density is achieved the product outlet valve is opened partially
11. And the circulation of product is continued to avoid scaling of product on inside walls of heat exchanger at same time care must taken to maintain minimum level in separator by introducing fresh feed from feed tank
12. While shutting down, turn off the feed pump and cut off the steam supply by closing steam valve
13. Allow the circulation pump to run for some time and collect all product in product tank

### **6.3.2 Normal operation sequence**

1. Make sure that feed tank has sufficient filled with solution
2. Observe the product concentration on controller
3. Check the performance of the parameters and carry the manipulations accordingly.
4. Once the unit is operating smoothly do not disturb any settings till the disturbance is to be generated.
5. Check the level of feed tank otherwise follow the shutdown sequence if the level drops down to its low limit

### **6.3.3 PLANT SHUT DOWN SEQUENCE**

1. STOP STEAM
2. STOP FEED
3. COOL ALL EFFECT TO 38 TO 40 DEG C
4. STOP PROCESS CONDENSATE PUMP
5. STOP VACUUM PUMP
6. STOP COOLING WATER PUMP
7. STOP COOLING WATER FAN
8. STOP CP/TP PUMP
9. STOP SEALING WATER PUMP

## **6.4 Origin of disturbance**

- Feed flow rate, density and enthalpy
- Calandria heat input rate, which may vary through changes in the heating medium supply pressure or temperature
- Condenser heat removal rate, which may vary because of changes in flow rate or temperature of the cooling medium (surface condenser) or flow rate (contact condenser)
- Pan pressure, through changes occurring in the condenser ejector system.
- Ambient conditions, which affect the rate of heat transfer from the equipment, or the operating pressure of any plant vented to the atmosphere.
- Variations in product withdrawal rate, originating in changing demands by some succeeding process.

Of these, the main source of disturbances is the feed stream, particularly as most evaporators have their own subsidiary control loops regulating the heating medium conditions, and the condenser-ejector conditions

In a similar fashion it would be possible to control separately the feed flow rate and temperature, but at the risk of controller redundancy

## 6.5 Piping And Instrument Diagram for Evaporator

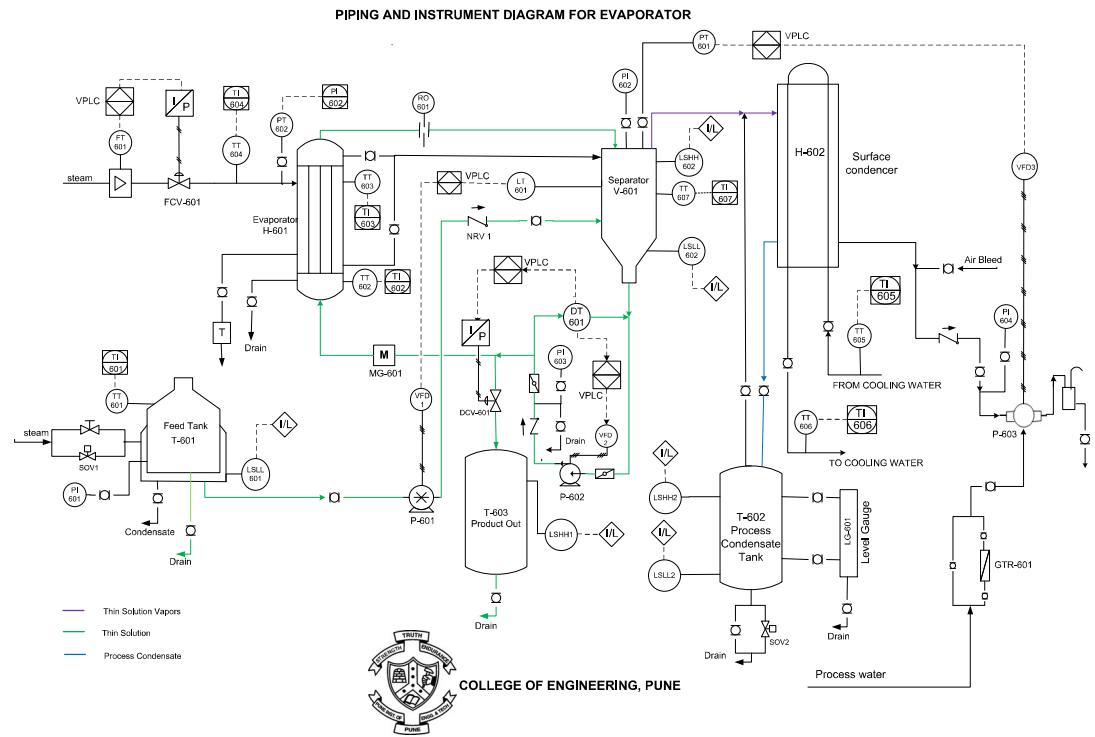


Figure 6.2: Piping And Instrument Diagram for Evaporator

## Chapter 7

# Modeling of Evaporator Pilot Plant

In this Modeling, it is assumed that:

- The overall heat transfer coefficient between milk and steam is constant
- It is considered that the liquid and vapor phase are at equilibrium condition
- Vapor accumulation in effects is negligible
- Heat transfer only occurs between milk and steam inside the shell and heat losses to environment are negligible
- by neglecting vapor space and Heat transfer Dynamics

### 7.0.1 The Non Linear Model:

#### Process Liquid mass balances

A mass balance on Total Process Liquid i.e. solvent and solute in the system yields

$$\rho A \frac{dL_2}{dt} = F_1 - F_4 - F_2 \quad (7.1)$$

where,

rho is liquid density,

A is cross sectional area of Evaporator,

the product  $\rho A$  is Assumed to be Constant

#### Process liquid solute mass balance

A mass balance on the solute in the process liquid phase

$$M \frac{dX_2}{dt} = F_1 X_1 - F_2 X_2 \quad (7.2)$$

where,

M is amount of liquid in the Evaporator

#### Process vapor mass balances:

A mass balance on the process vapour in the evaporator will express the total mass of water Vapour in the system

$$C \frac{dP_2}{dt} = F_4 - F_5 \quad (7.3)$$

where,

C is mass of vapor in to an equivalent pressure, This Constant can be derived from ideal gas Law

### Process Liquid Energy Balances

The process liquid is assumed to always exist in its boiling point and to be perfectly mixed

The product liquid temperature is :

$$T_2 = 0.5616P_2 + 0.3126X_2 + 48.43 \quad (7.4)$$

which is linearisation of saturated liquid line for water about saturated steady state value and include a term to approximate boiling point elevation due to presence of solute

The vapor temperature is :

$$T_3 = 0.507P_2 + 55.0 \quad (7.5)$$

which is linearisation of the saturated line for water about the standard steady state value

The Dynamics of the energy balance are assumed to be very fast

$$F_4 = (Q_{100} - F_1 C_p (T_2 - T_1)) / \lambda \quad (7.6)$$

## 7.1 Additional Relations

$$T_2 = 0.5616P_2 + 0.1326C_2 + 48.43 \quad (7.7)$$

$$T_3 = 0.507P_2 + 55.0 \quad (7.8)$$

$$F_2 = F_1 - F_4 \quad (7.9)$$

$$F_4 = \frac{|Q_{100} - F_1 C_p (T_2 - T_1)|}{\lambda} \quad (7.10)$$

$$T_{100} = 0.1538P_{100} + 90.0 \quad (7.11)$$

$$Q_{100} = F_{100}\lambda_s = UA_1(T_{100} - T_2) \quad (7.12)$$

$$Q_{200} = F_{200}C_p(T_{201} - T_{200}) \quad (7.13)$$

$$= UA_2(T_3 - 0.5(T_{200} - T_{201})) \quad (7.14)$$

$$F_5 = Q_{100}\lambda \quad (7.15)$$

$$UA_1 = 0.16(F_1 - F_3) \quad (7.16)$$

$$(7.17)$$

Where,

$M$  is Solute Holdup

$\lambda$  is Latent heat of Vaporisation of Water

$UA_2$  is Heat transfer coefficient times the Heat transfer Area

$C_p$  is Specific Heat

**Heat required for Evaporation:**

$$H = \frac{\left(\dot{w} \text{Product}\right) - \left(\dot{w} \text{Feed}\right)}{\lambda_s} + \lambda_s(\text{condensate}) \quad (7.18)$$

## 7.2 Heat Exchanger model equations

$$\frac{dT_{co}}{dt} = \frac{F_c}{(V_c \rho_c)}(T_{ci} - T_{co}) + \frac{U_{Ap}}{(C_{pc} C_c V_c)}(T_{ho} - T_{co}) \quad (7.19)$$

$$\frac{dT_{ho}}{dt} = \frac{F_h}{(V_h \rho_h)}(T_{hi} - T_{ho}) + \frac{U_{Ap}}{(C_{ph} \rho_h V_h)}(T_{co} - T_{ho}) \quad (7.20)$$

## 7.3 Plant Input And output Variables

Separator Variables

Input Variables	Output Variables	State Variables
$F_1$	$L_2$	$L_2$
$F_2$	$X_2$	$X_2$
$F_4$	$P_2$	$P_2$

Input Variables	Output Variables	State Variables
$F_3$	$T_{co}$	$T_{co}$
$F_{100}$	$T_{ho}$	$T_{ho}$
$T_{100}$		

### 7.3.1 Open loop non-linear model validation results

The whole evaporator plant was divided into three sections. one separator and two heat exchangers as shown above. The non linear model is validated in MATLAB and the validation results are as below.

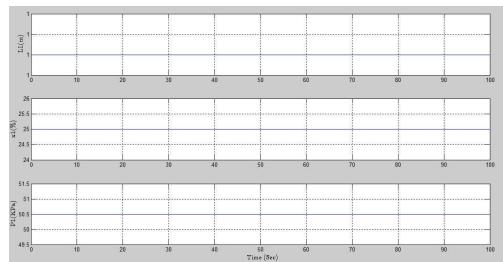


Figure 7.1: Steady state of separator

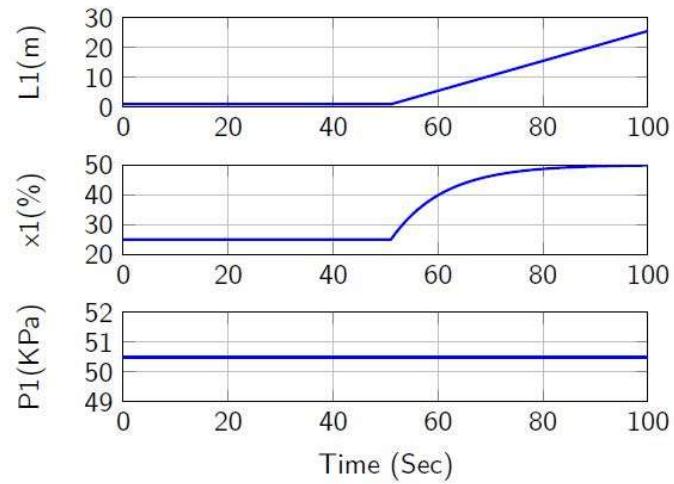


Figure 7.2: Plot when feed flow increases by 10 %

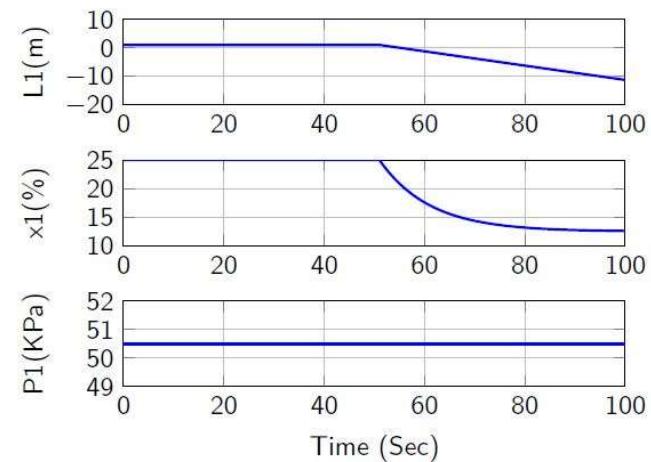


Figure 7.3: Plot when feed flow decreases by 10 %

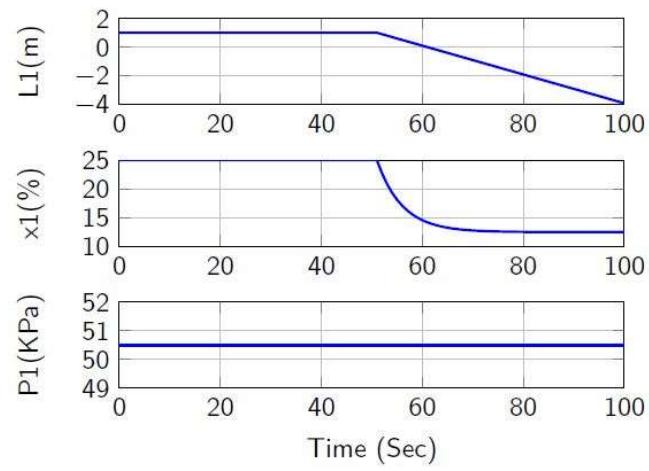


Figure 7.4: Plot when product flow increases by 10 %

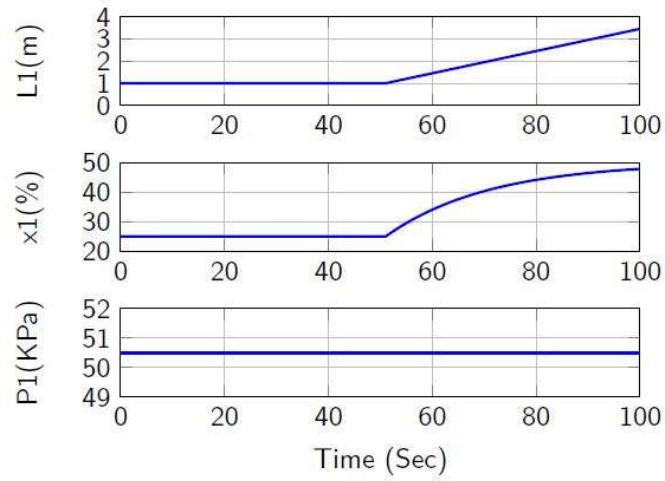


Figure 7.5: Plot when product flow decreases by 10 %

## Chapter 8

# Controlling From Various Domains

### 8.1 Overview

This chapter focuses on automation and control schemes for the evaporator pilot plant. Each section of this chapter tells us the scope of control strategies and their implementation in various domains such as local and remote. PID control is implemented in various domains. Generated square, sine, ramp and PRBS test signals are generated in Micrologix 1400 PLC for checking the robustness of PID controller.

### 8.2 Local Domain

Local domain is having Micrologix 1400 PLC. Programming is done in RS logix 500 version 9 for automation and control of the evaporator pilot plant. Through use of the Proportional-Integral-Derivative (PID) controller, automated control systems enable complex production process to be operated in a safe and profitable manner. We achieve this by continually measuring process operating parameters such as Temperature, Pressure, Level, Flow, and Concentration, and then by making decisions to open or close a valve, slow down or speed up a pump, or increase or decrease heat so that selected process measurements are maintained at the desired values.

Sr.No.	Controlled Variable	Manipulated Variable
1	Separator Level	Peristatic pump speed
2	Circulation Flow	Circulation pump speed
3	Separator Temperature	Circulation pump speed Or Control Valve
4	Separator Pressure	Vaccum pump speed
5	Product Flow	Product flow valve

Table 8.1: List of controlled and corresponding manipulated variable for Evaporator plant

The overriding motivation for modern control systems is safety. Safety encompasses the safety of people, the safety of the environment, as well as the safety of production equipment. The safety of plant personnel and people in the surrounding community should always be the highest priority in any plant operation. Good control is an individual control loops ability to achieve and maintain the desired control objective.

### 8.2.1 PID controller in micrologix 1400

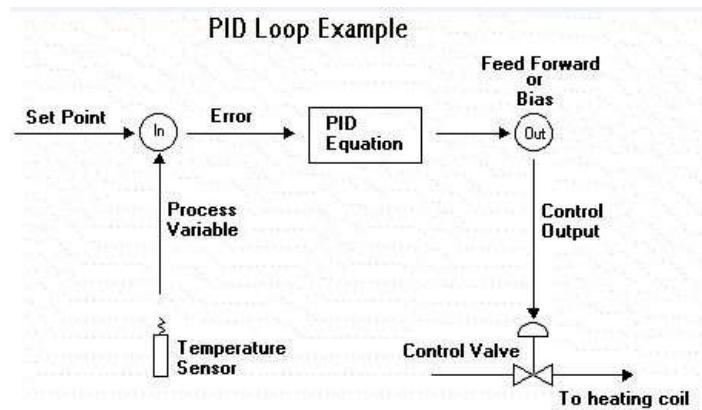


Figure 8.1: Typical PID program loop

This output instruction is used to control physical properties such as temperature, pressure, liquid level, or flow rate of process loops. The PID instruction normally controls a closed loop using inputs from an analog input module and providing an output to an analog output module as a response to effectively hold a process variable at a desired set point. The PID equation controls the process by sending an output signal to the actuator. The greater the error between the setpoint and the process variable input, the greater the output signal, and vice versa. An additional value (feed forward or bias) can be added to the control output as an offset. The result of the PID calculation (control variable) will drive the process variable you are controlling toward the set point Entering Parameters: PID File - (MicroLogix 1200, 1400 and 1500 only) Specify a PID file. If you have not already defined a PD filetype among your data files, it will be created for you. The file length is fixed at 23 words. The PD file replaces the old integer file control block. Control Block Length - (Not valid with MicroLogix 1200, 1400 or 1500) Specify an integer file, for example N7:0. The file length is fixed at 23 words.

**Process Variable PV** - The element address that stores the process input value. This address can be the location of the analog input word where the value of the input A/D is stored. You can also enter an integer address if you choose to pre-scale your input value to the range 0-16383.

**Control Variable CV** - The element address that stores the PID output. The output value ranges from 0-16383, with 16383 being the 100% "ON" value. This is normally an integer address, so that you can scale the PID output range to the particular analog range your application requires.

The PID controllers were implemented for the above mentioned loop and to test the robustness of a non integrating loop, created various test signals such as Square wave, Sine wave, Ramp wave and PRBS wave form. The response of the PID is checked by applying this waveform as set point and plotted the same in Factory talk view SCADA of micrologix. The

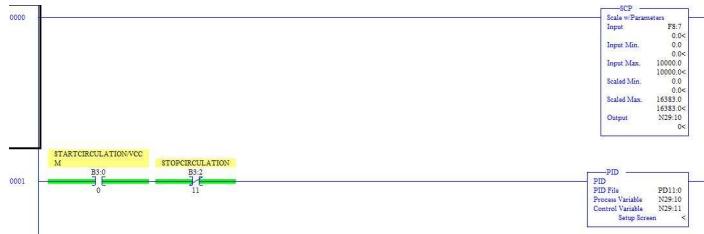


Figure 8.2: Typical PID program loop

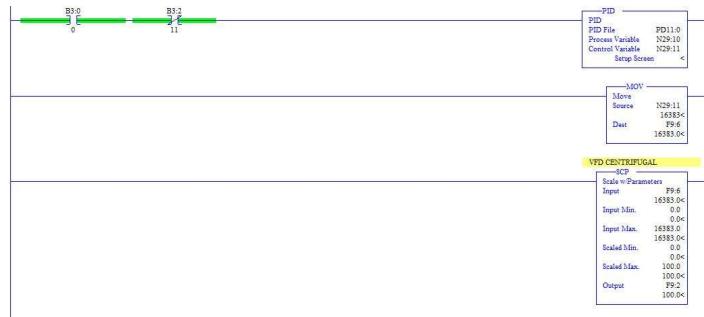


Figure 8.3: Typical PID program loop

programming is also shown in the appendix. The results are shown below where in which the Red line represents the SP green represents PV and blue for controller output.

### 8.3 Controlling from ControlLogix system 1756-L61

The ControlLogix system of series 1756-L61 is chassis-based and provides the option to configure a control system that uses sequential, process, motion, and drive control in addition to communication and I/O capabilities.

RSLogix 5000 is a programming software of ControlLogix which offers an easy to use IEC61131-3 compliant interface. It provides ladder logic, structured text, function block diagram and sequential function chart editors for program development as well as support for the S88 equipment phase state model for batch and machine control applications. We also used RSView32 works to develop SCADA and to log data. RSView32 is an integrated, component-based HMI for monitoring and controlling automation machines and processes. It also integrates Microsoft's popular Visual Basic for Applications (VBA) as a built-in programming language and supports OPC standards as both a server and a client for fast, reliable communications with a wide variety of hardware devices.

Ladder Programming for Evaporator pilot plant is done and developed the SCADA for the same in this domain.

### 8.4 Controlling from DeltaV DCS

#### 8.4.1 About DeltaV

- Control Module

Control strategies in the DeltaV system are configured in modules. A module, which is the smallest logical control entity in the system, contains algorithms, conditions,

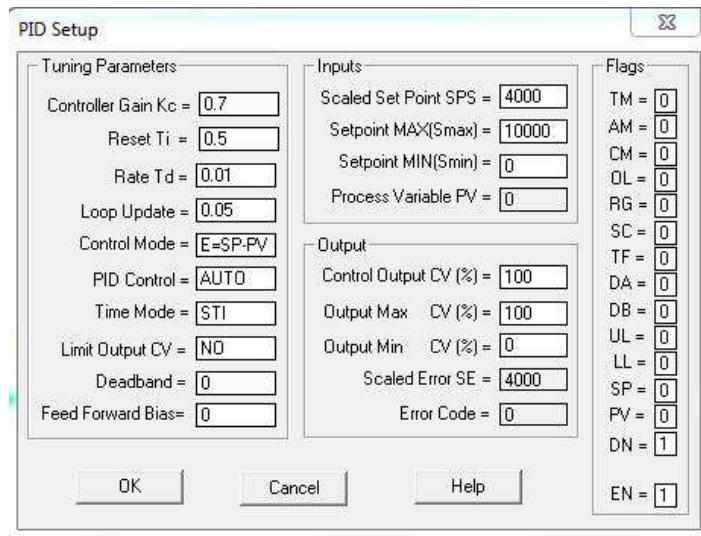


Figure 8.4: Typical PID set up screen

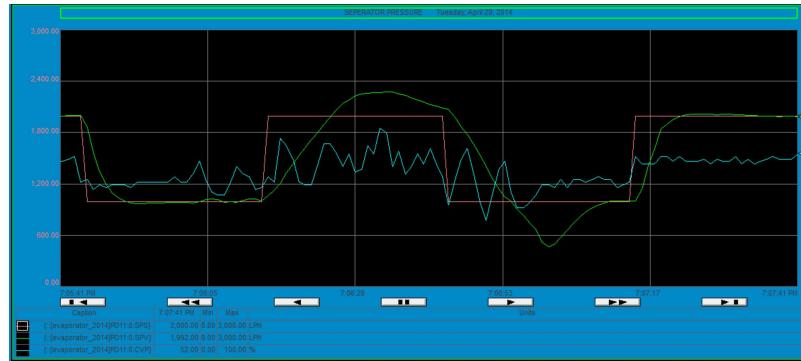


Figure 8.5: Tunning process with square wave.

alarms, displays, historical information, and other characteristics that define the process equipment. Function blocks are building blocks for creating the continuous and discrete algorithms that perform the control or monitoring for the process. The DeltaV Library contains function block templates for analog control (bias/gain, lead/lag, PID, etc.), Logical, I/O (analog and discrete input/output), and other basic functions. Each function block contains parameters that can be modified to customize the algorithm. Algorithms range from simple input conversions to complex control strategies. Function blocks can be combined into composite function blocks to build complex algorithms.

- Collecting Displaying Data

The DeltaV system supports the collection of user-specified parameter field values and alarms and events for long-term storage, retrieval, and presentation. There are three main aspects of continuous data collection and presentation:

- Detection by defining history collection in the modules and nodes
- Storage by the Continuous Historian subsystem
- Presentation through the Process History View application

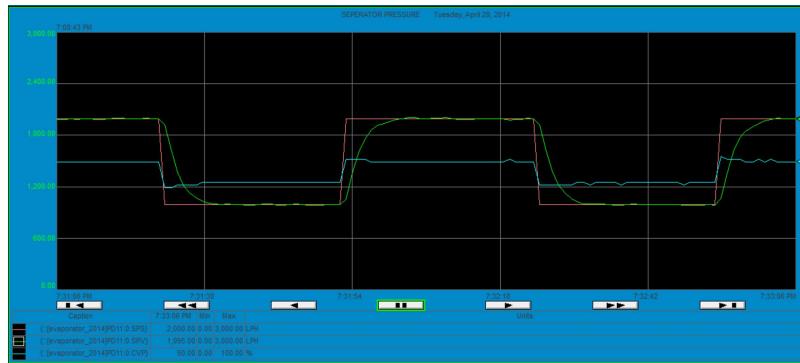


Figure 8.6: A tuned PID response for Square waveform when set point is varied between 1000 and 2000 lph

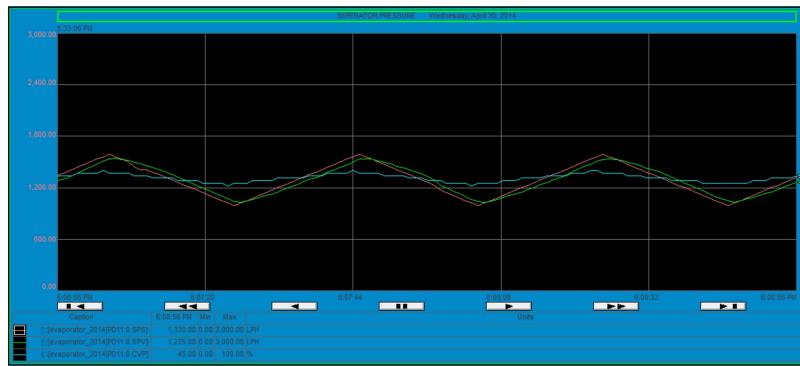


Figure 8.7: A tuned PID response for ramp waveform when set point is varied between 1000 and 1500 lph

The DeltaV system also lets you export data to the Microsoft Excel spreadsheet software so that you can use that application's extensive analysis and reporting features.

- Operator Picture

Delta V Operate in configure mode to create an operator picture for the process system. It is important to understand the operating environment for a Delta V process system before we start creating pictures to be used in that environment. The Delta V Operate application functions in two modes

1. Configure mode used to create pictures
2. Run mode used to run pictures in the Delta V Operate application

#### 8.4.2 Areas and Control Modules in Delta-V DCS for Evaporator Plant

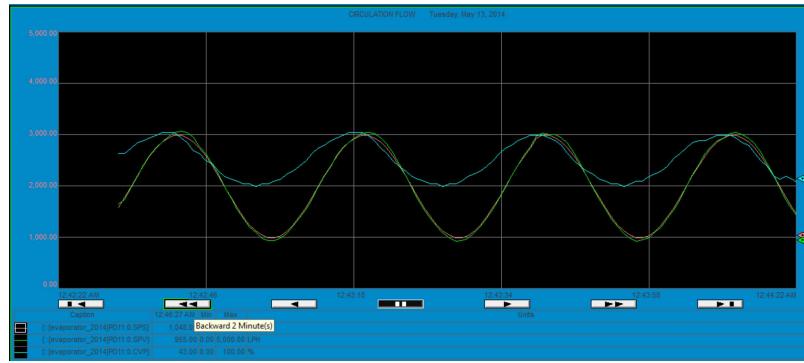


Figure 8.8: A tuned PID response for sine waveform when set point is varied between 1000 and 3000lph

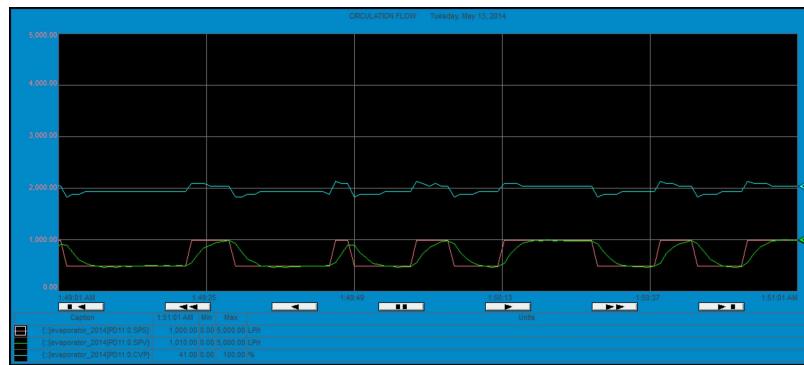


Figure 8.9: A tuned PID response for PRBS waveform when set point is varied between 500 and 1000lph

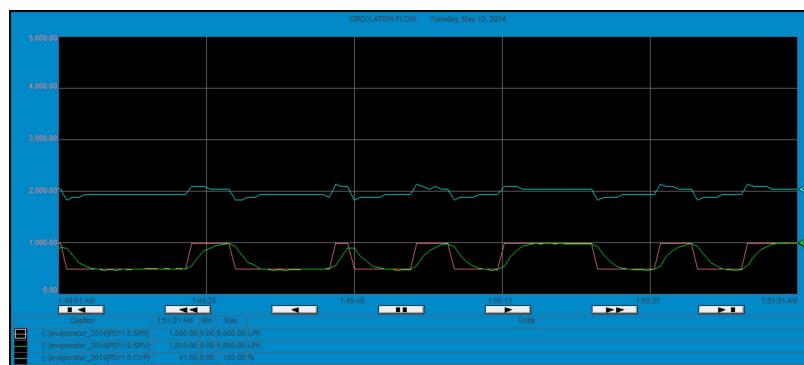


Figure 8.10: A tuned PID response for PRBS waveform, when setpoint is varied between 500 and 1000lph

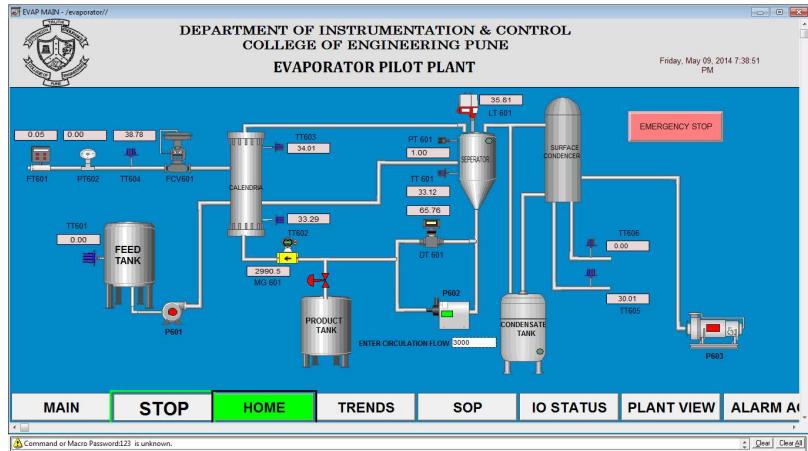


Figure 8.11: Evaporator main screen SCADA in local domain

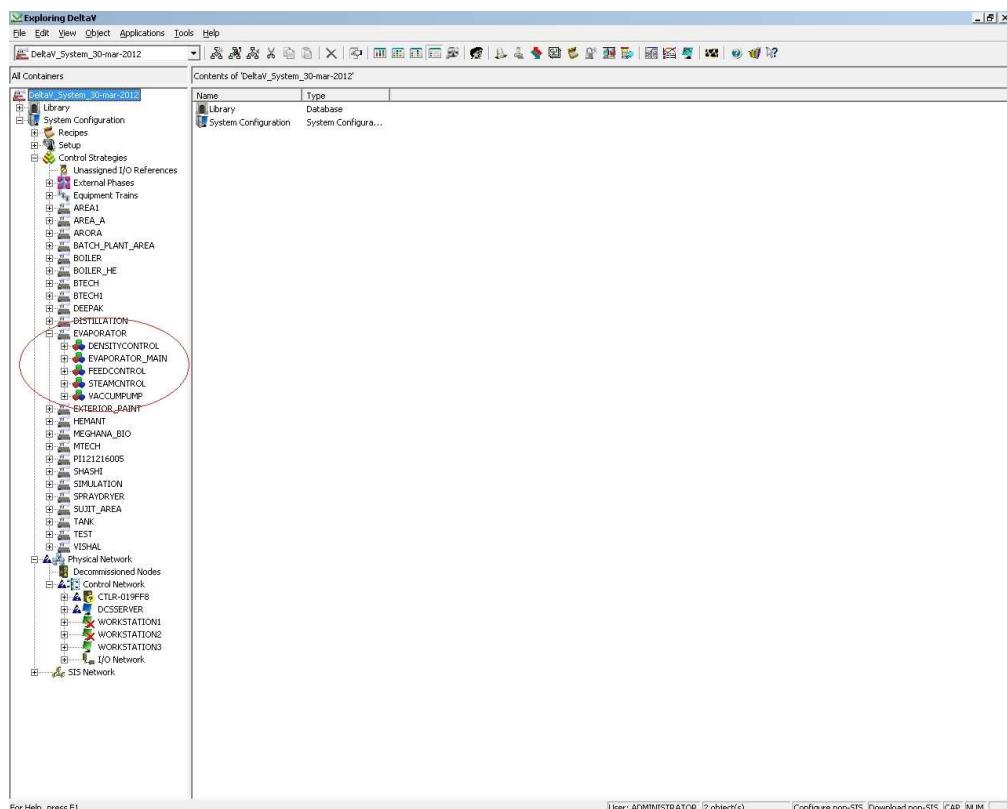


Figure 8.12: Area for Evaporator Plant in Delta-V Explorer

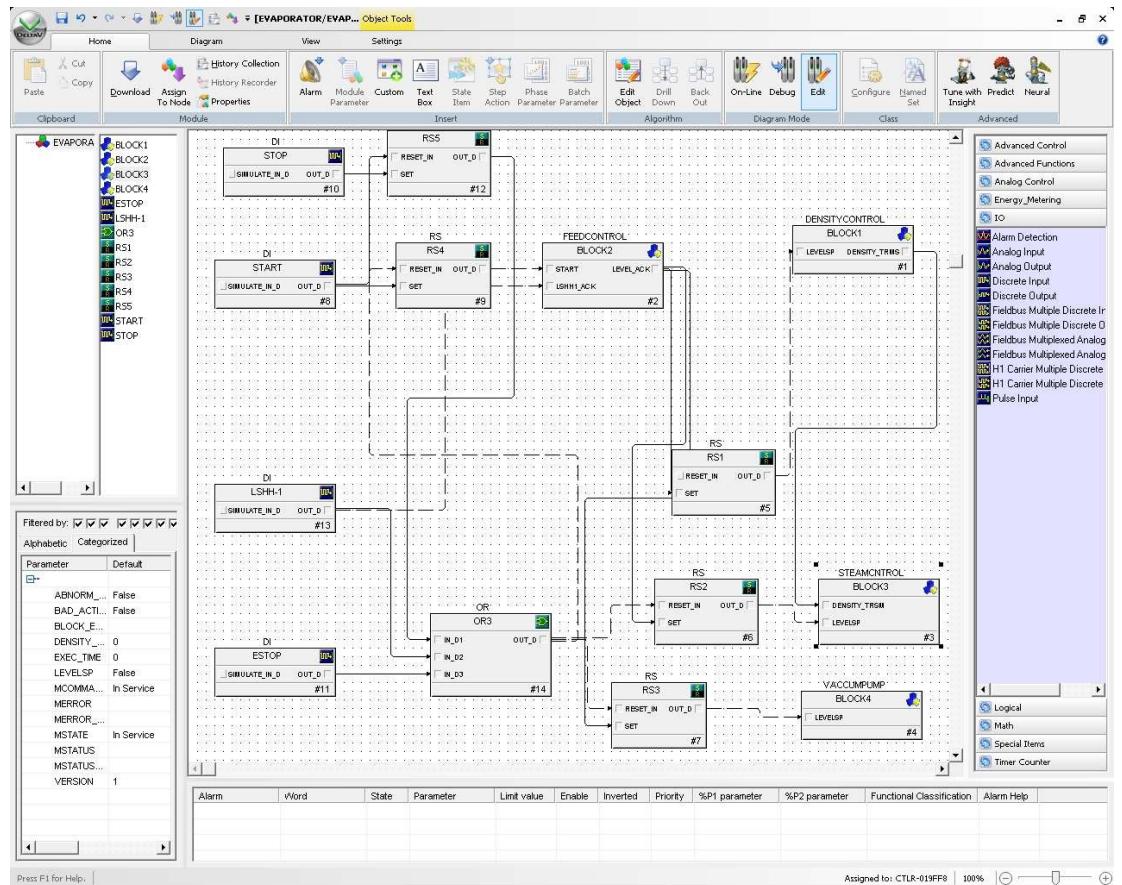


Figure 8.13: Evaporator Main module in Control Studio, Delta-V DCS

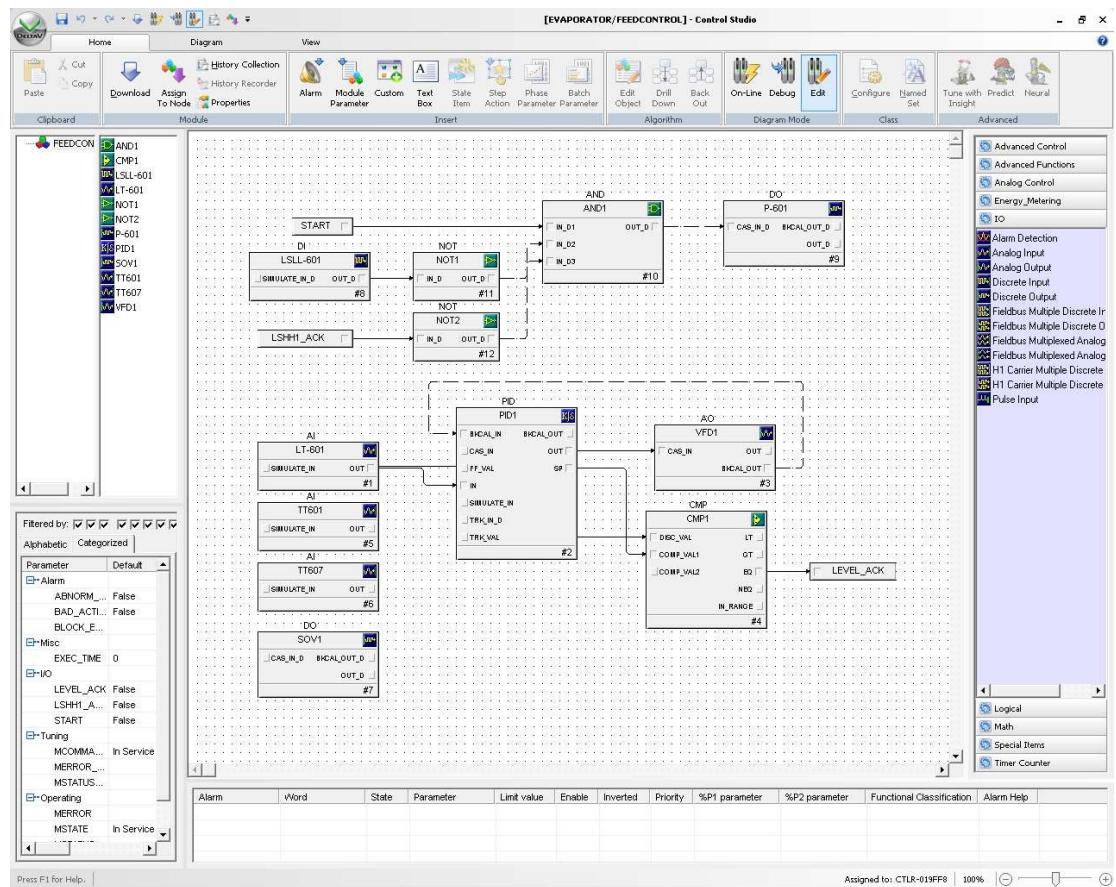


Figure 8.14: Separator feed Control module of Evaporator Pilot Plant In Control Studio Delta-V DCS

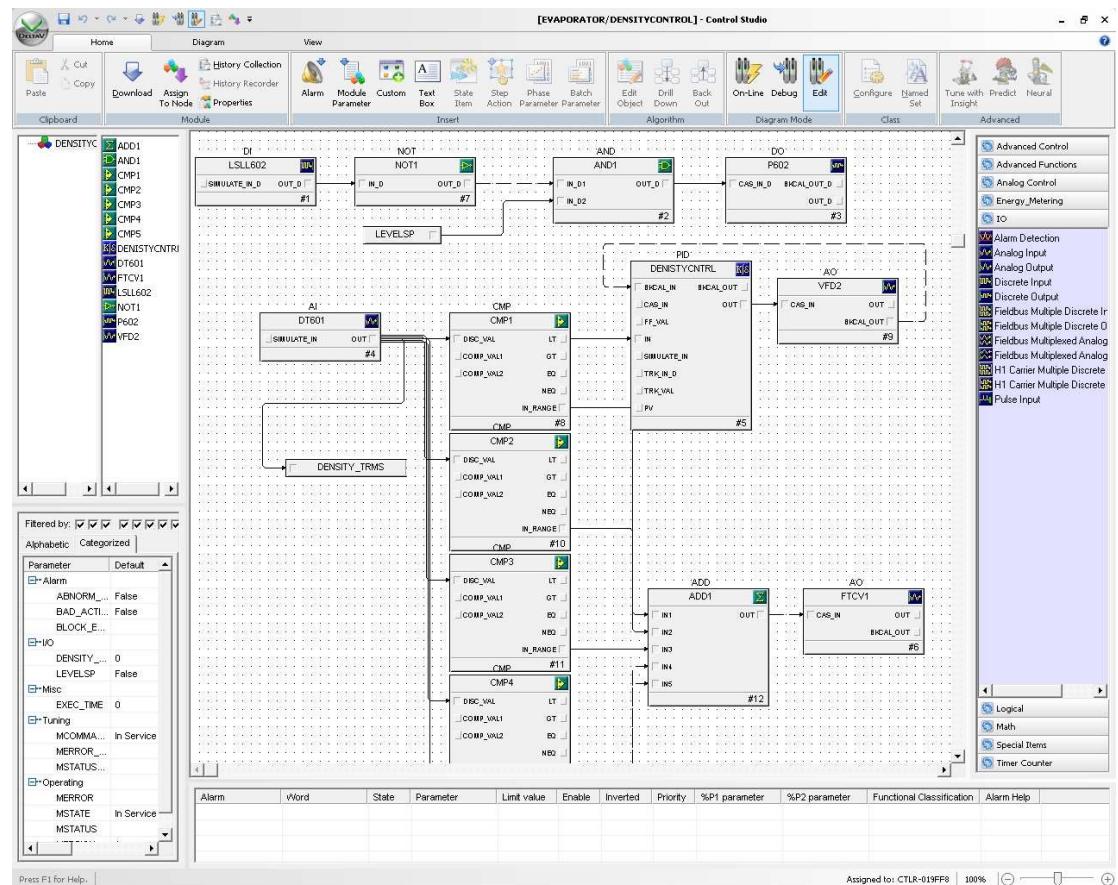


Figure 8.15: Density control module of Evaporator Pilot Plant In Control Studio Delta-V DCS

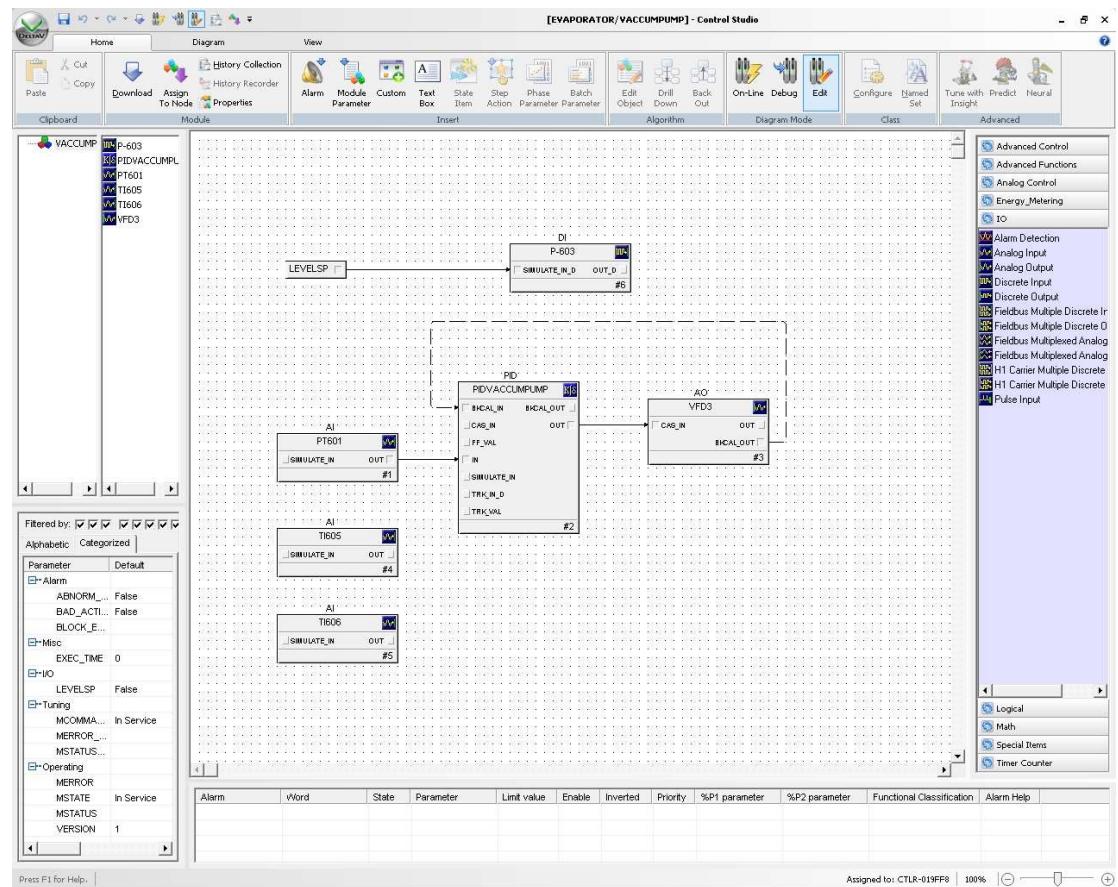


Figure 8.16: Vacuum pump speed control module of Evaporator Pilot Plant In Control Studio Delta-V DCS

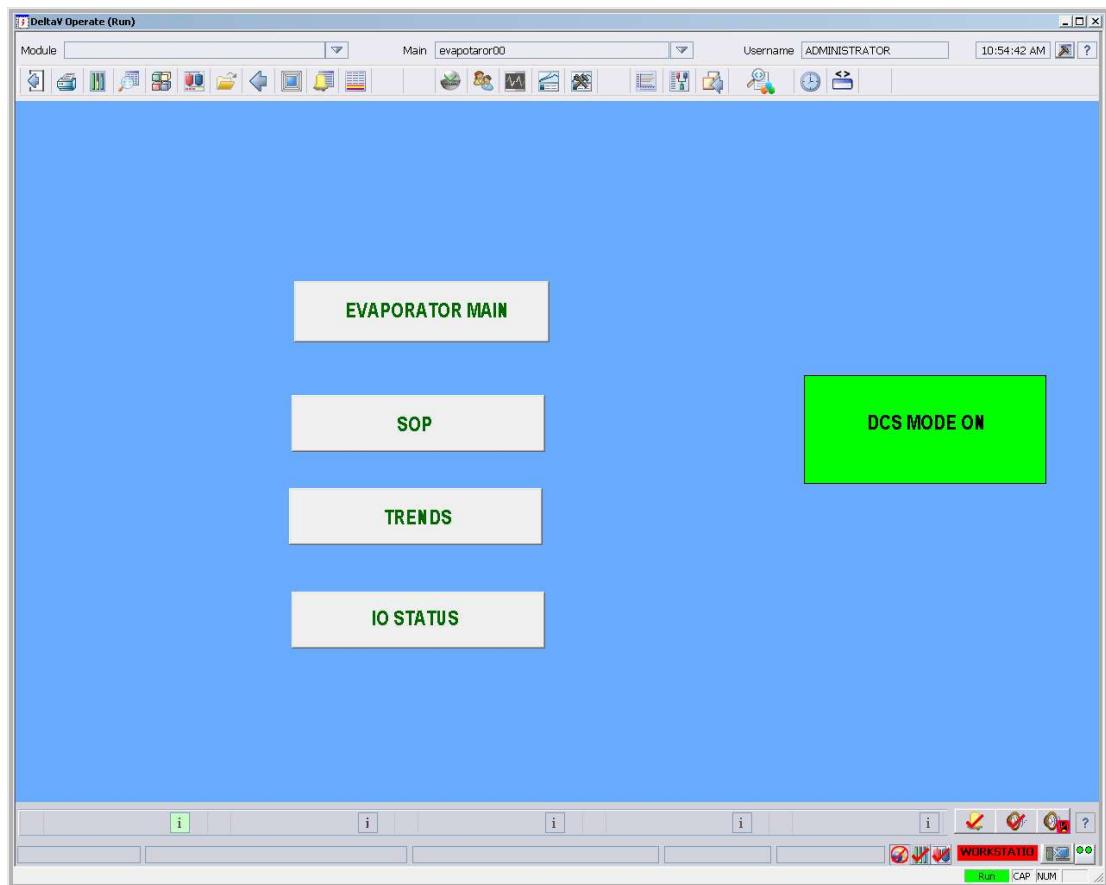


Figure 8.17: Home SCADA for Evaporator Pilot Plant in Delta-V DCS

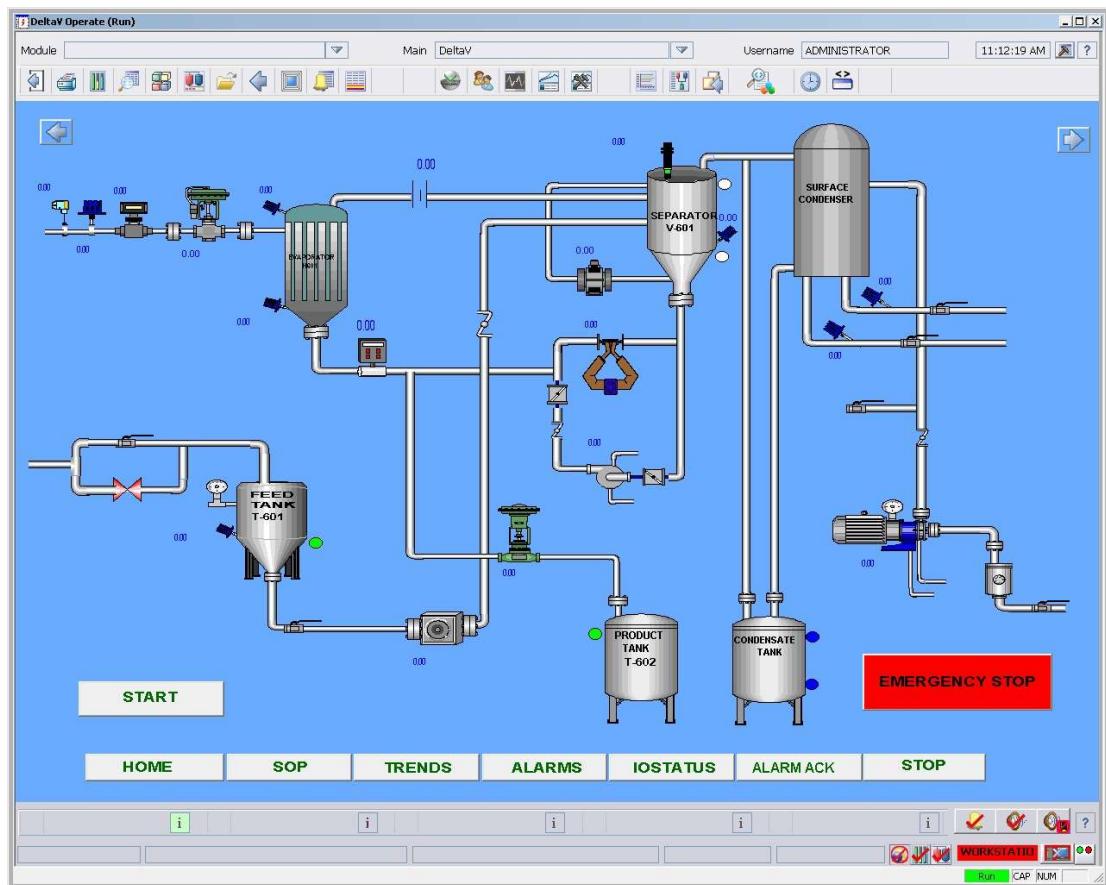


Figure 8.18: Main SCADA for Evaporator Pilot Plant in Delta-V DCS

# **Part III**

## **communication**

## Chapter 9

# Communication With Remote Domains

In this chapter we will discuss, how networking is done so that user can have multiple options to control. Local PLC provided two serial ports (one with RS232 compatible and other RS232/485) and Ethernet port utilizing Modbus and Ethernet IP protocols. We communicate Local Workstation PC (where MAT LAB and server for VPLC and VDCS resides) and local PLC with Modbus RTU RS232 serial protocol. Our objective is to run all the plants simultaneously from the DCS, for that we implemented daisy chaining using Modbus RTU 485 (Station ID for boiler & heat exchanger plant is 1). Contrologix PLC is connected with Ethernet IP protocol with the local machine as they are of same make . Communication for each end is explained briefly in different sections.

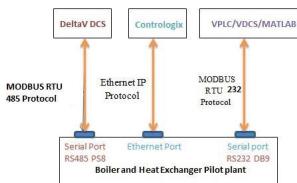


Figure 9.1: Communication Topology

### 9.1 Modbus RTU Protocol

Modbus Protocol is a messaging structure developed by Modicon in 1979. It is used to establish master-slave/client-server communication between intelligent devices. It is an open, serial (RS-232 or RS-485) protocol derived from the Master/Slave architecture. It is a widely accepted protocol due to its ease of use and reliability. Modbus RTU is widely used within

Building Management Systems (BMS) and Industrial Automation Systems (IAS). This wide acceptance is due in large part to MODBUS RTUs ease of use.

Modbus is considered an application layer messaging protocol, providing Master/Slave communication between devices connected together through buses or networks. On the OSI model, Modbus is positioned at level 7. Modbus is intended to be a request/reply protocol and delivers services specified by function codes. The function codes of Modbus are elements of Modbus request/reply PDUs (Protocol Data Unit).

The function code

eld of a MODBUS data unit is coded in one byte. Valid codes are in the range of 1 ... 255 decimal (128 255 reserved for exception responses). When a message is sent from a Client to a Server device the function code field tells the server what kind of action to perform. Function code "0" is not valid. For Establishing the communication we have to

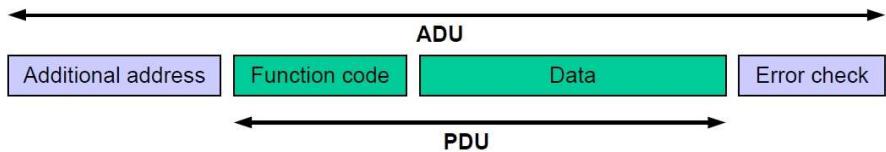


Figure 9.2: Data Packet Format

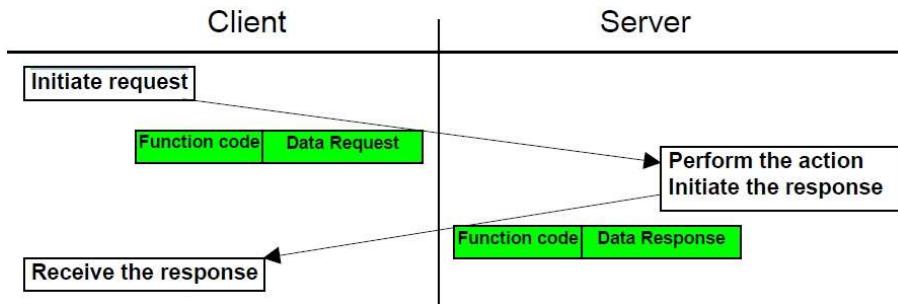


Figure 9.3: Server Client Communication

configure the channel setting in local PLC as shown in fig 9.5 for DCS & fig 9.7 for Virtual Lab/MATLAB. We created independent subroutine for each remote location so that when we select a specific remote location such as DCS by using hard switch the corresponding subroutine is enabled and executed .These subroutine in local logic for remote location will consists of only move instruction so that the remote terminals are able to access the input data, execute their logic and write the output data in the same subroutine.

In short when in remote domain the local PLC is not executing any logic but bypasses the input and output. At the same time the critical interlocks are taken care by hardware interlock as well so that we are not compromising any safety related issues.

We communicated MATLAB to Local PLC Micrologix 1400, with Modbus RTU protocol with RS232. For that, we used instructions like `fread('name of com port')` , `fwrite('name of com port')` to read and write from a slave PLC. For this, user has to configure port for settings shown in table, For example, code in MATLAB will be like following,

```
s=serial('COM1');
set(s,'BaudRate',19200)
set(s,'Timeout',0.1)
get(s)
```

open(s); this opens the port  
fcloses; this opens the port

To access any process value, user have to generate PDU, (for that dedicated functions are written in MATLAB as shown in appendix D). To read gen-Pdu-read("MODBUS address") is used where to write gen-pdu-write("MODBUS address", "value to be written") Thus we can have write or read operation on PLC with MATLAB.

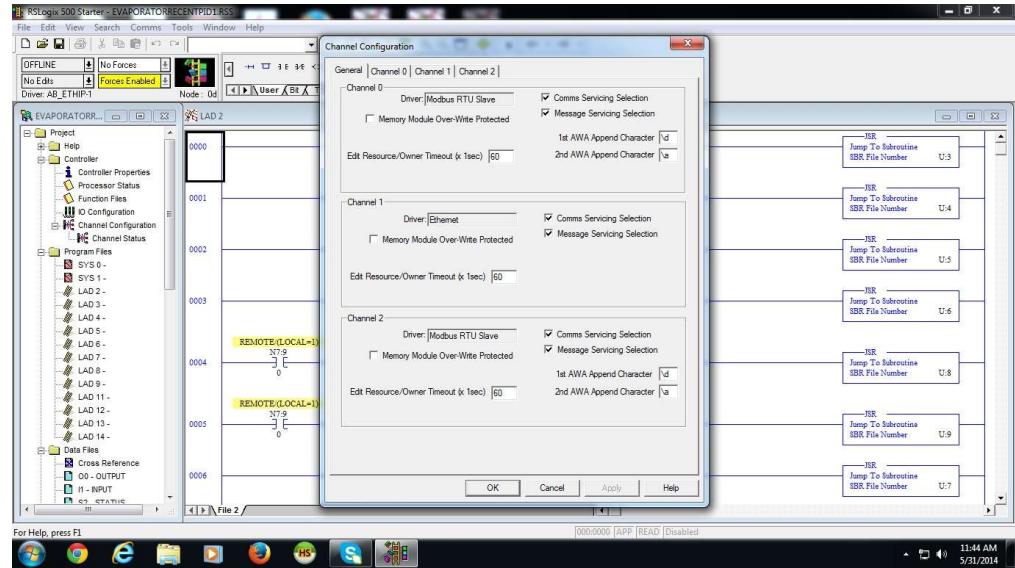


Figure 9.4: Channel configuration Genera1 in Micrologix 1400

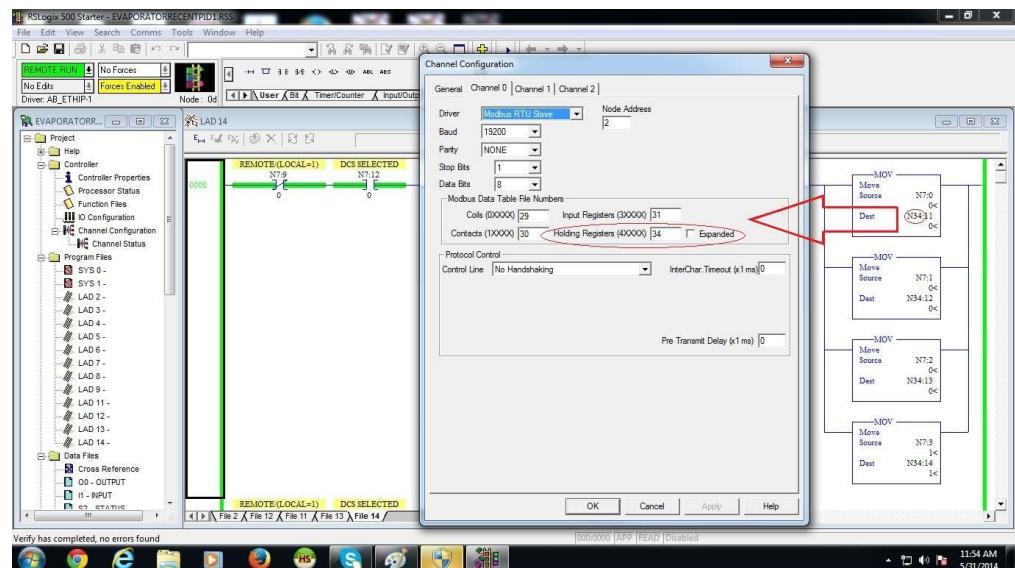


Figure 9.5: Channel configuration, channel 0 for DCS in Micrologix 1400

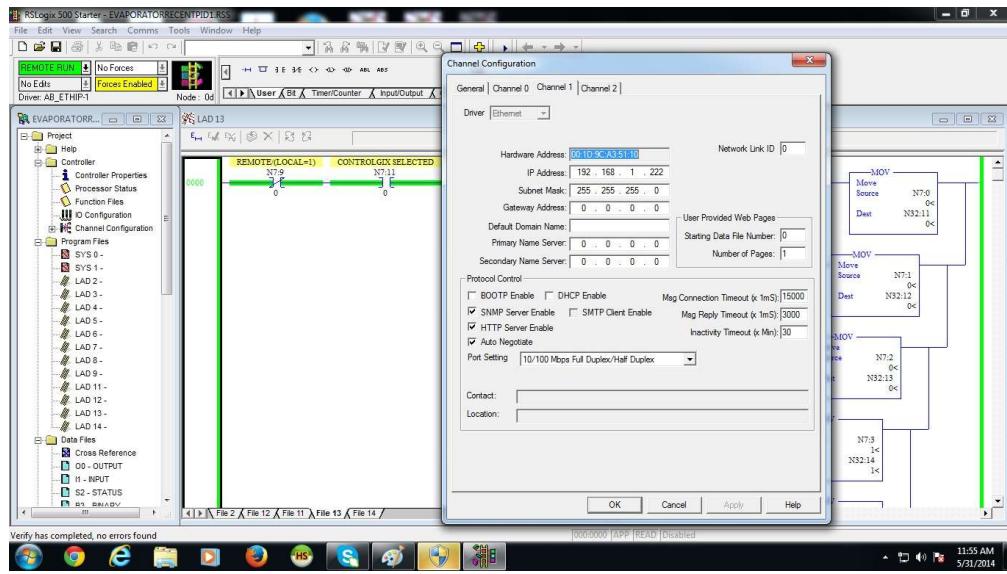


Figure 9.6: Channel configuration, channel 1 for Ethernet in Micrologix 1400

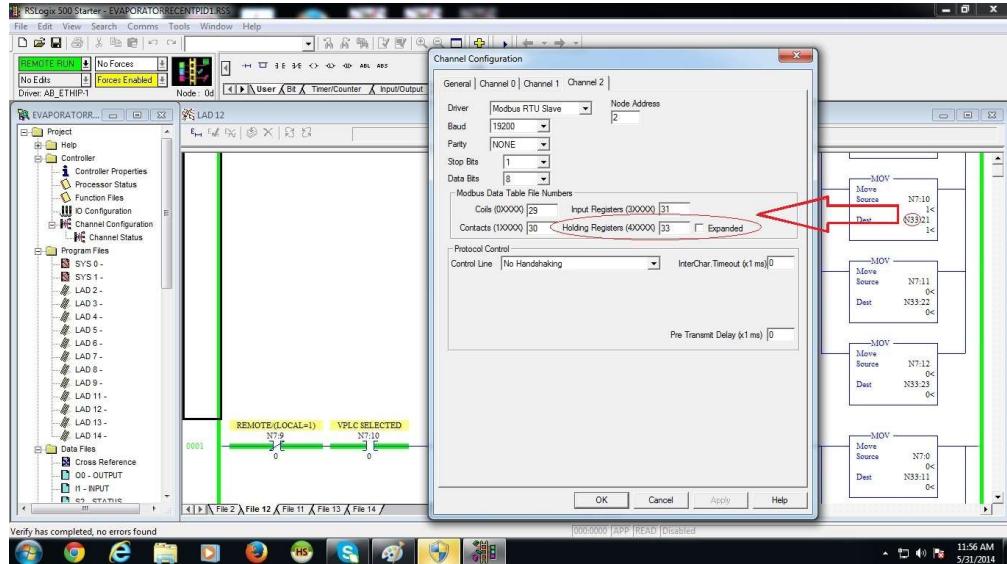


Figure 9.7: Channel configuration, channel 2 for Virtual Lab/MATLAB in Micrologix 1400

## 9.2 Contrologix PLC series 1756-L61 Communication Procedure

We are utilizing Contrologix Ethernet/IP module for communication with Micrologix 1400, with network defined by IP address of 192.168.1.xxx with subnet mask of 255.255.0.0. We have assigned an IP to Micrologix 1400 as 192.168.1.22x as static IP so that contrologix and micrologix will come in same network. Using RSLinx (v2.57.00) we add the node or slave

Micrologix 1400. We exchange data using messaging instruction in RSLogix5000. In ladder we add MSG instruction where we define from which register data is fetched from micrologix 1400 and new data file is defined with name SLC-AI[i] , SLC-AO[j] , SLC-DI[k] & SLC-DO[l] as array, where i,j,k,l represents the number of analog inputs,analog outputs,digital inputs & digital outputs respectively. Steps for messaging are shown as in figure(9.8 to 9.10). After downloading the main routine we can see the real time value in programming tags.

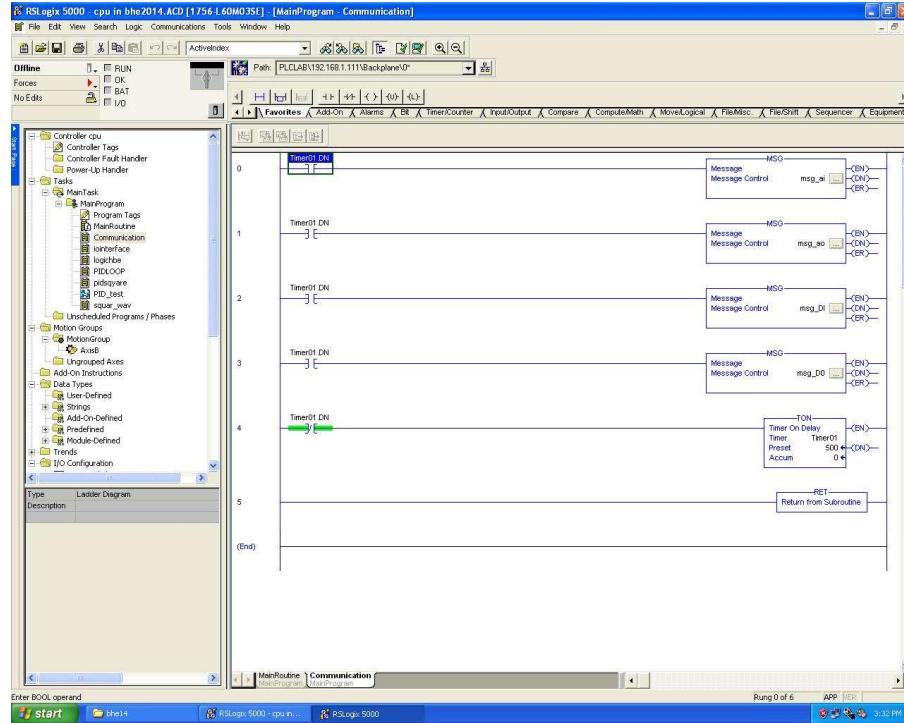


Figure 9.8: Communication subroutine in Contrologix 1756-L61

### 9.3 Delta V DCS Communication Procedure

We are utilizing the serial card Delta V DCS for our goal of daisy chaining. The standard Delta V Serial card supports serial devices that uses Modbus RTU or ASCII protocol. The programmable serial card supports custom protocols. Both cards communicate through RS232, RS 422/485 full duplex signals. The serial card support both master and slave modes of communications. Master mode is normally used to communicate with a PLC or other third party device supporting Modbus protocol. We are configuring the ports as master. The card is capable of emulating up to 16 slave devices on each port. we have to configure the device on the port and set them to different slave addresses.

### 9.4 Configuring Serial card

The serial card is one of the card type in the Delta V Explorer. Each serial card has two ports. Each port can support 16 serial devices. Once the serial card is configured we can set the serial port properties and add serial devices to the ports.

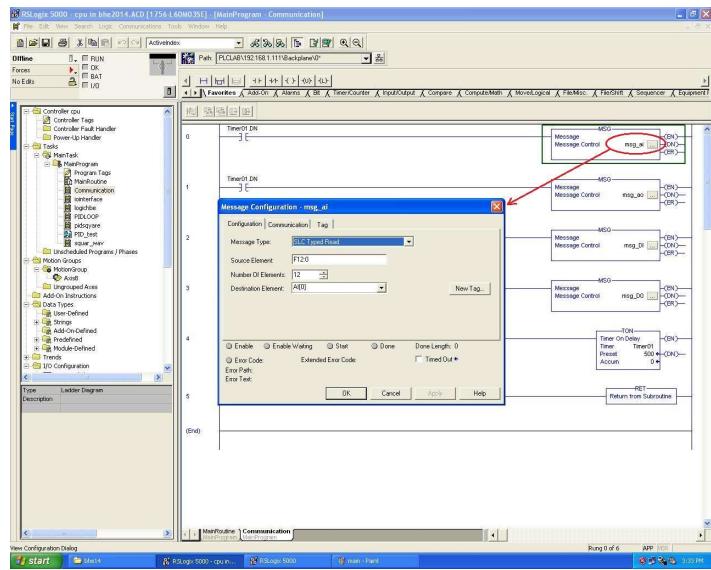


Figure 9.9: Message Instruction configuration for read operation in Contrologix 1756-L61



Figure 9.10: Message Instruction configuration (creating arrays in Contrologix 1756-L61)

#### 9.4.1 Configuring a Serial Device

To set a port to a specific modbus address, configure a device on the port and set the device address to the desired slave address. The DeltaV Explorer help provides step-by-

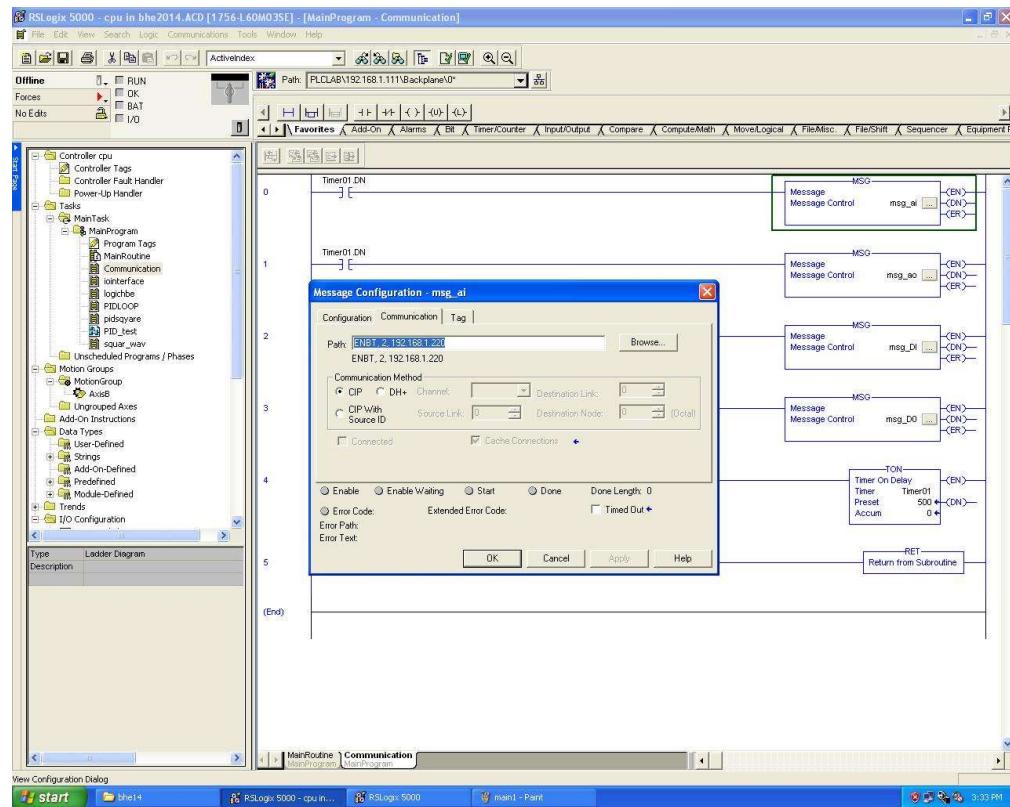


Figure 9.11: Message Instruction configuration (creating arrays in Contrologix 1756-L61)

step instructions for adding serial devices. For example, the following steps describe how to configure two serial devices (a multi-port configuration) connected to port 1 of a serial card. Select port 1 (PO1) of the serial card. Right-click and select New Serial device. Set the device address to match the address of the physical device connected to the serial card. Repeat steps 1 through 3 for the second device. Set the address of the second device to match the address of the physical device connected to the serial card Download card 7 to complete your procedure.

#### 9.4.2 Configuring a Dataset

In master mode, the Serial Card exchanges data with the serial device through a dataset. A dataset is a collection of parameters associated with a serial device. The parameters in the dataset hold data values that correspond to registers or data in a serial device. The dataset defines the type and amount of data being sent to or received from the serial device. All the data values for a dataset have the same properties. Properties include the data type, data direction, and so on. The data values in a dataset map to a contiguous series of serial device registers or data. **For example, the user needs a dataset with the following parameter values:**

- Output mode: Output
- DeltaV datatype: 16 bit uint with status
- PLC datatype: holding registers

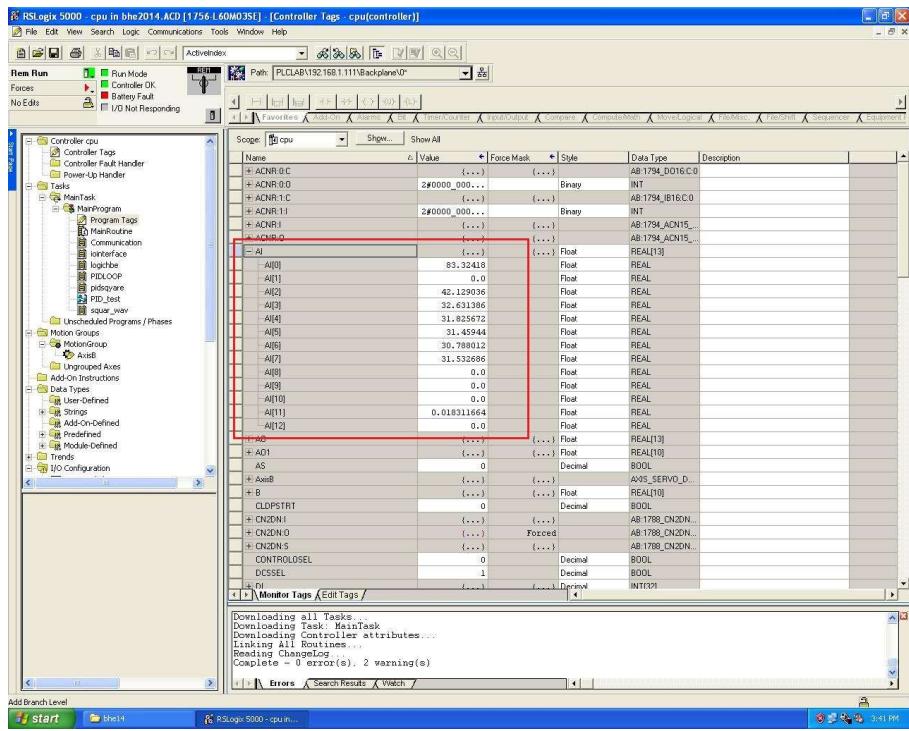


Figure 9.12: Online values from the field after succesfull communication in Contrologix 1756-L61

- PLC offset: 19
- Number of values: 13

#### The following steps describe how to configure the values:

- Select the device (for example, Dev01 under port PO1).
- Right click and select New Dataset.
- On the General tab select output in the Data direction field.
- On DeltaV tab select Floating point with status in the DeltaV data type field.
- On PLC tab select holding registers and set Number of values.

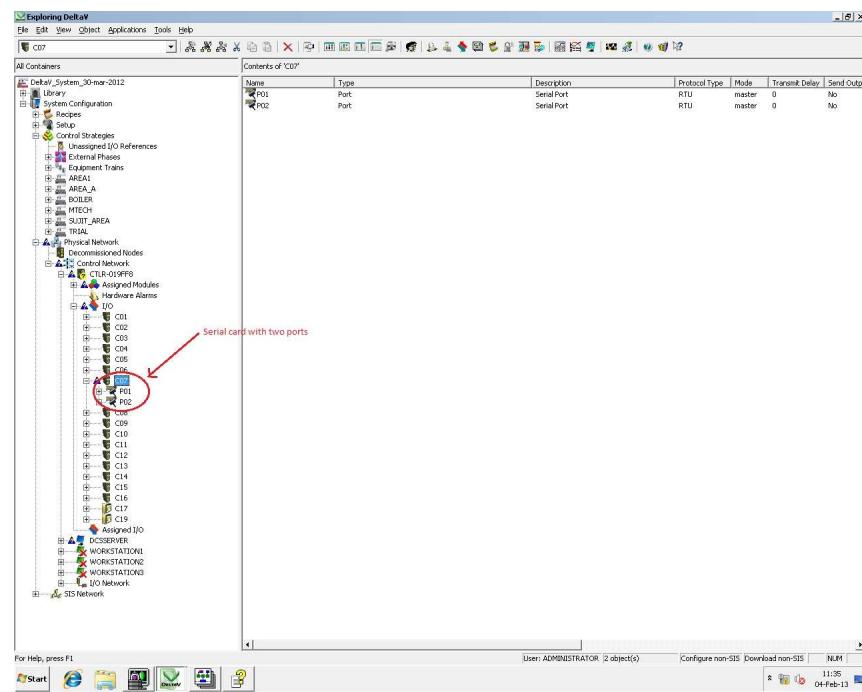


Figure 9.13: Delta V Explorer showing serial card 7 with two ports

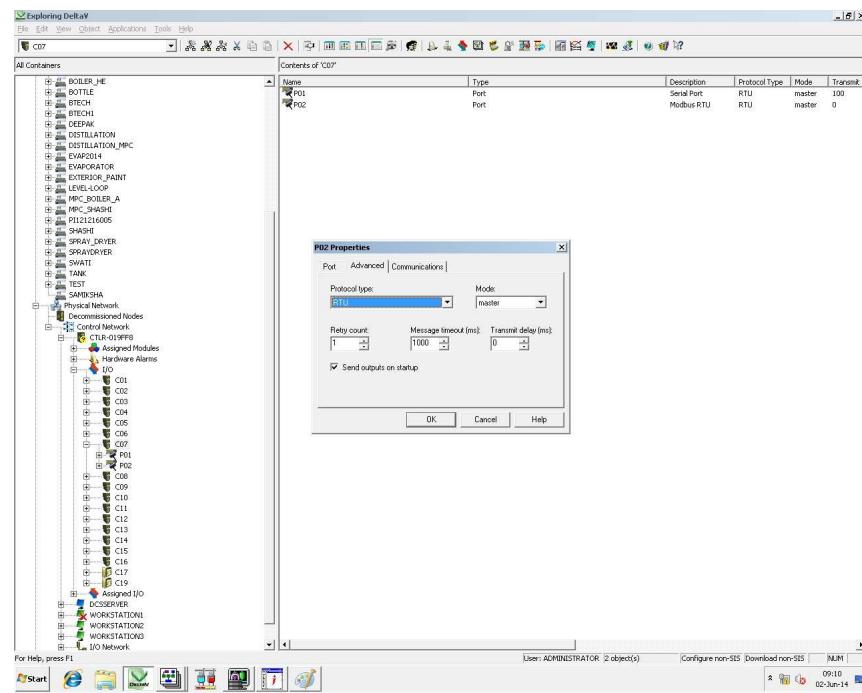


Figure 9.14: Delta V Explorer configuring ports

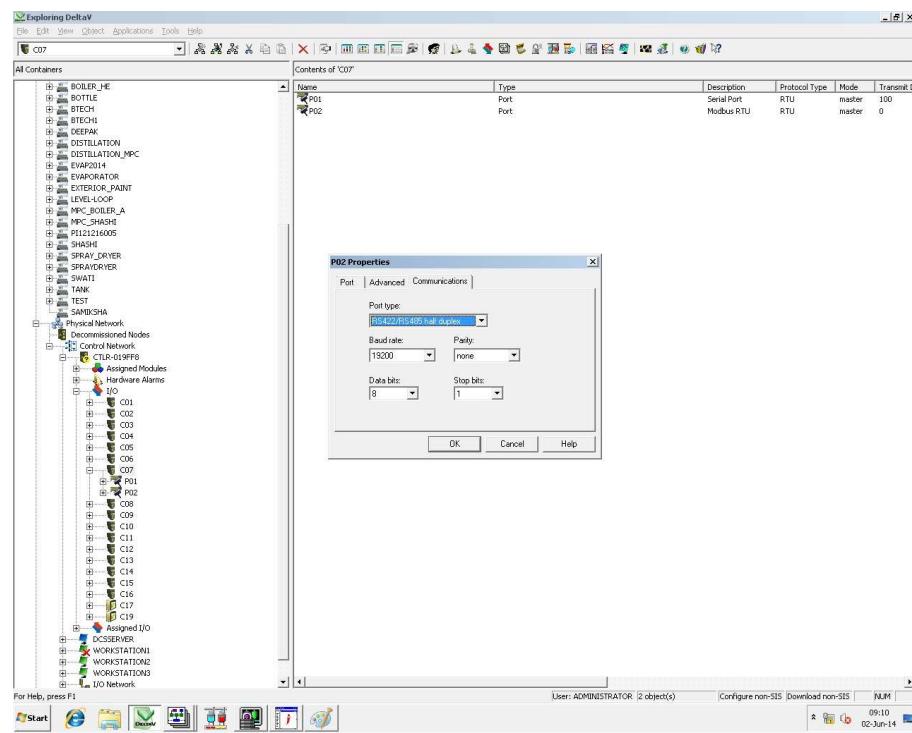


Figure 9.15: Delta V Explorer configuring ports



Figure 9.16: Delta V Explorer adding serial device

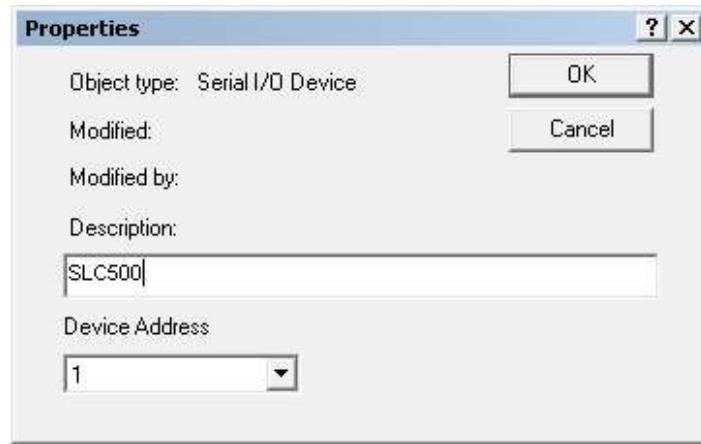


Figure 9.17: Delta V Explorer adding serial device

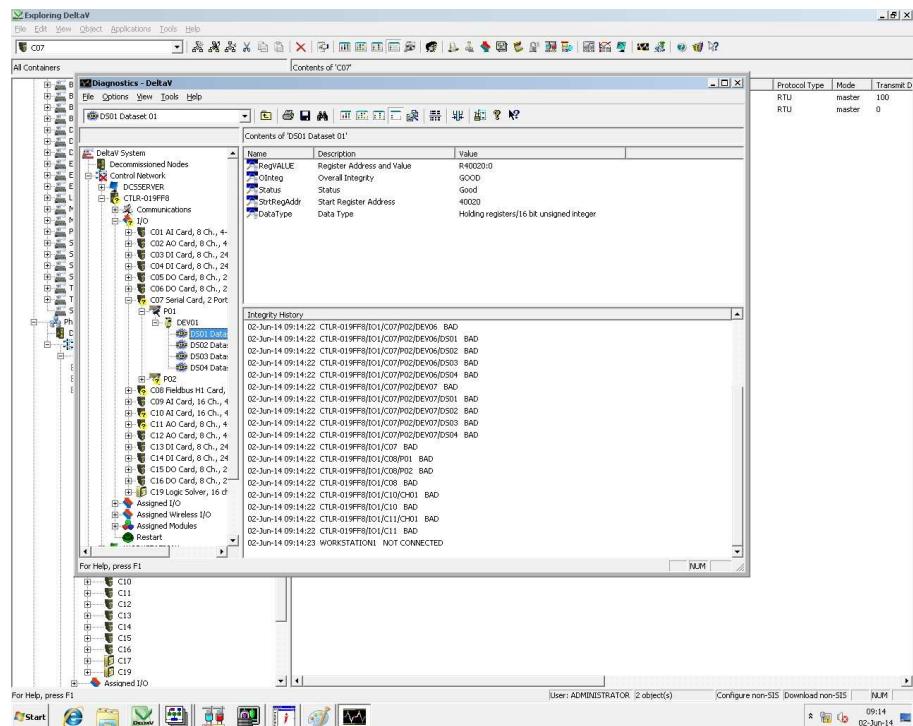


Figure 9.18: Delta V data diagnosing tool

#### 9.4.3 Conclusion

Once the communication is established select the particular device, right click and select diagnose to open Delta V Diagnose tool. If the communication is proper it will show all the register value status as good. If it is showing connection BAD or Device failure the we have to trouble shoot our communication procedure. If you click on register values in diagnosis screen you can see the online values after successful communication. All the related

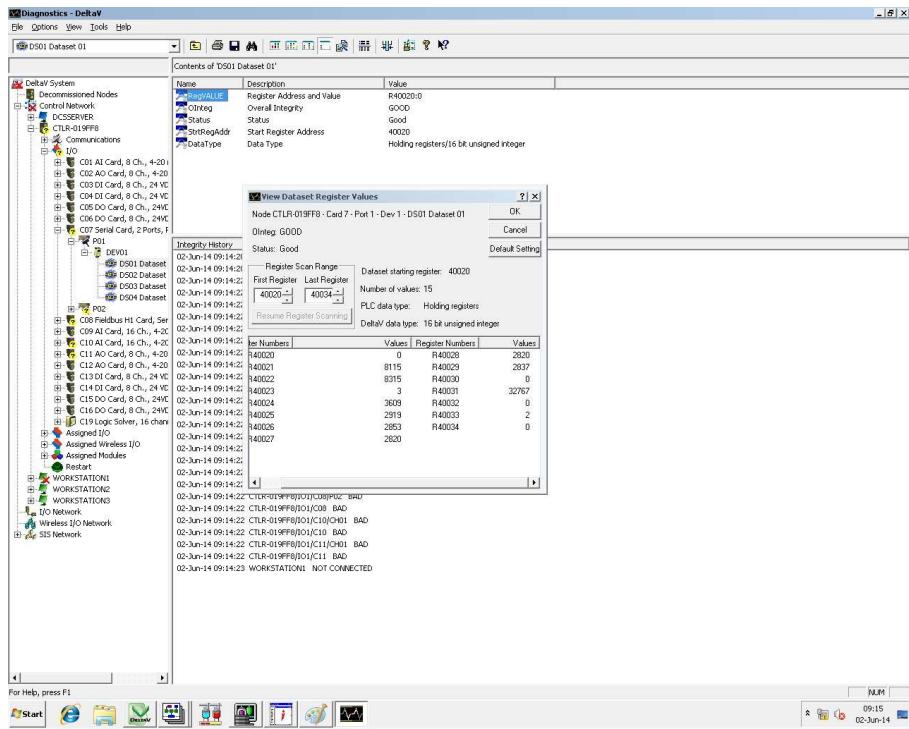


Figure 9.19: Delta V diagnosing tool shows online data after successful communication



Figure 9.20: RS 232 to 485 converter

procedures are shown in the figures.

We communicate Micrologix 1400 PLC in modbus RTU 485 using 8 PIN MINI DIN. Though this port is 485 compatible it is recommended to use a converter. So we used a 232 to 485 converter. The converter device used is shown in figure 9.20

Since the Boiler, Heat exchanger & Evaporator Plant have local PLC as Micrologix 1400. The communication procedure is same for all the devices. hence this chapter is common for both the plants

# Chapter 10

## Resultant Discussion

### 10.1 overview

The Pilot plants were erected commissioned and tested. All pilot plants were fully automated from various domains, developed SCADA for the same in all domains. Focused on control strategies simple PID , Cascade Control, 3 element control for boiler which helps to enhance the performance of pilot plants

### 10.2 Advantages of MPC

The implementation and commissioning of the MPC function block are far simpler and faster than traditional techniques such as cascade,feed forward etc in DCS domain.The difference is even more dramatic for applications involving a larger number of controlled, constraint, or disturbance parameters or the optimization of throughput.Applications that may benefit from MPC control can be identified based on application. It is best suited for the following applications.

- Single or multiple loop control that is characterized by either long delay or inverse process response. Since the control action taken by an MPC function block is based on a process response model, we can achieve better control than would be possible with PID feedback control or dead time compensation techniques, such as the Smith Predictor. The response model used by MPC is determined by the Predict application during commissioning
- The interaction of two or more control loops impact process operation (that is, a change in the output of one control loop impacts the control parameter of the other control loops in a significant manner). Such interaction is accounted for when control action is taken by the MPC function block. Therefore, control may be improved since any correction that is taken to adjust one control parameter only impacts that parameter.
- One or more disturbances to any controlled parameters are measured. By including these measurements in the control, the MPC function block compensates for the impact of disturbances. As such, changes in the disturbance input have little or no impact on the controlled parameters.
- One or more measurable constraints must be observed in control of the process. The MPC function block constantly calculates the impact of a disturbance or control action on constraint parameters. If the future value of a constraint output violates its limit,

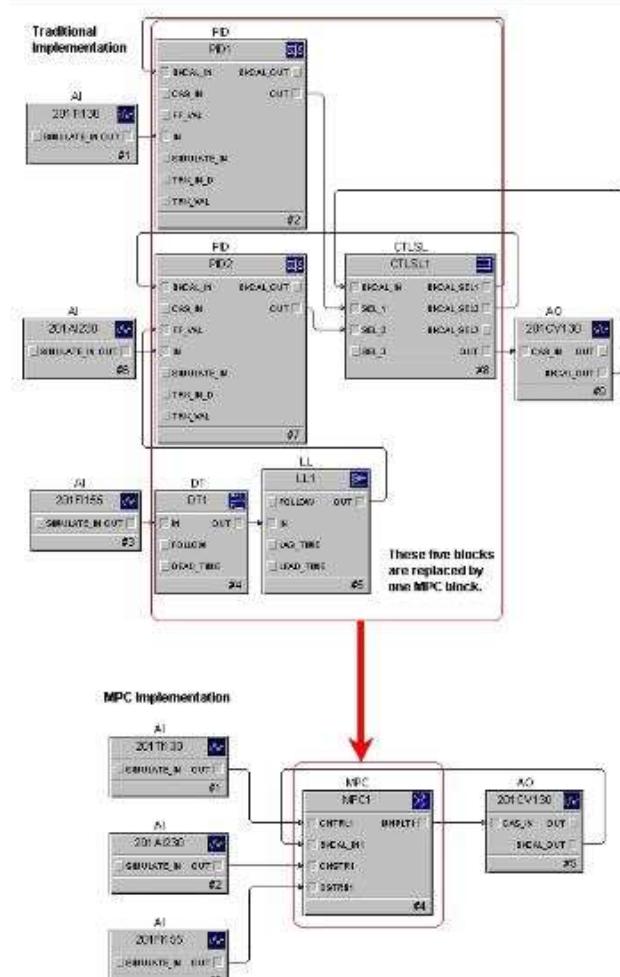


Figure 10.1: Comaprison of MPC with traditional Control

MPC takes the appropriate action to prevent the constraint limit from being violated.

- Production is limited by one or more inputs to a process. Control of the throughput may be included in the MPC along with the control associated with the inputs that limit production. Throughput is adjusted to maintain the process at its input limit and achieve maximum production

The execution rate of the MPC function block is limited to one second or slower. Therefore, MPC should be applied to processes where control requirements may be satisfied at these execution speeds.

### 10.3 Conclusion

Concluding the project by making the pilot plant fully functional and automatic. This project will help the future engineering aspirants a better practical way to understand and

analyze various engineering problems and explore their potential to solve them. The MATLAB interfacing with PLC will surely help the students not only to come out with just simulation results but help them to compare with practical results as well. The communication of pilot plant through Virtual Lab helps the enthusiastic students around the world with minimum practical resources to understand the process by making avail our user friendly virtual PLC and DCS and can visualize and feel the real industrial environment through on-line cameras. The testing process of PID by using various waveforms mentioned in chapter 8 is implemented in our Virtual LAB so as to provide a platform to learn PID tuning for non integrating processes.

# **Part IV**

# **Appendix**

## Appendix A

# IO Details Of Boiler And Heat Exchanger

Type	Sr.No	Parameter Description	Tag	Modbus	Micrologix1400	RSLogix500	RSLogix500_RT	RSLogix5000	VPLC/VDCS	DCS
AI	1	BOILER LEVEL TX.	L1-1	40011	I:1.0	F8:24	F12:0	SLC_AI 0	N24:10	F11:0
	2	BOILER PRESSURE TX.	PT1-1	40012	I:1:1	F8:29	F12:1	SLC_AI 1	N24:11	F11:1
	3	BOILER TEMPERATURE TX.1	TT1-1	40013	I:1:2	F8:34	F12:2	SLC_AI 2	N24:12	F11:2
	4	STATION TEMPERATURE TX.2	TT1-2	40014	I:1:3	F8:39	F12:3	SLC_AI 3	N24:13	F11:3
	5	O/L TEMPERATURE TX.3	TT1-3	40015	I:2:0	F8:44	F12:4	SLC_AI 4	N24:14	F11:4
	6	COLD WATER TEMPERATURE TX.4	TT1-4	40016	I:2:1	F8:49	F12:5	SLC_AI 5	N24:15	F11:5
	7	HOT WATER TEMPERATURE TX.5	TT1-5	40017	I:2:2	F8:54	F12:6	SLC_AI 6	N24:16	F11:6
	8	FEED WATER TEMPERATURE TX.6	TT1-6	40018	I:2:3	F8:59	F12:7	SLC_AI 7	N24:17	F11:7
	9	VERTEX FLOW METER (STEAM FLOW)	FT1	40019	I:3:0	F8:64	F12:8	SLC_AI 8	N24:18	F11:8
	10	ELECTROMAGNETIC FLOW METER (COOLANT FLOW)	FT1	40020	I:3:1	F8:69	F12:9	SLC_AI 9	N24:19	F11:9
	11	POSITIVE DISP PUMP WITH IN BUILT RPM METER (FEED FLOW)	FT1	40021	I:3:2	F8:74	F12:10	SLC_AI 10	N24:20	F11:10
	12	3 PHASE ENERGY METER	3PEM	40022	I:3:3	F8:79	F12:11	SLC_AI 11	N24:21	F11:11
	13	SPARE	SPARE	40023	-	-	-	SPARE	-	-
	14	SPARE	SPARE	40024	-	-	-	SPARE	-	-
	15	SPARE	SPARE	40025	-	-	-	SPARE	-	-
	16	SPARE	SPARE	40026	-	-	-	SPARE	-	-
	17	SPARE	SPARE	40027	-	-	-	SPARE	-	-
St.No	Parameter Description	Tag	Modbus	Micrologix1400	RSLogix500	RSLogix500_RT	RSLogix5000	VPLC/VDCS	DCS	
AO	1	VFD FOR BOILER FEED WATER PUMP	VFD 301	40031	O:0:4	F9:0	F12:30	SLC_AO 0	N24:31	F11:31
	2	VFD FOR COLD WATER PUMP	VFD 301	40032	O:0:5	F9:1	F12:31	SLC_AO 1	N24:32	F11:32
	3	SCR BASED FIRING RATE FOR HEATER MODULATION	SCR	40033	O:4:0	F9:2	F12:32	SLC_AO 2	N24:33	F11:33
	4	MODULATING SOLENOID VALVE	MSV 1	40034	O:4:1	F9:3	F12:33	SLC_AO 3	N24:34	F11:34
	5	MODULATING SOLENOID VALVE 2	MSV 2	40035	O:4:2	F9:4	F12:34	SLC_AO 4	N24:35	F11:35
	6	CONTROL VALVE FOR STEAM FLOW	VCV1	40036	O:4:3	F9:5	F12:35	SLC_AO 5	N24:36	F11:36
St.No	Parameter Description	Tag	Modbus	Micrologix1400	RSLogix500	RSLogix500_RT	RSLogix5000	VPLC/VDCS	DCS	
DI	1	BOILER DRUM LOW LEVEL SW	LSL_401	40031	I:0:0	N7:0	N26:41	SLC_DI 0	N24:41	N13:0
	2	BOILER DRUM HIGH TEMP SW	TSR_401	40042	I:0:1	N7:1	N26:42	SLC_DI 1	N24:42	F11:42
	3	BOILER DRUM HIGH PRESSURE SW	PSR_401	40043	I:0:2	N7:2	N26:43	SLC_DI 2	N24:43	F11:43
	4	BOILER TANK HIGH LEVEL SW	LSL_301	40044	I:0:3	N7:3	N26:44	SLC_DI 3	N24:44	F11:44
	5	HOT WATER TANK HIGH LEVEL SW	LSH_301	40045	I:0:4	N7:4	N26:45	SLC_DI 4	N24:45	F11:45
	6	HOT WATER TANK LOW LEVEL SW	LSL_301	40046	I:0:5	N7:5	N26:46	SLC_DI 5	N24:46	F11:46
	7	COLD WATER TANK HIGH LEVEL SW	LSH_301	40047	I:0:6	N7:6	N26:47	SLC_DI 6	N24:47	F11:47
	8	COLD WATER TANK LOW LEVEL SW	LSL_301	40048	I:0:7	N7:7	N26:48	SLC_DI 7	N24:48	F11:48
	9	BOILER FEED WATER PUMP RUN FB	P101_R	40049	I:0:8	N7:8	N26:49	SLC_DI 8	N24:49	F11:49
	10	BOILER FEED WATER PUMP TRIP FB	P101_T	40050	I:0:9	N7:9	N26:50	SLC_DI 9	N24:50	F11:50
	11	COLD WATER PUMP RUN FB	P201_R	40051	I:0:10	N7:10	N26:51	SLC_DI 10	N24:51	F11:51
	12	COLD WATER PUMP TRIP FB	P201_T	40052	I:0:11	N7:11	N26:52	SLC_DI 11	N24:52	F11:52
	13	REMOTE/LOCAL SELECTOR SW	R/L	40053	I:0:12	N7:12	N26:53	SLC_DI 12	N24:53	F11:53
	14	VIRTUAL PLC SELECTED	VPLC SEL	40054	I:0:13	N7:13	N26:54	SLC_DI 13	N24:54	F11:54
	15	DCS SELECTED	DCS SEL	40055	I:0:14	N7:15	N26:55	SLC_DI 14	N24:55	F11:55
	16	CONTROLLER SELECTED	CNTL1_LCX SEL	40056	I:0:15	N7:16	N26:56	SLC_DI 15	N24:56	F11:56
	17	SPARE	SPARE	40057	I:0:16	N7:17	N26:57	SLC_DI 16	N24:57	F11:57
	18	SPARE	SPARE	40058	I:0:17	N7:17	N26:58	SLC_DI 17	N24:58	F11:58
	19	SPARE	SPARE	40059	I:0:18	N7:18	N26:59	SLC_DI 18	N24:59	F11:59
	20	SPARE	SPARE	40060	I:0:19	N7:19	N26:60	SLC_DI 19	N24:60	F11:60
St.No	Parameter Description	Tag	Modbus	Micrologix1400	RSLogix500	RSLogix500_RT	RSLogix5000	VPLC/VDCS	DCS	
DO	1	FEED WATER PUMP START/STOP CMD	P_S01	40072	O:0:0	N10:0	N26:71	SLC_DO 0	N24:70	F11:71
	2	COLD WATER PUMP START/STOP CMD	P_S01	40073	O:0:1	N10:1	N26:72	SLC_DO 1	N24:73	F11:72
	3	HEATER ON/OFF CMD	HEATER	40074	O:0:2	N10:2	N26:73	SLC_DO 2	N24:73	F11:73
	4	HOT WATER TANK SOLENOID VALVE ON/OFF CMD	SOV_201	40075	O:0:3	N10:3	N26:74	SLC_DO 3	N24:74	F11:74
	5	HOT TOWER SOLENOID VALVE ON/OFF CMD	HOTOWER	40076	O:0:4	N10:4	N26:75	SLC_DO 4	N24:75	F11:75
	6	SPARE	SPARE	40077	O:0:5	N10:5	N26:76	SLC_DO 5	N24:76	F11:76
	7	SPARE	SPARE	40078	O:0:6	N10:6	N26:77	SLC_DO 6	N24:77	F11:77
	8	SPARE	SPARE	40079	O:0:7	N10:7	N26:78	SLC_DO 7	N24:78	F11:78
	9	SPARE	SPARE	40080	O:0:8	N10:8	N26:79	SLC_DO 8	N24:79	F11:79
	10	SPARE	SPARE	40081	O:0:9	N10:9	N26:80	SLC_DO 9	N24:80	F11:80
	11	SPARE	SPARE	40082	O:0:10	N10:10	N26:81	SLC_DO 10	N24:81	F11:81
	12	SPARE	SPARE	40083	O:0:11	N10:11	N26:82	SLC_DO 11	N24:82	F11:82

Figure A.1: IO details For Boiler And Heat Exchanger

## **Appendix B**

# **IO Details Of Evaporator Pilot Plant**

VPLC MODBUS LIST						
DIGITAL INPUT						
Sr. No.	DESCRIPTION	TAG NAME	MODBUS ADDRESS	Micrologix 1400	RsLogix 500	RsLogix 5000
1	Vibration Type Low Level Switch for Separator(V-601)	LSLL	40011	I:0.0	N7:0.0	N32:11
2	Vibration Type High Level Switch for Separator(V-601)	LSHH	40012	I:0.1	N7:1.0	N32:12
3	Vibration Type Low Level Switch for Feed Tank(T-601)	LSLL1	40013	I:0.2	N7:2.0	N32:13
4	Vibration Type High Level Switch for Product Tank	LSSH1	40014	I:0.3	N7:3.0	N32:14
5	Low Level Switch for Condensate Tank(T-602)	LSLL2	40015	I:0.4	N7:4.0	N32:15
6	High Level Switch for Condensate Tank(T-602)	LSSH2	40016	I:0.5	N7:5.0	N32:16
7	Peristaltic Pump Run Feedback	P-601-R	40017	I:0.6	N7:6.0	N32:17
8	Centrifugal Pump Run Feedback	P-602-R	40018	I:0.7	N7:7.0	N32:18
9	Vacuum Pump Run Feedback	P-603-R	40019	I:0.8	N7:8.0	N32:19
10	REMOTE/LOCAL SELECTOR SWITCH	R/L	40020	I:0.9	N7:9.0	N32:20
11	Virtual PLC Selector	VPLC SEL	40021	I:0.10	N7:10.0	N32:21
12	DCS Selected	DCS SEL	40022	I:0.12	N7:12.0	N32:23
13	Control Logix Selected	CNTRL LGX	40023	I:0.11	N7:11.0	N32:22
14	ACK PB	ACK	40024	I:0.13	N7:13.0	N32:24
15	Peristaltic Pump Selector Switch Feedback	P-601-SW	40025	I:0.15	N7:15.0	N32:26
16	Centrifugal Pump Selector Switch Feedback	P-602-SW	40026	I:0.14	N7:14.0	N32:25
17	Vacuum Pump Selector Switch Feedback	P-603-SW	40027	I:0.16	N7:16.0	N32:27
18	(SPARE) Product Tank Low Level Switch	SPARE	40028	I:0.17	N7:17.0	N32:28
19	SPARE	SPARE	40029	I:0.18	N7:18.0	N32:29
20	Emergency Stop	EM	40030	I:0.19	N7:19.0	N32:30

DIGITAL OUTPUT						
Sr. No.	DESCRIPTION	TAG NAME	MODBUS ADDRESS	Micrologix 1400	RsLogix 500	RsLogix 5000
1	Peristaltic Pump on/off	P-601	40031	O:0.0	N7:20.0	N32:31
2	Centrifugal Pump on/off	P-602	40032	O:0.1	N7:21.0	N32:32
3	Vacuum Pump on/off	P-603	40033	O:0.2	N7:22.0	N32:33
4	Hooter	H	40034	O:0.3	N7:23.0	N32:34
5	SPARE	SPARE	40035	O:0.4	N7:24.0	N32:35
6	SPARE	SPARE	40036	O:0.5	N7:25.0	N32:36
7	SPARE	SPARE	40037	O:0.6	N7:26.0	N32:37

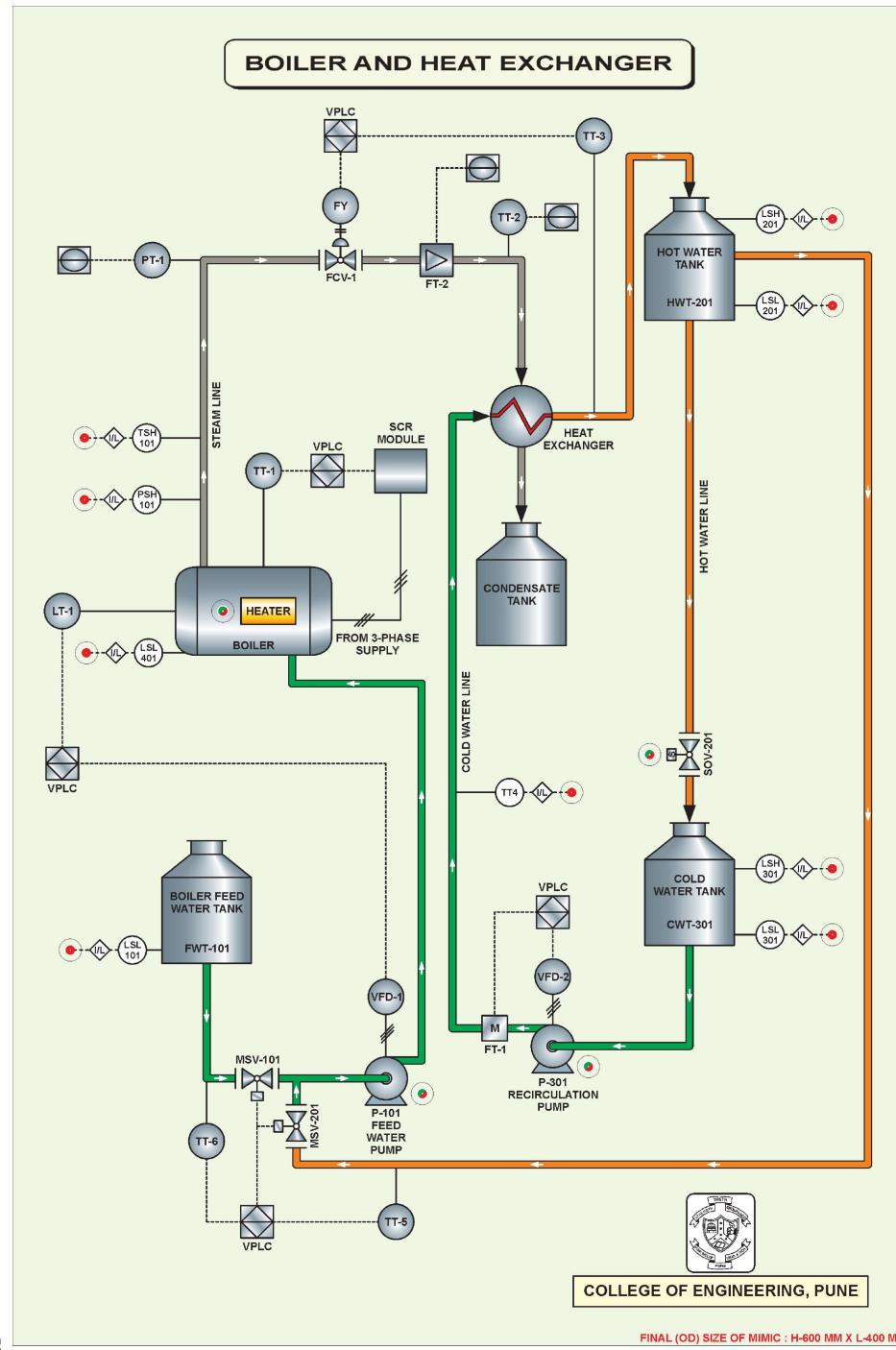




## **Appendix C**

# **MIMIC Of Boiler,Heat Exchanger and Evaporator Pilot Plant**

## C.1 Boiler And Heat Exchanger



SS

Figure C.1: Mimic Of Boiler and Heat Exchanger

## C.2 MIMIC of Evaporator Pilot Plant

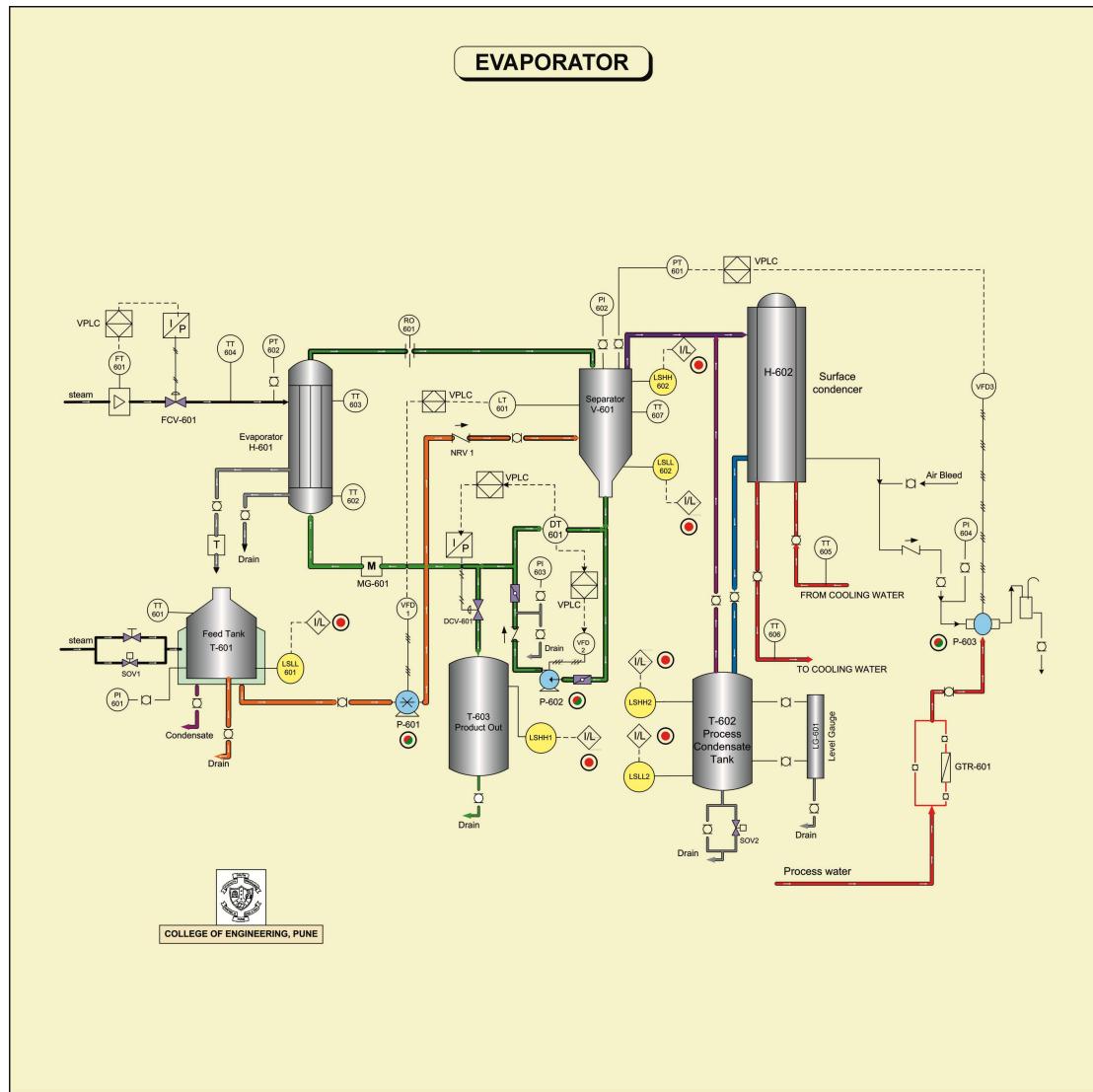


Figure C.2: Mimic of Evaporator Pilot Plant

# **Appendix D**

## **Panel Drawings**

### **D.1 Boiler & Heat Exchanger Panel Drawing**

	9	8	7	6	5	4	3	2	1
F	TITLE	<b>- BILL OF MATERIAL FOR VFD PANEL</b>							
E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>							
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>							
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>							
B	CONSULTANT	<b>- --</b>							
A	VFD PANEL								A
			SCALE : NTS	CHK.BY :	TITLE : BILL OF MATERIAL				
			DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE				
O	ORIGINAL ISSUE	01/06/2012	DATE:01 /06 /2012	APD.BY :	CONSULTANT : --				
REV.	DESCRIPTION	DATE	BY	SHEET NO :1/3	PROJECT : BOILER & HEAT EXCHANGER		REV: 0	ORG.NO.2012-13/20/BOM2	
	9	8	7	6	5	4	3	2	1



9      8      7      6      5      4      3      2      1

**BILL OF MATERIAL ( BOUGHT - OUTS )**

SR.NO.	TAG. NO.	DESCRIPTION	SPECIFICATIONS	MAKE		QTY
1	ENCLOSURE	1100x100 (H) x 600 (W) x 500 (D)		LOGICON	-	1
2	FAN1	LOUVER WITH FAN & FILTER 4"	230V,AC I/P	REXNORD	-	1
3	-	LOUVER WITH FILTER 4"	-	REXNORD	-	1
4	TL1	CFL LAMP WITH FITTING ACCESSORIES	230V,AC I/P	PHILIPS	-	1
5	DS1	DOOR LIMIT SWITCH	10A, AC	SIEMENS	-	1
6	NCB1	MCB, 4 POLE ( AC SUPPLY )	4P/32A,10KA	SIEMENS	-	1
7	NCB2	MCB, 1 POLE ( AC SUPPLY )	1P/2A,10KA	SIEMENS	-	1
8	NCB3	MCB, 2 POLE ( AC SUPPLY )	2P/2A,10KA	SIEMENS	-	1
9	NCB4	MCB, 2 POLE ( AC SUPPLY )	2P/6A,10KA	SIEMENS	-	1
10	NCB5	MCB, 2 POLE ( AC SUPPLY )	2P/10A,10KA	SIEMENS	-	1
11	NCB6	MCB, 3 POLE ( AC SUPPLY )	3P/16A,10KA	SIEMENS	-	1
12	E1	ELECTRICAL EARTH BUSBAR	150x25x3mm	REPUTED	-	2
13	CT1, 2 & 3	CT	50/5 VA	JD	STARLITE	AE
14	-	CT LINKS	-	-	-	3
15	TERMINALS ( SCREW TYPE )	SINGLE DECKER FUSE TERMINALS	4 Sq. mm	ELMEX	-	*
16	TERMINALS ( SCREW TYPE )	SINGLE DECKER TERMINALS	2.5 Sq. mm	ELMEX	-	*
17	TBP	POWER TERMINAL	10 Sq. mm	ELMEX	-	*
17	L1 TO L3	INDICATING LAMPS (RED,YELLOW,BLUE)	230V,AC	TEKNIC	-	3
18	THYR	THREE PHASE BURST FIRING THYRISTOR (TE_300)	20A	SAVIK	-	1
19	F7...F9	FUSES FOR THYRISTORISED MODULE	20A	SAVIK	-	3
20	3PEM	3PH. ENERGY METER WITH 4-20 MA OP	3 PH	SOCOMEK	-	1
21	NL	NEUTRAL LINK	20A	STANDARD	-	1

\* - AS PER POWER DISTRIBUTION / WIRING

VFD PANEL

			SCALE : NTS	CHK.BY :	TITLE : BILL OF MATERIAL		
			DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE		
0	ORIGINAL ISSUE	21/06/2012	DATE:21/06/2012	APD.BY :	CONSULTANT : --	PROJECT : BOILER & HEAT EXCHANGER	REV: 0 DRG.NO.2012-13/20/BOM2
REV:	DESCRIPTION	DATE	BY	SHEET NO .3/3			

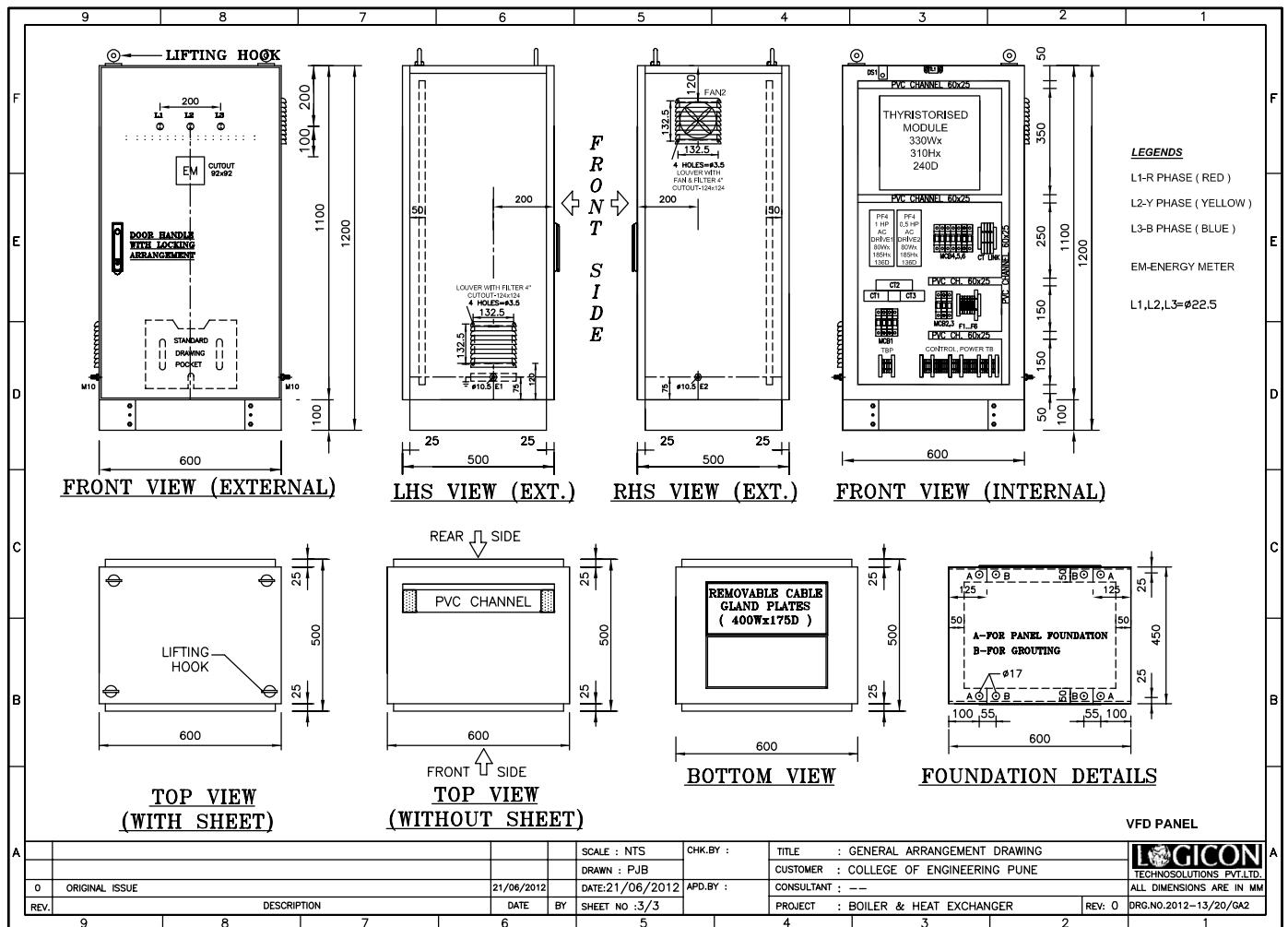
**LOGICON**  
TECHNOSOLUTIONS PVT.LTD.

ALL DIMENSIONS ARE IN MM

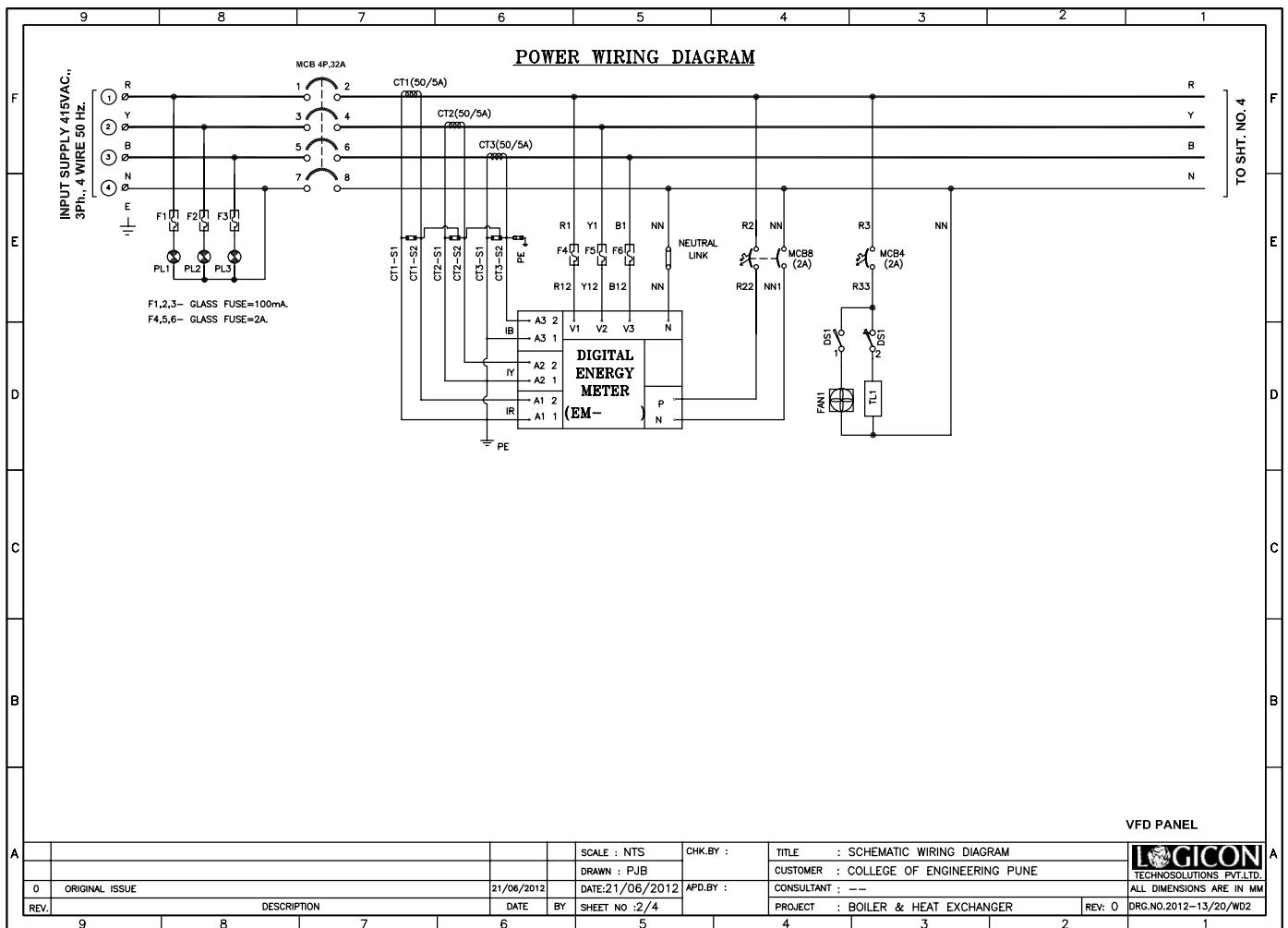
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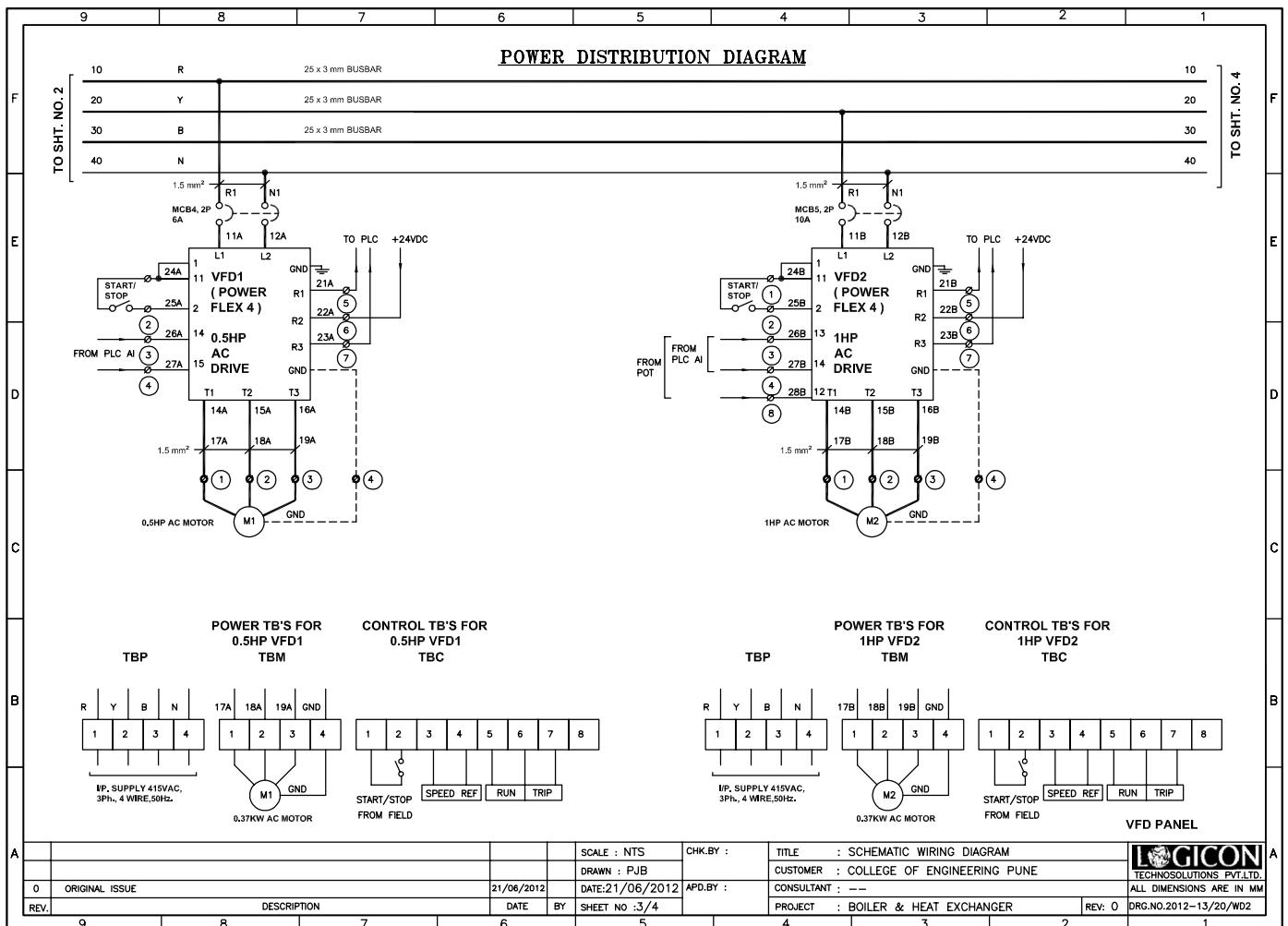
	9	8	7	6	5	4	3	2	1
F	<b>TITLE</b> - <i>GENERAL ARRANGEMENT DRAWING FOR VFD PANEL</i>								F
E	<b>CUSTOMER</b> - <i>COLLEGE OF ENGINEERING PUNE</i>								E
D	<b>PROJECT</b> - <i>BOILER &amp; HEAT EXCHANGER</i>								D
C	<b>PROJ. NO.</b> - <i>LTPL/2012-13/20</i>								C
B	<b>CONSULTANT</b> - --								B
A	<b>VFD PANEL</b>								A
				SCALE : NTS	CHK.BY :	TITLE : GENERAL ARRANGEMENT DRAWING			
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE			 LOGICON TECHNOSOLUTIONS PVT.LTD.
0	ORIGINAL ISSUE		21/06/2012	DATE:21/06/2012	APD.BY :	CONSULTANT : --			ALL DIMENSIONS ARE IN MM
REV.	DESCRIPTION		DATE	BY	SHEET NO :1/3	PROJECT : BOILER & HEAT EXCHANGER			REV: 0 DRG.NO.2012-13/20/GA2
	9	8	7	6	5	4	3	2	1

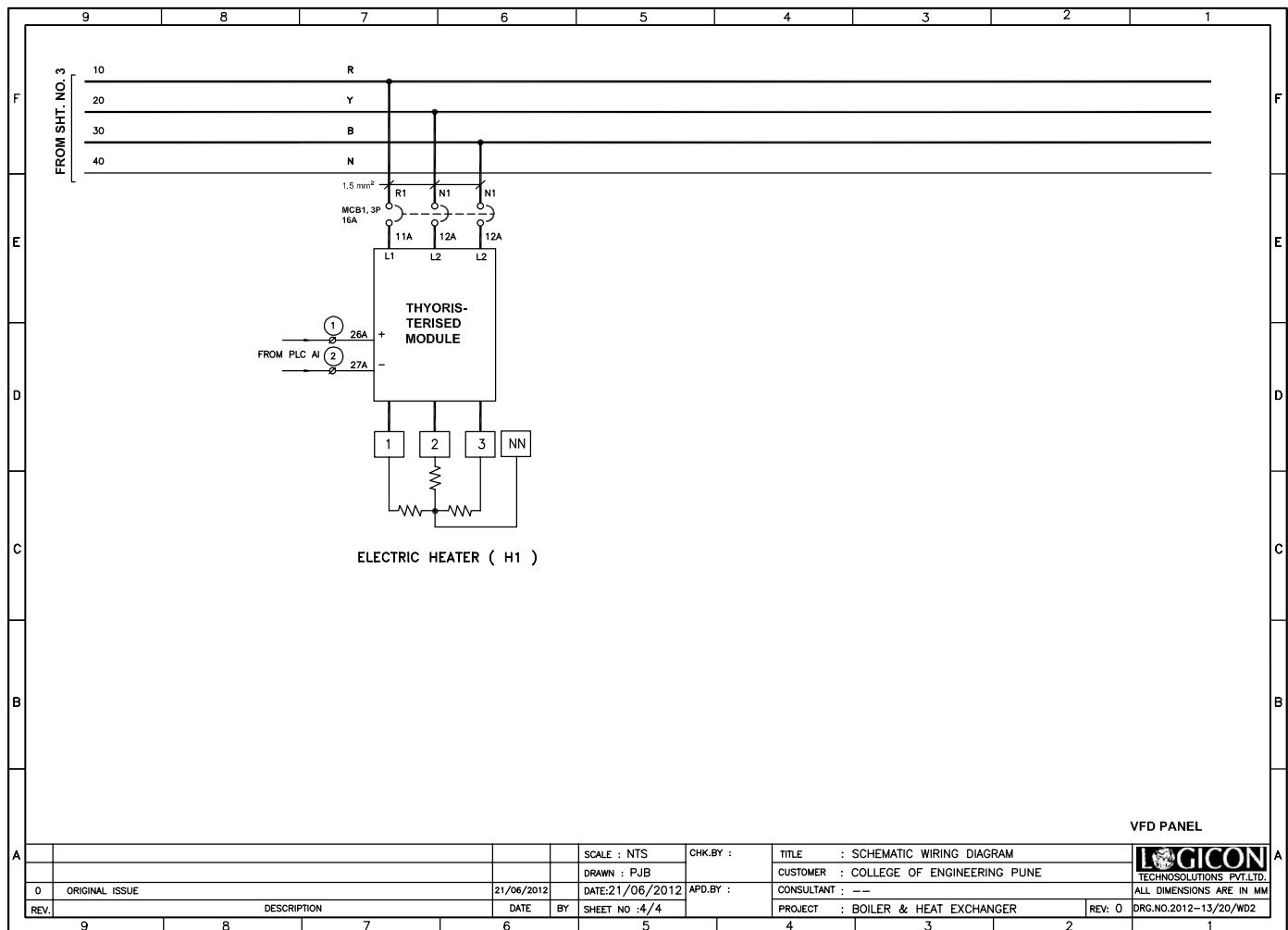
	9	8	7	6	5	4	3	2	1								
F	<b><u>GENERAL SPECIFICATIONS :-</u></b>								F								
<b>- PANEL FRONT DOOR SHALL BE 2mm. THICK CRCA SHEET STEEL.</b>																	
<b>- PANEL FRAME TOP / REAR / SIDE COVER SHALL BE 1.6 mm. THICK CRCA SHEET STEEL.</b>																	
<b>- BASE PLATE SHALL BE 2 mm. THICK CRCA SHEET STEEL.</b>																	
<b>- PANEL SHADE INSIDE / OUTSIDE - SIEMENS GREY (RAL-7032), BASE PLATE - ORANGE. ( POWDER COATED )</b>																	
<b>- DEGREE OF PROTECTION IP - 42</b>																	
<b>- FRONT DOOR SHALL BE PROJECTED, REMOVABLE &amp; LOCKABLE TYPE WITH KEY, PANEL IS FRONT ACCESIBLE ONLY</b>																	
<b>- FRONT DOOR SWING SHALL BE 120 DEG.</b>																	
<b>- CABLE ENTRY SHALL BE FROM BOTTOM.</b>																	
<b>- PANEL SHALL HAVE 4 NOS. REMOVABLE LIFTING HOOKS AT TOP.</b>																	
<b>- STANDARD DRAWING POCKET SHALL BE PROVIDED ON FRONT DOOR.</b>																	
<b>- CABLE TERMINATION SHALL BE DONE WITH PIN TYPE LUGS &amp; USING TUBE FERRULES.</b>																	
<b>- 3 mm. THICK REMOVABLE, UNDRILLED GLAND PLATES SHALL BE PROVIDED.</b>																	
<b>- PVC / RUBBER GASKETING WILL BE PROVIDED FOR DOORS.</b>																	
<b>- 50x100x50x3 mm. THK. M.S. PLINTH SHALL BE USED &amp; PAINTED BLACK. ( FRONT &amp; BACK COVER OF PLINTH SHALL BE REMOVABLE TYPE )</b>																	
<b>- EARTH BOLTS SHALL BE PROVIDED AT BOTH ENDS, WITH CU. BUSBAR OF 150x25X3 mm. SIZE FROM PANEL INSIDE FOR ELECTRICAL EARTHING.</b>																	
<b>- TOLERANCE +/- 5 mm OF PANEL DIMENSIONS.</b>																	
<b>- FOUNDATION DETAILS AS SHOWN IN DRAWING.</b>																	
<b>- PANEL MAKE : LOGICON</b>																	
<b>- EARTHING WIRE WILL BE PROVIDED BETWEEN PANEL DOOR &amp; ELECTRICAL EARTH BUSBAR.</b>																	
<b>VFD PANEL</b>																	
A				SCALE : NTS	CHK.BY :	TITLE : GENERAL ARRANGEMENT DRAWING											
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE											
O	ORIGINAL ISSUE		21/06/2012	DATE:21/06/2012	APD.BY :	CONSULTANT : --											
REV.	DESCRIPTION		DATE	BY	SHEET NO : 2/3	PROJECT : BOILER & HEAT EXCHANGER	REV: 0	ORG.NO:2012-13/20/GA2									
	9	8	7	6	5	4	3	2	1								



	9	8	7	6	5	4	3	2	1																																																								
F	<b>TITLE</b> - <i>SCHEMATIC WIRING DIAGRAM FOR VFD PANEL</i>								F																																																								
E	<b>CUSTOMER</b> - <i>COLLEGE OF ENGINEERING PUNE</i>								E																																																								
D	<b>PROJECT</b> - <i>BOILER &amp; HEAT EXCHANGER</i>								D																																																								
C	<b>PROJ. NO.</b> - <i>LTPL/2012-13/20</i>								C																																																								
B	<b>CONSULTANT</b> - --								B																																																								
A	<b>NOTES</b>								A																																																								
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2  THIS SYMBOL REPRESENTS SCREEN / INSTRUMENTS EARTH.																																																																	
<b>VFD PANEL</b>																																																																	
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			DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE																																																												
0	ORIGINAL ISSUE	21/06/2012	DATE:21/06/2012	APD.BY :	CONSULTANT : --																																																												
REV.	DESCRIPTION	DATE	BY	SHEET NO :1/4	PROJECT : BOILER & HEAT EXCHANGER			REV: 0	ORG.NO:2012-13/20/WD2																																																								
9	8	7	6	5	4	3	2	1																																																									







	9	8	7	6	5	4	3	2	1		
F	TITLE	<b>- WIRING SPECIFICATION FOR VFD PANEL</b>									F
E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>									E
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>									D
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>									C
B	CONSULTANT	<b>--</b>									B
A	<b>VFD PANEL</b>										
				SCALE : NTS	CHK.BY :	TITLE : WIRING SPECIFICATION					
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE					
0	ORIGINAL ISSUE		01/06/2012	DATE: 01 / 06 / 2012	APD.BY :	CONSULTANT : --					
REV.	DESCRIPTION		DATE	BY	SHEET NO : 1/2	PROJECT : BOILER & HEAT EXCHANGER	REV: 0	ORG.NO:2012-13/20/WS2			
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### WIRING SPECIFICATION

F E D C B	230V AC SUPPLY	PHASE ( UPTO DISTRIBUTION TB )	RED	4 mm <sup>2</sup>	
		NEUTRAL ( UPTO DISTRIBUTION TB )	BLACK	4 mm <sup>2</sup>	
		PHASE ( AFTER DISTRIBUTION TB )	RED	1.5 mm <sup>2</sup>	
		NEUTRAL ( AFTER DISTRIBUTION TB )	BLACK	1.5 mm <sup>2</sup>	
E D C B	110V AC SUPPLY	PHASE ( UPTO DISTRIBUTION TB )	RED	4 mm <sup>2</sup>	
		NEUTRAL ( UPTO DISTRIBUTION TB )	BLACK	4 mm <sup>2</sup>	
		PHASE ( AFTER DISTRIBUTION TB )	RED	1.5 mm <sup>2</sup>	
		NEUTRAL ( AFTER DISTRIBUTION TB )	BLACK	1.5 mm <sup>2</sup>	
D C	24V DC +VE	UPTO BUSBAR	BLUE	1.5 mm <sup>2</sup>	
		AFTER BUSBAR	BLUE	1.0 mm <sup>2</sup>	
C B	24V DC -VE	UPTO BUSBAR	WHITE	1.5 mm <sup>2</sup>	
		AFTER BUSBAR	WHITE	1.0 mm <sup>2</sup>	
D/I WIRING			GREY	0.5 mm <sup>2</sup>	
C B	D/O WIRING	MODULE TO RELAY COIL	GREY	0.5 mm <sup>2</sup>	
		RELAY CONTACT TO TERMINALS ( PF )	BROWN	1.0 mm <sup>2</sup>	
		RELAY CONTACT TO TERMINALS ( 24VDC )	BLUE (+), WHITE (-)	1.0 mm <sup>2</sup>	
		RELAY CONTACT TO TERMINALS ( 230/110V AC )	RED (P), BLACK (N)	1.0 mm <sup>2</sup>	
A/I WIRING			ORANGE (+), WHITE (-)	0.5 mm <sup>2</sup>	
A/O WIRING			YELLOW (+), WHITE (-)	0.5 mm <sup>2</sup>	
B	EARTH	POWER	GREEN/YELLOW	2.5 mm <sup>2</sup>	
		INSTRUMENT	GREEN	1.5 mm <sup>2</sup>	

VFD PANEL

A			SCALE : NTS	CHK.BY :	TITLE : WIRING SPECIFICATION				
			DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE				
0	ORIGINAL ISSUE	01/06/2012	DATE: 01/06/2012	APD.BY :	CONSULTANT : --				
REV.	DESCRIPTION	DATE	BY	SHEET NO : 2/2	PROJECT : BOILER & HEAT EXCHANGER	REV: 0	ORG.NO:2012-13/26/WS2		



TECHNOLOGIES SOLUTIONS PVT.LTD.

ALL DIMENSIONS ARE IN MM

9

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7

6

5

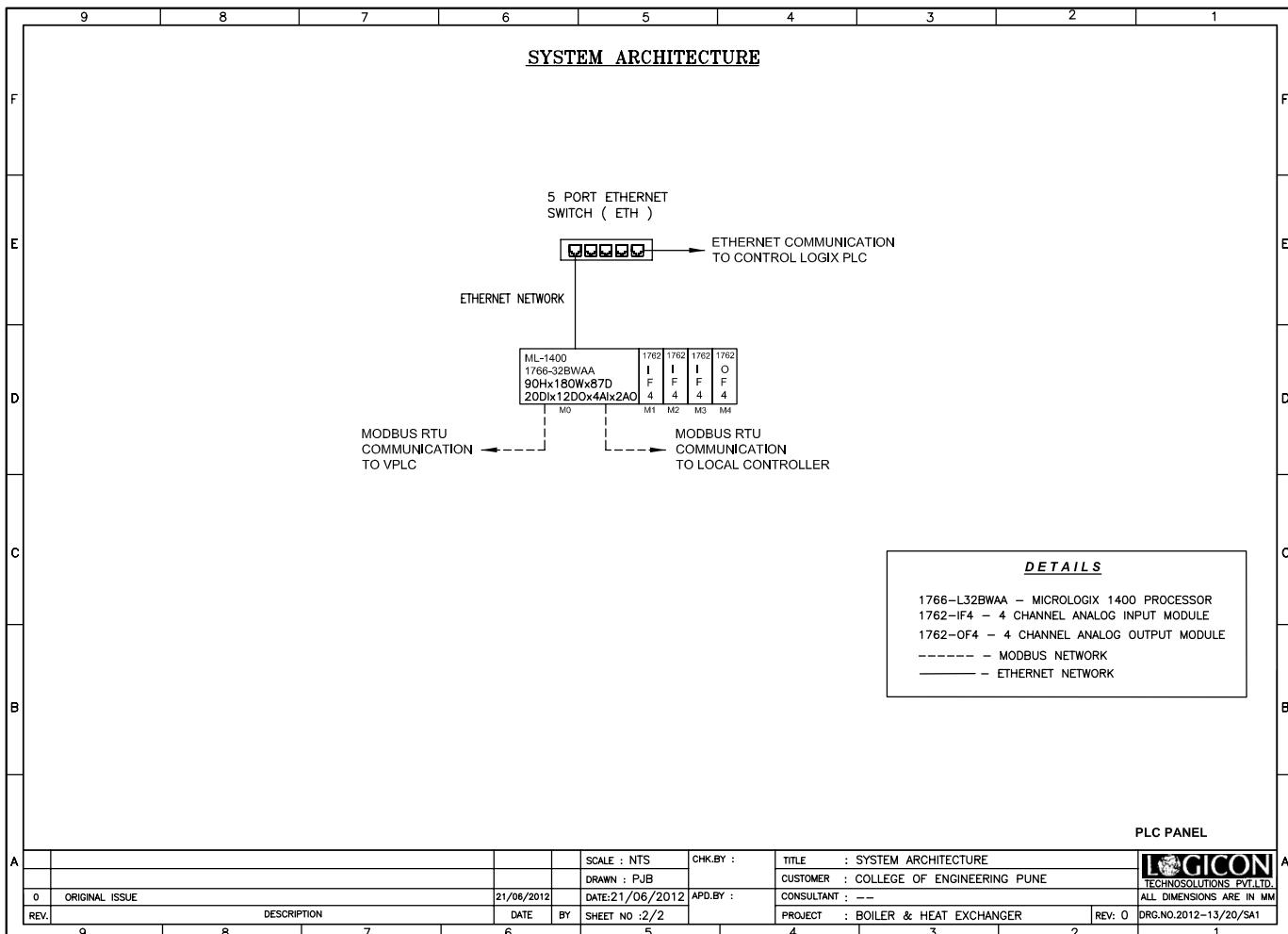
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2

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E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>									E
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>									D
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>									C
B	CONSULTANT	<b>- --</b>									B
A	PLC PANEL										
				SCALE : NTS	CHK.BY :	TITLE : SYSTEM ARCHITECTURE			LOGICON		
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE			TECHNOSOLUTIONS PVT.LTD.		
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E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>									E
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>									D
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>									C
B	CONSULTANT	<b>--</b>									B
A	<b>PLC PANEL</b>										
				SCALE : NTS	CHK.BY :	TITLE : BILL OF MATERIAL					
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE					
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**BILL OF MATERIAL ( ROCKWELL AUTOMATION )**

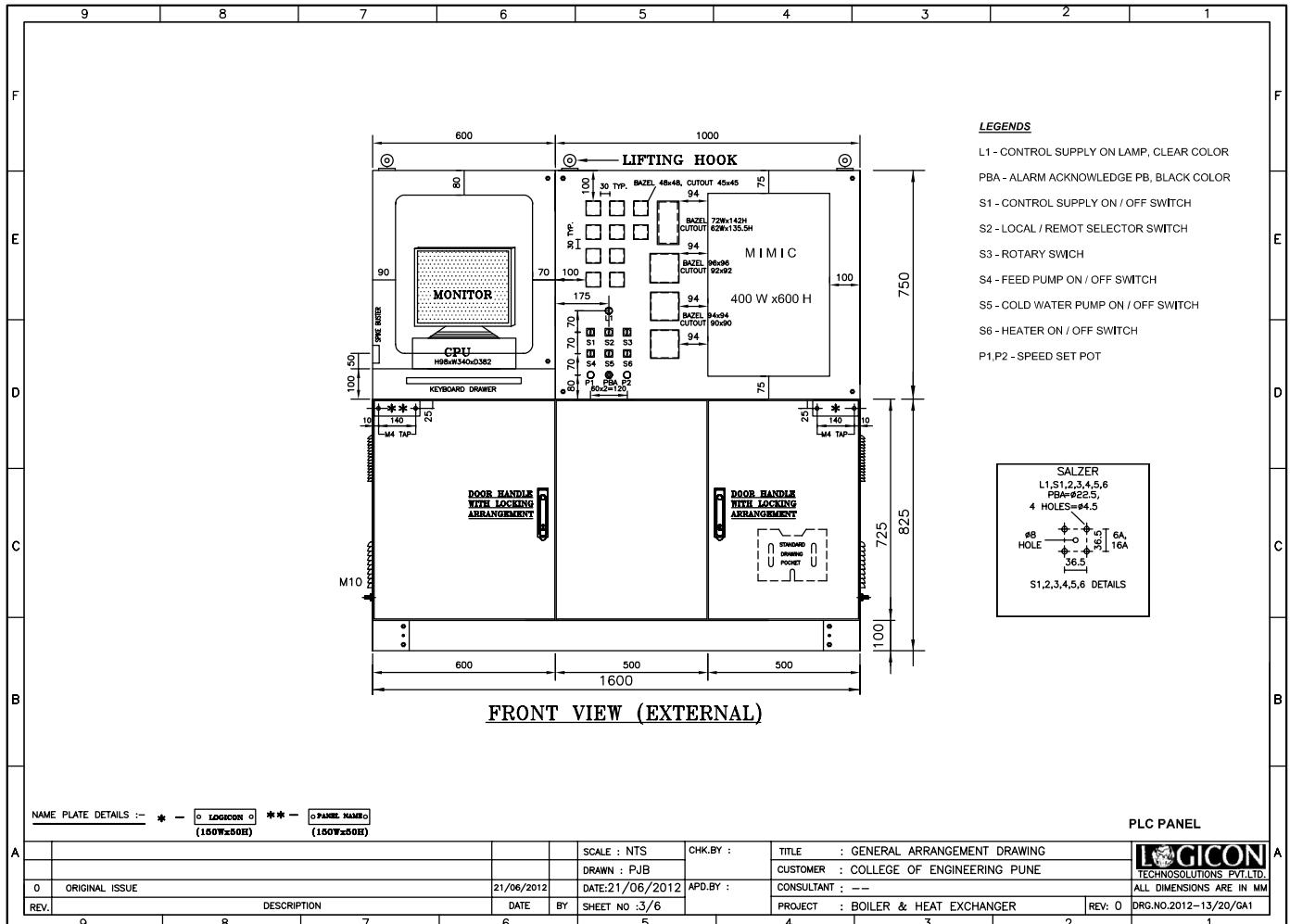
1	1766-L32BWAA	MICROLOGIX 1400 BASE UNIT WITH 20 DI & 12 DO, 4 AI & 2 AO	1
2	1762-IF4	4 CH. ANALOG INPUT MODULE	3
3	1762-OF4	4 CH. ANALOG OUTPUT MODULE	1

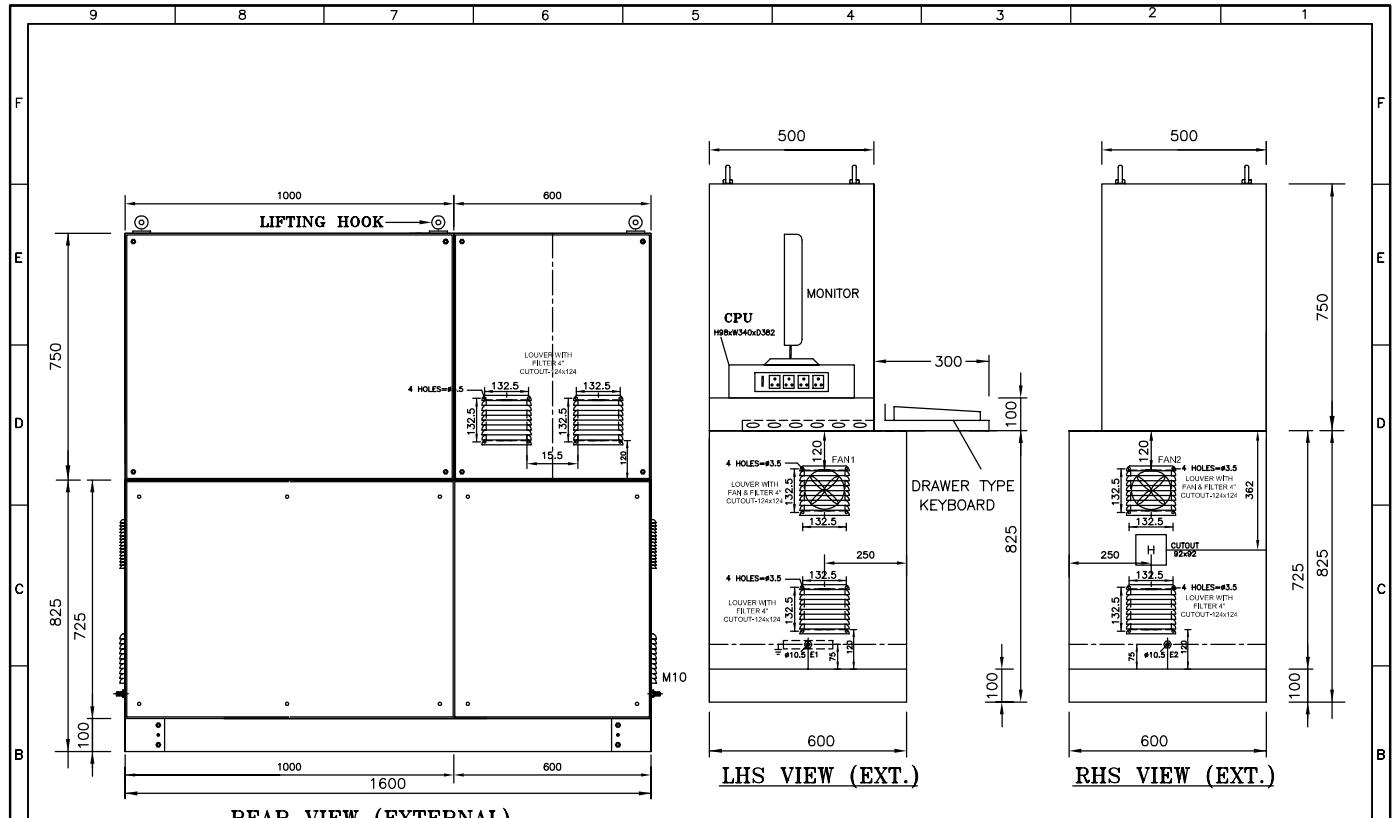
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PLC PANEL																																																			
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REV.	ORIGINAL ISSUE	DATE: 21/06/2012	DRAWN : PJB																																																
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<b>BILL OF MATERIAL ( BOUGHT - OUTS )</b>									
Sr.No.	<b>Description</b>				Tag No	Catalog No.	Make	Qty	
1	PANEL ENCLOSURE SIZE : 1475+100(H) X 1600(W) X 600(D)				-	-	LOGICON	1	
2	COOLING FAN 4", 230VAC				FAN1, 2	-	REXNORD	2	
3	LOUVER WITH FILTER, 4"				-	-	REPUTED	6	
4	CFL LAMP WITH ITS ACCESSORIES,230VAC SUPPLY				TL1, TL2	-	PHILIPS	2	
5	DOOR INTERLOCK SWITCH ASSEMBLY WITH 1NO +1NC CONTACT,230VAC				DS1, DS2	-	SIEMENS	2	
6	UTILITY SOCKET , 230VAC,5A				SOC	-	ANCHOR	1	
7	POWER SUPPLY,I/P 230VAC,O/P 24VDC,5A				PS	-	NHP	1	
8	16 CHANNEL, 24VDC RELAY CARD WITH 2C/O OMRON RELAY				RC1	UL-24-DI6-2COB	UL	1	
9	4 CHANNEL, 24VDC RELAY CARD WITH 1C/O OMRON RELAY				RC2,5,6	UL-24-D04-2COB	UL	3	
10	8 CHANNEL, 24VDC RELAY CARD WITH 1C/O OMRON RELAY				RC3	UL-24-D08-1COB	UL	1	
11	4 CHANNEL, 24VDC RELAY CARD WITH 1C/O OMRON RELAY				RC4	UL-24-D04-1COB	UL	1	
12	4 C/O RELAY, 24VDC				RL-LR	MY4N DC24V	OMRON	1	
13	BASE FOR 4 C/O RELAY				-	PYF14A-N	OMRON	1	
14	CLIP FOR 4 C/O RELAY				-	PYC-A1	OMRON	1	
15	MINIATURE CIRCUIT BREAKER, 2P / 16A,10KA				MCB1	5SX42167RC	SIEMENS	1	
16	MINIATURE CIRCUIT BREAKER, 1P / 2A,10KA				MCB3,4,5	5SX41027RC	SIEMENS	3	
17	MINIATURE CIRCUIT BREAKER, 2P / 6A,10KA				MCB6	5SX42067RC	SIEMENS	1	
17	MINIATURE CIRCUIT BREAKER, 1P / 4A,10KA				MCB2	5SX41047RC	SIEMENS	1	
18	LED TYPE INDICATION LAMP, CLEAR COLOUR, CONTROL SUPPLY ON , 230 VAC				L1	-	SIEMENS / TEKNIC	1	
19	1 POLE 2 WAY COTROL SUPPLY ON/OFF SWITCH,16A				S1	-	SALZER	1	
20	1 POLE 2 WAY ON/OFF SWITCH				S2,4,5,6	-	SALZER	4	
21	1 POLE 3 WAY ROTARY SWITCH, 10A				S3	61049	SALZER	1	
22	PUSH BUTTON FOR ACK (BLACK)				ACK	2AF	TEKNIC	1	
23	5 PORT ETHERNET SWITCH,24VDC SUPPLY				ETH.SW.	SFN5BTX	PHOENIX	1	
24	FUSE TERMINALS,4 SQMM				-	-	ELMEX	AS REQD	
25	NON FUSE TERMINALS,2.5 SQMM				-	-	ELMEX	AS REQD	
26	HOOTER,230VAC SUPPLY				H	-	CAPTAIN / CANDS	1	
27	EARTHENING BUSBAR 25 X 3 MM THROUGHOUT PANELWITH M12 BOLTS				-	-	STD	1	
28	INSTRUMENT EARTH BUSBAR 25 X 3 MM				-	-	STD	AS REQD	
29	1:2 ISOLATOR FOR ANALOG INPUT & NOUTPUT				IS1,2.....11	-	SAPRE	11	
30	INDICATORS FOR ANALOG I/P & O/P				P1,2.....10	-	NISHKO	10	
31	FLOW INDICATOR & TOTALISER (FREE ISSUE)				P11,12	Aics 3000	-	2	
32	50 Mtr ETHERNET CABLE				-	CAT5	DLINK	1	
33	MIMIC 600(H) x 400(W)				-	-	STANDARD	1	
34	THREE ELEMENT LEVEL CONTROLLER (FREE ISSUE)				-	UCS 1000	YOKOGAVA	1	
35	TEMPERATURE CONTROLLER (FREE ISSUE)				-	3204	EUROTHERM	1	
36	SPIKE GUARD				-	-	-	1	
37	SPEED SET POT				P1,P2	-	STANDARD	2	
PLC PANEL									
A					SCALE : NTS	CHK.BY :	TITLE : BILL OF MATERIAL		
					DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE		
O	ORIGINAL ISSUE				DATE:21/06/2012	APD.BY :	CONSULTANT : --		
REV.	DESCRIPTION				DATE:	BY	PROJECT : BOILER & HEAT EXCHANGER	REV: 0	ALL DIMENSIONS ARE IN MM DRG.NO.2012-13/20/BOM1
					SHEET NO .3/3				
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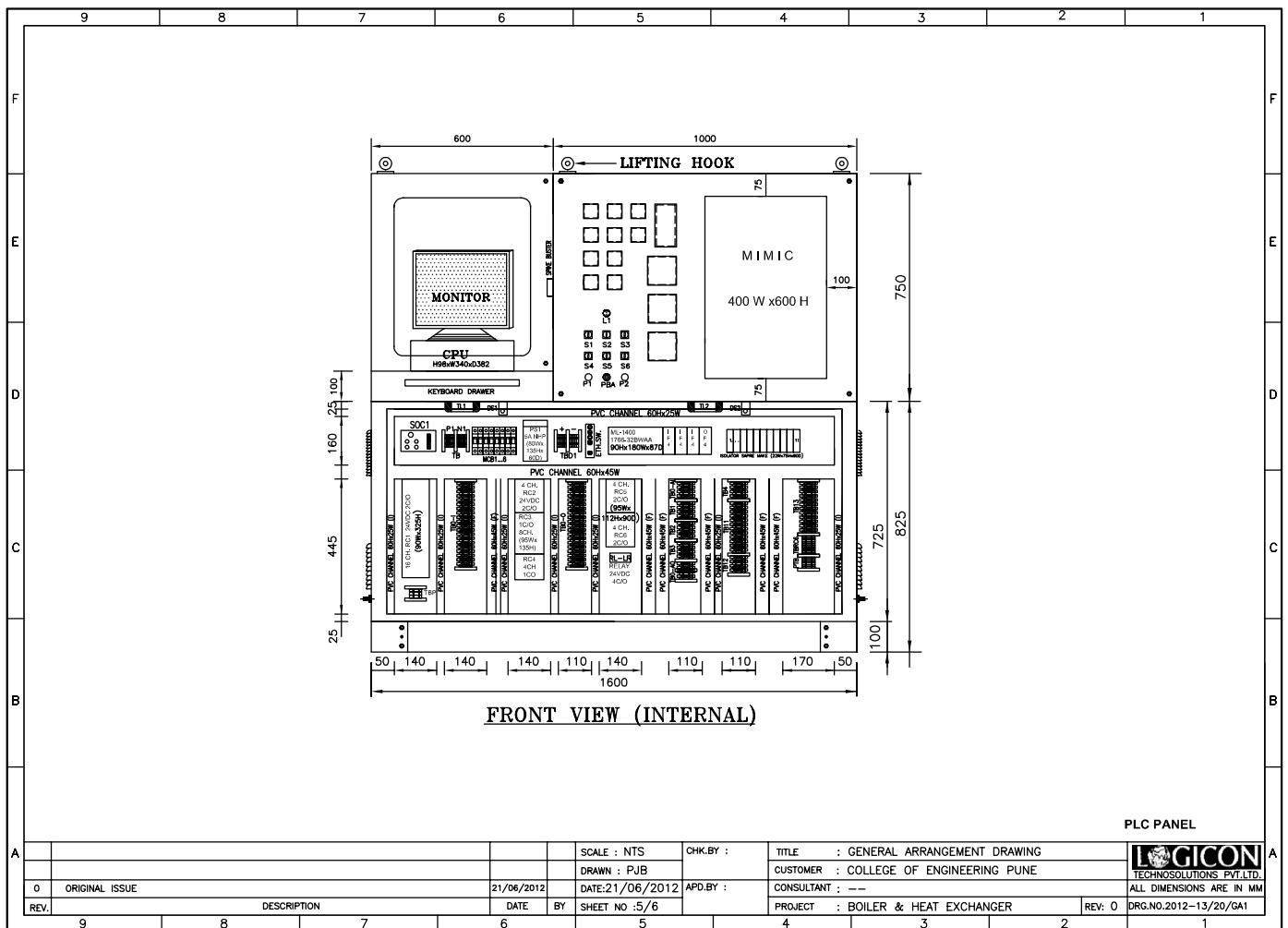
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F	TITLE	<b>- GENERAL ARRANGEMENT DRAWING FOR PLC PANEL</b>									F
E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>									E
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>									D
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>									C
B	CONSULTANT	<b>--</b>									B
A	PLC PANEL										A
				SCALE : NTS	CHK.BY :	TITLE : GENERAL ARRANGEMENT DRAWING			LOGICON		
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE			TECHNOSOLUTIONS PVT LTD.		
O	ORIGINAL ISSUE	21/06/2012	DATE: 21/06/2012	APD.BY :	CONSULTANT :	--			ALL DIMENSIONS ARE IN MM		
REV.	DESCRIPTION	DATE	BY	SHEET NO : 1/6	PROJECT	BOILER & HEAT EXCHANGER			REV: 0	ORG.NO:2012-13/20/GA1	
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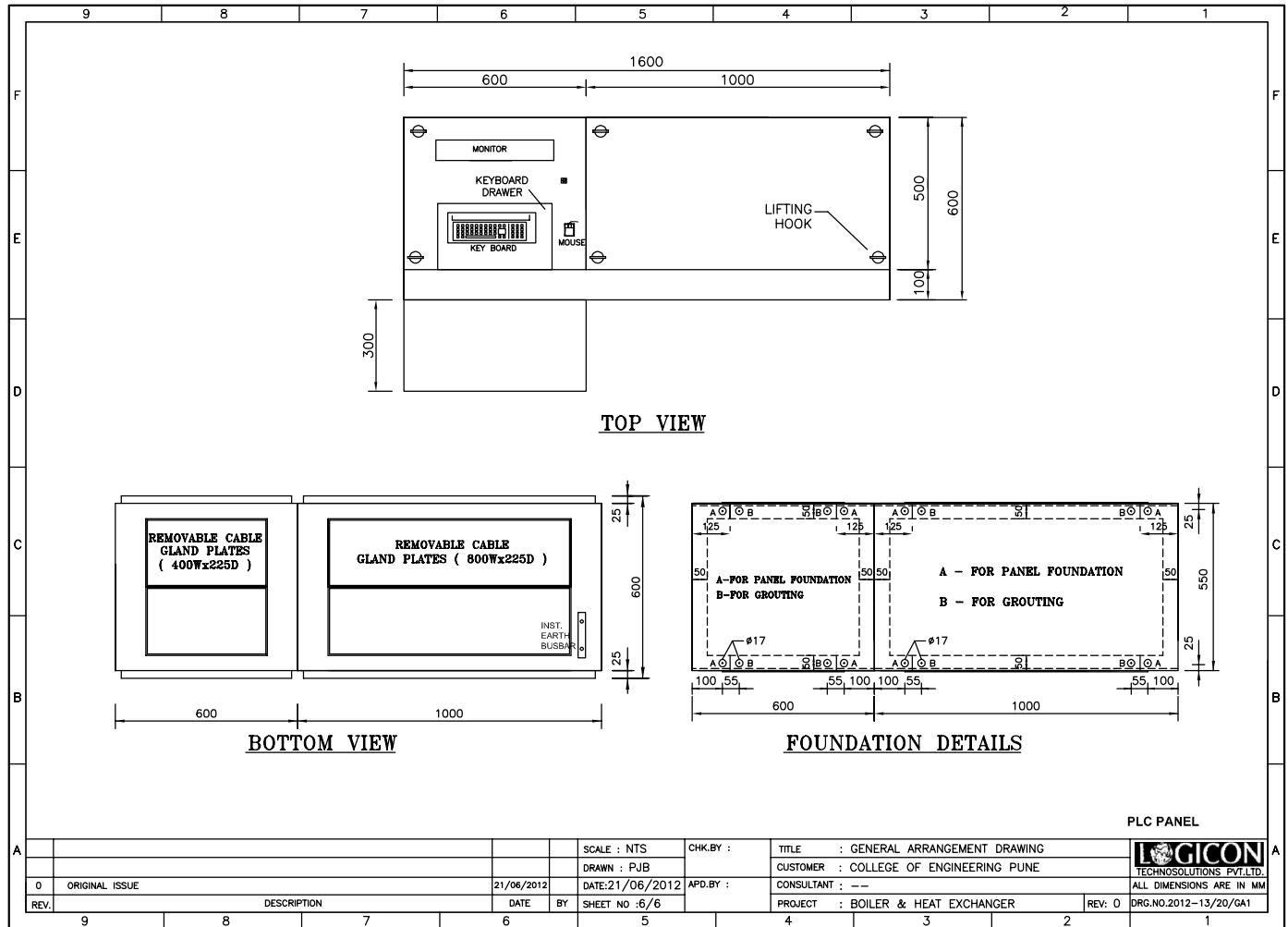




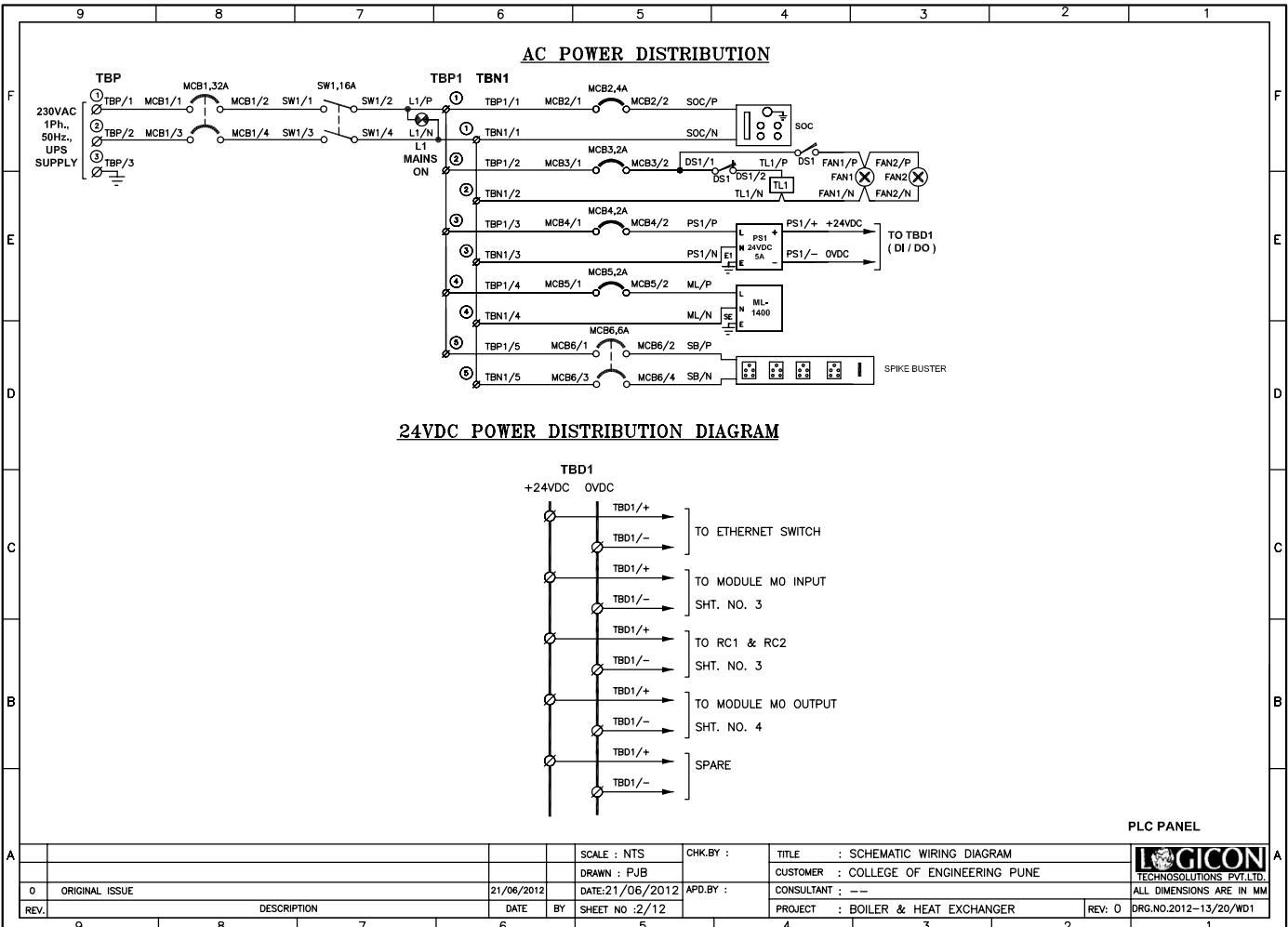


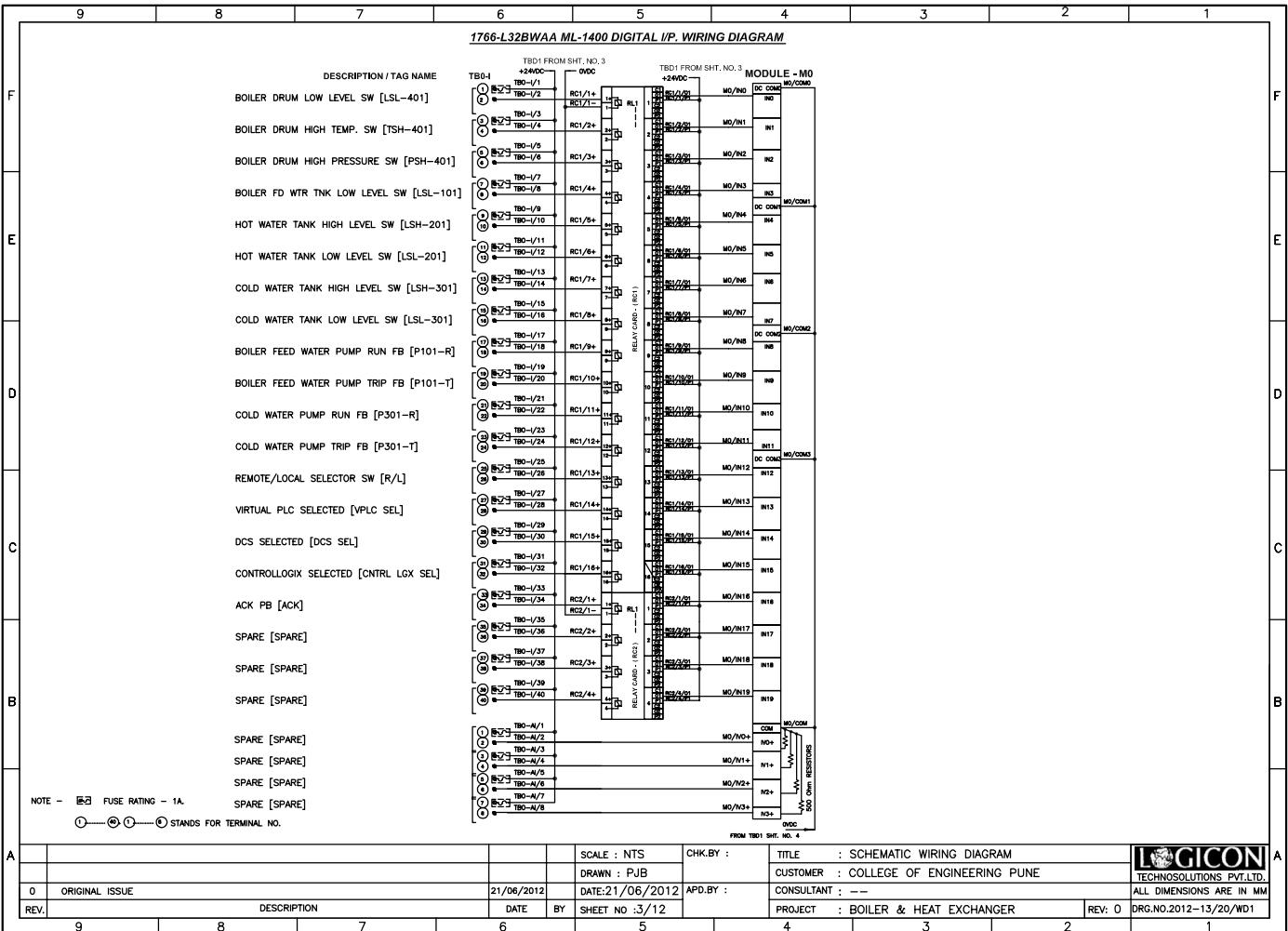
PLC PANEL									
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REV.	DESCRIPTION	DATE	BY	SHEET NO : 4 / 6	APD.BY	CONSULTANT : --	PROJECT : BOILER & HEAT EXCHANGER	REV. O	DRG.NO.2012-13/20/GA1
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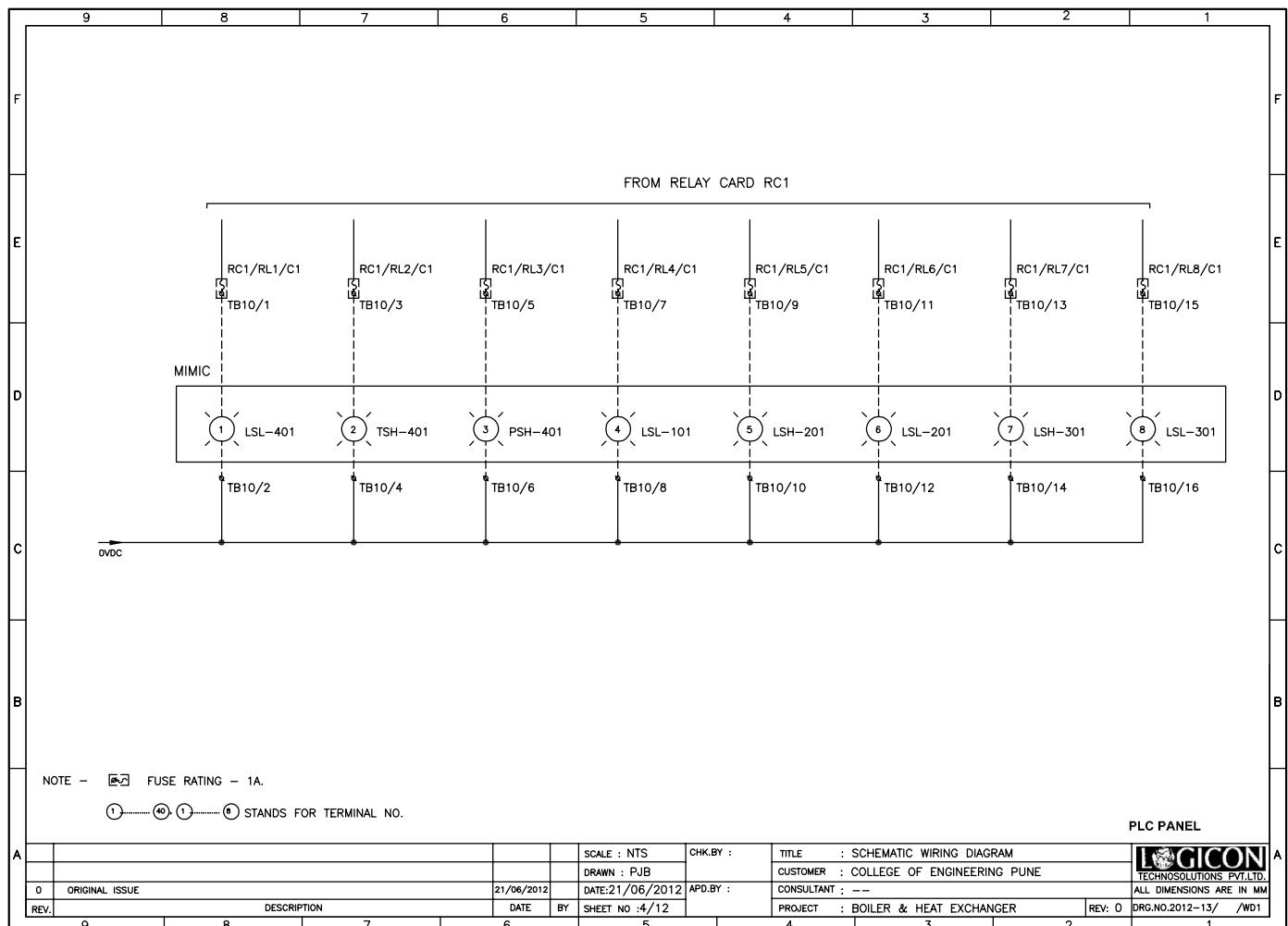


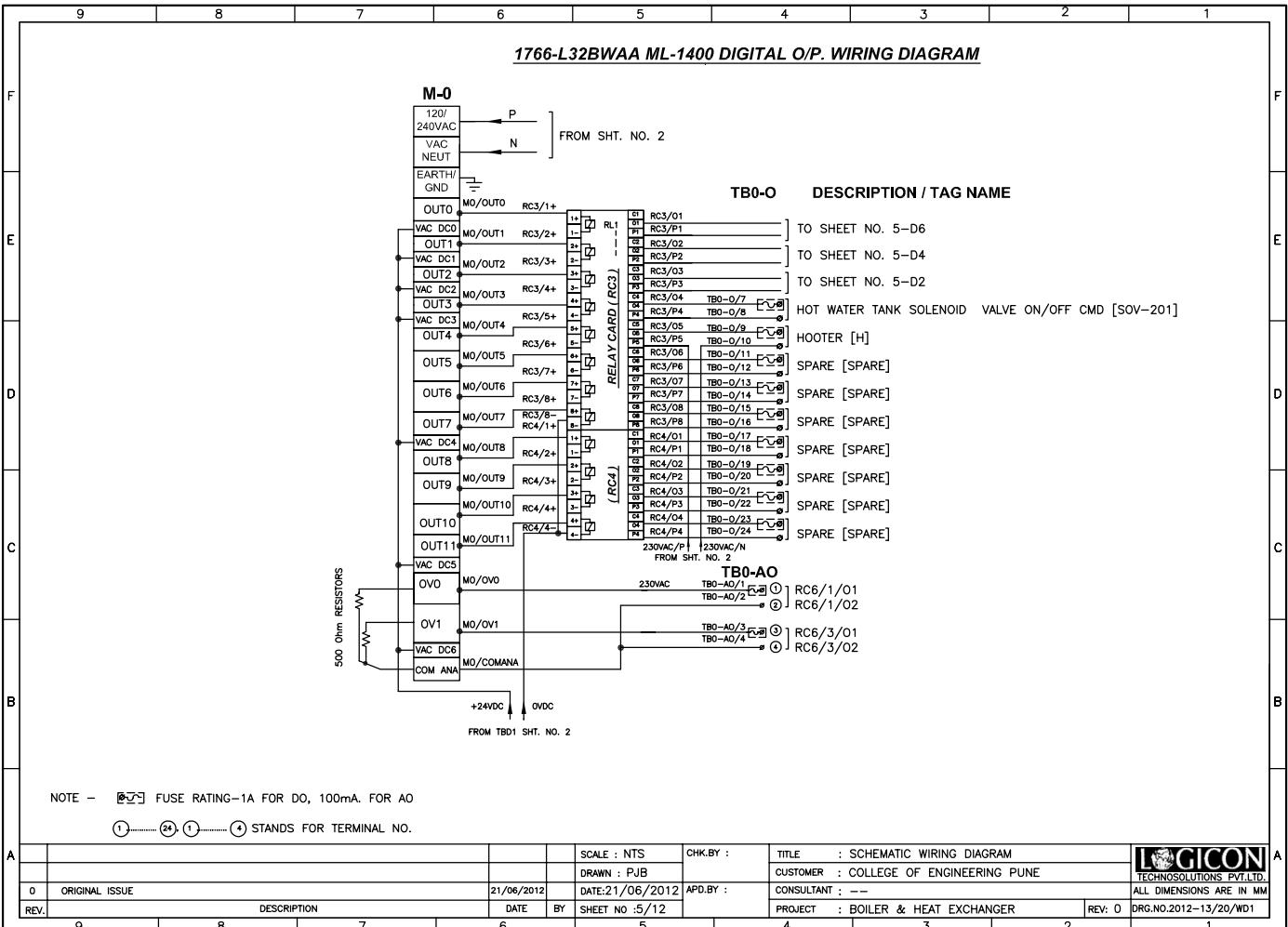


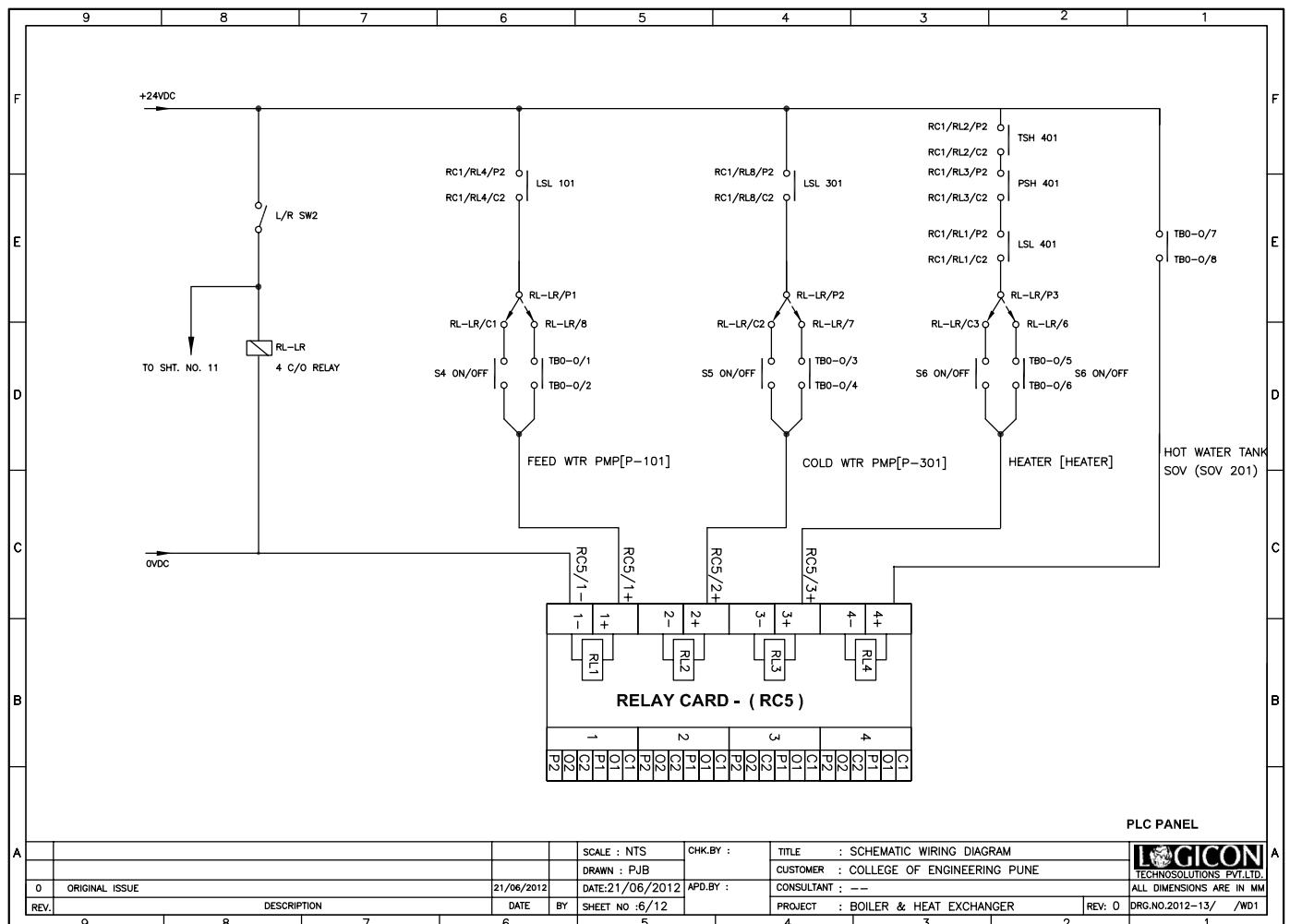
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E	<b>CUSTOMER</b> - <i>COLLEGE OF ENGINEERING PUNE</i>								E																																																
D	<b>PROJECT</b> - <i>BOILER &amp; HEAT EXCHANGER</i>								D																																																
C	<b>PROJ. NO.</b> - <i>LTPL/2012-13/20</i>								C																																																
B	<b>CONSULTANT</b> - --								B																																																
A	<b>NOTES</b>								A																																																
1  THIS SYMBOL REPRESENTS ELECTRICAL EARTH.																																																									
2  THIS SYMBOL REPRESENTS SCREEN / INSTRUMENTS EARTH.																																																									
PLC PANEL																																																									
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			SCALE : NTS	CHK.BY :	TITLE : SCHEMATIC WIRING DIAGRAM																																																				
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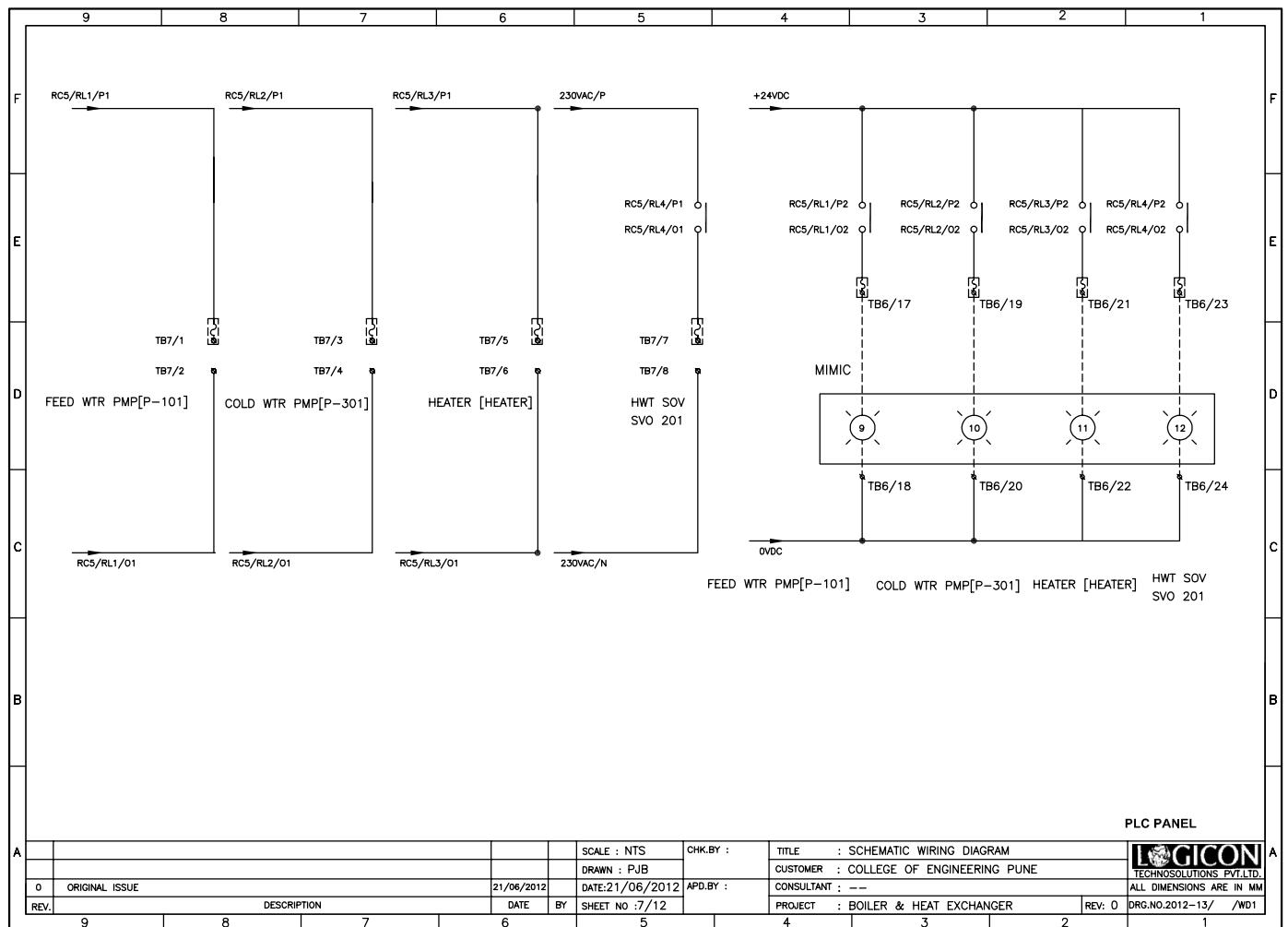


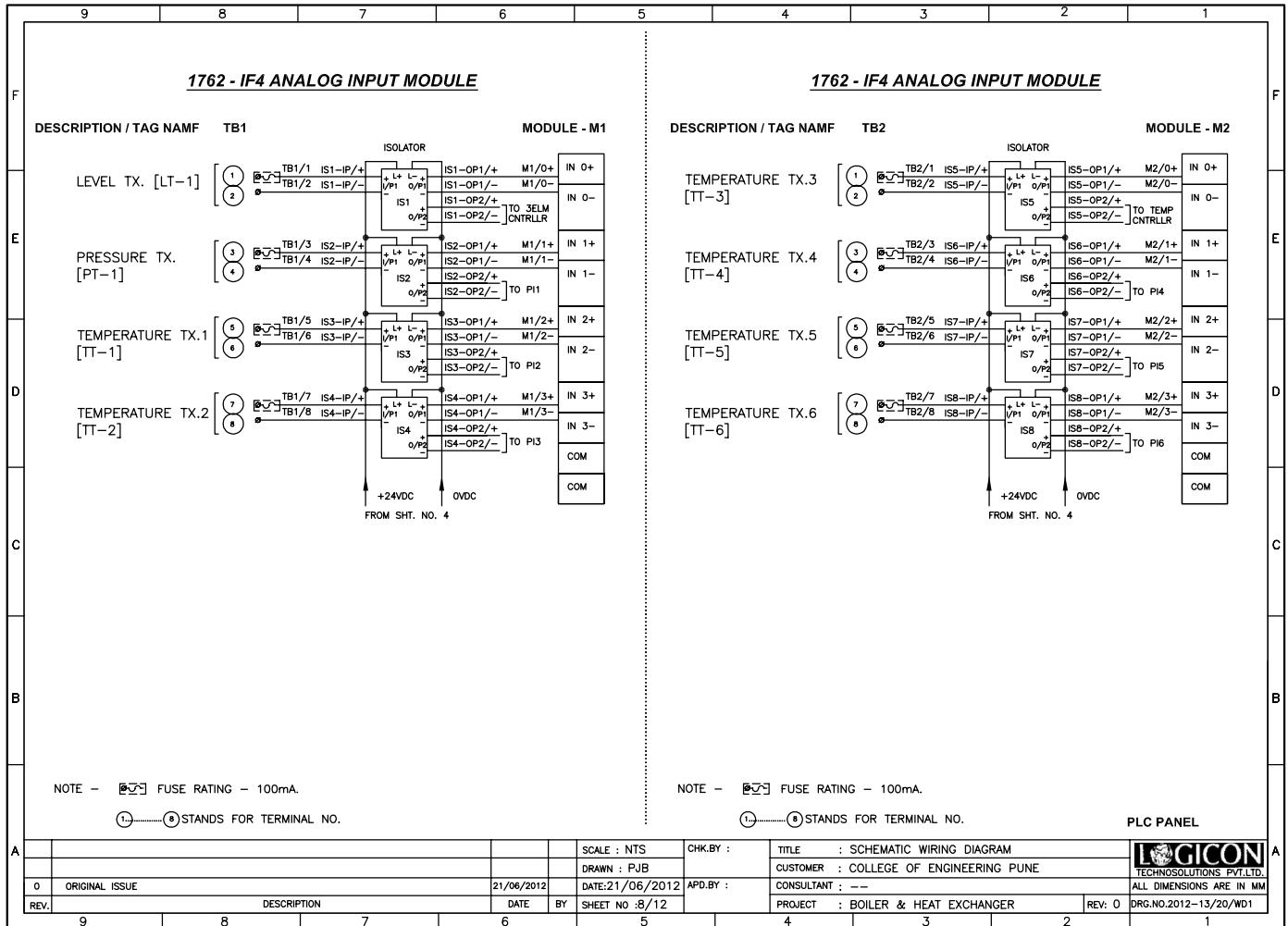


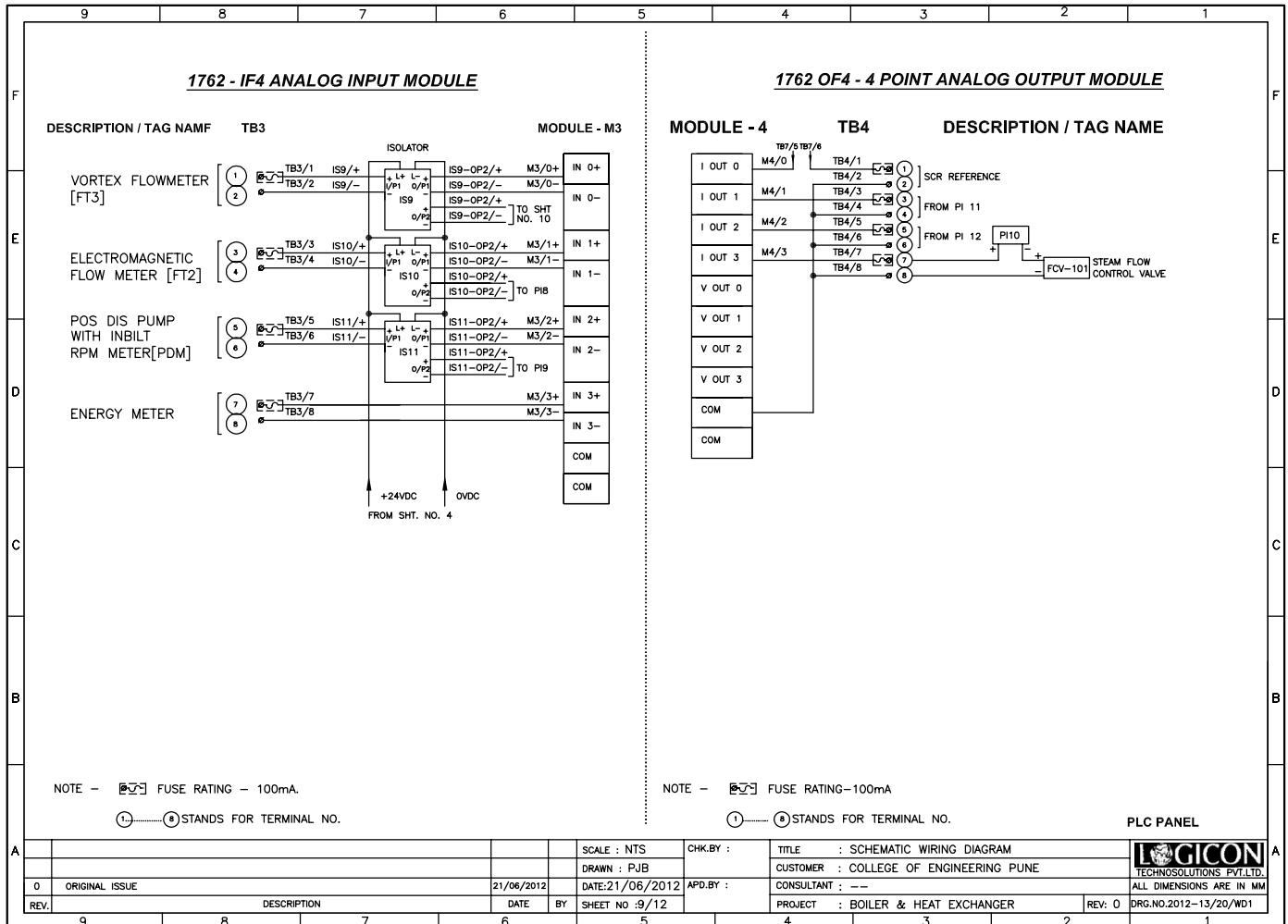


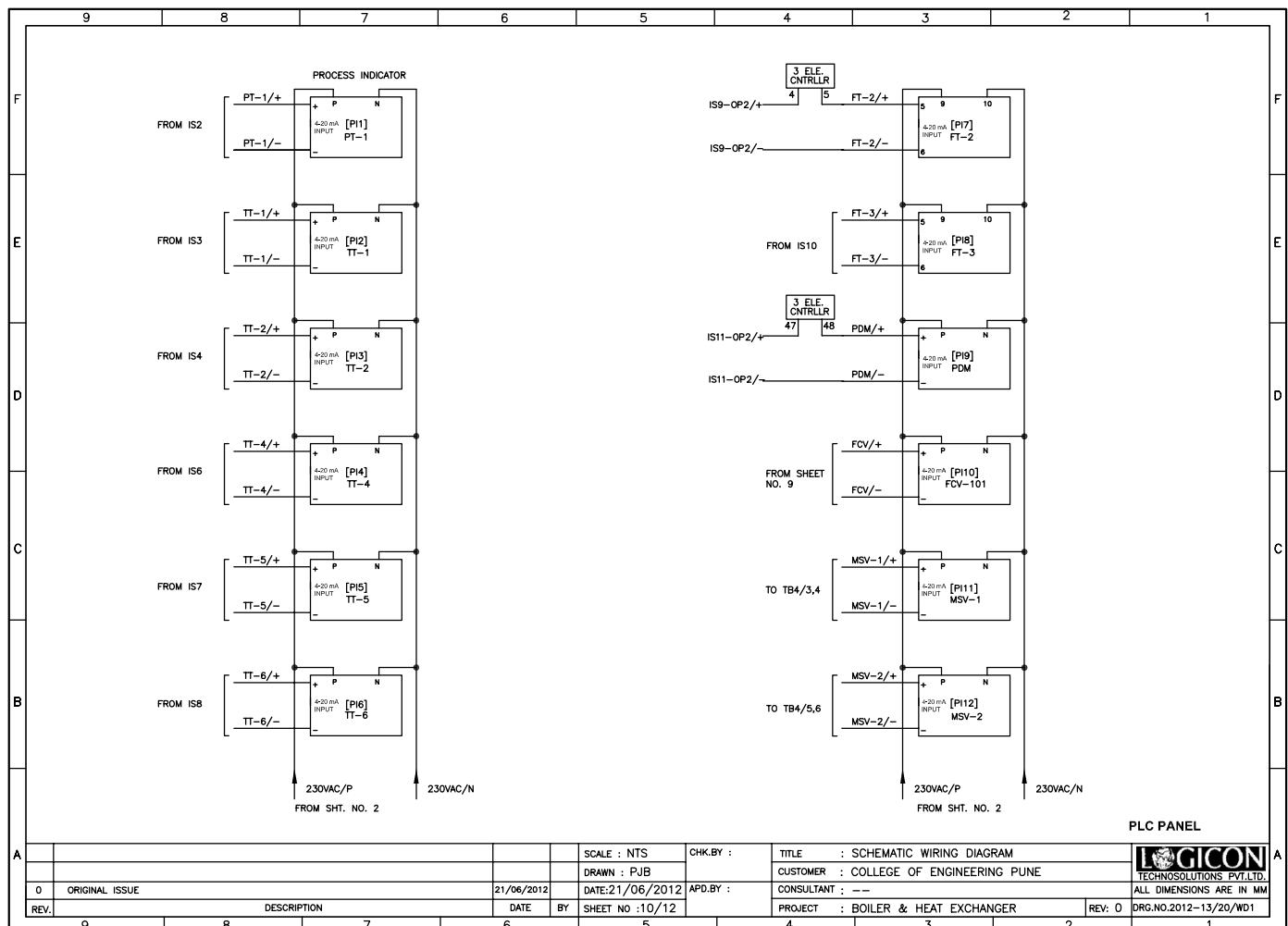


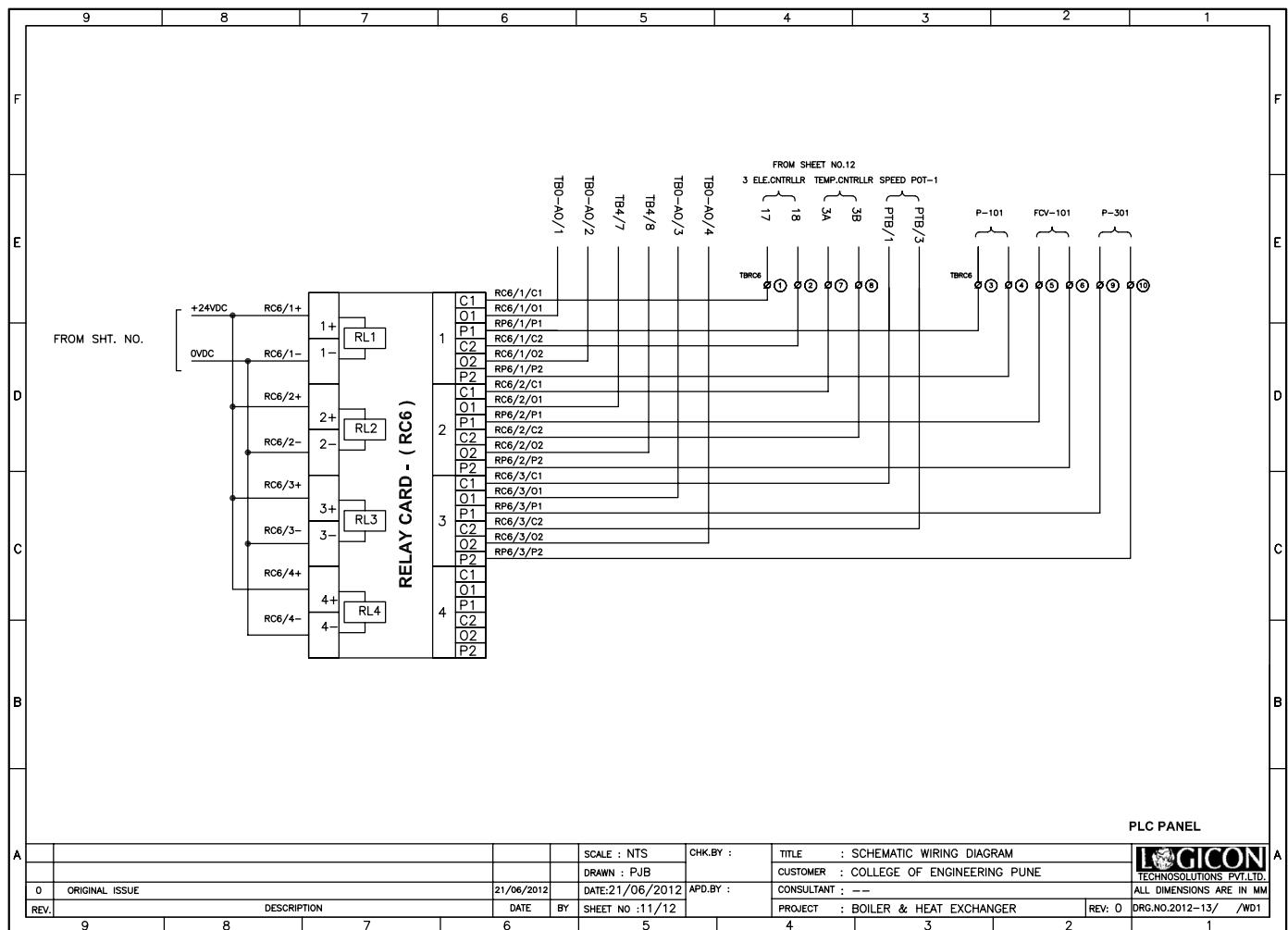


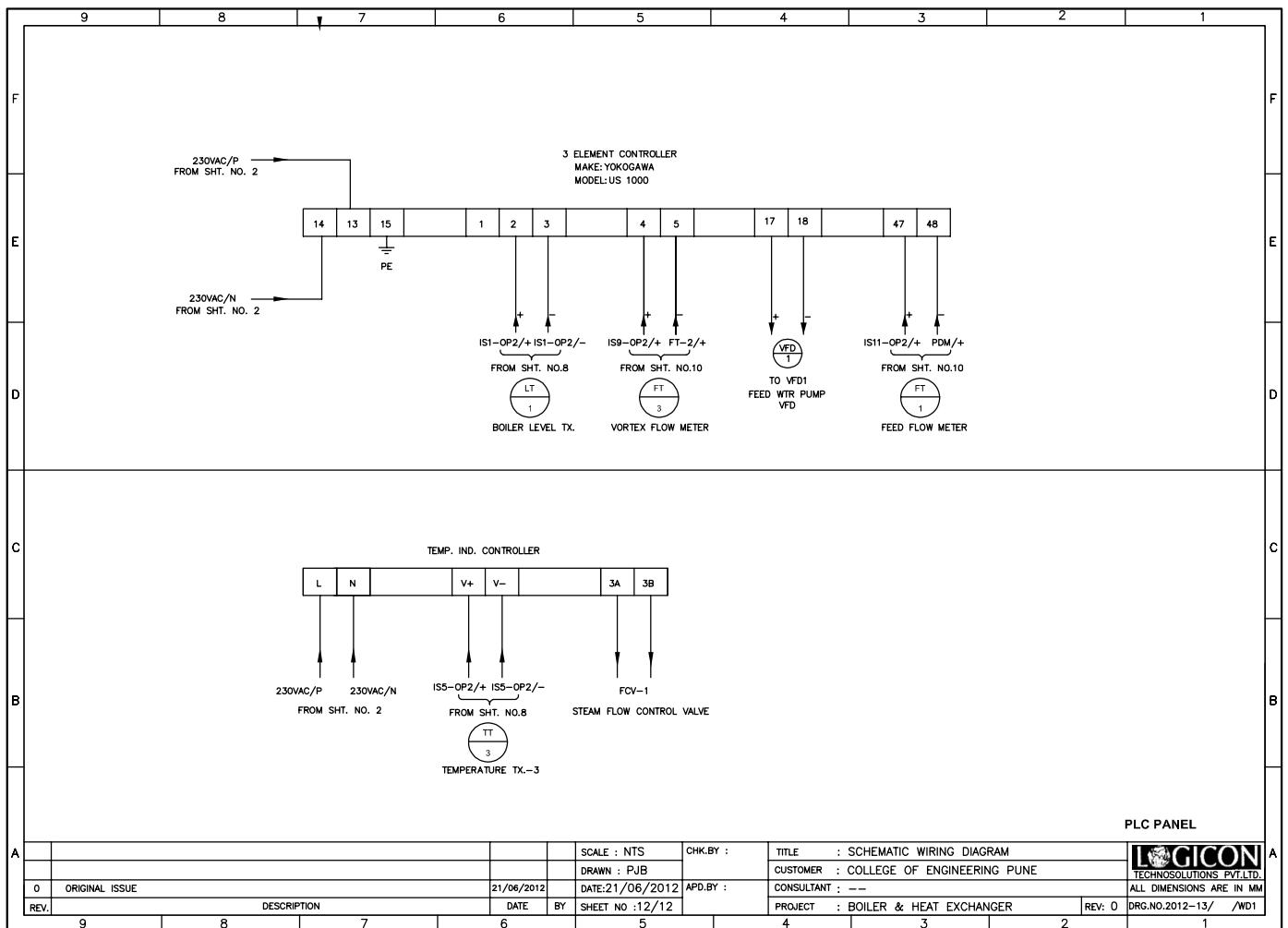












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F	TITLE	<b>- WIRING SPECIFICATION FOR PLC PANEL</b>									F
E	CUSTOMER	<b>- COLLEGE OF ENGINEERING PUNE</b>									E
D	PROJECT	<b>- BOILER &amp; HEAT EXCHANGER</b>									D
C	PROJ. NO.	<b>- LTPL/2012-13/20</b>									C
B	CONSULTANT	<b>- --</b>									B
A	PLC PANEL										
				SCALE : NTS	CHK.BY :	TITLE : WIRING SPECIFICATION					
				DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE					
O	ORIGINAL ISSUE		21/06/2012	DATE:21/06/2012	APD.BY :	CONSULTANT : --					
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F	9	8	7	6	5	4	3	2	1
E									
D									
C									
B									
A									
<b>WIRING SPECIFICATION</b>									
230V AC SUPPLY	PHASE	( UPTO DISTRIBUTION TB )	RED	4 mm <sup>2</sup>					
	NEUTRAL	( UPTO DISTRIBUTION TB )	BLACK	4 mm <sup>2</sup>					
	PHASE	( AFTER DISTRIBUTION TB )	RED	1.5 mm <sup>2</sup>					
	NEUTRAL	( AFTER DISTRIBUTION TB )	BLACK	1.5 mm <sup>2</sup>					
110V AC SUPPLY	PHASE	( UPTO DISTRIBUTION TB )	RED	4 mm <sup>2</sup>					
	NEUTRAL	( UPTO DISTRIBUTION TB )	BLACK	4 mm <sup>2</sup>					
	PHASE	( AFTER DISTRIBUTION TB )	RED	1.5 mm <sup>2</sup>					
	NEUTRAL	( AFTER DISTRIBUTION TB )	BLACK	1.5 mm <sup>2</sup>					
24V DC +VE	UPTO BUSBAR		BLUE	1.5 mm <sup>2</sup>					
	AFTER BUSBAR		BLUE	1.0 mm <sup>2</sup>					
24V DC -VE	UPTO BUSBAR		WHITE	1.5 mm <sup>2</sup>					
	AFTER BUSBAR		WHITE	1.0 mm <sup>2</sup>					
D/I WIRING			GREY	0.5 mm <sup>2</sup>					
D/O WIRING	MODULE TO RELAY COIL		GREY	0.5 mm <sup>2</sup>					
	RELAY CONTACT TO TERMINALS ( PF )		BROWN	1.0 mm <sup>2</sup>					
	RELAY CONTACT TO TERMINALS ( 24VDC )		BLUE (+), WHITE (-)	1.0 mm <sup>2</sup>					
	RELAY CONTACT TO TERMINALS ( 230/110V AC )		RED (P), BLACK (N)	1.0 mm <sup>2</sup>					
A/I WIRING			ORANGE (+), WHITE (-)	0.5 mm <sup>2</sup>					
A/O WIRING			YELLOW (+), WHITE (-)	0.5 mm <sup>2</sup>					
EARTH	POWER		GREEN/YELLOW	2.5 mm <sup>2</sup>					
	INSTRUMENT		GREEN	1.5 mm <sup>2</sup>					
PLC PANEL									
A			SCALE : NTS	CHK.BY :	TITLE : WIRING SPECIFICATION				
			DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE				
	0 ORIGINAL ISSUE	21/06/2012	DATE: 21/06/2012	APD.BY :	CONSULTANT : --				
	REV.	DESCRIPTION	DATE	BY	SHEET NO : 2/2	PROJECT : BOILER & HEAT EXCHANGER	REV: 0	ORG.NO:2012-13/20/WS1	
	9	8	7	6	5	4	3	2	1

**LOGICON**  
TECHNOSOLUTIONS PVT.LTD.

ALL DIMENSIONS ARE IN MM

## D.2 Evaporator Panel Drawing

**TITLE** - **SYSTEM ARCHITECTURE FOR PLC PANEL**

**CUSTOMER** - **COLLEGE OF ENGINEERING PUNE**

**PROJECT** - **EVAPORATOR PROJECT**

**PROJ. NO.** - **L TPL/2012-13/037**

**CONSULTANT** - **--**

**PLC PANEL**



TECHNOSOLUTIONS PVT LTD

ALL DIMENSIONS ARE IN MM

DRG.NO.2012-13/037/S1

1

**A**

**LOGICON**

TECHNOSOLUTIONS PVT LTD

ALL DIMENSIONS ARE IN MM

DRG.NO.2012-13/037/S1

1

**B**

**C**

**D**

**E**

**F**

1

2

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4

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8

9

9      8      7      6      5      4      3      2      1

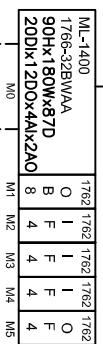
## SYSTEM ARCHITECTURE

5 PORT ETHERNET  
SWITCH ( ETH )



ETHERNET COMMUNICATION  
TO CONTROL LOGIX PLC

ETHERNET NETWORK



### DETAILS

- 1766-L32BWA – MICROLOGIX 1400 PROCESSOR
- 1762-OB8 – 8 CHANNEL DIGITAL INPUT MODULE
- 1762-IF4 – 4 CHANNEL ANALOG INPUT MODULE
- 1762-OF4 – 4 CHANNEL ANALOG OUTPUT MODULE
- – MODBUS NETWORK
- – ETHERNET NETWORK

PLC PANEL	
A	SCALE : NTS
DRAWN : PJB	CHK-BY : KKZ
0	TITLE : SYSTEM ARCHITECTURE
ORIGINAL ISSUE	CUSTOMER : COLLEGE OF ENGINEERING PUNE
01/10/2012	DATE:01/10/2012
REV.	APD-BY : SBA
9	CONSULTANT : --
8	PROJECT : EVAPORATOR PROJECT
7	REV. 0
6	DATE SHEET NO : 2/2
5	ALL DIMENSIONS ARE IN MM
4	DESIGN NO:2012-13/037/SAC
3	TECHNOSOLUTIONS PVT LTD.
2	LOGICON
1	PLC PANEL

							9	8	7	6	5	4	3	2	1
F															F
TITLE	- BILL OF MATERIAL FOR PLC PANEL														
CUSTOMER	- COLLEGE OF ENGINEERING PUNE														
PROJECT	- EVAPORATOR PROJECT														
PROJ. NO.	- LTPL/2012-13/037														
CONSULTANT	--														
D															D
C															C
B															B
A															A
							SCALE : NTS	CHK-BY : KKZ	TITLE : BILL OF MATERIAL						
							DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE						
O	ORIGINAL ISSUE						01/10/2012	DATE:01/10/2012	REQD-BY : SBA	CONSULTANT : --					
REV.		DESCRIPTION					DATE	BY	SHEET NO : 1/3	PROJECT : EVAPORATOR PROJECT	REV. 0	DGS NO:2012-13/037/BOM1			
	9	8	7	6	5	4	3	2	1						

PLC PANEL

LOGICON	TECHNO SOLUTIONS PVT LTD.	ALL DIMENSIONS ARE IN MM

9      8      7      6      5      4      3      2      1

### **BILL OF MATERIAL ( ROCKWELL AUTOMATION )**

F	F
1	1766-L32BWA
2	1762-OB8
3	1762-IF4
4	1762-OF4

A	B	C	D	E	F
<p style="text-align: center;"><b>PLC PANEL</b></p>					
<p>SCALE : NTS      CHK-BY : KZ      TITLE : BILL OF MATERIAL DRAWN : PJB      CUSTOMER : COLLEGE OF ENGINEERING PUNE</p>					
<p>0      ORIGINAL ISSUE      DATE:01/10/2012      APD BY : SBA REV:      DESCRIPTION      DATE      BY      SHEET NO : 2/3      PROJECT : EVAPORATOR PROJECT</p>					
<p>9      8      7      6      5      4      3      2      1</p>					
<p><b>L</b> <b>GICON</b> TECHNOSOLUTIONS PVT.LTD. ALL DIMENSIONS ARE IN MM ORG.NO:2012-13/037/BOM1</p>					

9	8	7	6	5	4	3	2	1
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## BILL OF MATERIAL ( BOUGHT - OUTS )

Sr.No.	Description	Tag No	Catalog No.	Make	Qty
1	PANEL ENCLOSURE SIZE : 1475+100(H) X 1900(W) X 600(D)	-	-	LOGICON	1
2	COOLING FAN 4", 230VAC	FAN1.2.3	-	REXNORD	3
3	LOUVER WITH FILTER, 4"	-	-	REPUTED	6
4	CFL LAMP WITH ITS ACCESSORIES 230VAC SUPPLY	TL1, TL2	-	PHILIPS	2
5	DOOR INTERLOCK SWITCH ASSEMBLY WITH 1NO + 1NC CONTACT 230VAC	DS1, DS2	-	SIEMENS	2
6	UTILITY SOCKET, 230V/AC,5A	SOC	-	ANCHOR	1
7	POWER SUPPLY,IP 230V/AC,OP 24VDC,5A	PS	-	NHP	1
8	16 CHANNEL, 24VDC RELAY CARD WITH 2CIO OMRON RELAY	RC1	UL-24-DI6-2C0B	UL	1
9	8 CHANNEL, 24VDC RELAY CARD WITH 2CIO OMRON RELAY	RC3.4	UL-24-D08-2C0B	UL	2
10	4 CHANNEL, 24VDC RELAY CARD WITH 2CIO OMRON RELAY	RC2.5	UL-24-D04-2C0B	UL	2
11	MINIATURE CIRCUIT BREAKER, 2P/32A,10KA	MCB1	5SX4232TRC	SIEMENS	1
12	MINIATURE CIRCUIT BREAKER, 1P/2A,10KA	MCB3.4.6	5SX4102TRC	SIEMENS	3
13	MINIATURE CIRCUIT BREAKER, 2P/4A,10KA	MCB5	5SX4204TRC	SIEMENS	1
14	MINIATURE CIRCUIT BREAKER, 2P/6A,10KA	MCB7	5SX4206TRC	SIEMENS	1
15	MINIATURE CIRCUIT BREAKER, 1P/4A,10KA	MCB2	5SX4104TRC	SIEMENS	1
16	LED TYPE INDICATION LAMP, CLEAR COLOUR, CONTROL SUPPLY ON 230VAC	L1	-	SIEMENS / TEKNIC	1
17	1 POLE 2 WAY ON/OFF SWITCH,16A	S1	-	SALZER	1
18	1 POLE 2 WAY ON/OFF SWITCH	S2.4.5.6	-	SALZER	4
19	1 POLE 3 WAY ROTARY SWITCH, 10A	S3	6049	SALZER	1
20	PUSH BUTTON FOR RACK (BLACK)	ACK	24F	TEKNIC	1
21	5 PORT ETHERNET SWITCH,24VDC SUPPLY	ETH.SW.	SNB5TX	PHOENIX	1
22	FUSE TERMINALS,4 SQMM	-	-	ELMEX	AS REQD
23	NON FUSE TERMINALS,2.5 SQMM	-	-	ELMEX	AS REQD
24	HOOTER,230V/AC SUPPLY	H	-	CAPTAIN CANDS	1
25	EARTHENING BUSBAR 25 X 3 MM THROUGHOUT PANEL WITH M12 BOLTS	-	-	STD	1
26	INSTRUMENT EARTH BUSBAR 25 X 3 MM	-	-	STD	AS REQD
27	1:2 ISOLATOR FOR ANALOG INPUT & OUTPUT	IS1.2....20	-	SAPRE	20
28	INDICATORS FOR ANALOG IP & OP	PI1.2....20	-	NISHKO	20
29	1 Mtr ETHERNET CABLE	-	CAT5	DLINK	1
30	10 Mtr ETHERNET CABLE	-	CAT5	DLINK	1
31	MIMIC 600(H) x 600(W)	-	-	STANDARD	1
32	SPIKE GUARD	-	-	-	1
33	MUSHROOM TYPE EMERGENCY PUSH BUTTON	EM PB	-	-	1

PLC PANEL

A			SCALE : NTS	CHK BY : KKZ	ITLE : BILL OF MATERIAL	 <b>LOGICON</b> <small>TECHNOSOLUTIONS PVT LTD.</small> <small>ALL DIMENSIONS ARE IN MM</small> <small>DESIGN NO.2012-13/037/BOM1</small>
O	ORIGINAL ISSUE		DRAWN : PJB	CUSTOMER : COLLEGE OF ENGINEERING PUNE		
REV.	0	DATE:01/10/2012	APD BY : SBA	CONSULTANT : --		
		DATE : SHEET NO : 3/3	PROJECT : EVAPORATOR PROJECT	REV. 0		
A	9	8	7	6	5	4
B					3	2

9      8      7      6      5      4      3      2      1

**TITLE** - GENERAL ARRANGEMENT DRAWING FOR PLC PANEL

**CUSTOMER** - COLLEGE OF ENGINEERING PUNE

**PROJECT** - EVAPORATOR PROJECT

**PROJ. NO.** - LTPL/2012-13/037

**CONSULTANT** --

A	B	C	D	E	F
PLC PANEL					
9	8	7	6	5	4
0	ORIGINAL ISSUE	DESCRIPTION	DATE	BY	SHEET NO.:1/6
REV.					
1					
5	4	3	2	1	
6	5	4	3	2	1
7	6	5	4	3	2
8	7	6	5	4	3
9	8	7	6	5	4
A	B	C	D	E	F

SCALE : NTS      CHK-BY : KKZ      TITLE : GENERAL ARRANGEMENT DRAWING  
DRAWN : PJB      CUSTOMER : COLLEGE OF ENGINEERING PUNE  
01/10/2012      DATE:01/10/2012      APP-BY : SBA  
ORIGINAL ISSUE      CONSULTANT : --  
DESCRIPTION      DATE      BY      SHEET NO.:1/6  
REV. 0      PROJECT : EVAPORATOR PROJECT      REV. 0  
LOGICON TECHNO SOLUTIONS PVT LTD.  
ALL DIMENSIONS ARE IN MM  
Dwg. No. 2012-13/037/GA1

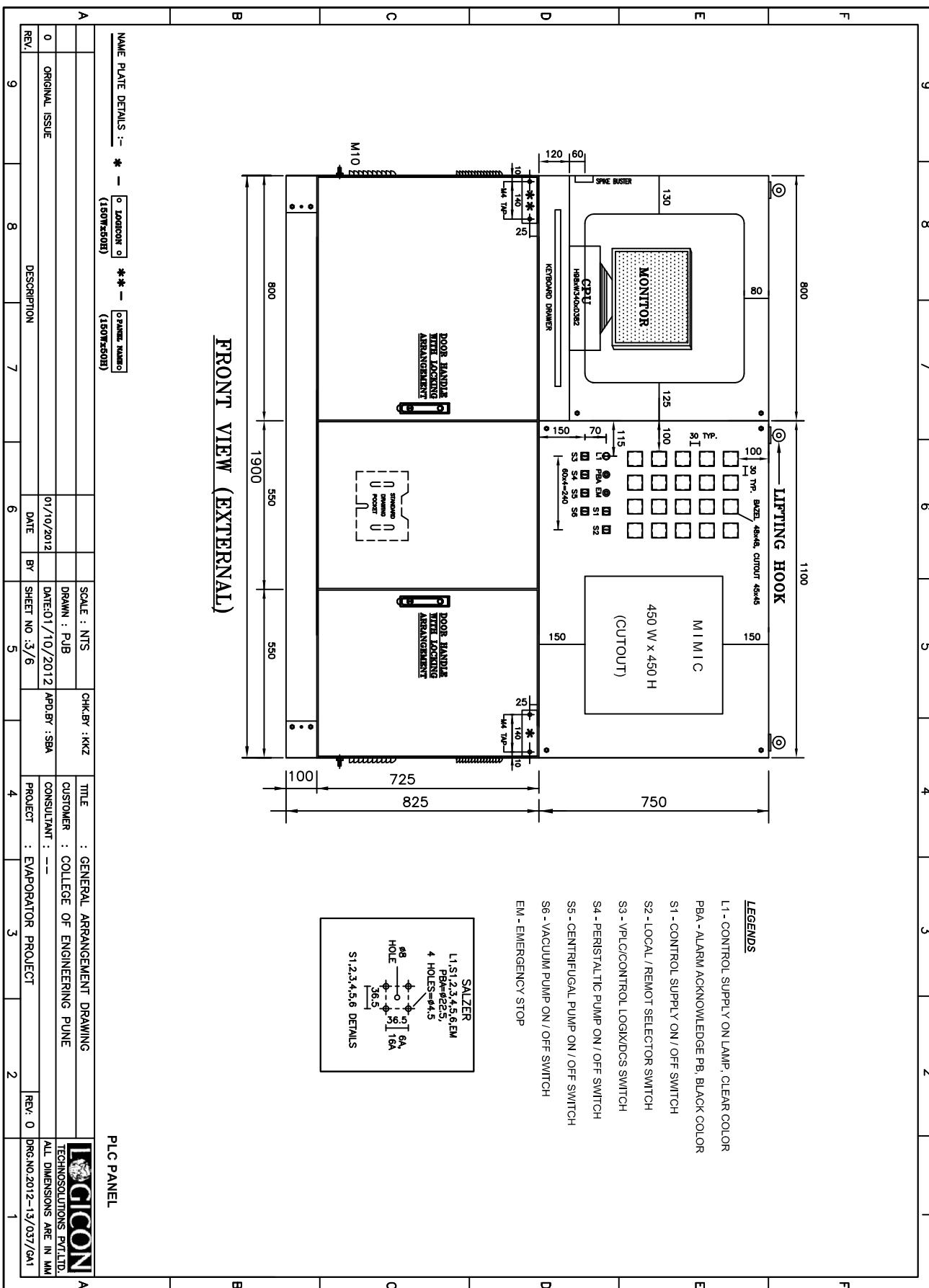
9	8	7	6	5	4	3	2	1
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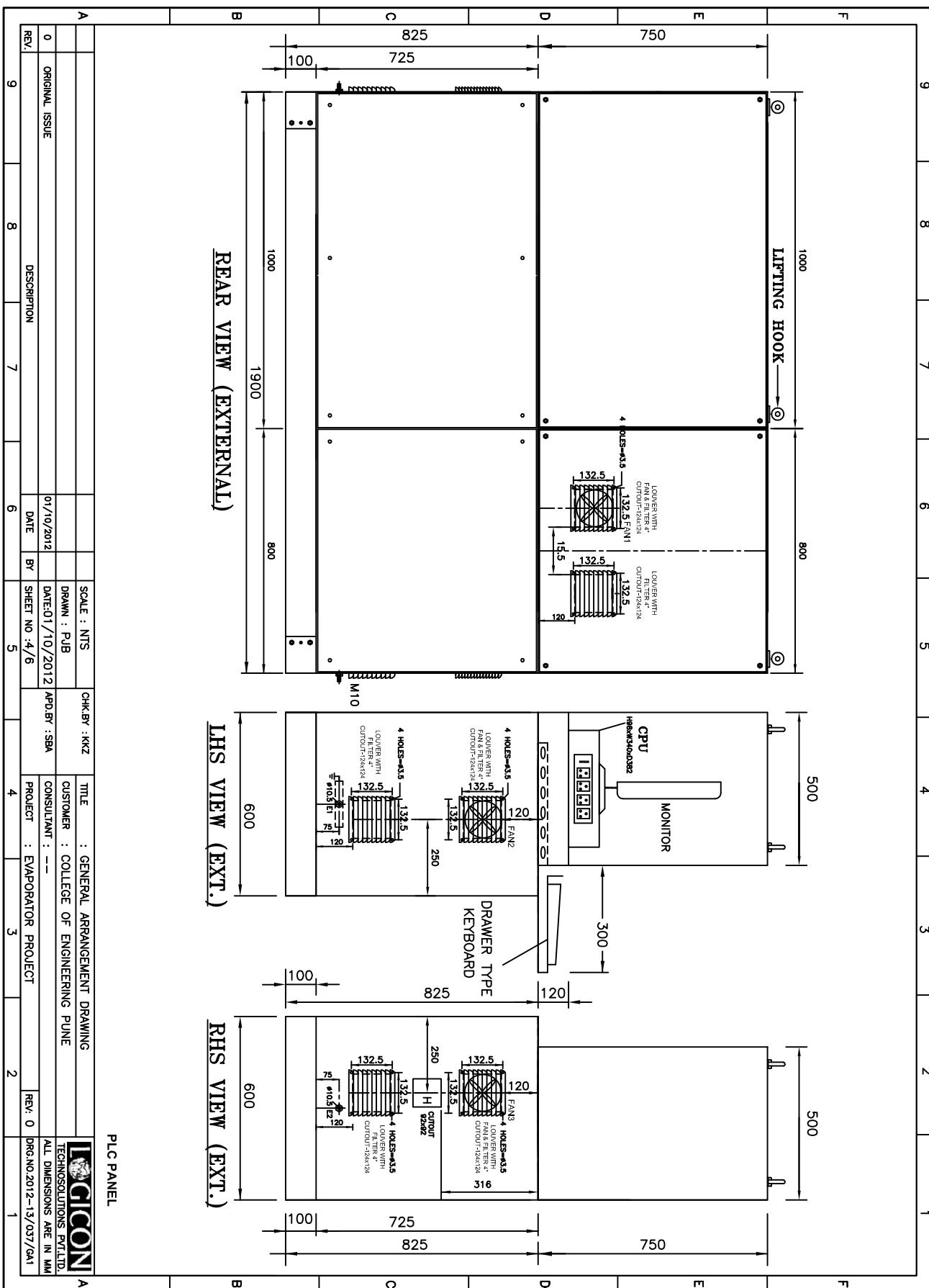
### GENERAL SPECIFICATIONS :-

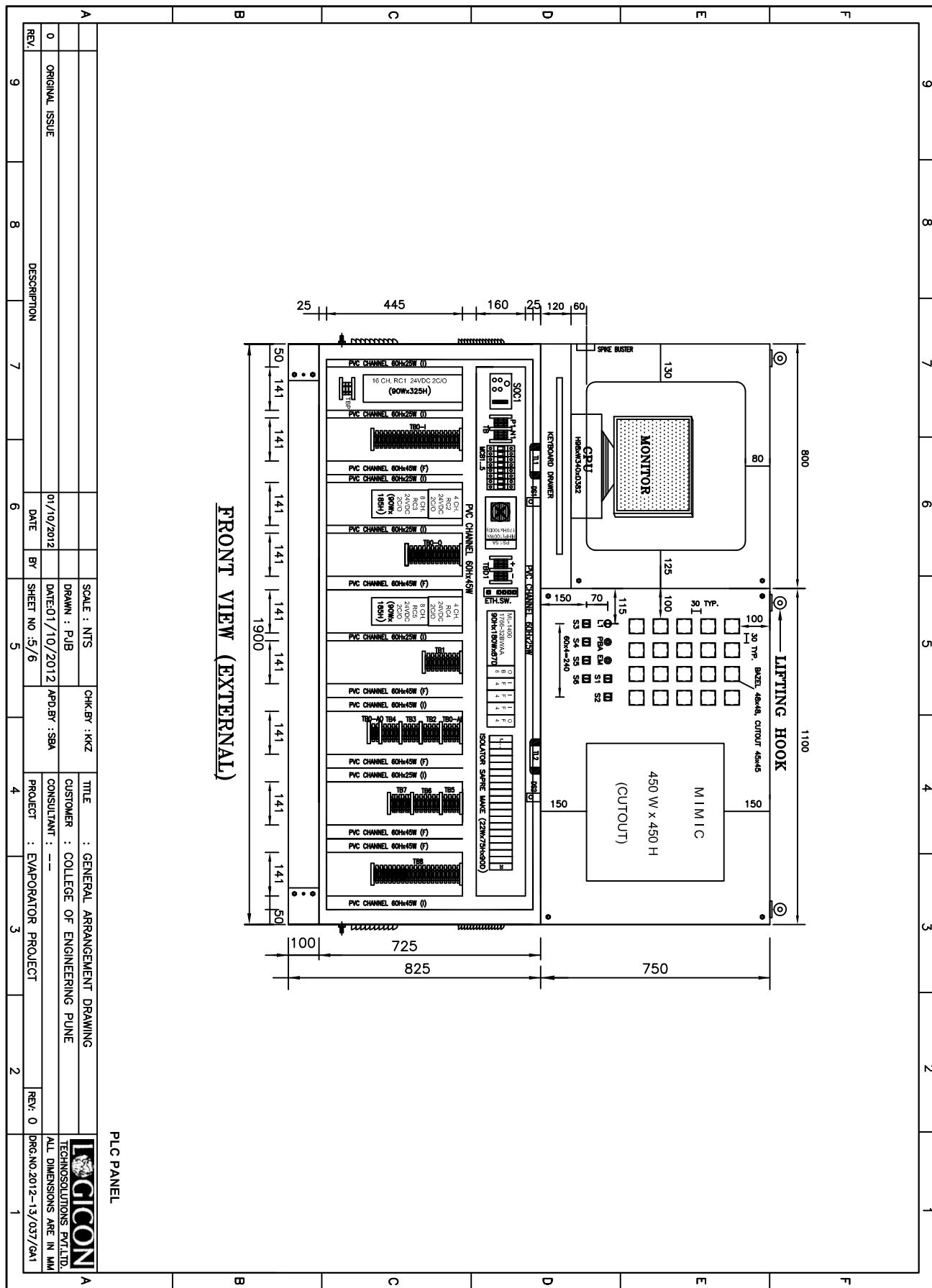
- F
  - PANEL FRONT DOOR SHALL BE 2mm. THICK CRCA SHEET STEEL.
  - PANEL FRAME TOP / REAR / SIDE COVER SHALL BE 1.6 mm. THICK CRCA SHEET STEEL.
  - BASE PLATE SHALL BE 2 mm. THICK CRCA SHEET STEEL.
  - PANEL SHADE INSIDE / OUTSIDE - SIEMENS GREY (RAL-7032), BASE PLATE - ORANGE. ( POWDER COATED )
  - DEGREE OF PROTECTION IP - 42
  - FRONT DOOR SHALL BE PROJECTED, REMOVABLE & LOCKABLE TYPE WITH KEY, PANEL IS FRONT ACCESIBLE ONLY
  - FRONT DOOR SWING SHALL BE 120 DEG.
  - CABLE ENTRY SHALL BE FROM BOTTOM.
  - PANEL SHALL HAVE 6 NOS. REMOVABLE LIFTING HOOKS AT TOP.
  - STANDARD DRAWING POCKET SHALL BE PROVIDED ON FRONT DOOR.
  - CABLE TERMINATION SHALL BE DONE WITH PIN TYPE LUGS & USING TUBE FERRULES.
  - PVC / RUBBER GASKETING WILL BE PROVIDED FOR DOORS.
  - 3 mm. THICK REMOVABLE, UNDRILLED GLAND PLATES SHALL BE PROVIDED.
  - PVC / RUBBER GASKETING WILL BE PROVIDED FOR DOORS.
  - 50x100x50x3 mm. THK. M.S. PLINTH SHALL BE USED & PAINTED BLACK. ( FRONT & BACK COVER OF PLINTH SHALL BE REMOVABLE TYPE )
  - EARTH BOLTS SHALL BE PROVIDED AT BOTH ENDS, WITH CU. BUSBAR OF 150x25x3 mm. SIZE FROM PANEL INSIDE FOR ELECTRICAL EARTHING.
  - INSTRUMENT EARTH BUSBAR OF SUITABLE SIZE OF 25x3 mm. PROVIDED.
  - TOLERANCE +/- 5 mm OF PANEL DIMENSIONS.
  - FOUNDATION DETAILS AS SHOWN IN DRAWING.
  - PANEL MAKE : LOGICON
  - EARTHING WIRE WILL BE PROVIDED BETWEEN PANEL DOOR & ELECTRICAL EARTH BUSBAR.

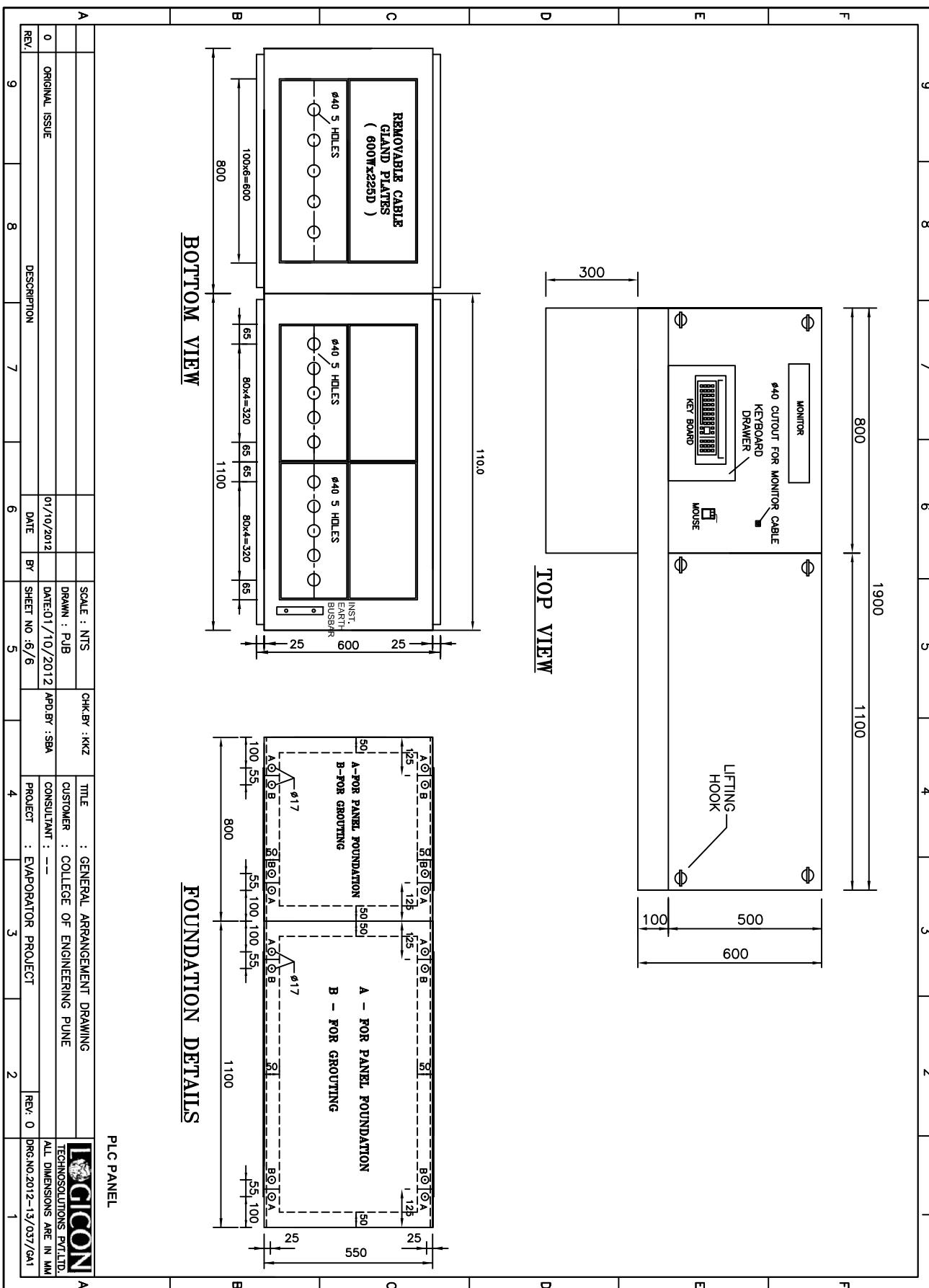
PLC PANEL

A			SCALE : N/T	CHK BY : KKZ	TITLE : GENERAL ARRANGEMENT DRAWING	 LOGICON TECHNOSOLUTIONS PVT LTD.
O	ORIGINAL ISSUE		DRAWN : PJB	CUSTOMER : COLLEGE OF ENGINEERING PUNE	CONSULTANT : --	ALL DIMENSIONS ARE IN MM
REV.		DESCRIPTION	DATE:01/10/2012	APD BY : SBA	PROJECT : EVAPORATOR PROJECT	REV. 0
9			DATE	BY	SHEET NO 2/6	DES. NO.2012-13/037/GA1









9      8      7      6      5      4      3      2      1

**TITLE** - SCHEMATIC WIRING DIAGRAM FOR PLC PANEL

**CUSTOMER** - COLLEGE OF ENGINEERING PUNE

**PROJECT** - EVAPORATOR PROJECT

**PROJ. NO.** - LTPL/2012-13/037

**CONSULTANT** --

D

C

B

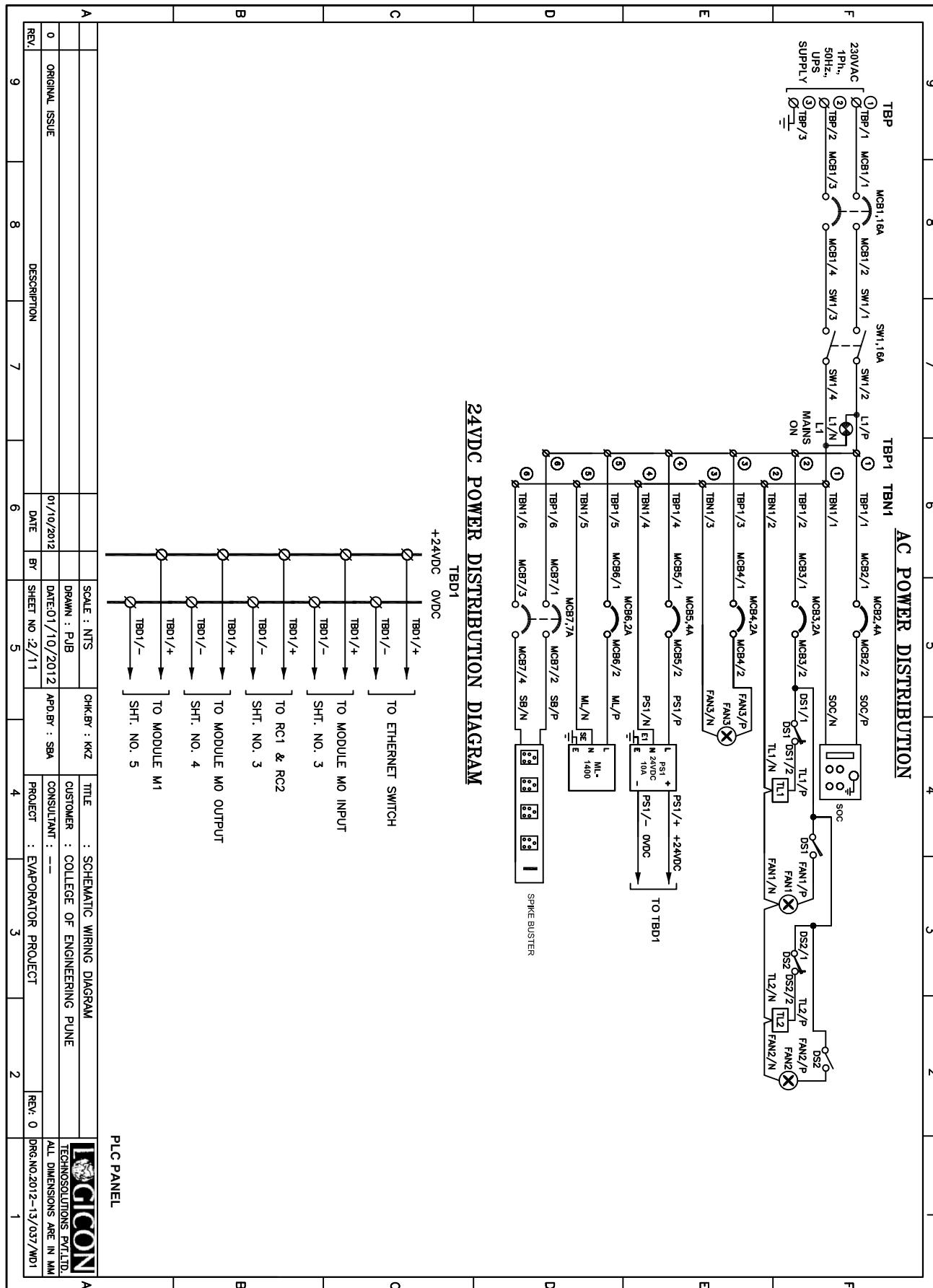
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NOTES

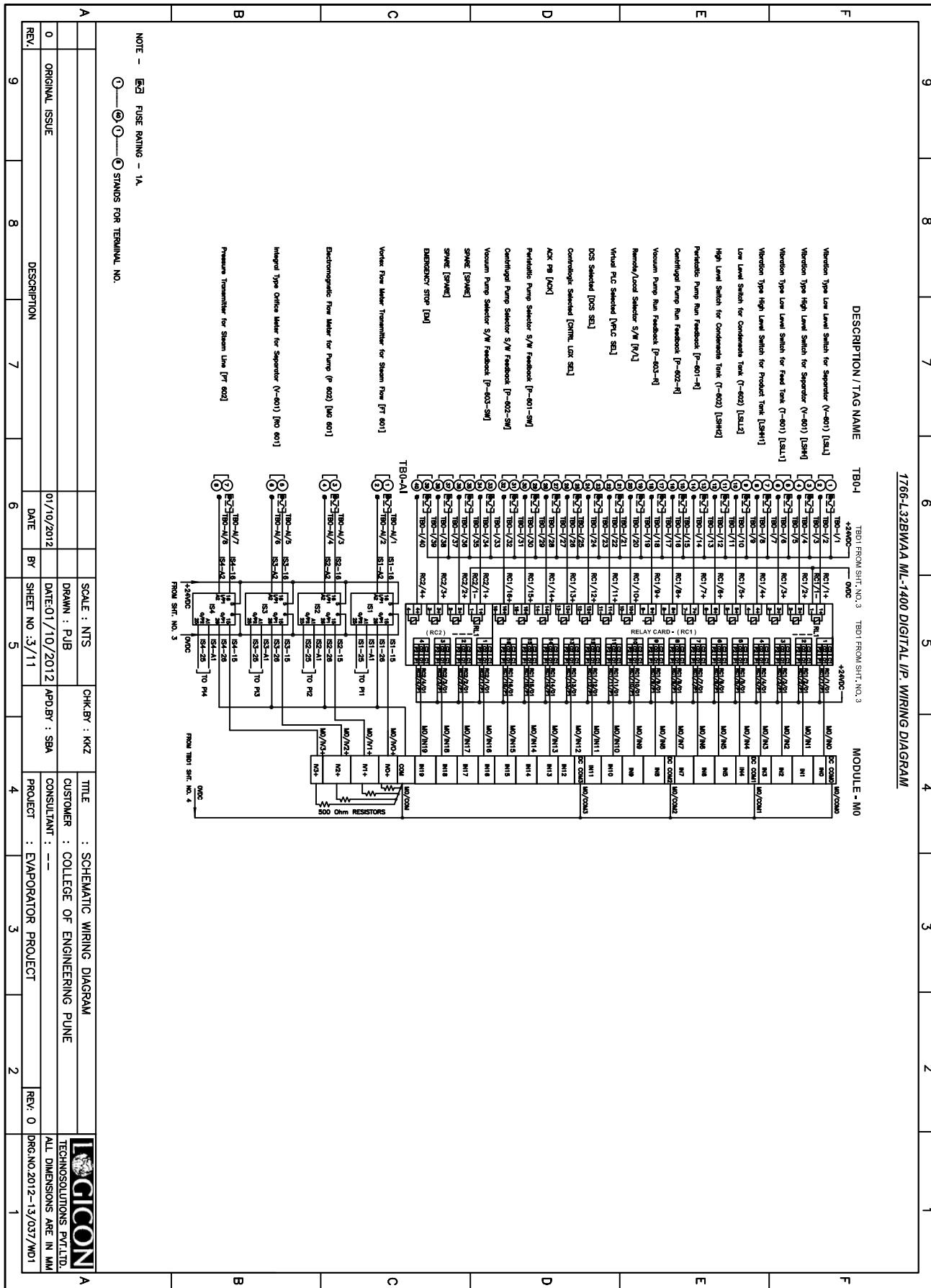
- 1  THIS SYMBOL REPRESENTS ELECTRICAL EARTH.
- 2  THIS SYMBOL REPRESENTS SCREEN / INSTRUMENTS EARTH.

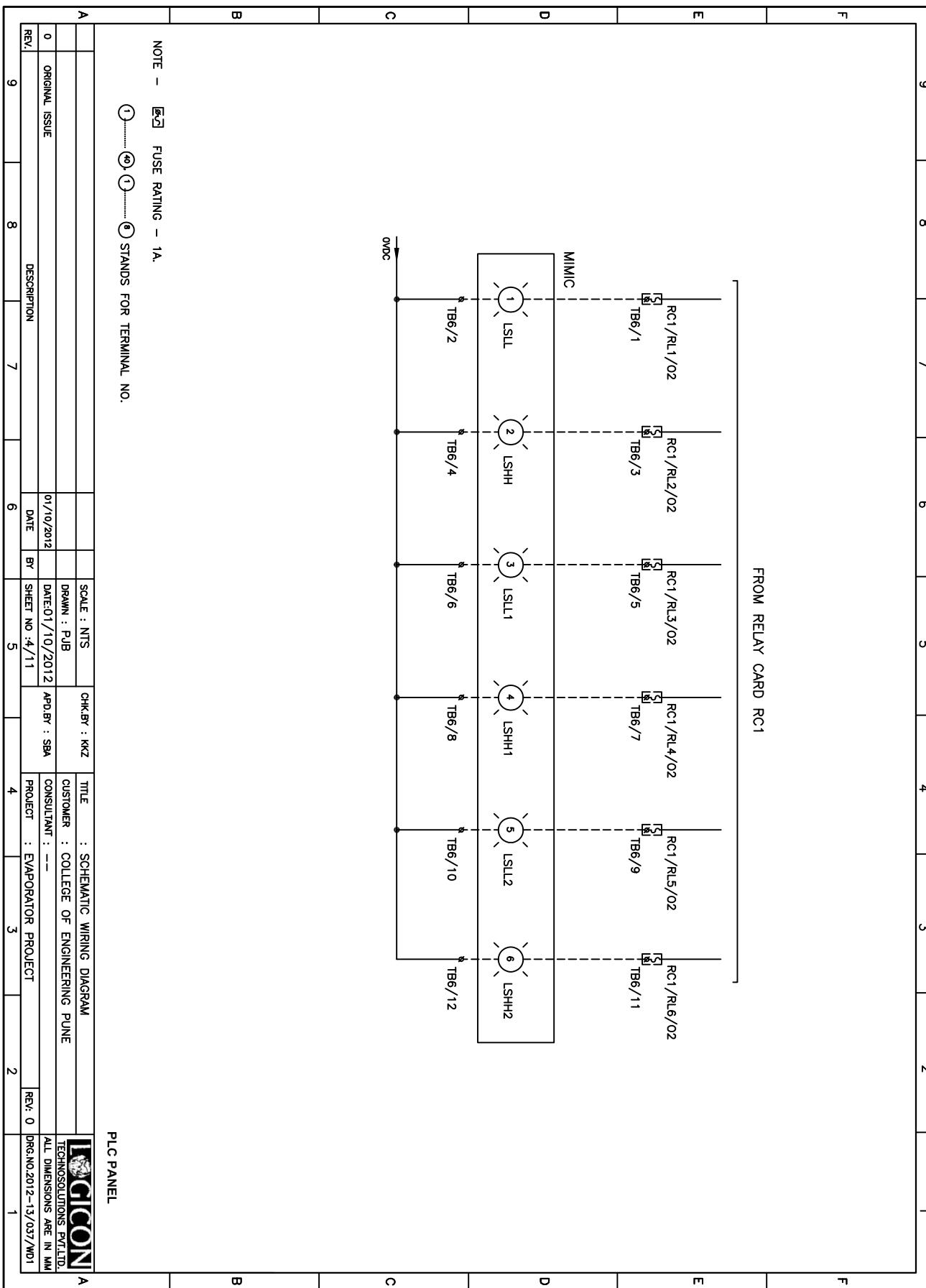
PLC PANEL

A			SCALE : NTS	CHK BY : KKZ	TITLE : SCHEMATIC WIRING DIAGRAM	 LOGICON TECHNOSOLUTIONS PVT LTD. ALL DIMENSIONS ARE IN MM Dwg No. 2012-13/037/WD1
O	ORIGINAL ISSUE		DRAWN : PJB		CUSTOMER : COLLEGE OF ENGINEERING PUNE	
REV.		01/10/2012	DATE:01/10/2012	APD BY : SBA	CONSULTANT : --	
9	DESCRIPTION		DATE	BY	PROJECT : EVAPORATOR PROJECT	
			SHEET NO : 1/11		REV. 0	
			5	4	3	
			6	7	8	
			1			



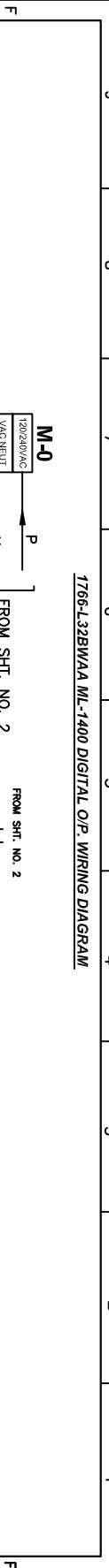
1766-L32BWAA ML-1400 DIGITAL I/P. WIRING DIAGRAM





**1766-L32BWAA ML-1400 DIGITAL O/P. WIRING DIAGRAM**

9      8      7      6      5      4      3      2      1



**M-0**

FROM SHT. NO. 2

DESCRIPTION / TAG NAME



VAC DCO

MO/OUT1

Pneumatic Pump on/off cmd [P=601]

VAC DC1

MO/OUT2

Cooling Pump on/off cmd [P=602]

VAC DC2

MO/OUT3

Vacuum Pump on/off cmd [P=603]

VAC DC3

MO/OUT4

SPNE [SPNE]

VAC DC4

MO/OUT5

SPNE [SPNE]

VAC DC5

MO/OUT6

SPNE [SPNE]

VAC DC6

MO/OUT7

SPNE [SPNE]

VAC DC7

MO/OUT8

SPNE [SPNE]

VAC DC8

MO/OUT9

SPNE [SPNE]

VAC DC9

MO/OUT10

SPNE [SPNE]

VAC DC10

MO/OUT11

SPNE [SPNE]

VAC DC11

MO/OUT12

SPNE [SPNE]

VAC DC12

MO/OUT13

SPNE [SPNE]

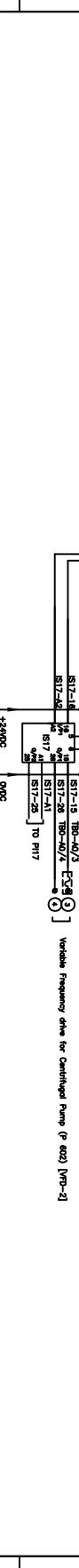
NOTE -

■ 25 FUSE RATING 1A FOR DO, 100mA FOR AO  
○—◎—◎ STANIS FOR TERMINAL NO.

A	SCALE : NTS	CHK-BY : KKRZ	TITLE : SCHEMATIC WIRING DIAGRAM
O	DRAWN : PJB	CUSTOMER : COLLEGE OF ENGINEERING PUNE	
ORIGINAL ISSUE	01/10/2012	CONSULTANT : --	
REV.	DATE BY SHEET NO 5/11	PROJECT : EVAPORATOR PROJECT	REV. 0 DRS NO.2012-13/037/WD1

9	8	7	6	5	4	3	2	1
FROM SHT. NO. 3								

B



C

FROM SHT. NO. 2

TBD-AO

0DC

+24VDC

FROM SHT. NO. 3

D

E

F

G

**LOGICON**  
TECHNOSOLUTIONS PVT LTD.  
ALL DIMENSIONS ARE IN MM

9      8      7      6      5      4      3      2      1

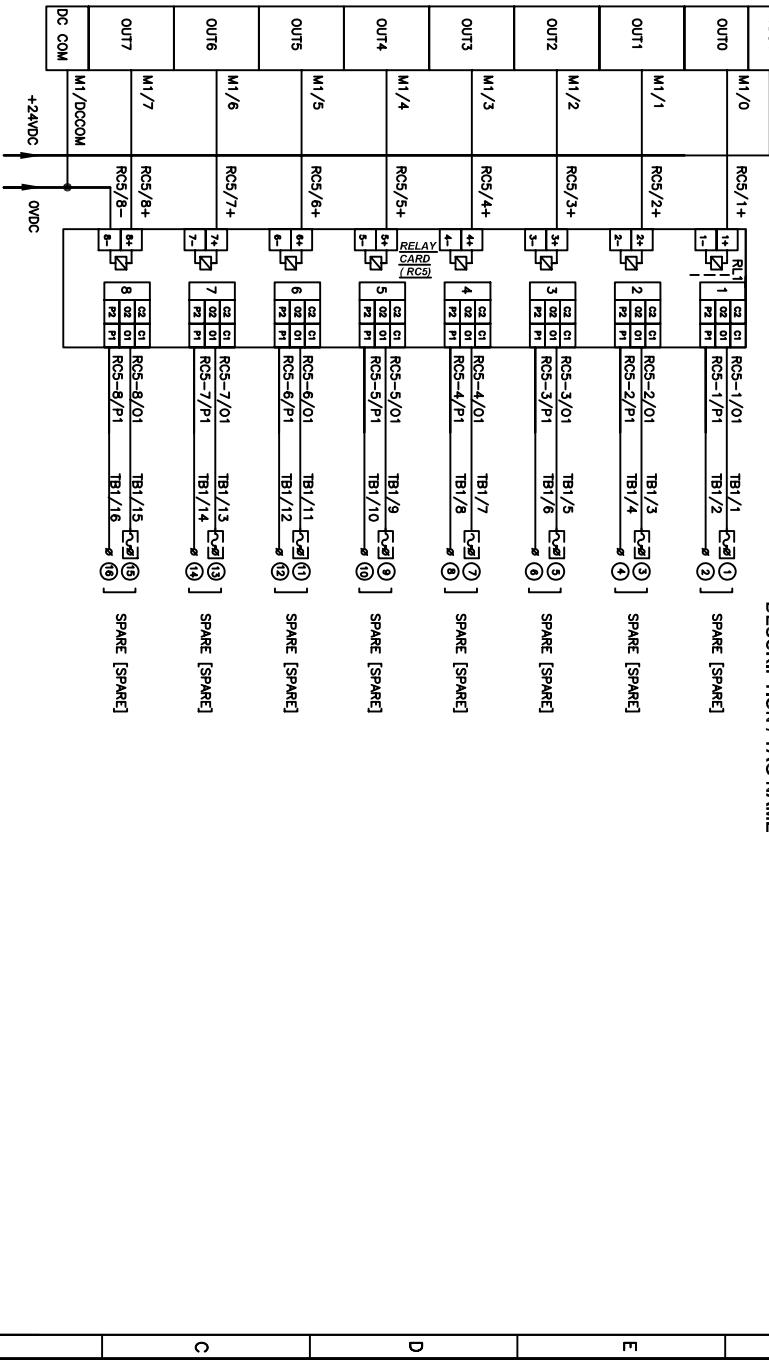
### 1762 - OB8 DIGITAL OUTPUT WIRING DIAGRAM.

#### MODULE - M1

VDC +

M1/VDC+

DESCRIPTION / TAG NAME:



FROM TBD1 SHT. NO. 3    FROM TBD3 SHT. NO. 4

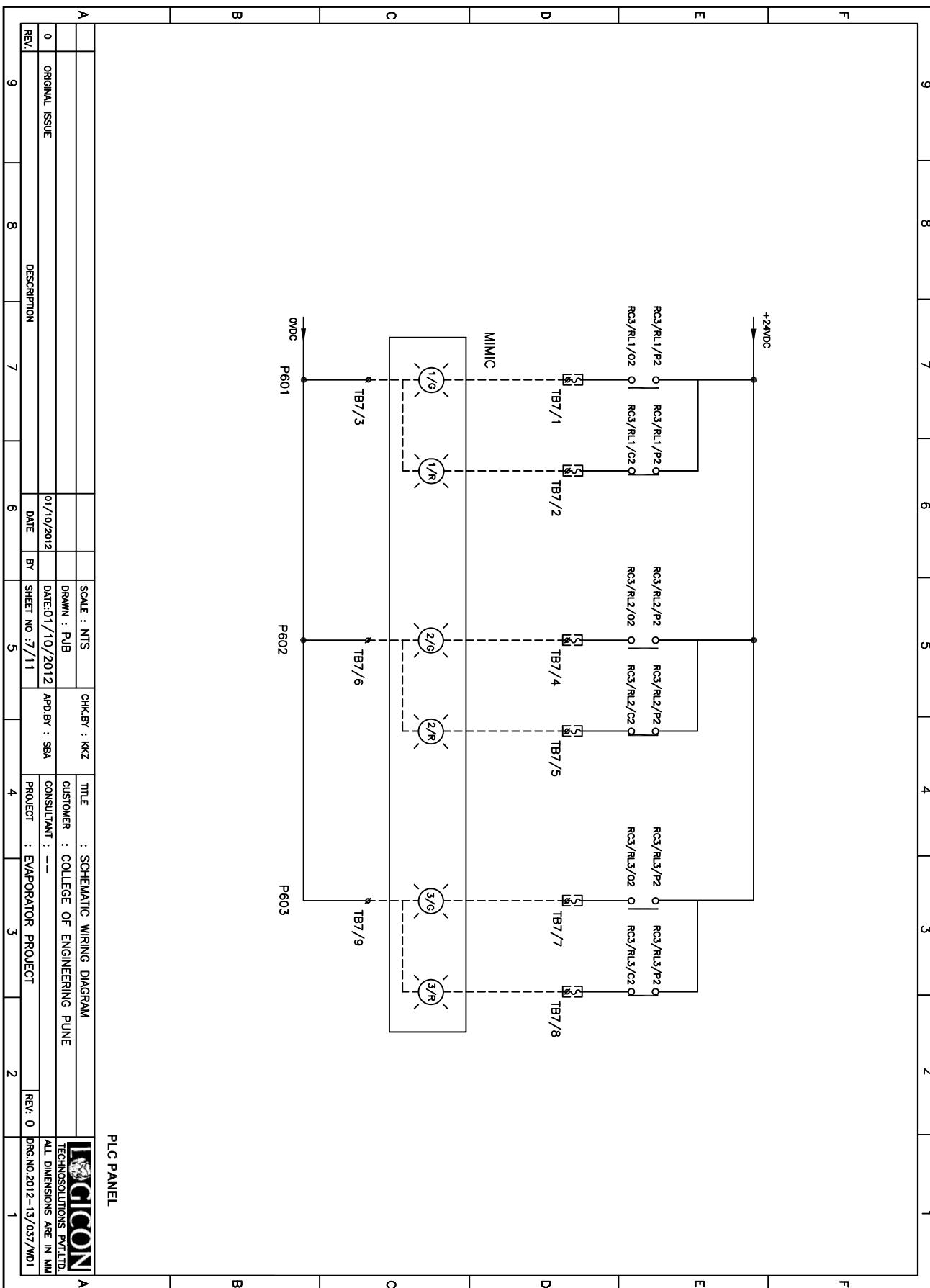
NOTE - FUSE RATING--1A  
 ①.....⑯ STANDS FOR TERMINAL NO.

PLC PANEL

A	SCALE : NTS	CHK BY : KRCZ	TITLE : SCHEMATIC WIRING DIAGRAM
O	ORIGINAL ISSUE	DRAWN : PJB	CUSTOMER : COLLEGE OF ENGINEERING PUNE
REV.	DESCRIPTION	DATE : 01/10/2012	CONSULTANT : --
9	8	DATE : SHEET NO : 6/11	PROJECT : EVAPORATOR PROJECT

A	TECHNOSOLUTIONS PVT LTD.
	ALL DIMENSIONS ARE IN MM

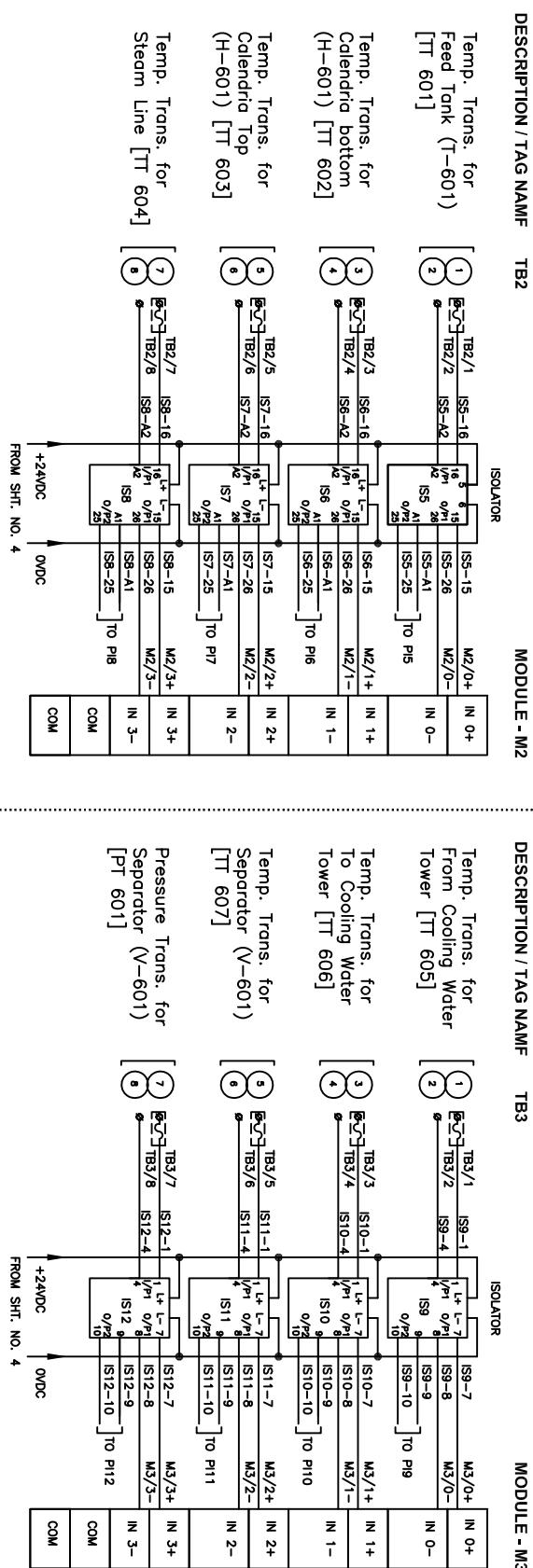
1	REV. 0	DESIGN NO. 2012-13/037/WD1
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9      8      7      6      5      4      3      2      1

### 1762 - IF4 ANALOG INPUT MODULE

### 1762 - IF4 ANALOG INPUT MODULE



NOTE - FUSE RATING - 100mA.

(1).....(1) STANDS FOR TERMINAL NO.

NOTE - FUSE RATING - 100mA.

(1).....(1) STANDS FOR TERMINAL NO.

DESCRIPTION / TAG NAME		TB2		MODULE - M2		DESCRIPTION / TAG NAME		TB3		MODULE - M3	
A		SCALE : NTS	CHK BY : KKZ	TITLE : SCHEMATIC WIRING DIAGRAM				ISOLATOR		ISOLATOR	
O	ORIGINAL ISSUE	DRAWN : PUB	DATE : 01/10/2012	CUSTOMER : COLLEGE OF ENGINEERING PUNE	TECHNOSOLUTIONS PVT.LTD.	CONSULTANT : ---	ALL DIMENSIONS ARE IN MM				
REV.		APD BY : SBA	DATE : 01/10/2012	PROJECT : EVAPORATOR PROJECT	REV: 0	SHEET NO : 8/11	ORG.NO:2012-13/037/W01				
9		BY		DATE		4	3	2			1
B											
C											
D											
E											
F											

PLC PANEL

**LOGICON**

A

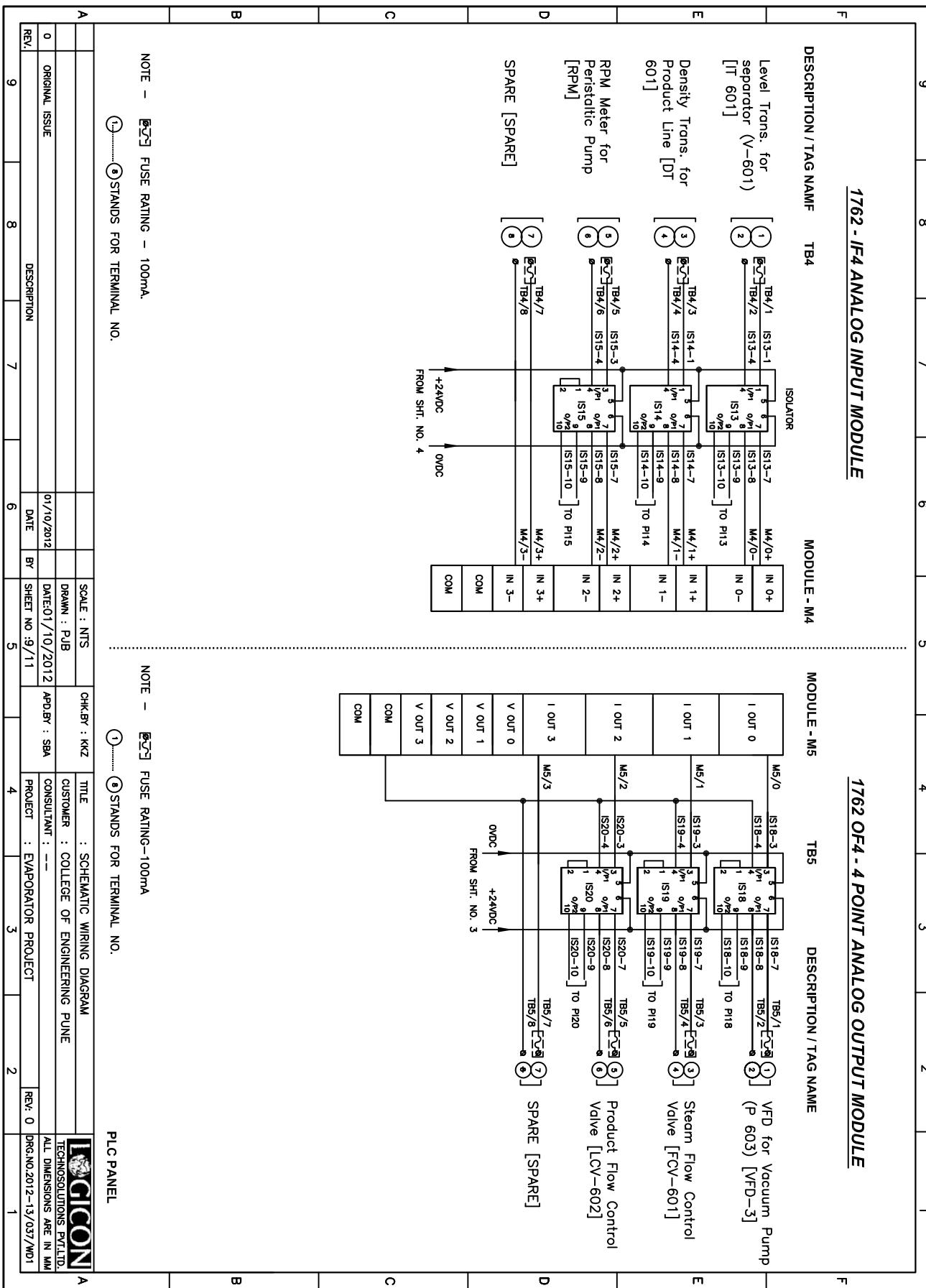
B

C

9      8      7      6      5      4      3      2      1

## 1762 - IF4 ANALOG INPUT MODULE

## 1762 OF4 - 4 POINT ANALOG OUTPUT MODULE



**LOGICON**

A

B

C

D

E

F

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H

I

J

K

L

M

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Q

R

S

T

U

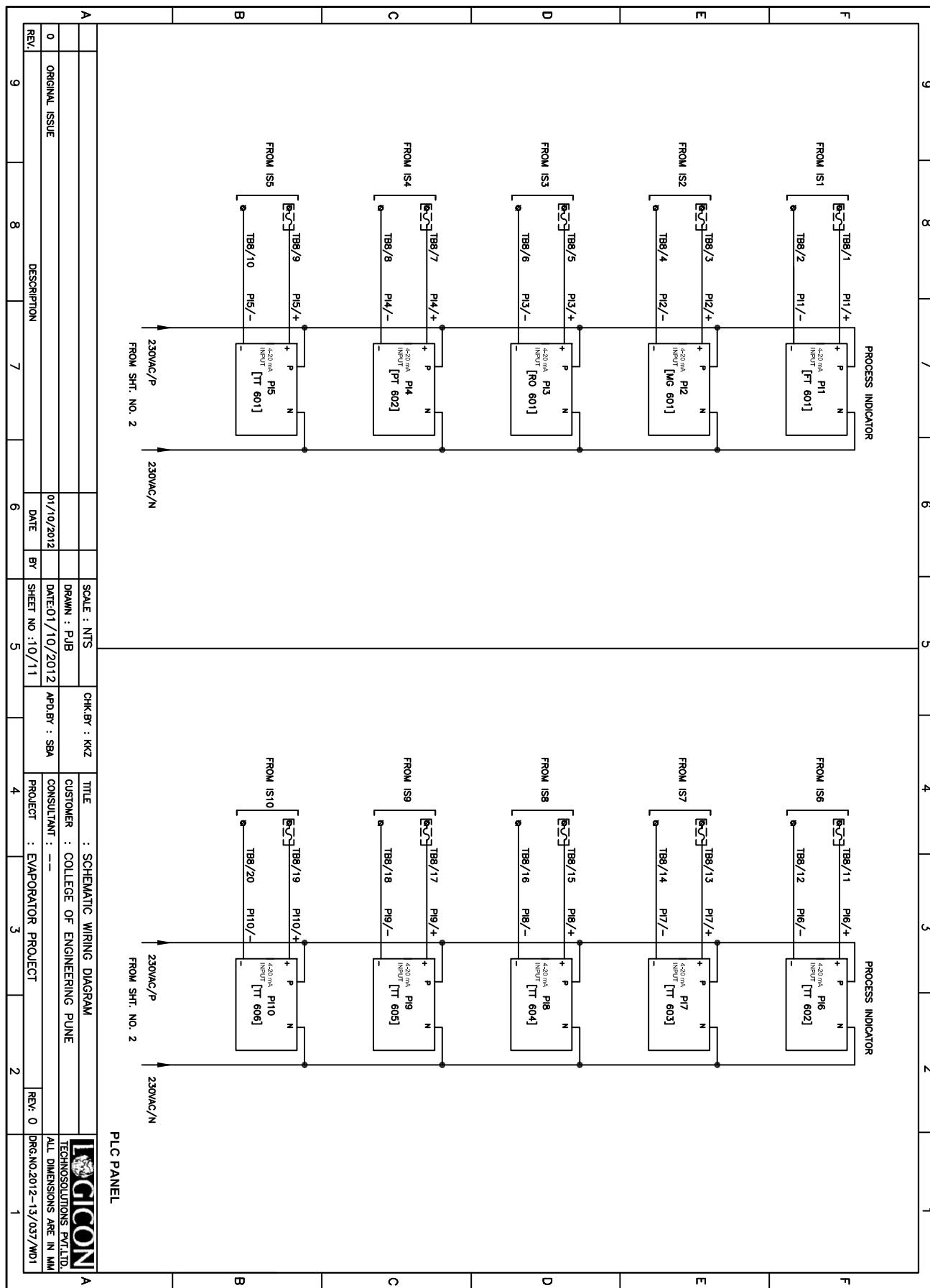
V

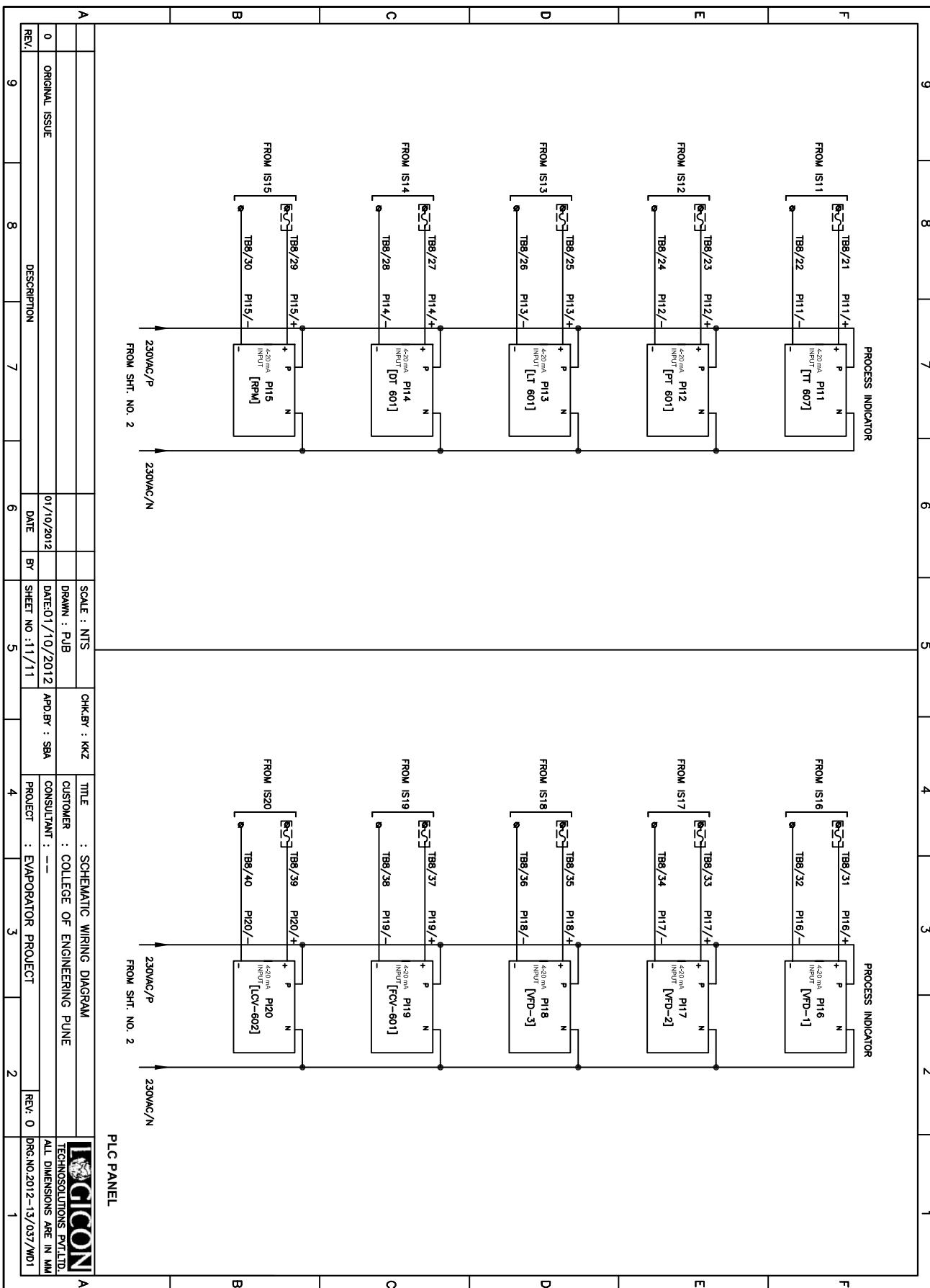
W

X

Y

Z





A	SCALE : NTS	CHK/BY : KRCZ	TITLE : SCHEMATIC WIRING DIAGRAM
O	CUSTOMER : COLLEGE OF ENGINEERING PUNE	TECHNOSOLUTIONS PVT LTD.	ALL DIMENSIONS ARE IN MM
ORIGINAL ISSUE	01/10/2012	DATE:01/10/2012	DESIGN NO.2012-13/037/W01
REV.	DESCRIPTION	BY SHEET NO:11/11	REV. 0
9	8	7	6
5	4	3	2
1			

**LOGICON**

**A**

**PLC PANEL**



9	8	7	6	5	4	3	2	1
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### WIRING SPECIFICATION

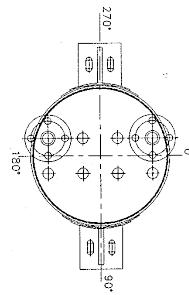
F		F	
	230V AC SUPPLY	PHASE ( UPTO DISTRIBUTION TB )	RED 4 mm <sup>2</sup>
		NEUTRAL ( UPTO DISTRIBUTION TB )	BLACK 4 mm <sup>2</sup>
		PHASE ( AFTER DISTRIBUTION TB )	RED 1.5 mm <sup>2</sup>
		NEUTRAL ( AFTER DISTRIBUTION TB )	BLACK 1.5 mm <sup>2</sup>
	110V AC SUPPLY	PHASE ( UPTO DISTRIBUTION TB )	RED 4 mm <sup>2</sup>
		NEUTRAL ( UPTO DISTRIBUTION TB )	BLACK 4 mm <sup>2</sup>
		PHASE ( AFTER DISTRIBUTION TB )	RED 1.5 mm <sup>2</sup>
		NEUTRAL ( AFTER DISTRIBUTION TB )	BLACK 1.5 mm <sup>2</sup>
D	24V DC +VE	UPTO BUSBAR	BLUE 1.5 mm <sup>2</sup>
D	24V DC -VE	AFTER BUSBAR	BLUE 1.0 mm <sup>2</sup>
		UPTO BUSBAR	WHITE 1.5 mm <sup>2</sup>
		AFTER BUSBAR	WHITE 1.0 mm <sup>2</sup>
	D/I WIRING		
C	MODULE TO RELAY COIL	GREY	0.5 mm <sup>2</sup>
C	D/O WIRING		
C	RELAY CONTACT TO TERMINALS ( PF )	BROWN	1.0 mm <sup>2</sup>
C	RELAY CONTACT TO TERMINALS ( 24VDC )	BLUE (+), WHITE (-)	1.0 mm <sup>2</sup>
C	RELAY CONTACT TO TERMINALS ( 230/110V AC )	RED (P), BLACK (N)	1.0 mm <sup>2</sup>
	A/I WIRING		
A	A/I WIRING	ORANGE (+), WHITE (-)	0.5 mm <sup>2</sup>
A	A/O WIRING	YELLOW (+), WHITE (-)	0.5 mm <sup>2</sup>
B	POWER	GREEN/YELLOW	2.5 mm <sup>2</sup>
B	EARTH	GREEN	1.5 mm <sup>2</sup>

PLC PANEL

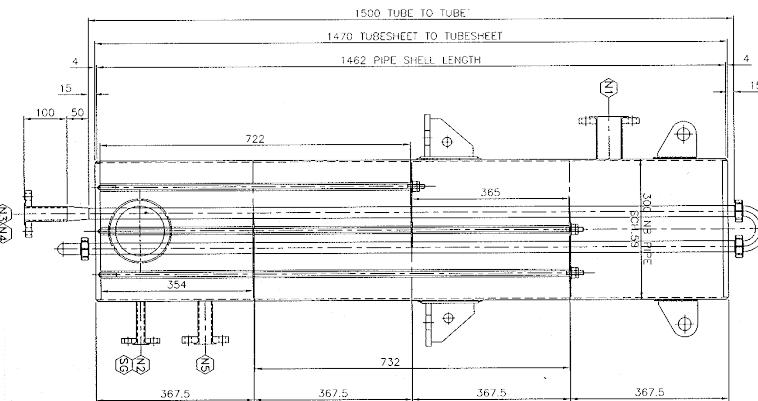
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O	ORIGINAL ISSUE		DRAWN : PJB	CUSTOMER : COLLEGE OF ENGINEERING PUNE		
REV.	0	01/10/2012	DATE:01/10/2012	CONSULTANT : --	TECHNOSOLUTIONS PVT LTD.	ALL DIMENSIONS ARE IN MM
	DESCRIPTION	DATE	BY	PROJECT : EVAPORATOR PROJECT	REV. 0	DRG NO.2012-13/037/WST
	9	8	7	6	5	4
					3	2
					1	

			C	D	E	F	G	H																																	
10	9	8	7	6	5	4	3	2																																	
<p>1003 TUBESHEET TO TUBESHEET 1000 TUBE TO TUBE 100 NB PIPE SH-105</p>																																									
<p>ORIENTATION PLAN (HOLD)</p>																																									
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">REV. NO.</th> <th rowspan="2">DESCRIPTION</th> <th colspan="3">DRAWN : CHD</th> <th colspan="3">APR'D.</th> <th rowspan="2">DATE</th> </tr> <tr> <th>M.A.Z</th> <th>R.A.M.</th> <th>S.A.M.</th> <th>01.10.12</th> </tr> </thead> <tbody> <tr> <td>0</td> <td>FOR FABRICATION</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>									REV. NO.	DESCRIPTION	DRAWN : CHD			APR'D.			DATE	M.A.Z	R.A.M.	S.A.M.	01.10.12	0	FOR FABRICATION																		
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		M.A.Z	R.A.M.	S.A.M.	01.10.12																																				
0	FOR FABRICATION																																								
<p>CLIENT : PLANT : LOCATION :</p>																																									
<p><b>RAJ PROCESS EQUIPMENTS &amp; SYSTEMS PVT. LTD.</b> RAJ PROCESS EQUIPMENTS &amp; SYSTEMS PVT. LTD. JAI GANESH VISION, 8 WING-3RD FLOOR AKROB PARK-410053.</p>																																									
<p><b>TITLE :</b> I.D. NO. — JOB NO. RP-12-105 DWG. NO. — FALLING FILM EFFECT - 1 (H-601) SHEET OF 1 REV. 0</p>																																									
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<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td colspan="3">NOTES: SIZE SERVICE ISOPROPYL ELEVATION</td> </tr> <tr> <td colspan="3">N1 15 NB STEAM INLET</td> </tr> <tr> <td colspan="3">N2 15 NB RECYCLE LIQUID INLET</td> </tr> <tr> <td colspan="3">N3 15 NB RECYCLE LIQUID OUTLET</td> </tr> <tr> <td colspan="3">N4 15 NB COUSIBLE CABLE</td> </tr> <tr> <td colspan="3">N5 15 NB SIGHT GLASS PLUG</td> </tr> <tr> <td colspan="3">N6 1/2" NPT SIGHT GLASS PLUG</td> </tr> <tr> <td colspan="3">N7 1/2" NPT SIGHT GLASS PLUG</td> </tr> <tr> <td colspan="3">N8 1/2" NPT SIGHT GLASS PLUG</td> </tr> <tr> <td colspan="3">N9 1/2" NPT SIGHT GLASS PLUG</td> </tr> <tr> <td colspan="3">N10 1/2" NPT SIGHT GLASS PLUG</td> </tr> </table>									NOTES: SIZE SERVICE ISOPROPYL ELEVATION			N1 15 NB STEAM INLET			N2 15 NB RECYCLE LIQUID INLET			N3 15 NB RECYCLE LIQUID OUTLET			N4 15 NB COUSIBLE CABLE			N5 15 NB SIGHT GLASS PLUG			N6 1/2" NPT SIGHT GLASS PLUG			N7 1/2" NPT SIGHT GLASS PLUG			N8 1/2" NPT SIGHT GLASS PLUG			N9 1/2" NPT SIGHT GLASS PLUG			N10 1/2" NPT SIGHT GLASS PLUG		
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N10 1/2" NPT SIGHT GLASS PLUG																																									

3  
45°  
90°  
135°  
180°



ORIENTATION PLAN (HOLD)



ELEVATION  
SCALE - 1/2

CLIENT :  
PLANT :  
LOCATION :

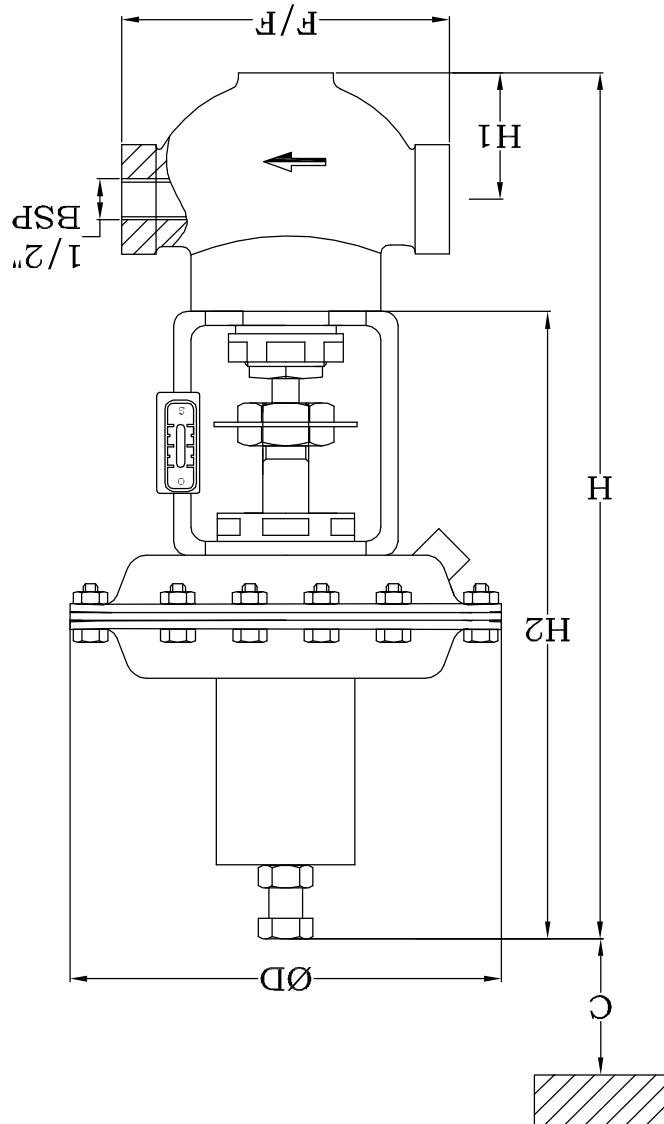


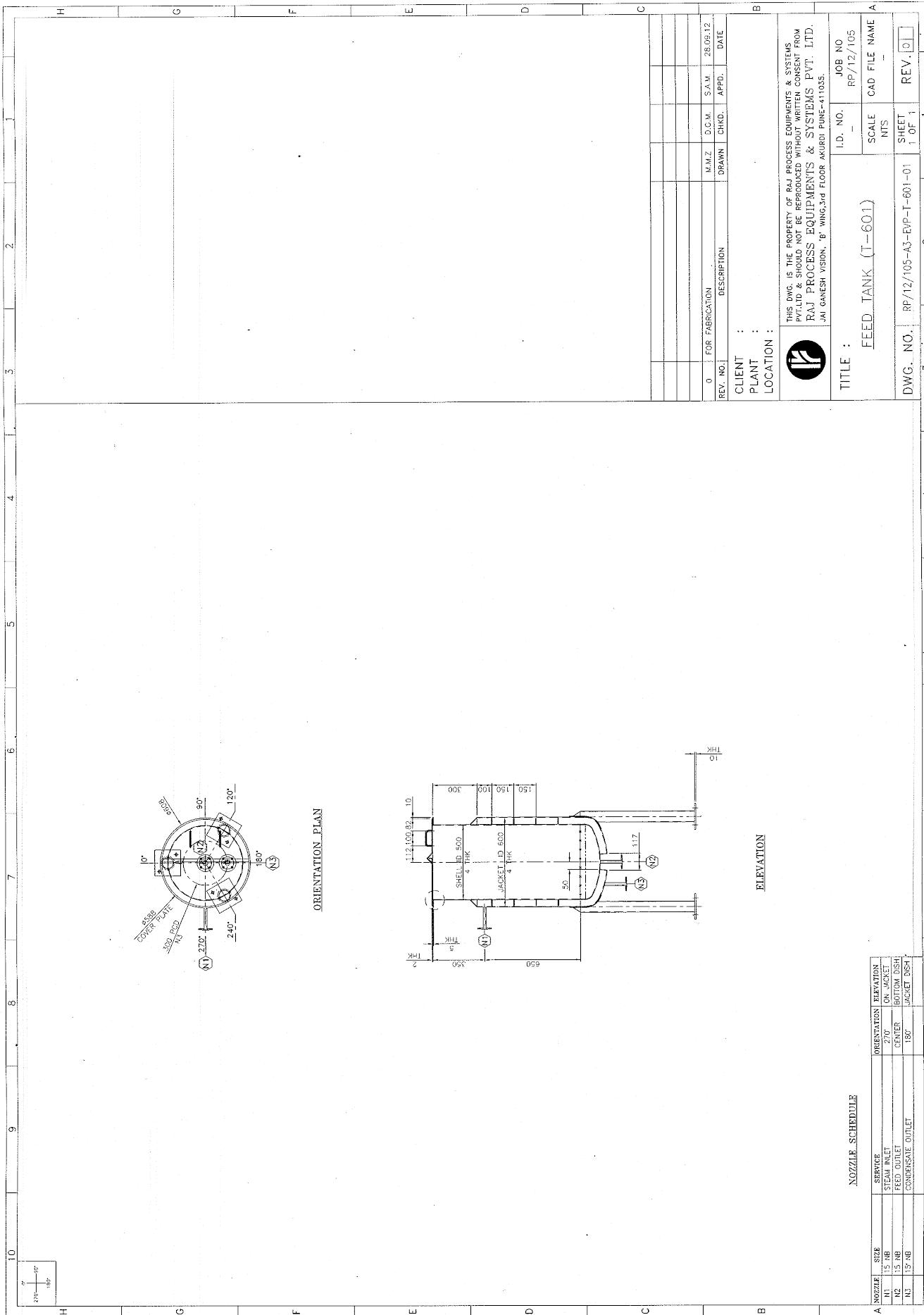
THIS DWG. IS THE PROPERTY OF RAJ PROCESS EQUIPMENTS & SYSTEMS  
PVT. LTD. & SHOULD NOT BE REPRODUCED WITHOUT WRITTEN CONSENT FROM  
RAJ GANESH VISION, B- WING 3RD FLOOR AKROD PUNE-411035.

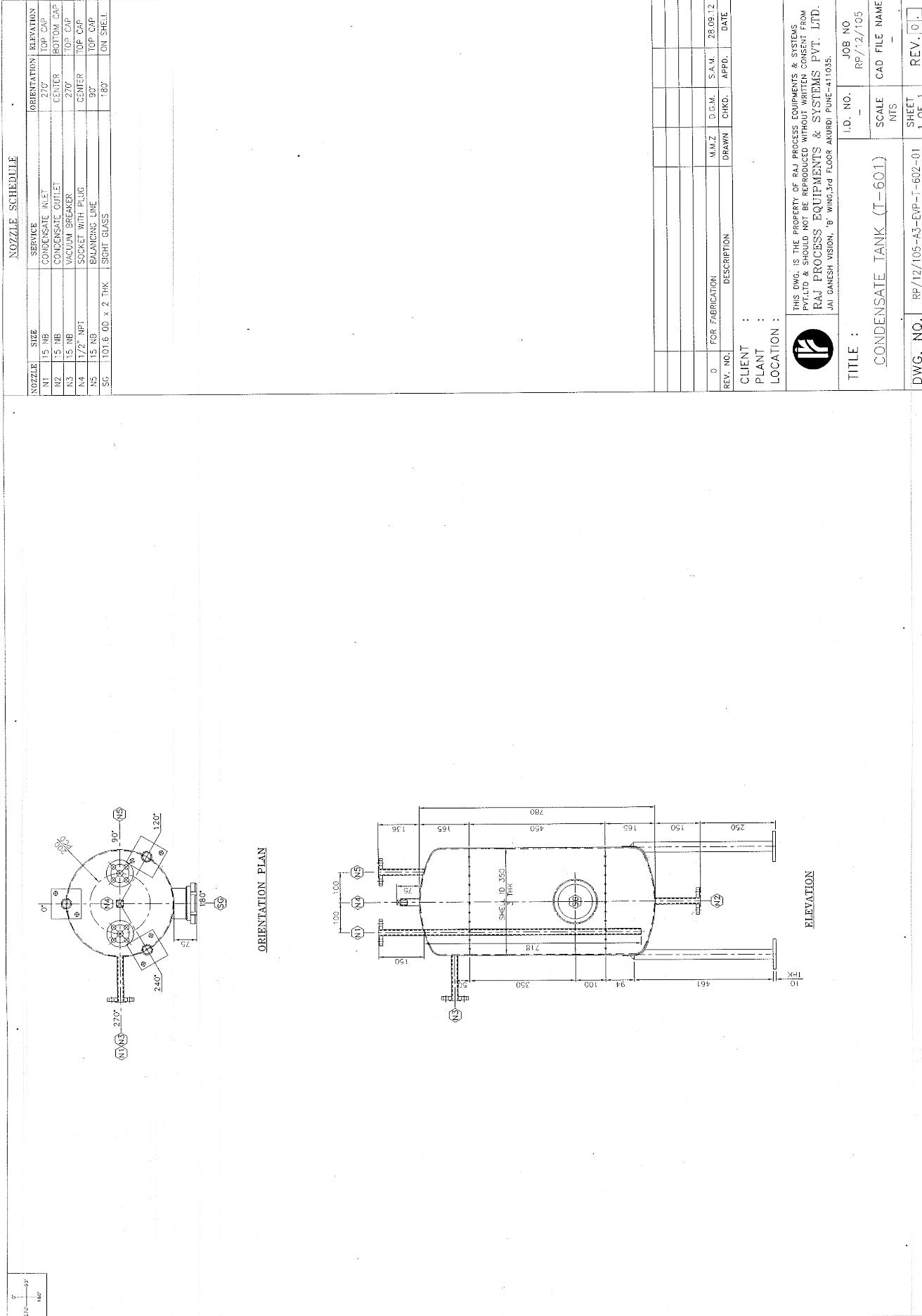
TITLE :	I.D. NO.	JOB NO.
SURFACE CONDENSER (H-602)	—	RP/12/105
DWG. NO.	SHFT. OR/1	REV. 0

PROJECT	-		SUBJECT	G.A. DRAWING - 1/2" X 150# GLOBE-2 WAY CONTROL VALVE (SERIES-119)
CONSULTANT	-	Drg. No	Drge. No.	GAI9015151C61
W.O. No.	PVW-1213-1158	DRG. No	PVW/1213/1158/01	SCALE
P. O. No.	-	DATE	18.12.2012	N.T.S.
CUSTOMER	Date Process Control Instruments Pvt.Ltd.	CHECKED	J.N.C.	
P.D.	PNEUCON	APPROVED	D.M.G.	
DRAWN	L.G.	REV'D		
REV. No.	DATE	REVISION		SIGN

DESCRIPTION										MOUNTING DIMENSIONS (mm.)										
VALVE	ST. NO.	TAG	VALVE	ACTUATOR	FLANGE	F/F	H	H1	H2	C	D	150	200	341	114	150#	PDC-012	1/2"	-	30869







# **Appendix E**

# **Micrologix Programming**

## **E.1 Evaporator Programming**

## RSLogix 500 Project Report



Table Of Contents

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I/O Config	4
Channel Config	5
Program File List	6
Data File List	7
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Program Files	9
Data Files	75

Processor Information

---

Processor Type: Bul.1766 MicroLogix 1400 Series A

Processor Name: UNTITLED

Total Memory Used: 1072 Instruction Words Used - 1316 Data Table Words Used

Total Memory Left: 11362 Instruction Words Left

Program Files: 14

Data Files: 22

Program ID: 9d9a

I/O Configuration

---

0 Bul.1766 MicroLogix 1400 Series A  
1 1762-OB8 8-Output (TRANS-SRC) 10/50 VDC  
2 1762-IF4 Analog 4 Chan. Input  
3 1762-IF4 Analog 4 Chan. Input  
4 1762-IF4 Analog 4 Chan. Input  
5 1762-OF4 4-Channel Analog I/V Output Module  
6  
7

## Channel Configuration

---

CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave Edit Resource/Owner Timeout: 60  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave Passthru Link ID: 1  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave Write Protected: No  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave Comms Servicing Selection: Yes  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave Message Servicing Selection: Yes  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave 1st AWA Append Character: \d  
 CHANNEL 0 (SYSTEM) - Driver: Modbus RTU Slave 2nd AWA Append Character: \a

Node : 2 (decimal)  
 Baud: 19200  
 Parity: NONE  
 File Number for Coils: 29  
 File Number for Contacts: 30  
 File Number for Input Registers: 31  
 File Number for Holding Registers: 34  
 Expanded: No  
 Control Line : No Handshaking  
 InterCharacter Timeout(x1 ms): 0  
 Pre Transmit Delay(x1 ms): 0

CHANNEL 1 (SYSTEM) - Driver: Ethernet  
 CHANNEL 1 (SYSTEM) - Driver: Ethernet Edit Resource/Owner Timeout: 60  
 CHANNEL 1 (SYSTEM) - Driver: Ethernet Passthru Link ID: 1  
 CHANNEL 1 (SYSTEM) - Driver: Ethernet Write Protected: No  
 CHANNEL 1 (SYSTEM) - Driver: Ethernet Comms Servicing Selection: Yes  
 CHANNEL 1 (SYSTEM) - Driver: Ethernet Message Servicing Selection: Yes

Hardware Address: 00:1D:9C:A3:51:10  
 IP Address: 192.168.1.225  
 Subnet Mask: 255.255.255.0  
 Gateway Address: 0.0.0.0  
 Msg Connection Timeout (x 1mS): 15000  
 Msg Reply Timeout (x mS): 3000  
 Inactivity Timeout (x Min): 30  
 Bootp Enable: No  
 Dhcp Enable: No  
 SMTP Enable: No  
 SNMP Enable: Yes  
 HTTP Enable: Yes  
 Auto Negotiate Enable: Yes  
 Port Speed Enable: 10/100 Mbps Full Duplex/Half Duplex  
 Contact:  
 Location:

CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave Edit Resource/Owner Timeout: 60  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave Passthru Link ID: 1  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave Write Protected: No  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave Comms Servicing Selection: Yes  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave Message Servicing Selection: Yes  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave 1st AWA Append Character: \d  
 CHANNEL 2 (SYSTEM) - Driver: Modbus RTU Slave 2nd AWA Append Character: \a

Node : 2 (decimal)  
 Baud: 19200  
 Parity: NONE  
 File Number for Coils: 29  
 File Number for Contacts: 30  
 File Number for Input Registers: 31  
 File Number for Holding Registers: 33  
 Expanded: No  
 Control Line : No Handshaking  
 InterCharacter Timeout(x1 ms): 0  
 Pre Transmit Delay(x1 ms): 0

## Program File List

Name	Number	Type	Rungs	Debug	Bytes
[SYSTEM]	0	SYS	0	No	0
	1	SYS	0	No	0
	2	LADDER	12	No	130
	3	LADDER	17	No	1587
	4	LADDER	7	No	556
	5	LADDER	21	No	349
	6	LADDER	20	No	307
	7	LADDER	8	No	221
	8	LADDER	13	No	387
	9	LADDER	26	No	647
	11	LADDER	9	No	180
	12	LADDER	14	No	1288
	13	LADDER	13	No	1165
	14	LADDER	15	No	1185

## Data File List

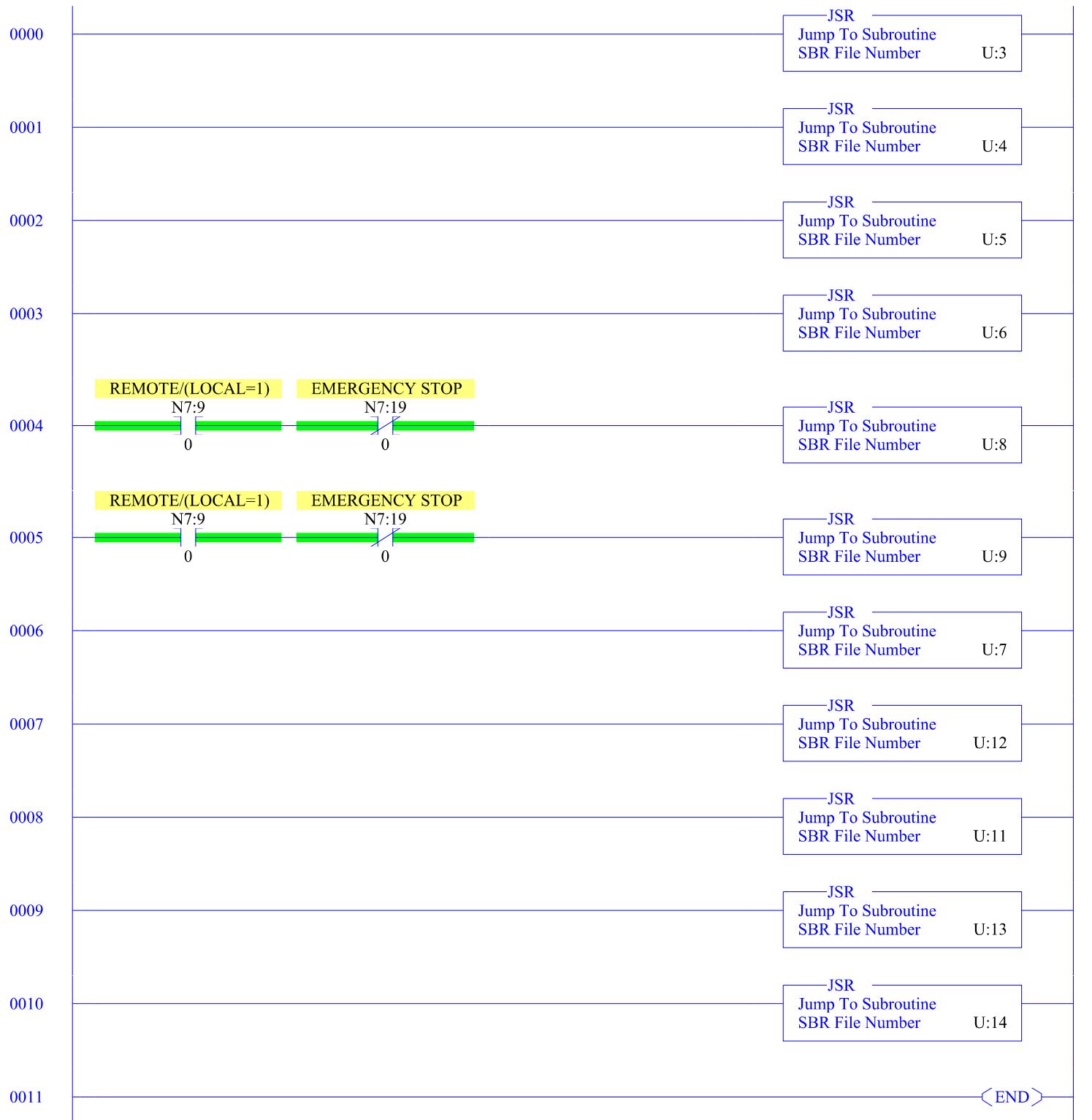
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OUTPUT	0	O	Global	No	33	11	O:10
INPUT	1	I	Global	No	93	31	I:30
STATUS	2	S	Global	No	0	66	S:65
BINARY	3	B	Global	No	20	20	B3:19
TIMER	4	T	Global	No	3	1	T4:0
COUNTER	5	C	Global	No	3	1	C5:0
CONTROL	6	R	Global	No	3	1	R6:0
INTEGER	7	N	Global	No	52	52	N7:51
FLOAT	8	F	Global	No	180	90	F8:89
	9	F	Global	No	60	30	F9:29
	10	N	Global	No	9	9	N10:8
	11	PD	Global	No	230	10	PD11:9
	12	F	Global	No	16	8	F12:7
	16	PD	Global	No	230	10	PD16:9
	23	N	Global	No	23	23	N23:22
	24	N	Global	No	40	40	N24:39
	29	N	Global	No	30	30	N29:29
	30	N	Global	No	13	13	N30:12
	31	N	Global	No	1	1	N31:0
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	33	N	Global	No	100	100	N33:99
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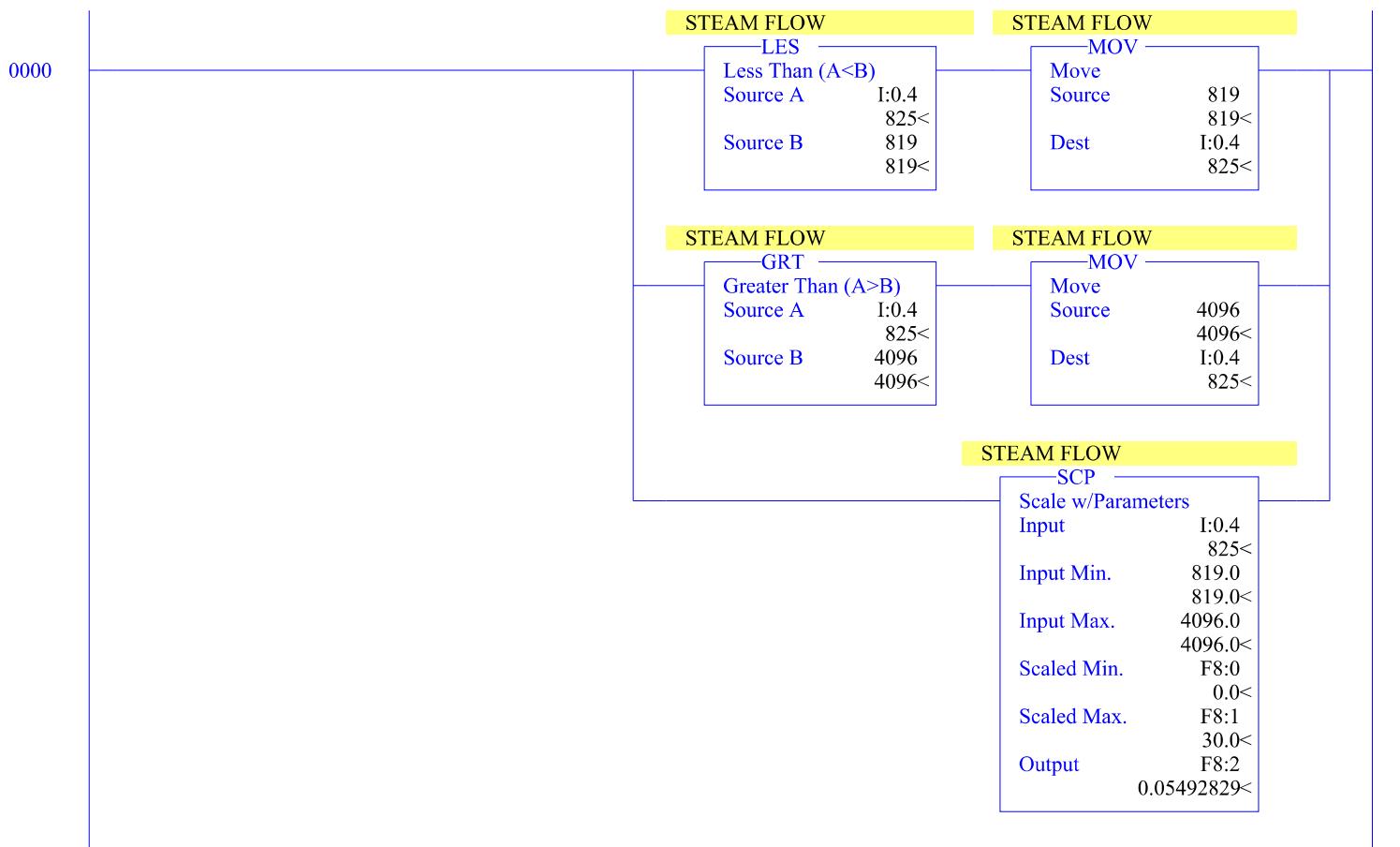
File      Rung      Page Title

Page

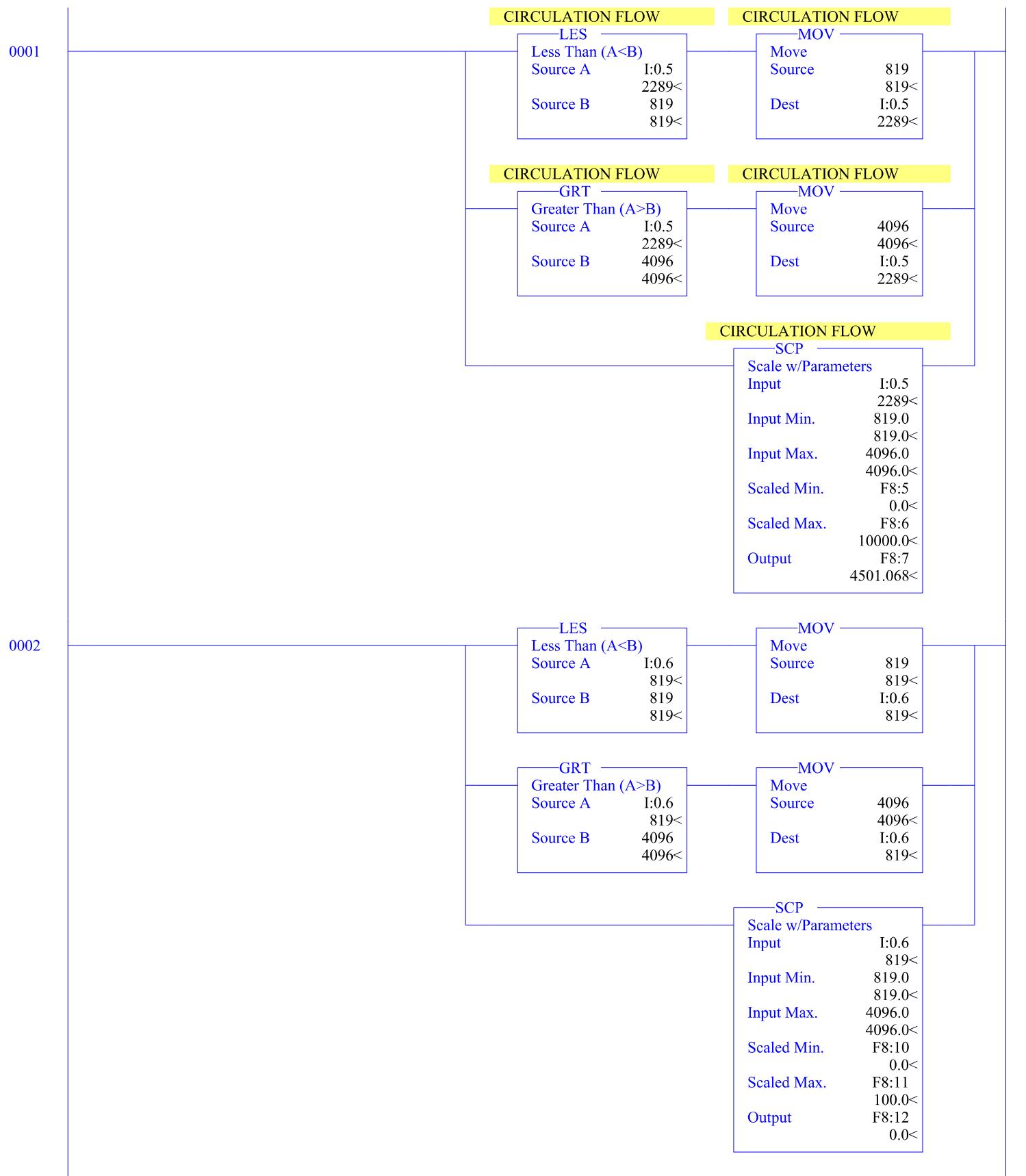
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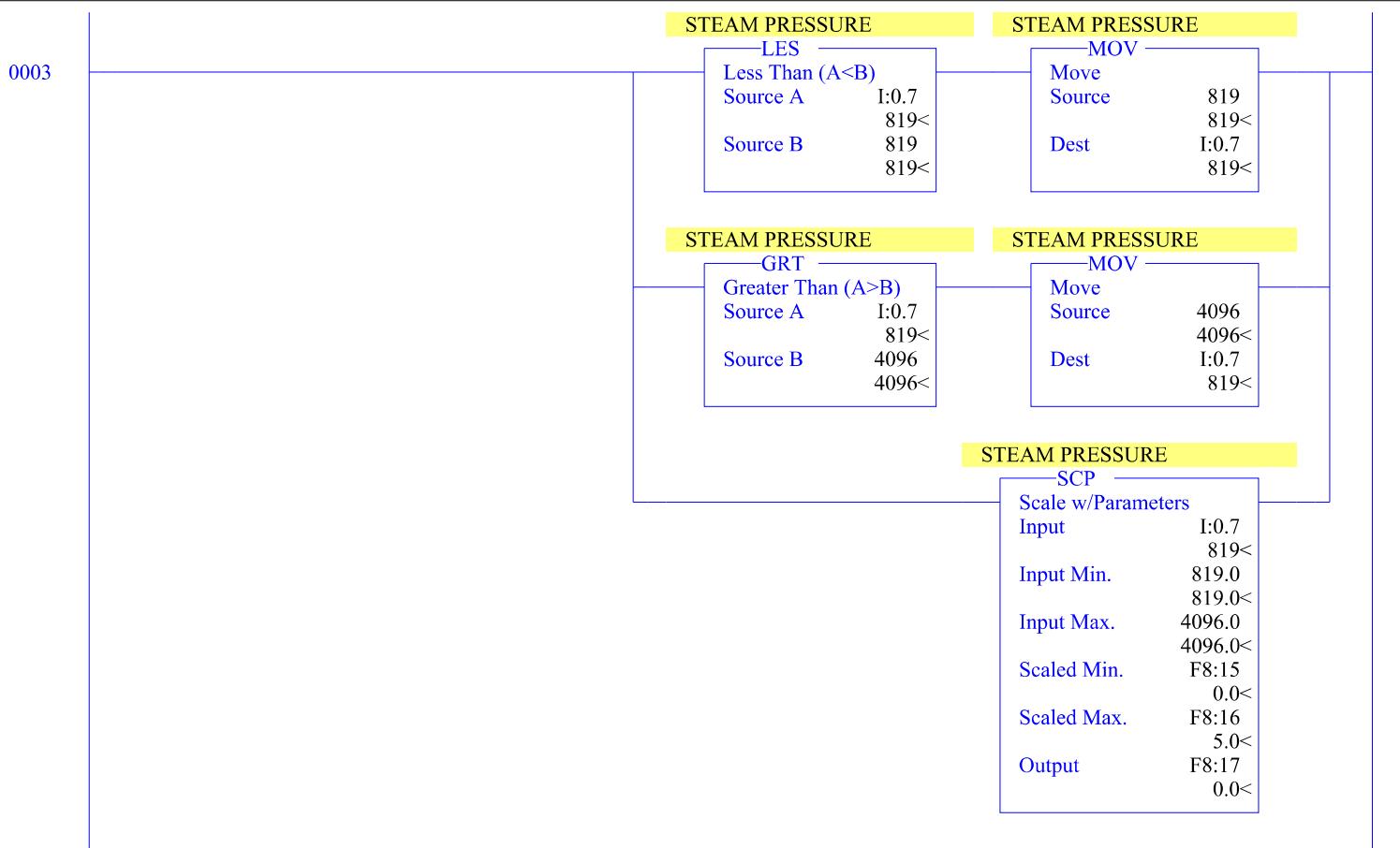
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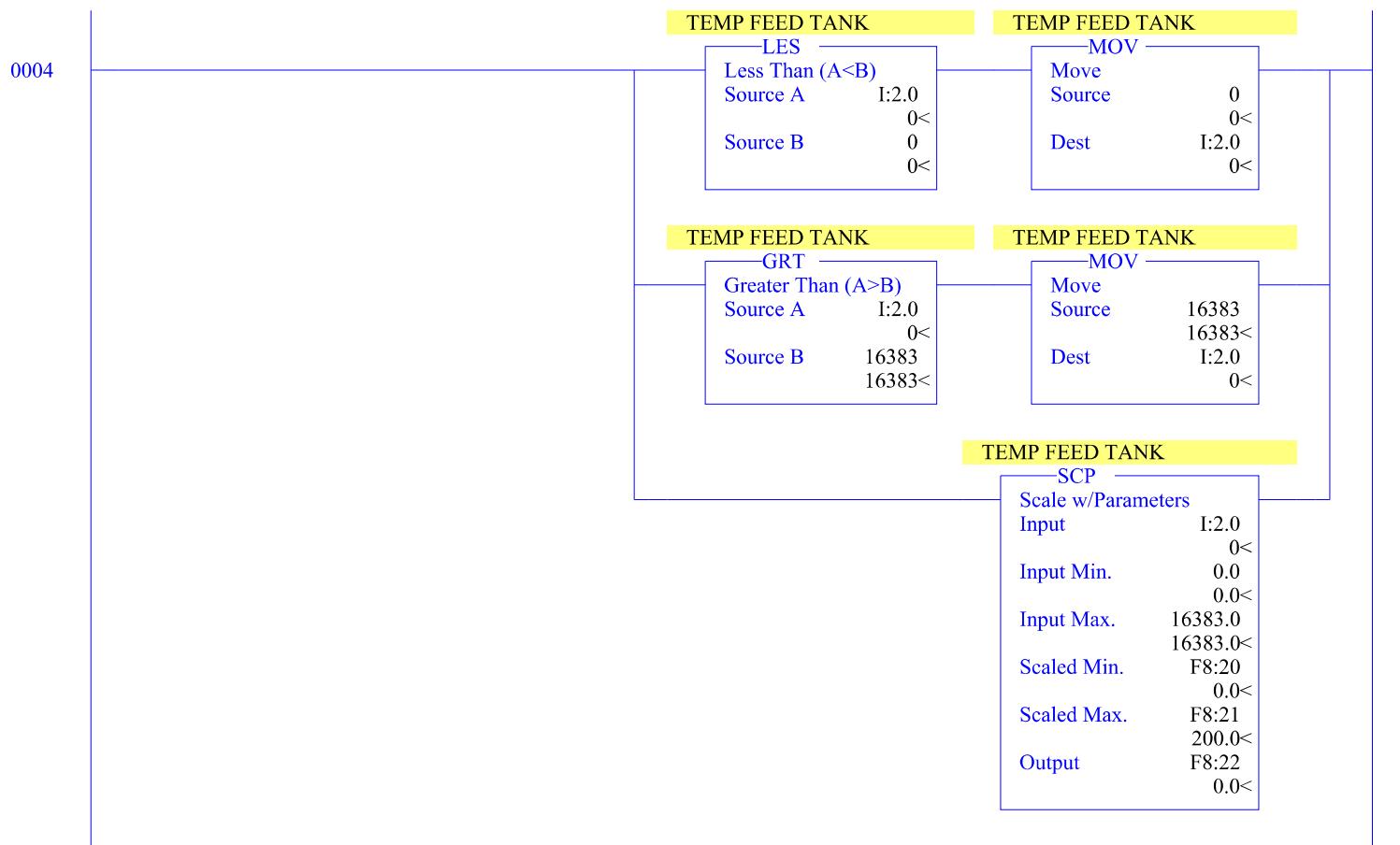
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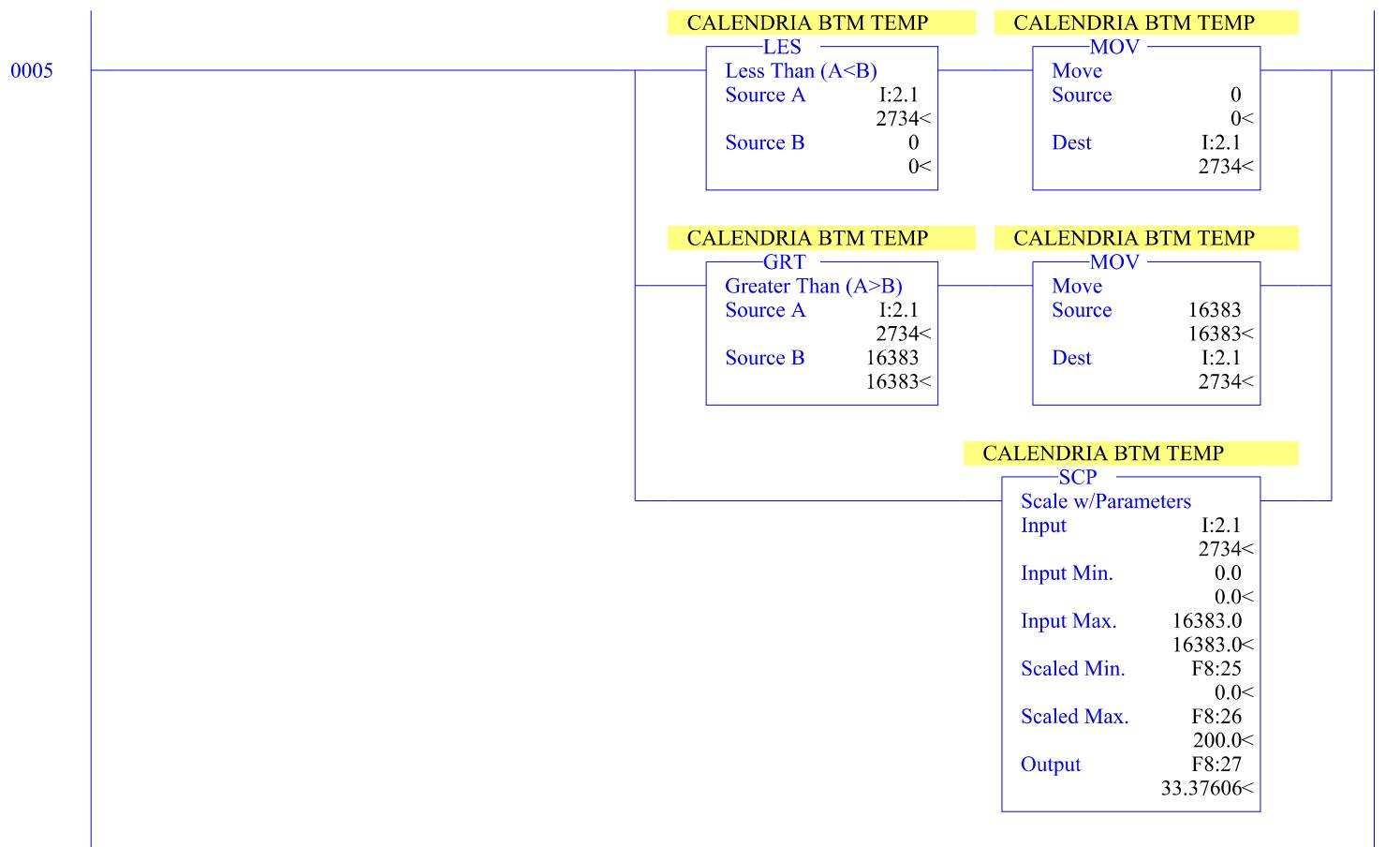
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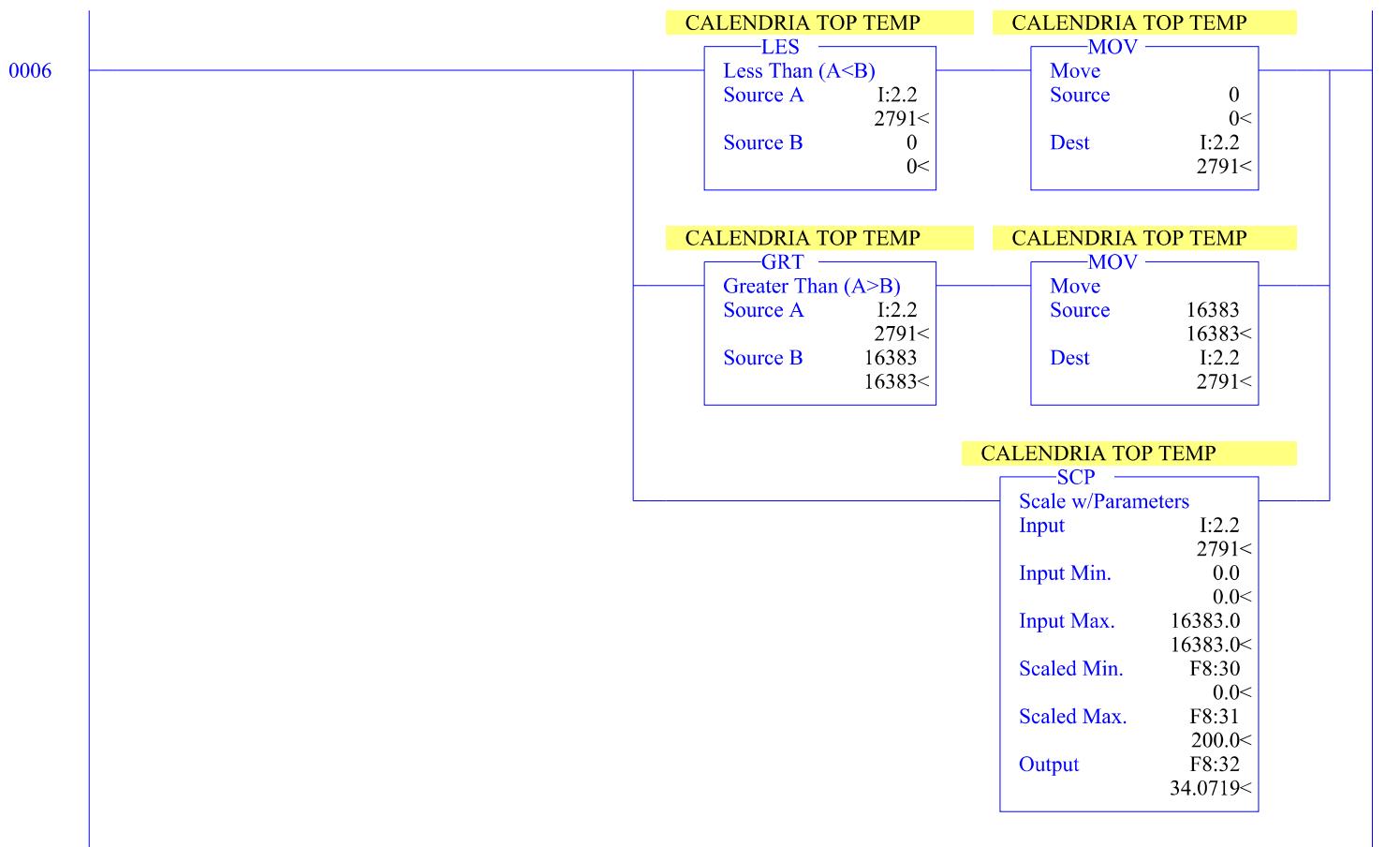
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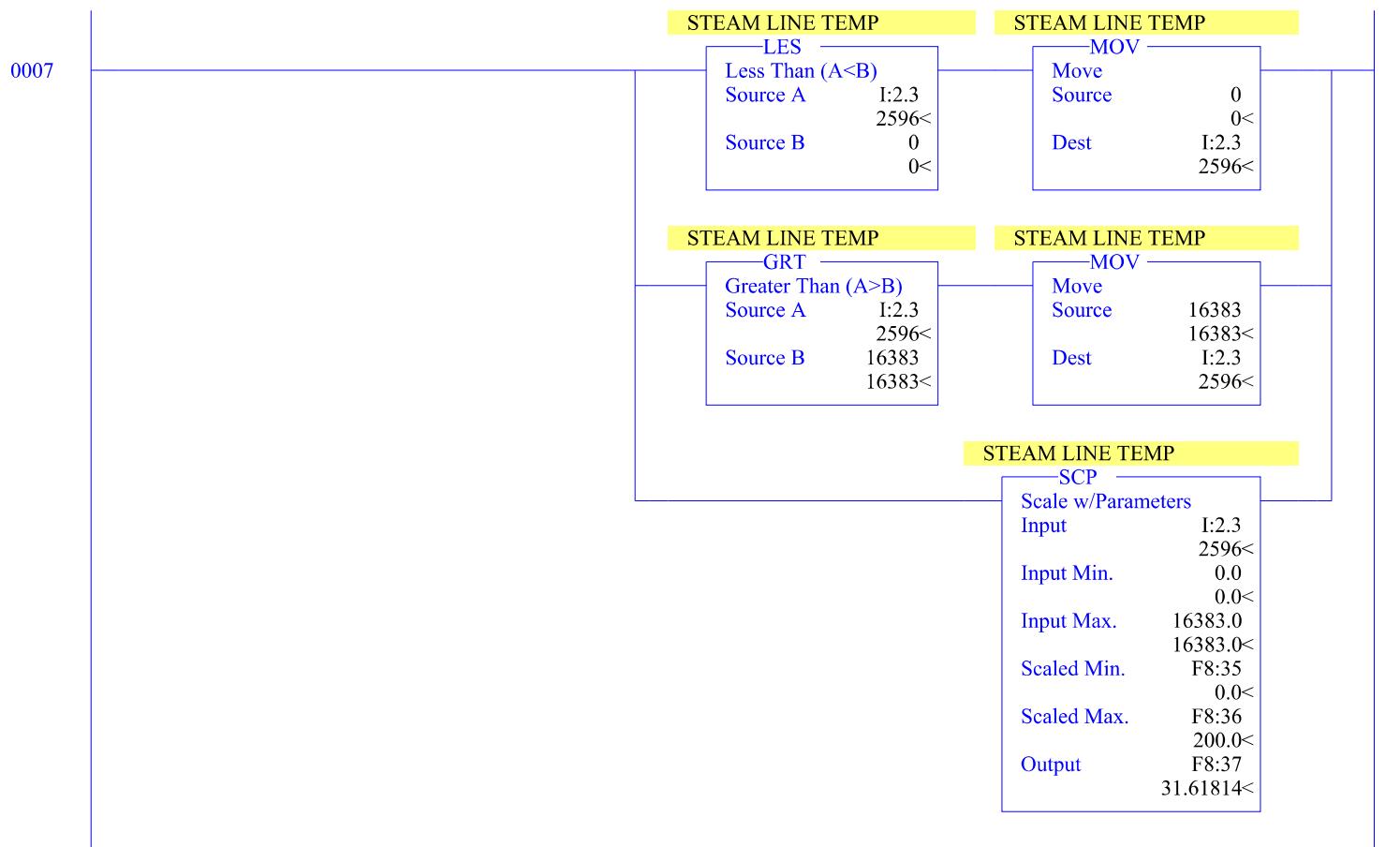
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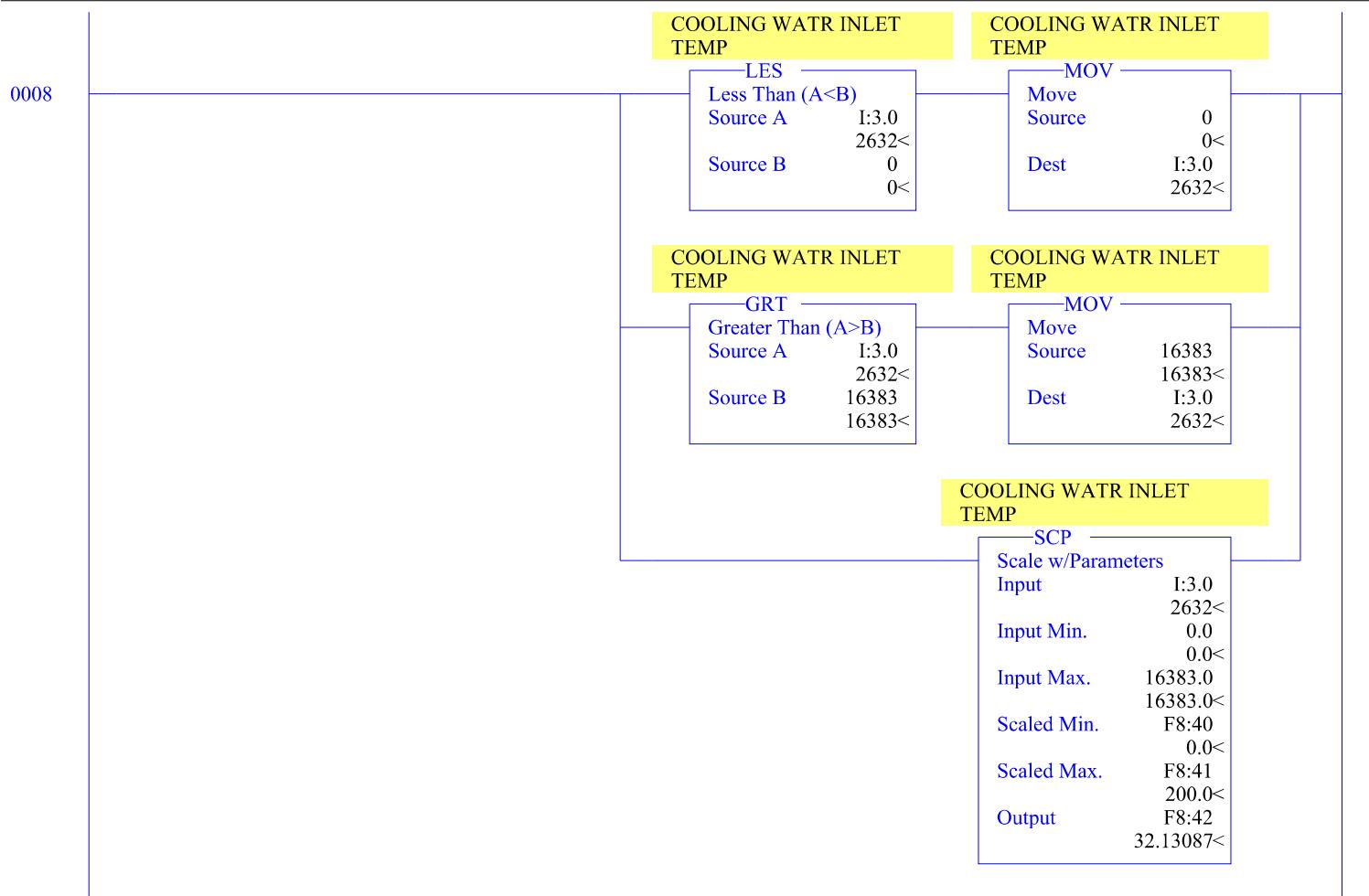
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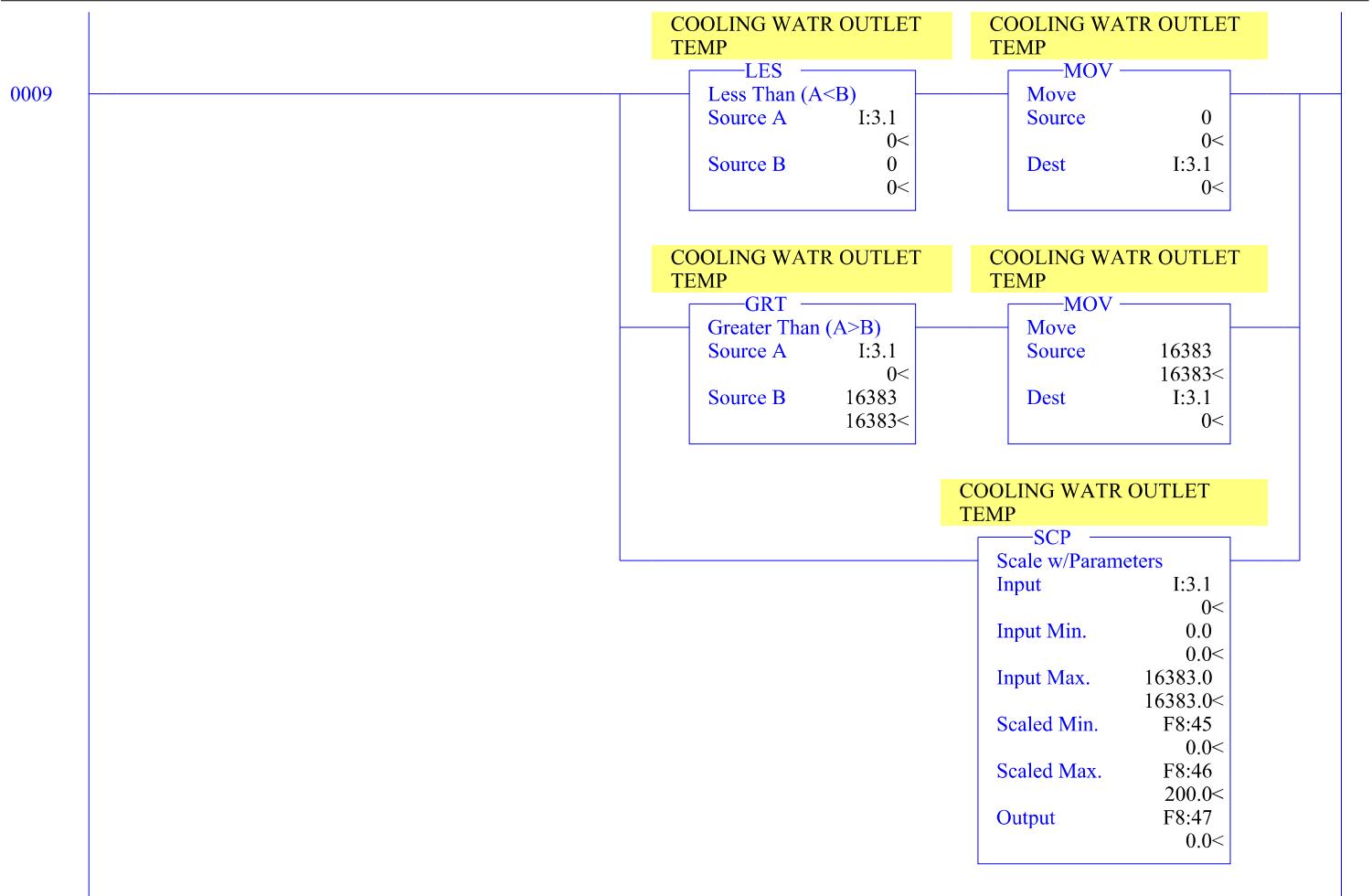
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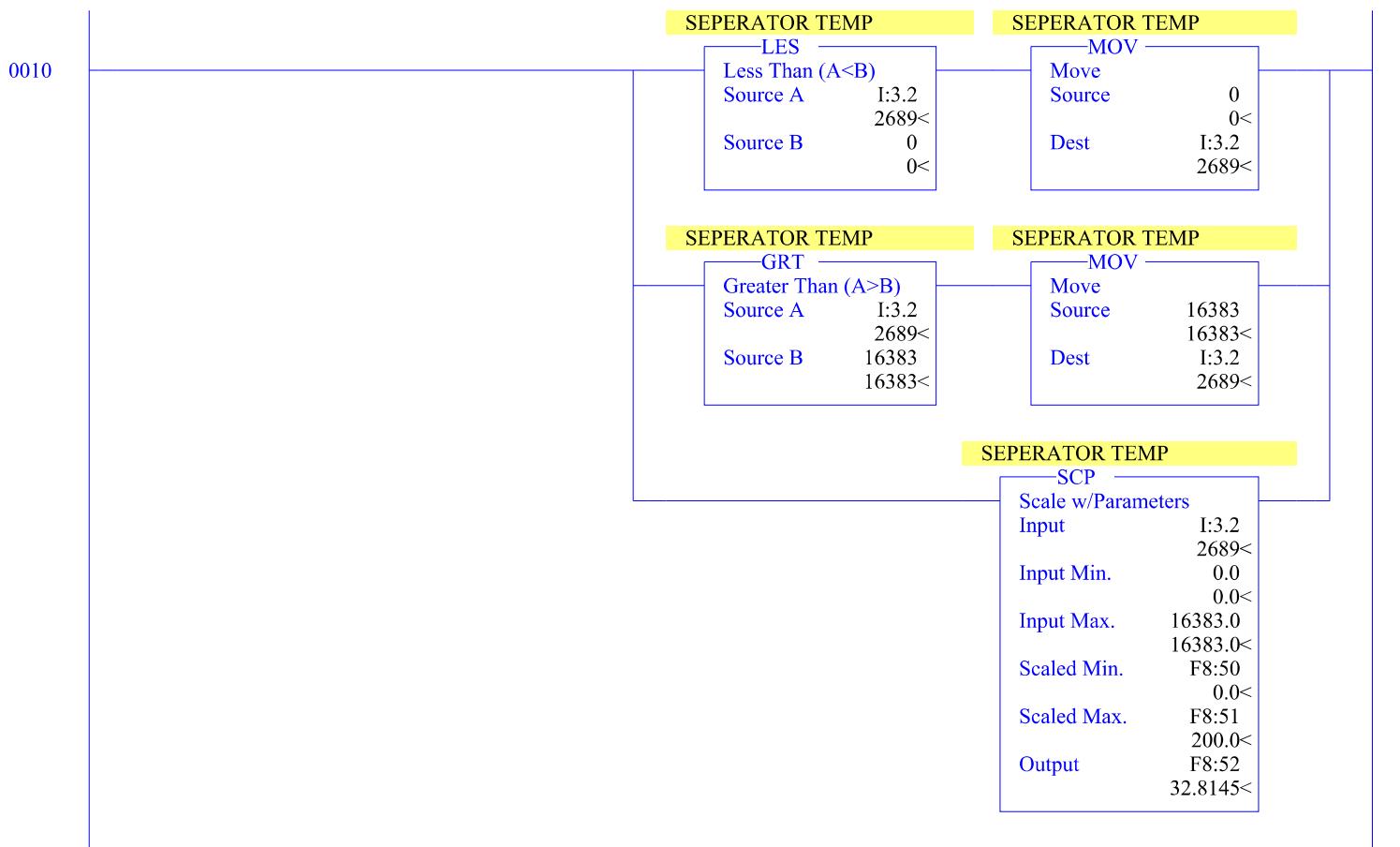
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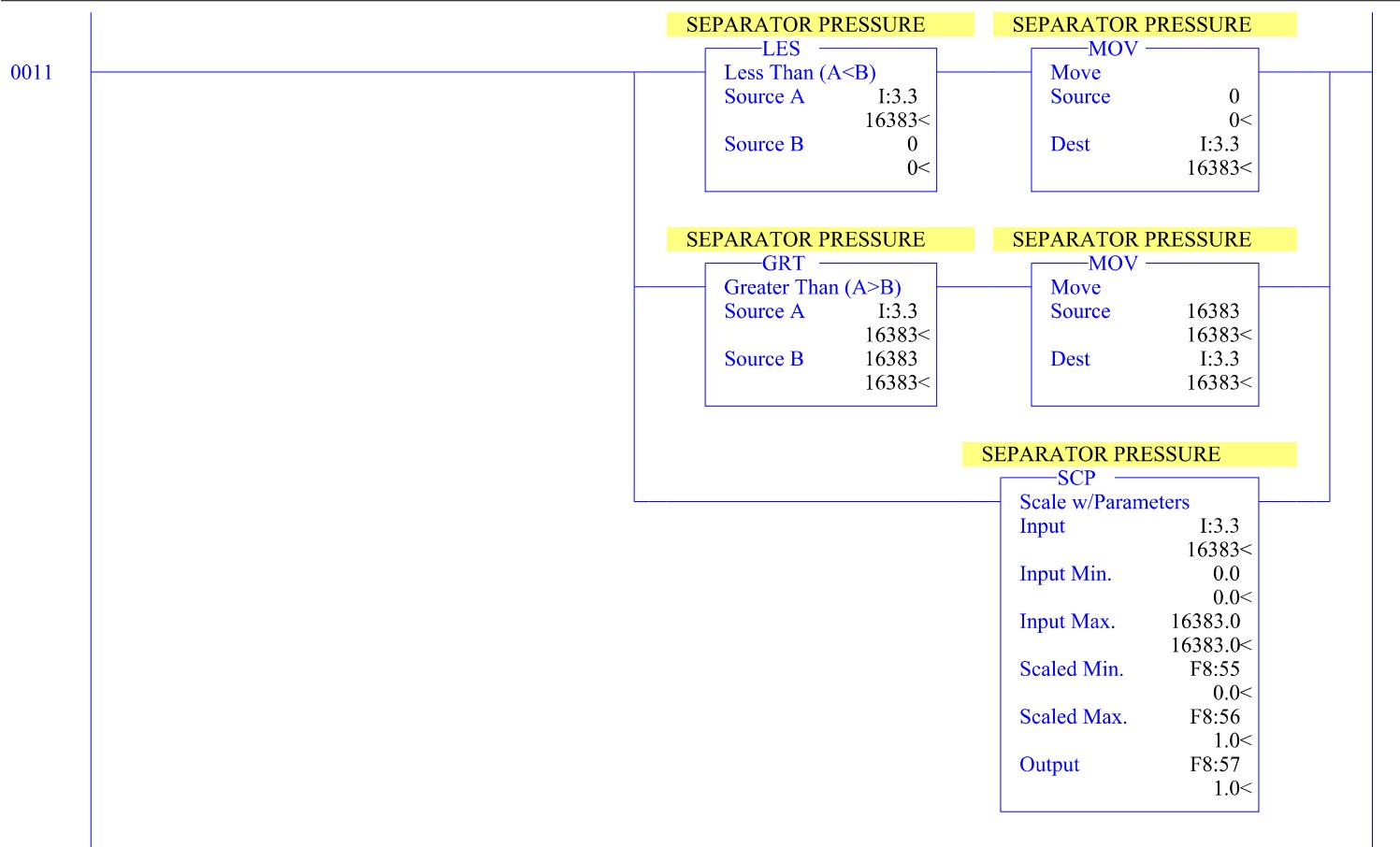
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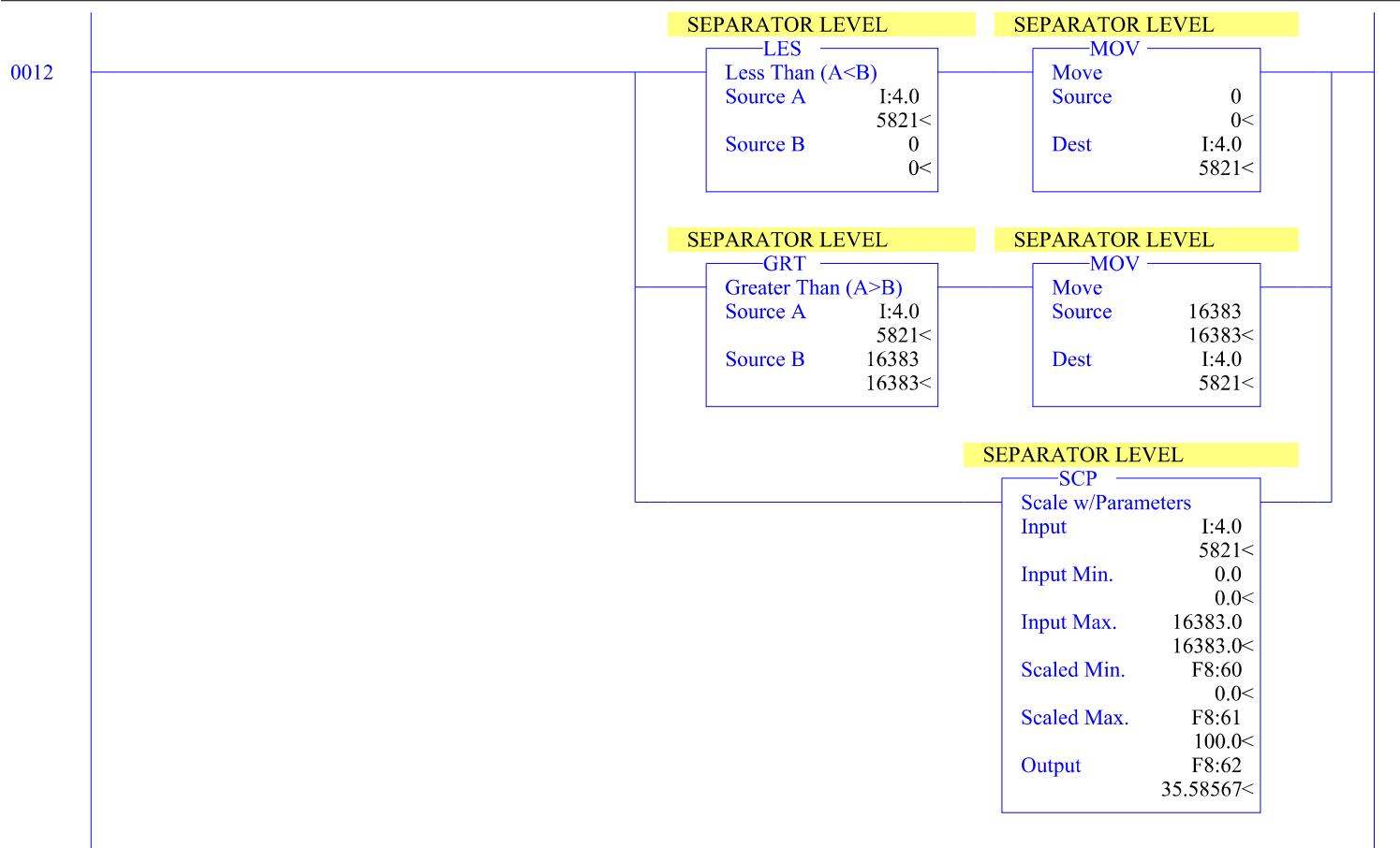
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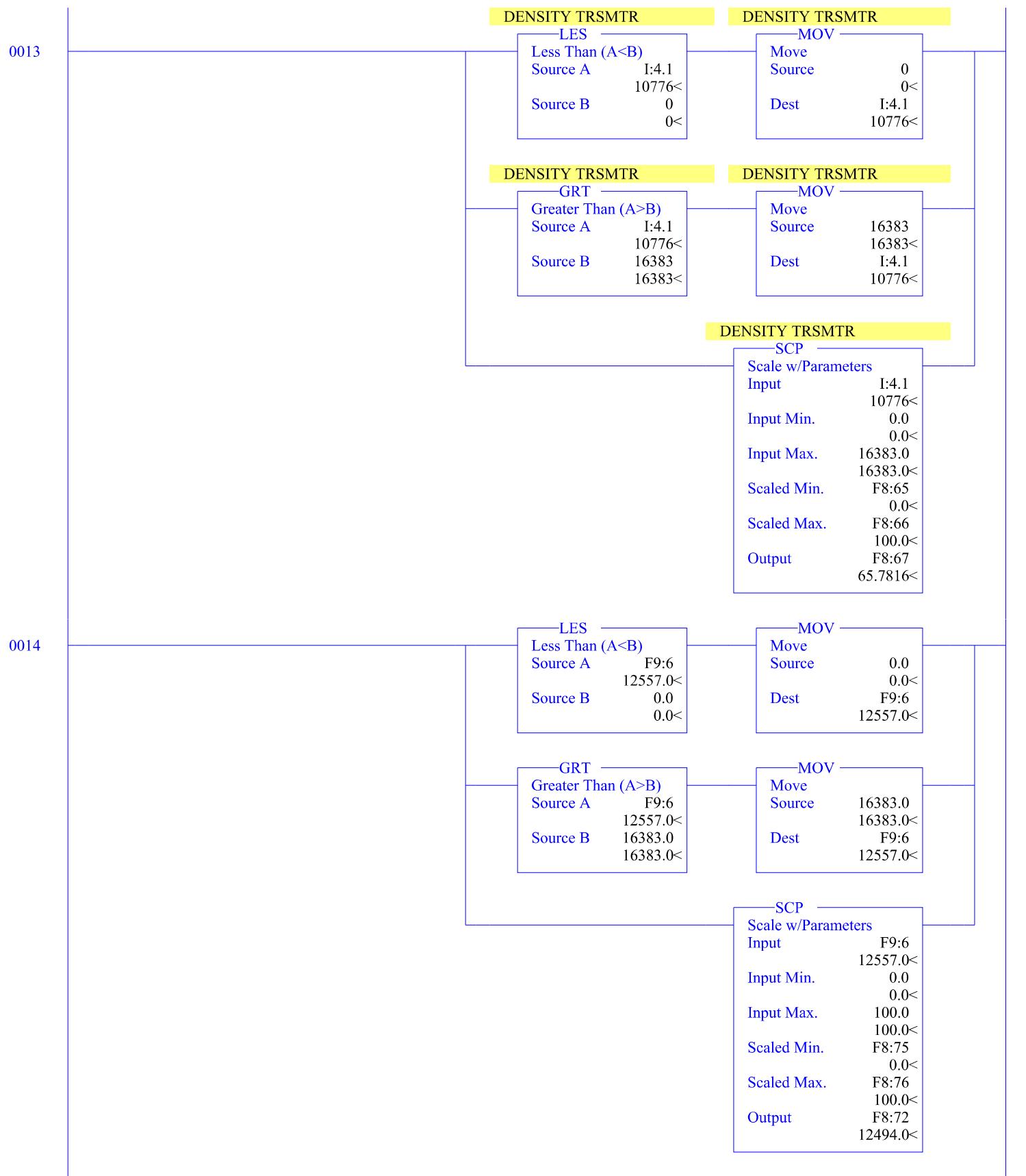
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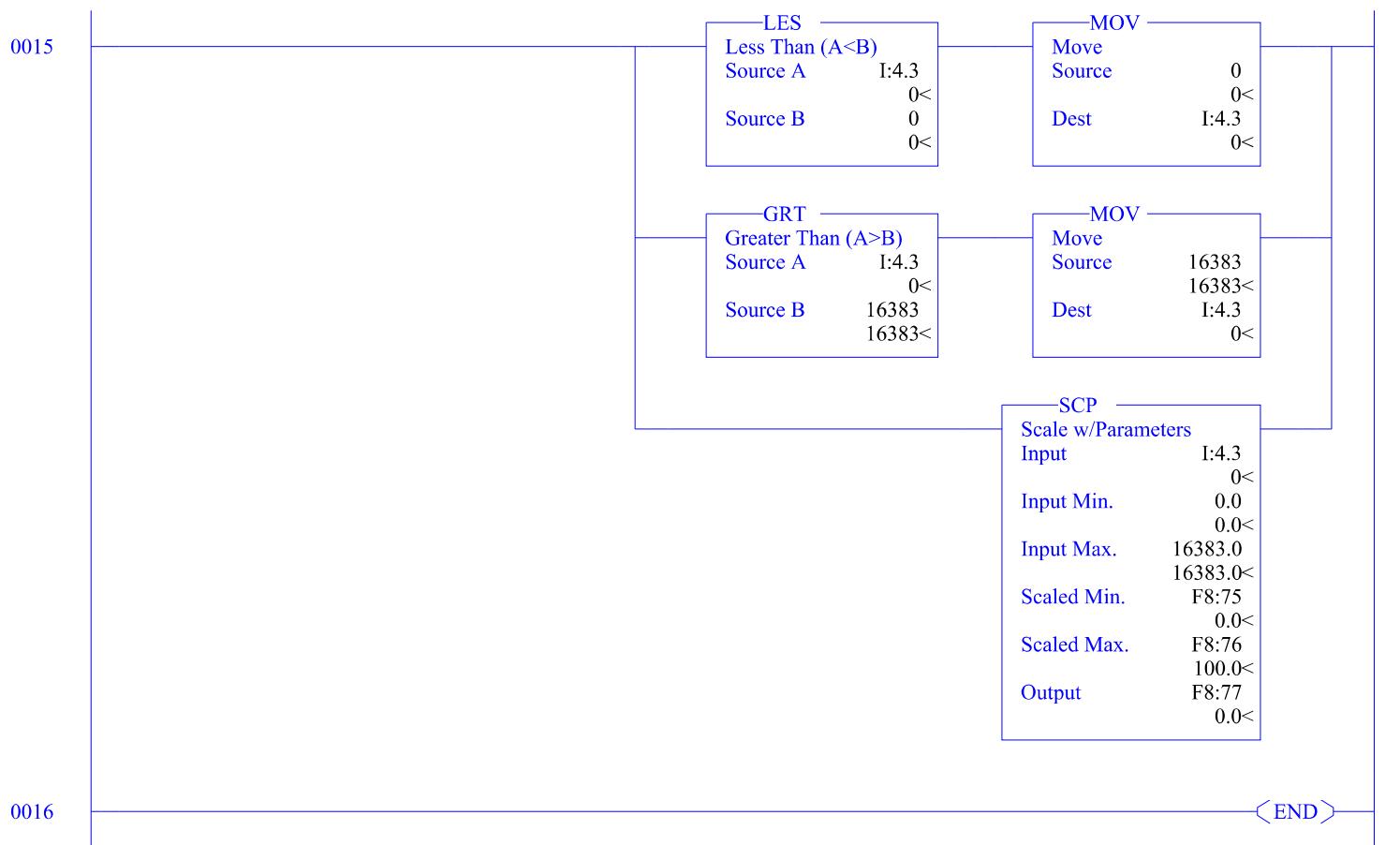
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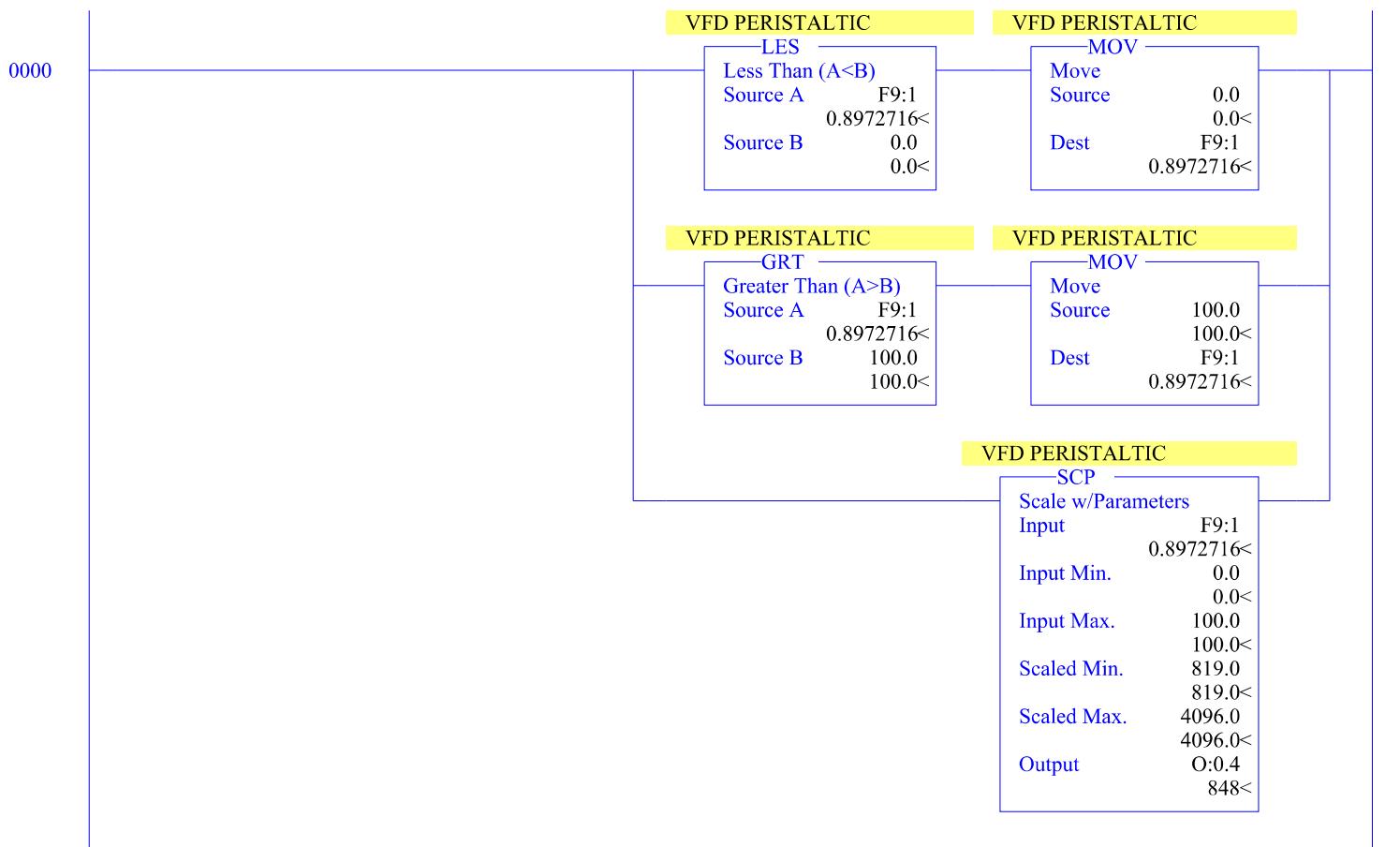
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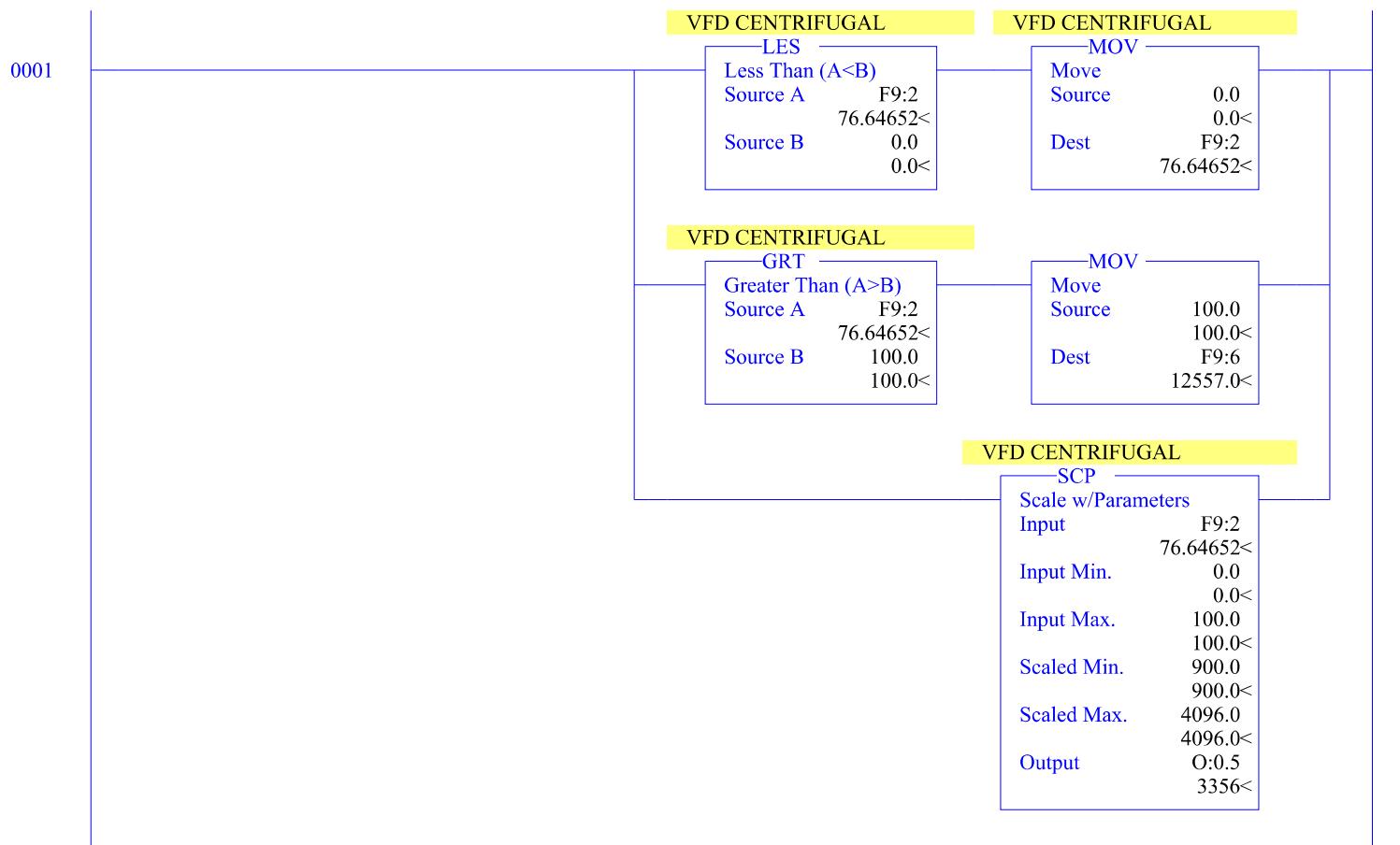
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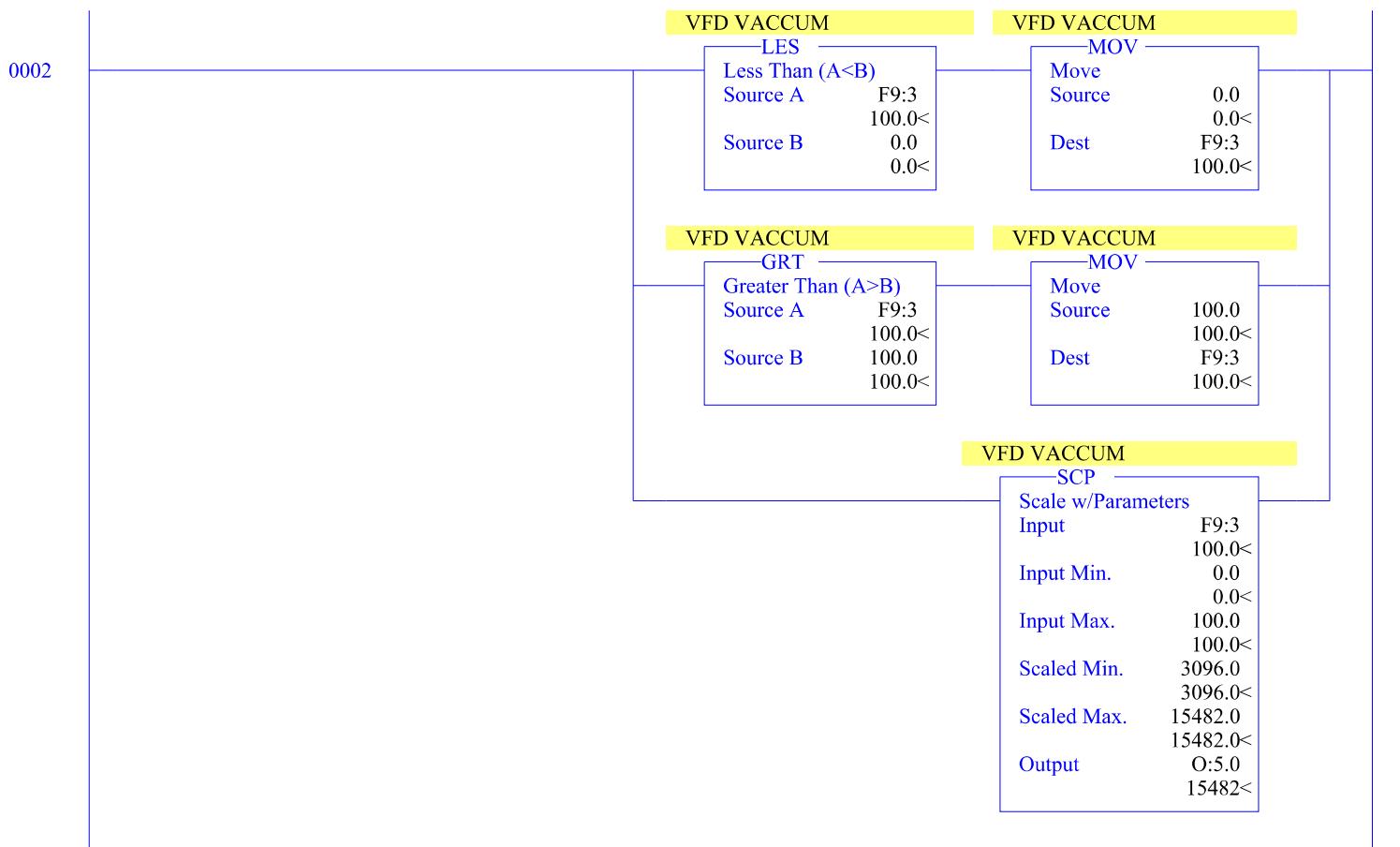
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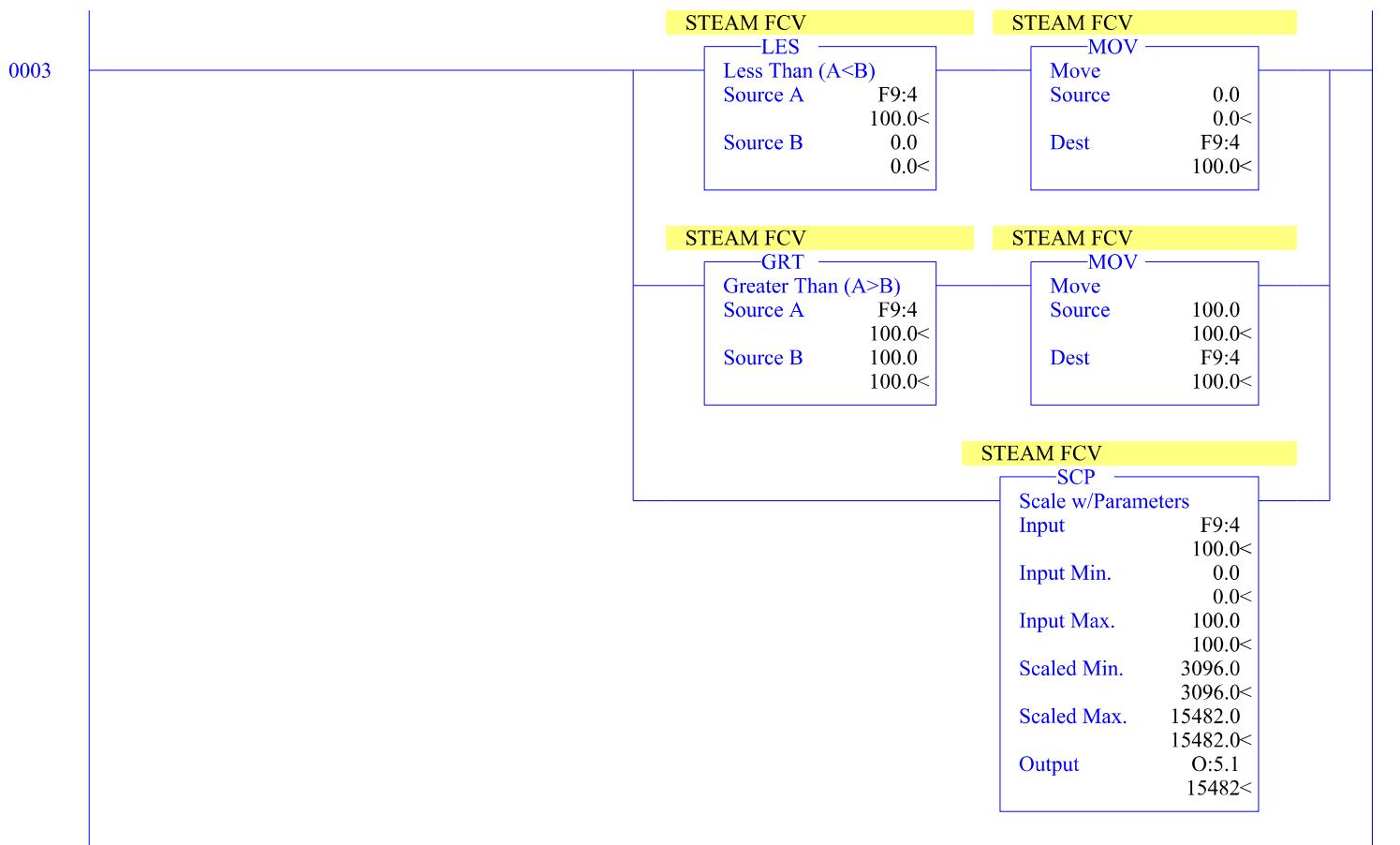
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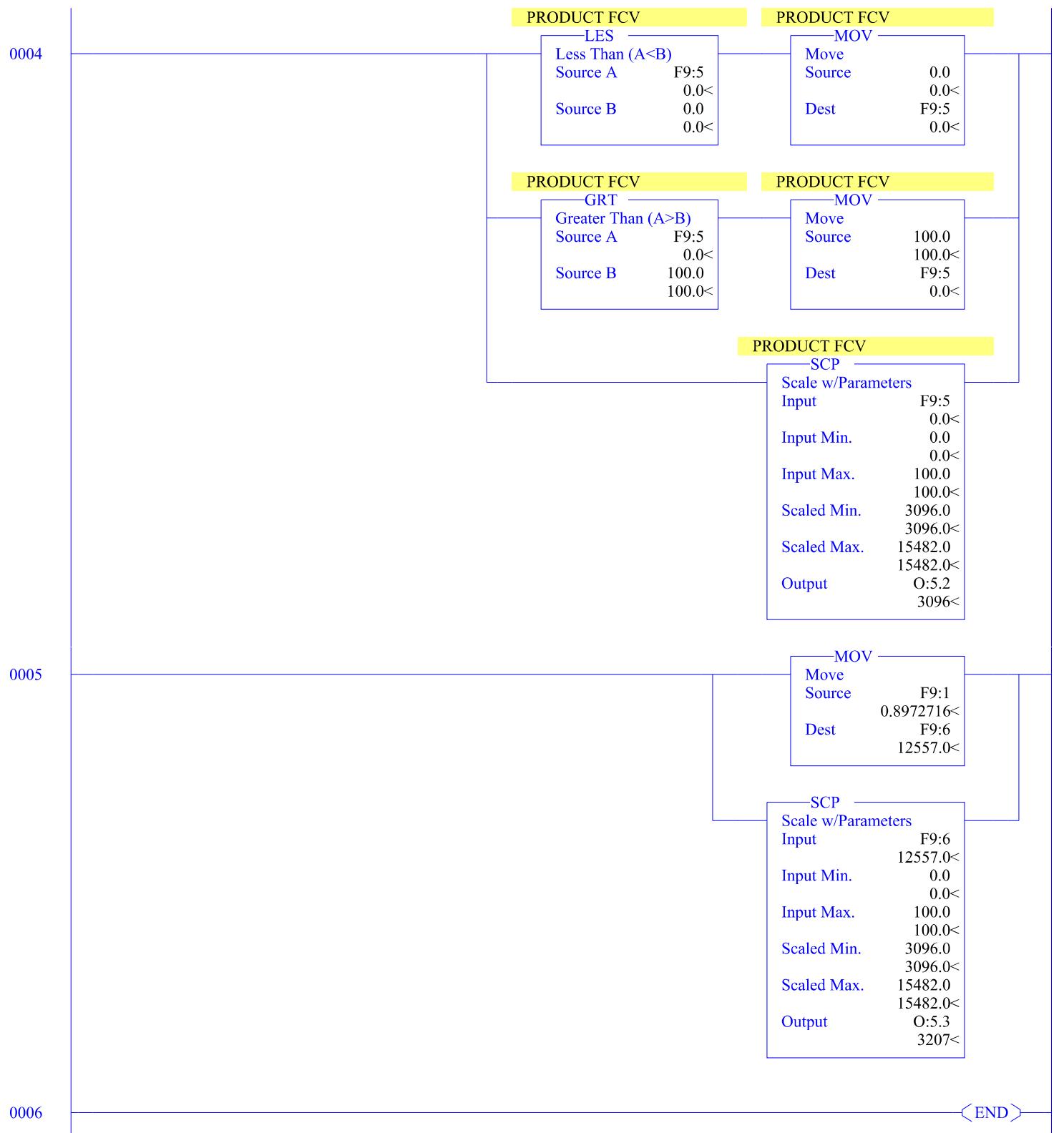
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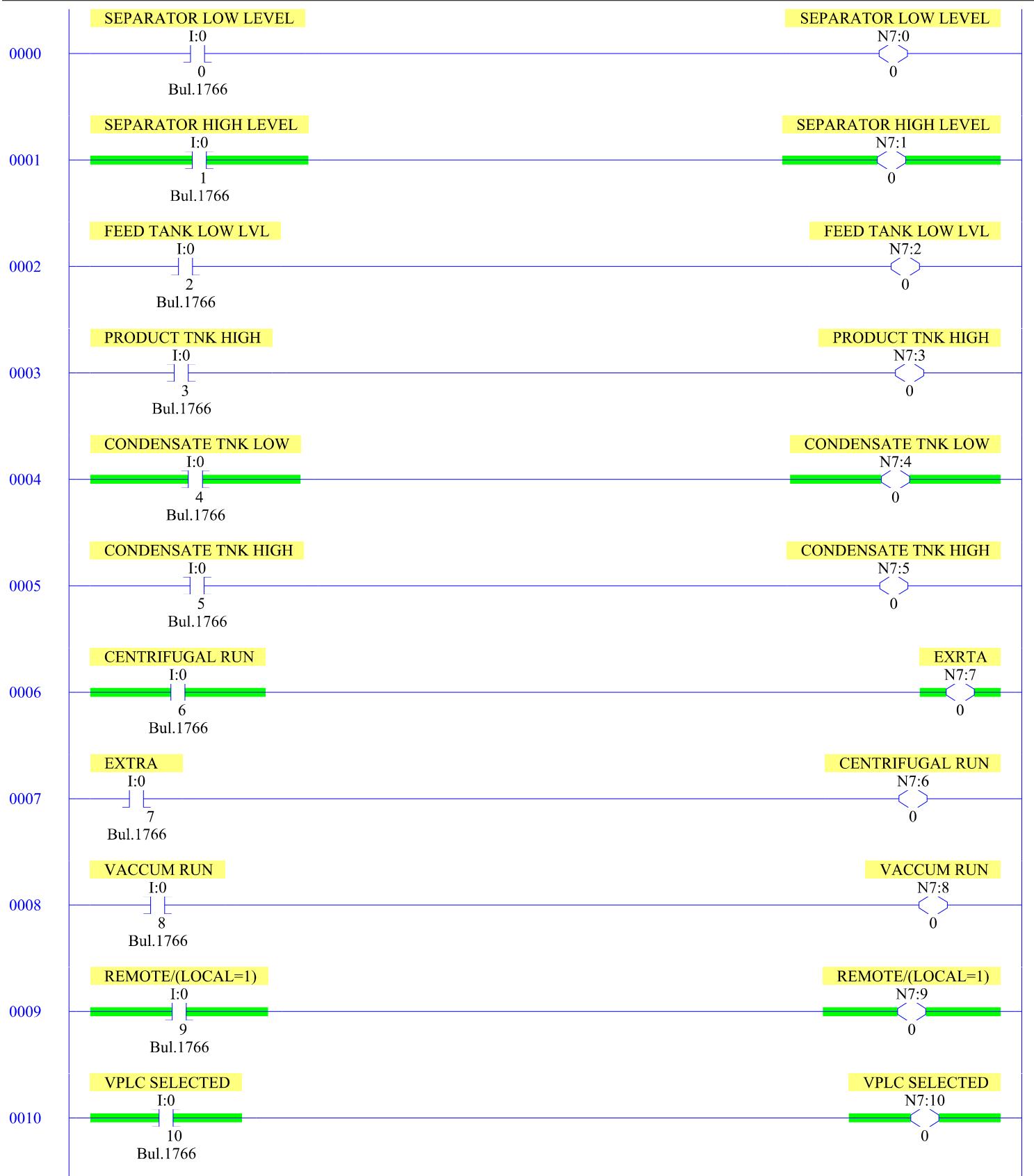
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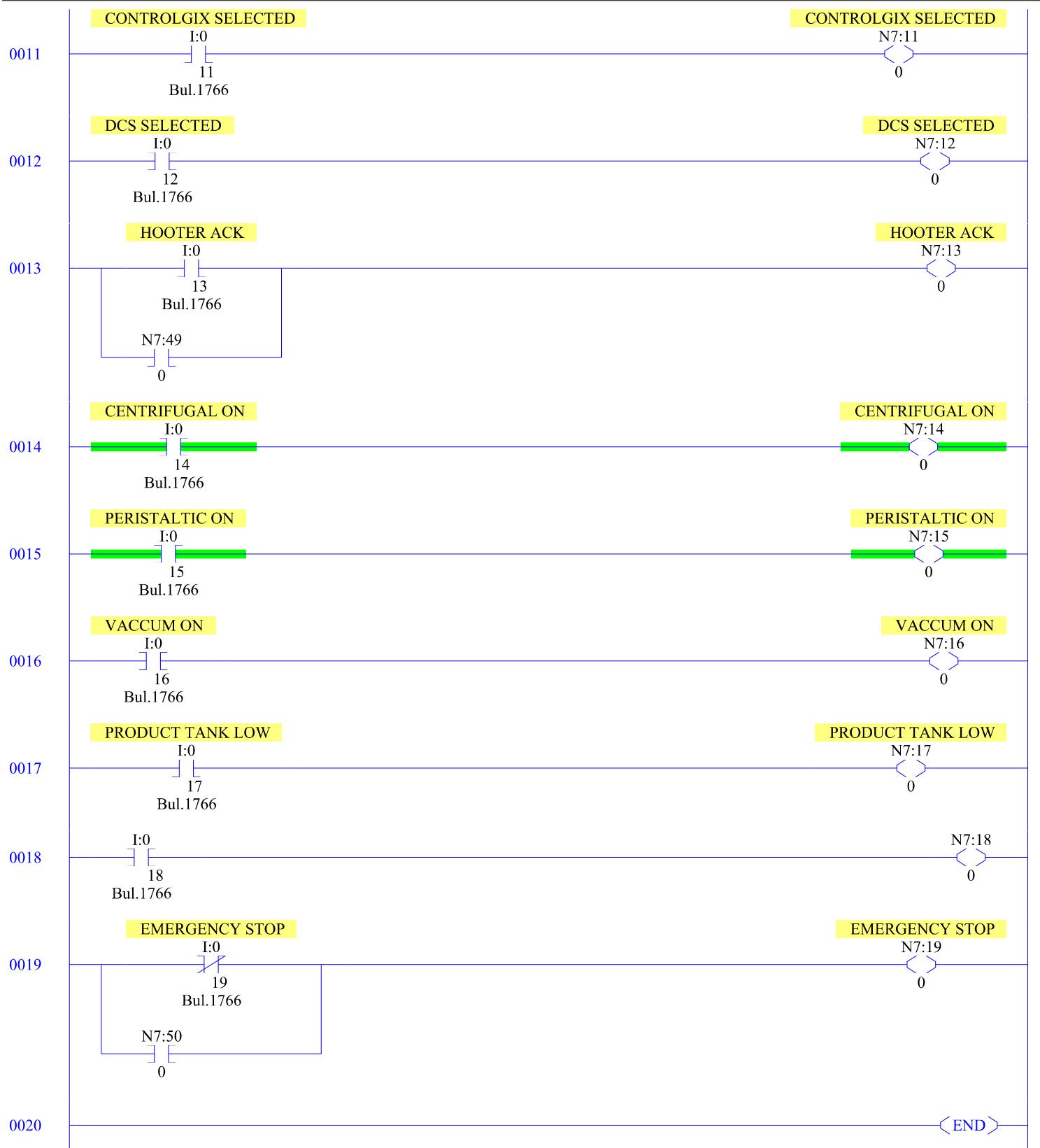


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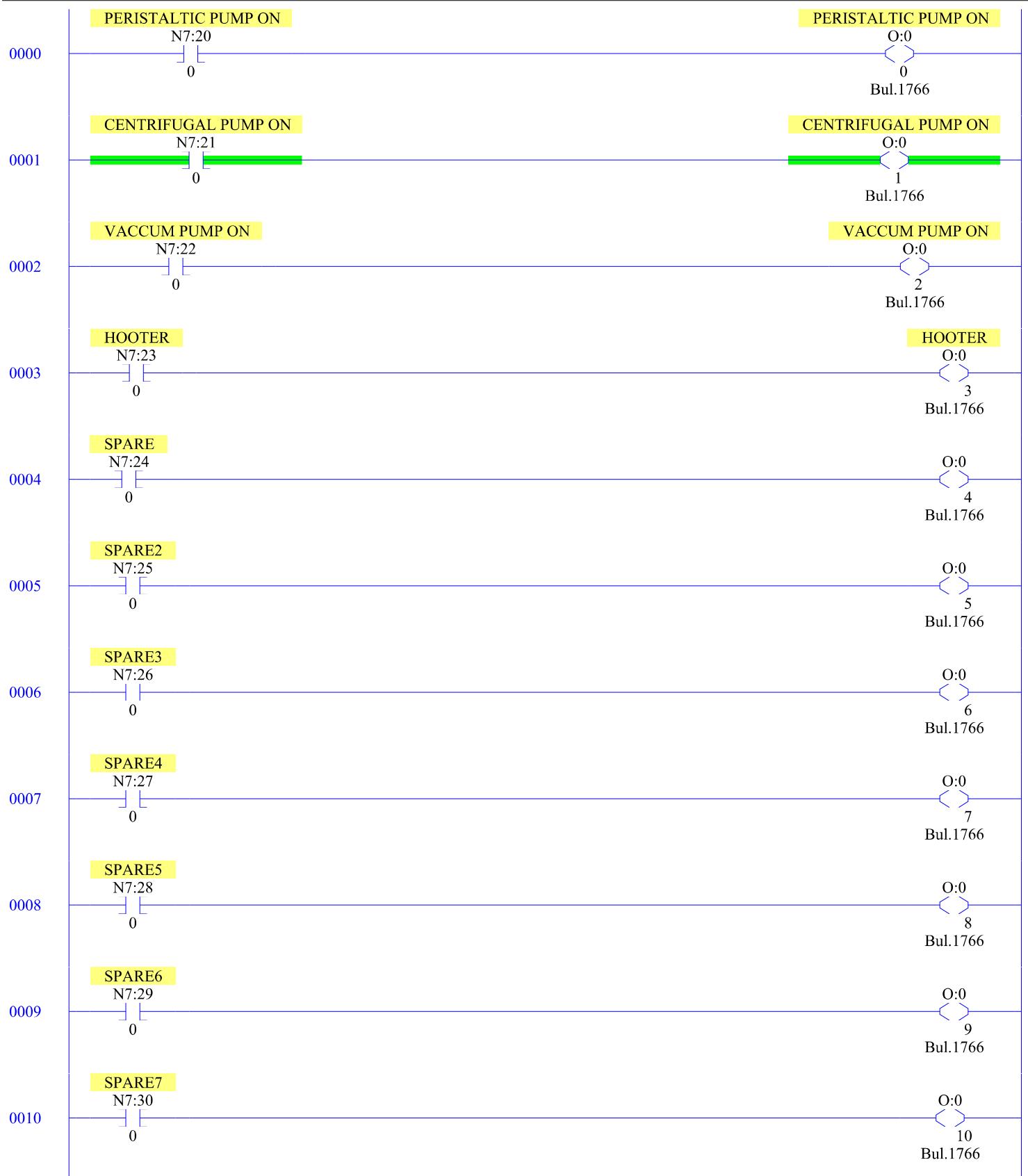


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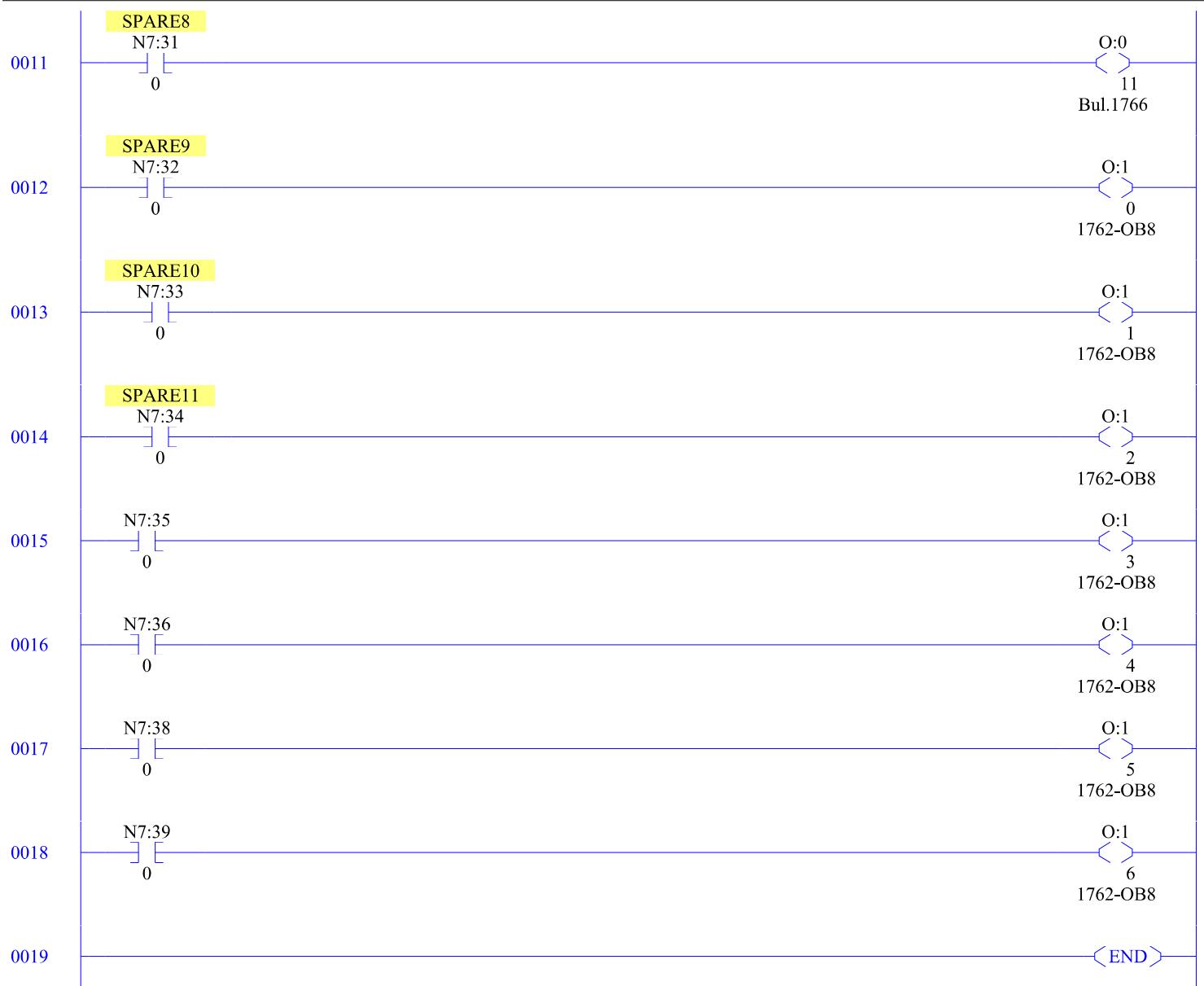




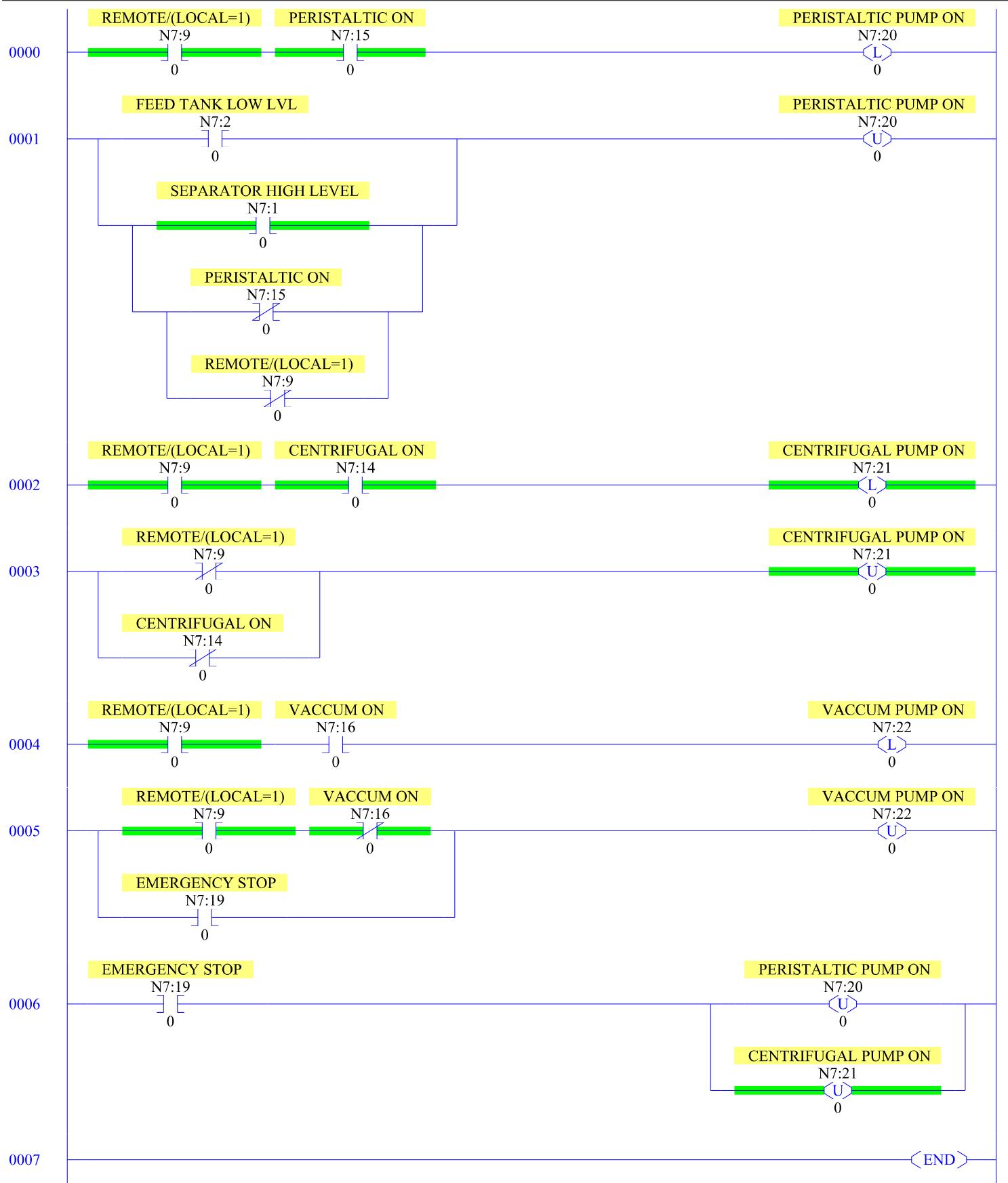
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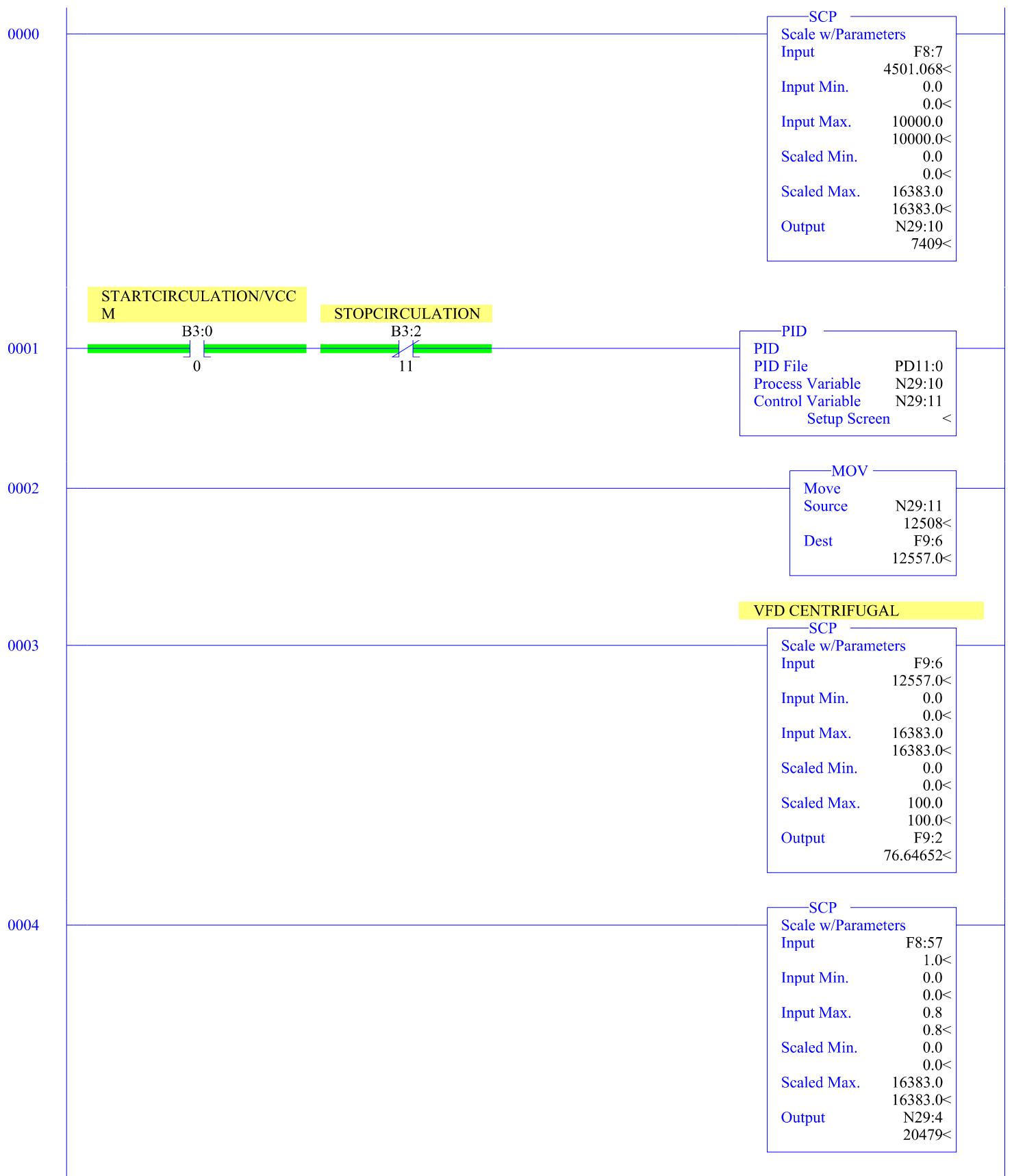


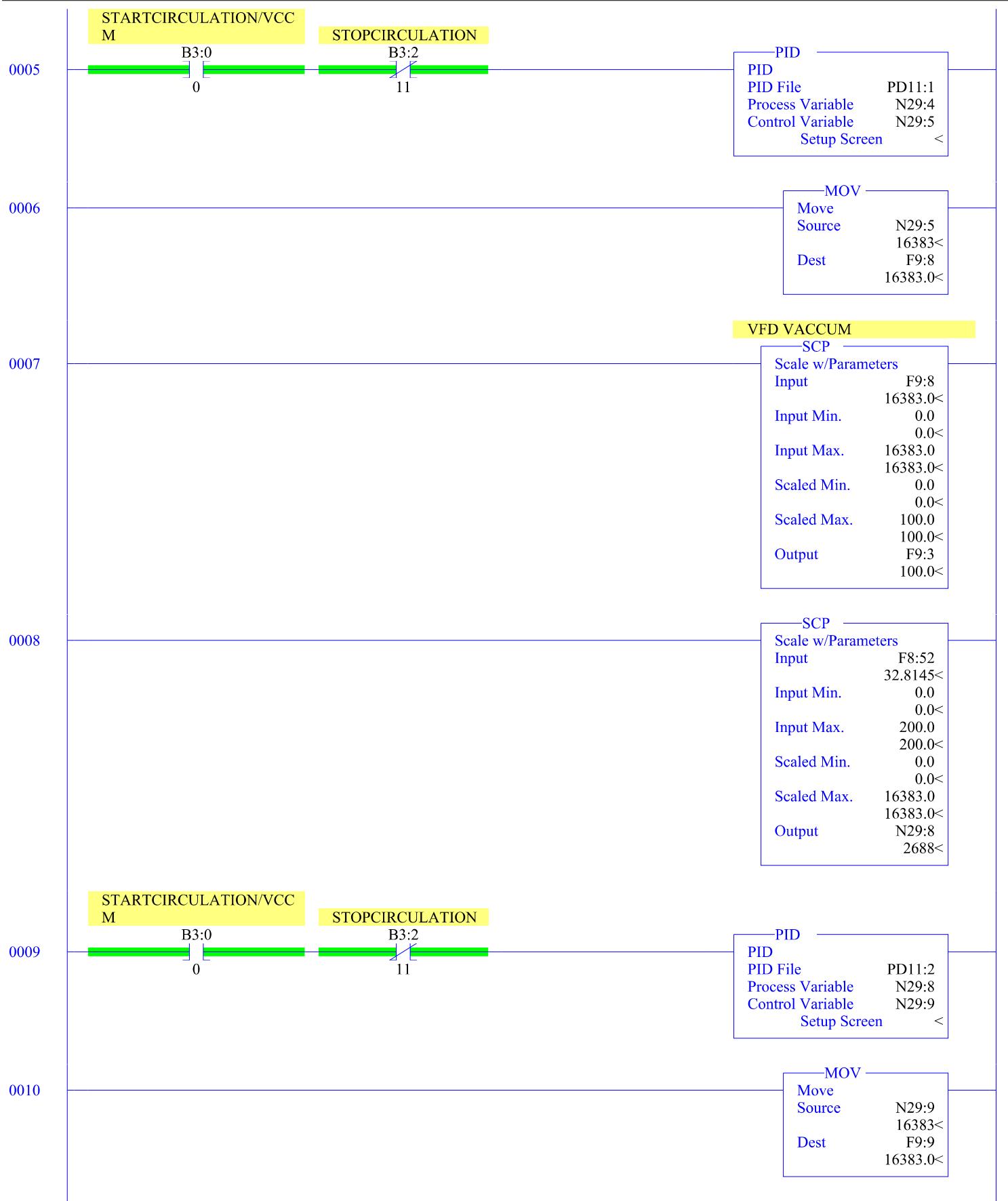
LAD 6 - --- Total Rungs in File = 20



LAD 7 - --- Total Rungs in File = 8

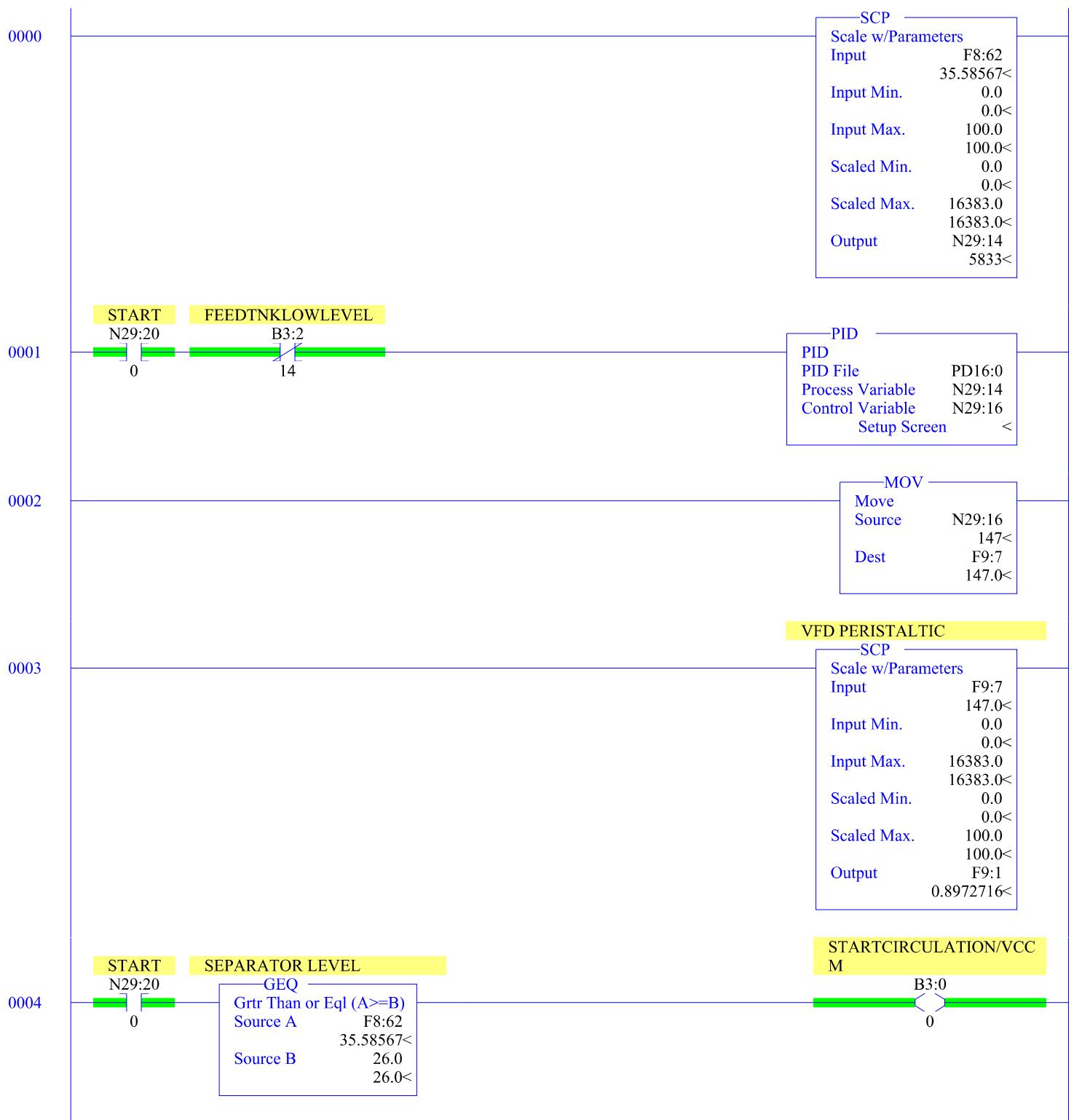


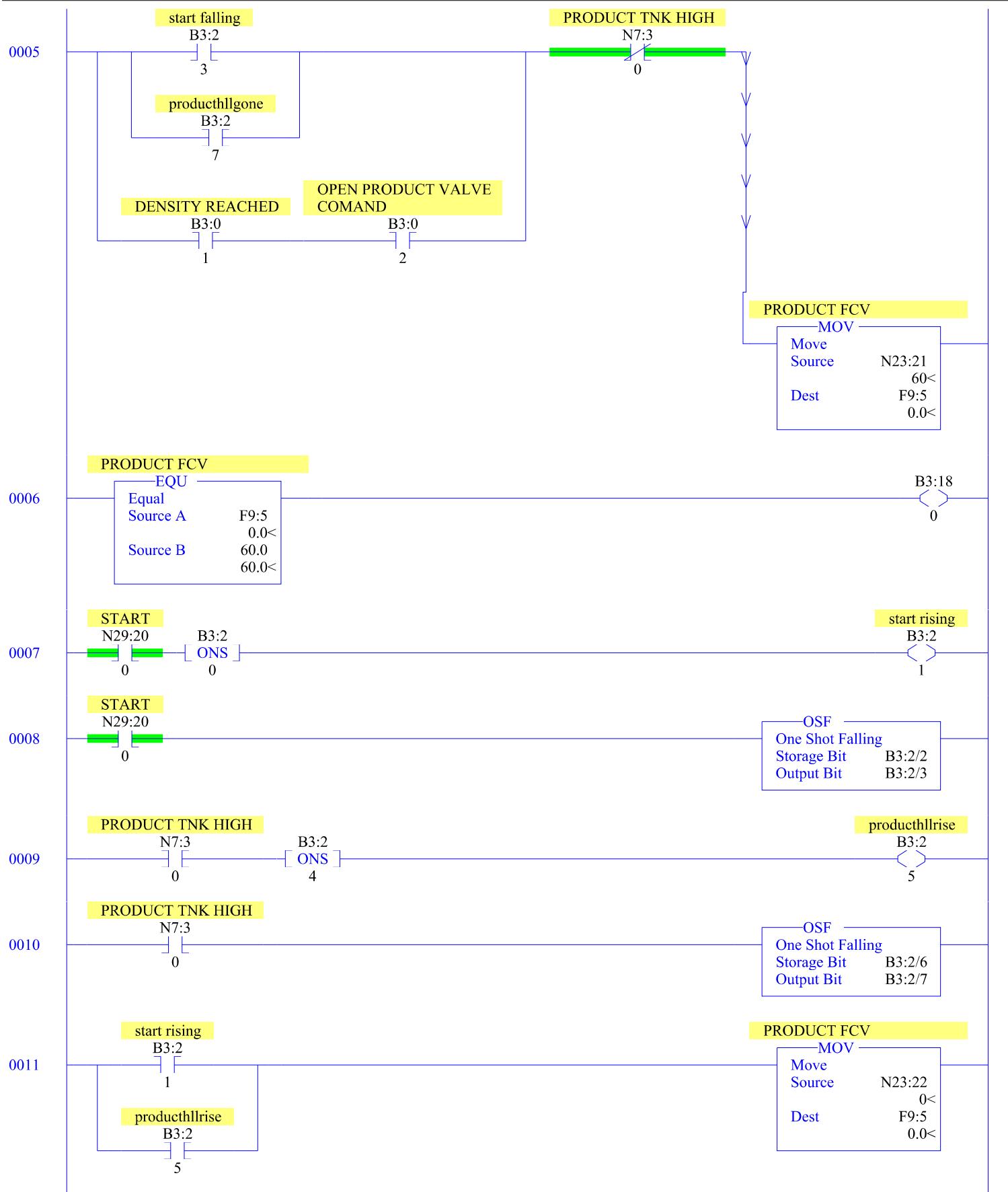


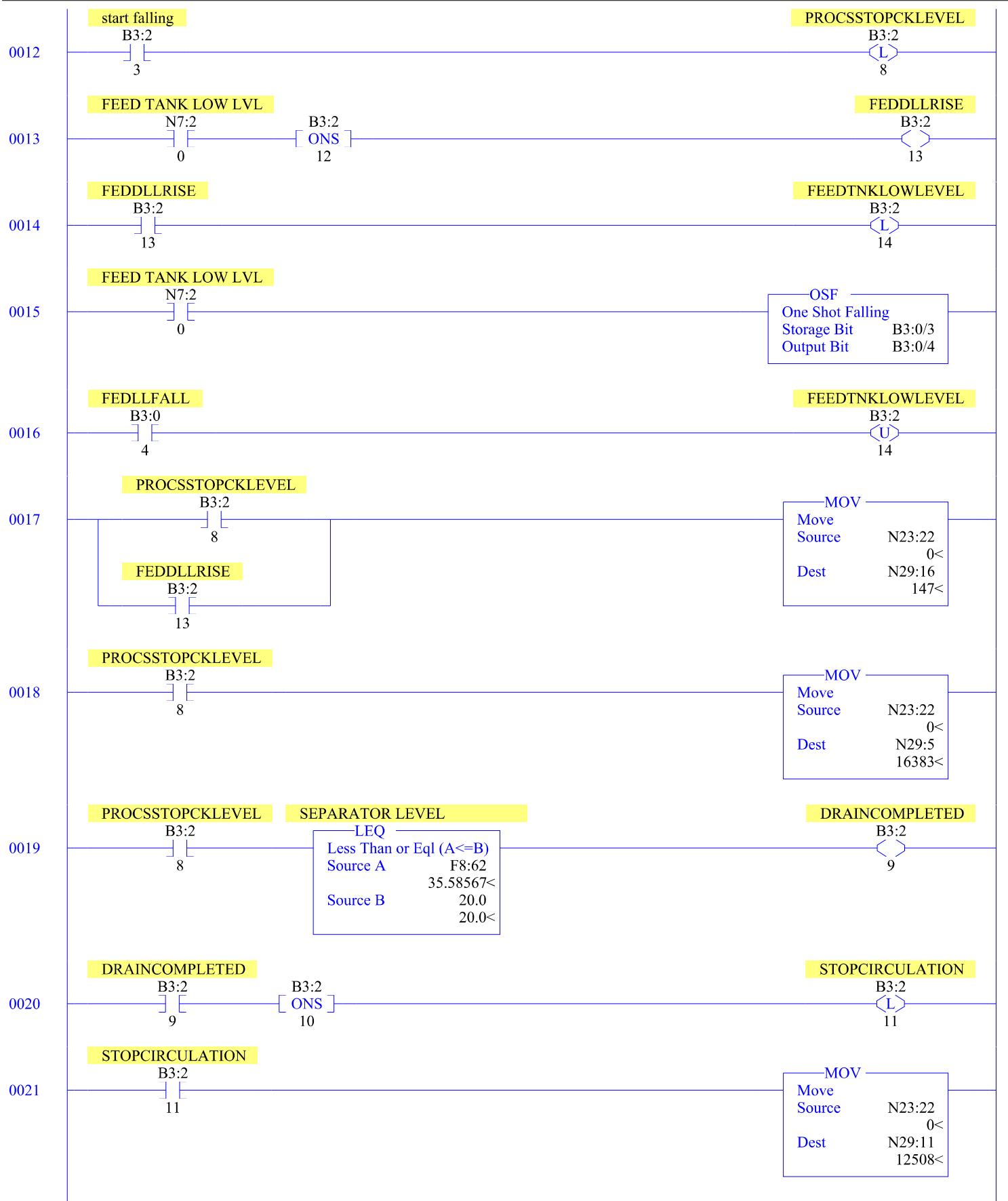


LAD 8 - --- Total Rungs in File = 13





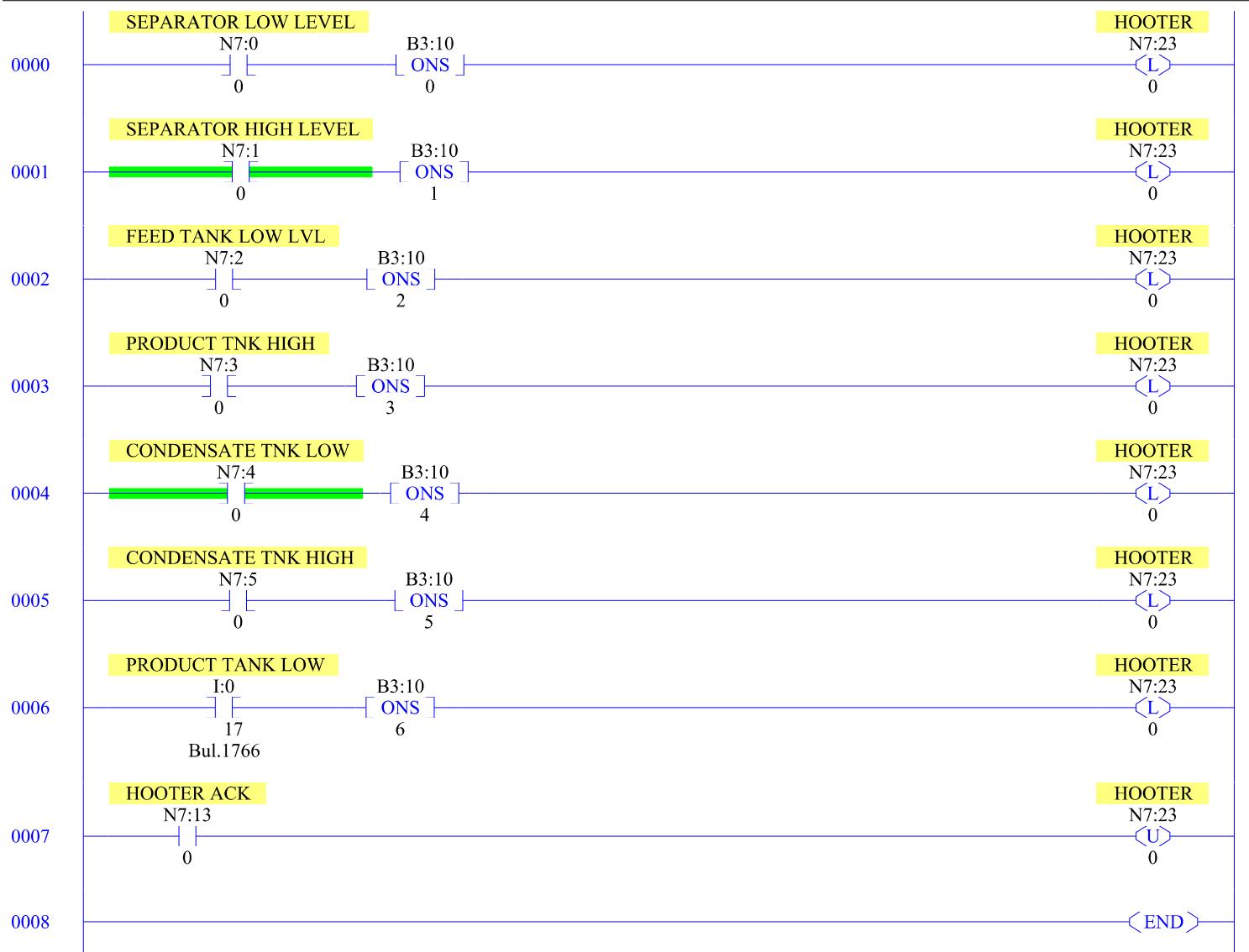




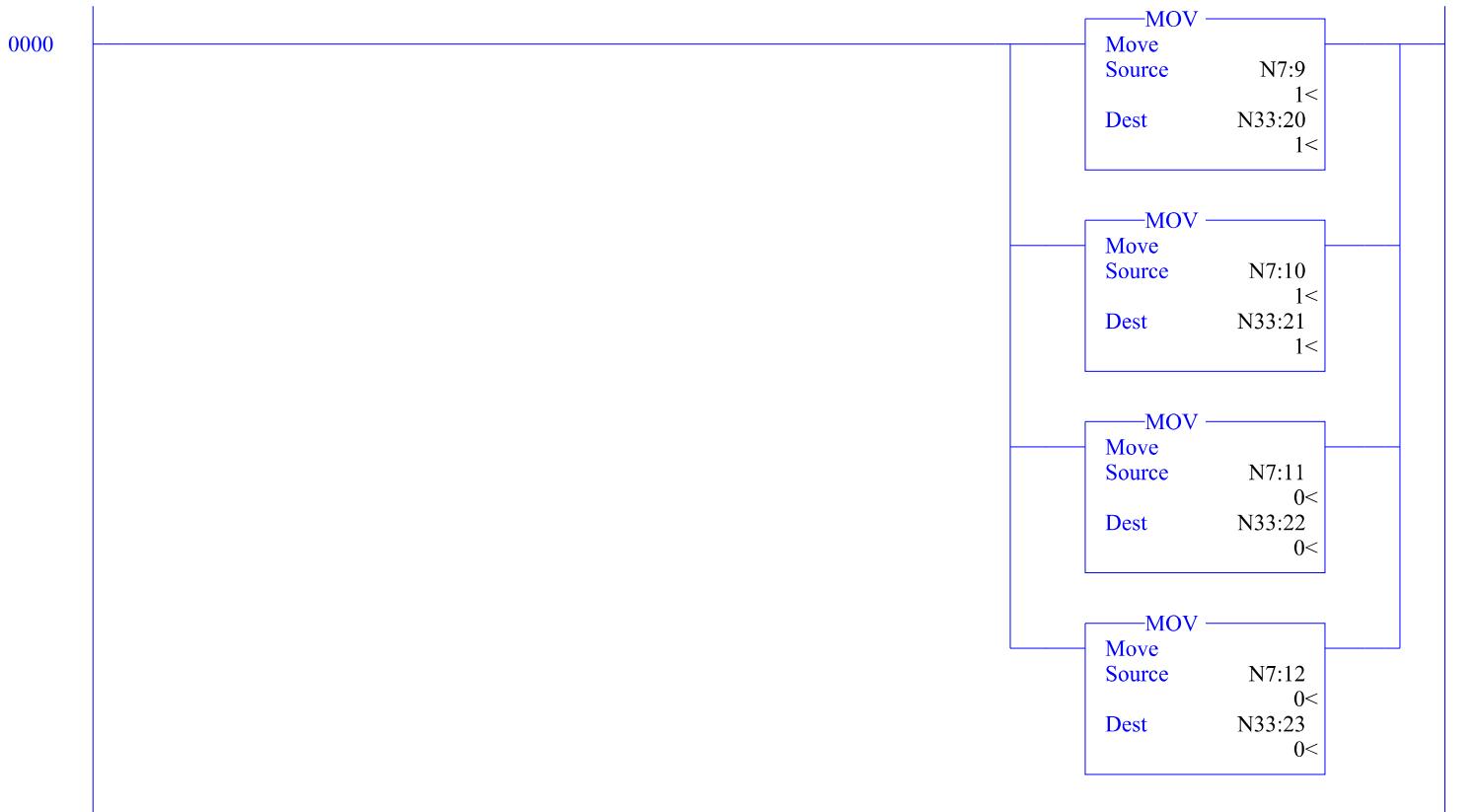
LAD 9 - --- Total Rungs in File = 26



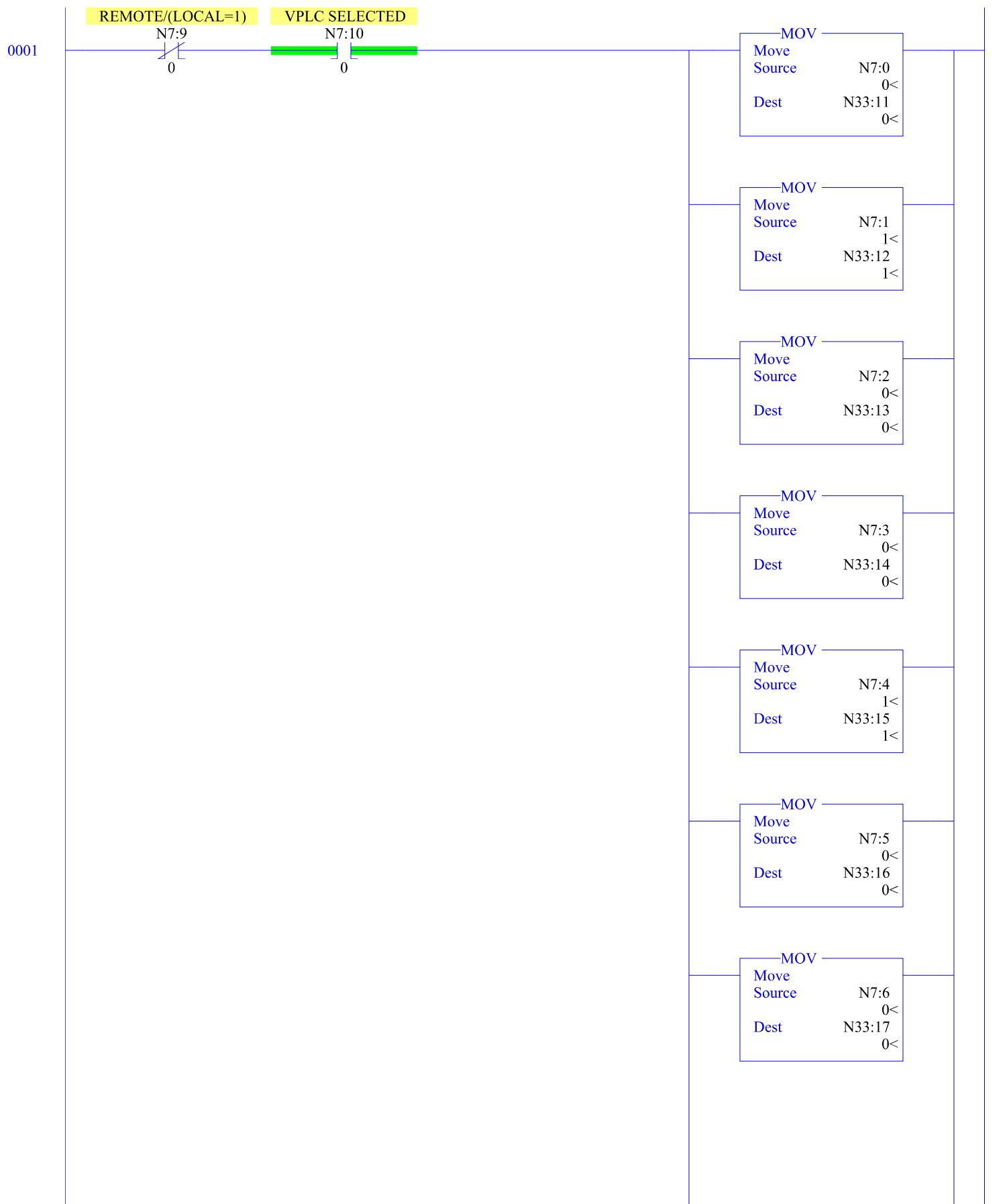
LAD 11 - --- Total Rungs in File = 9

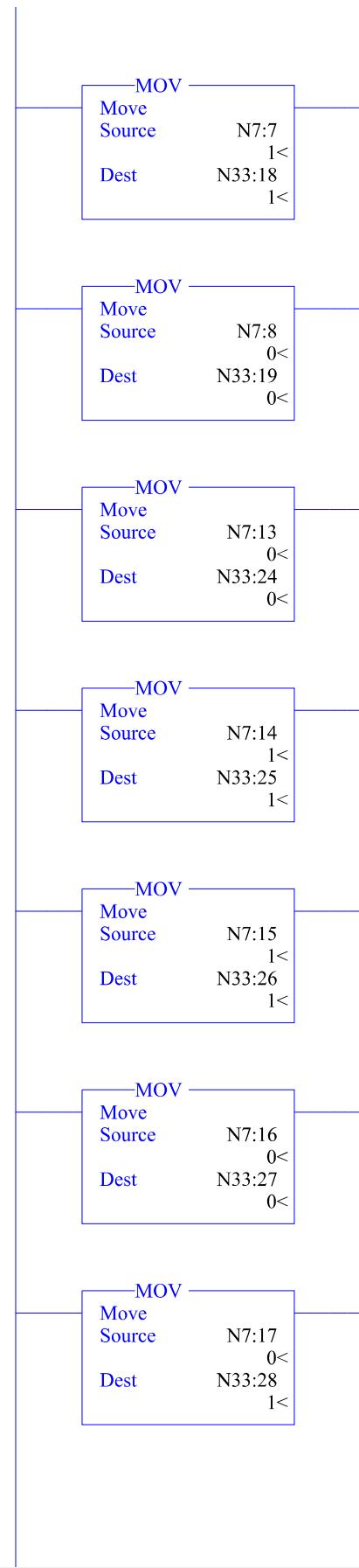


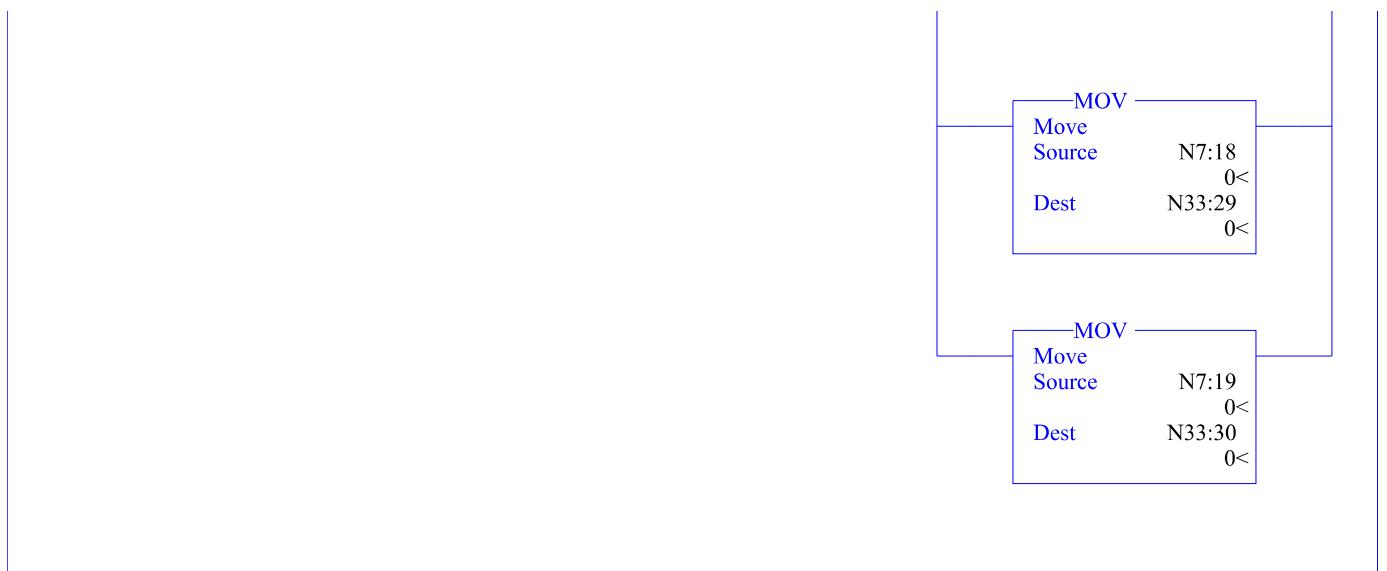
LAD 12 - --- Total Rungs in File = 14



LAD 12 - --- Total Rungs in File = 14

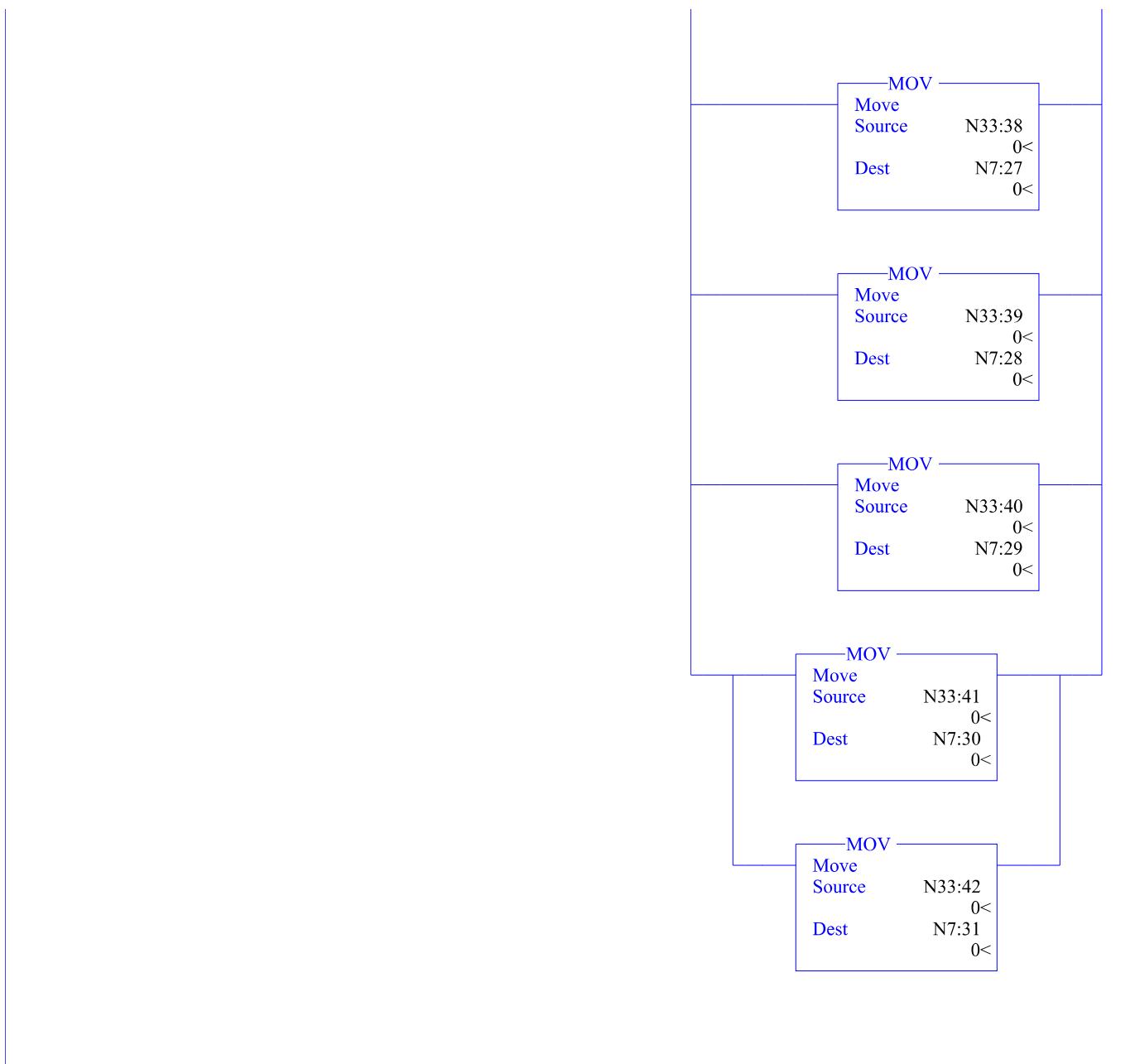




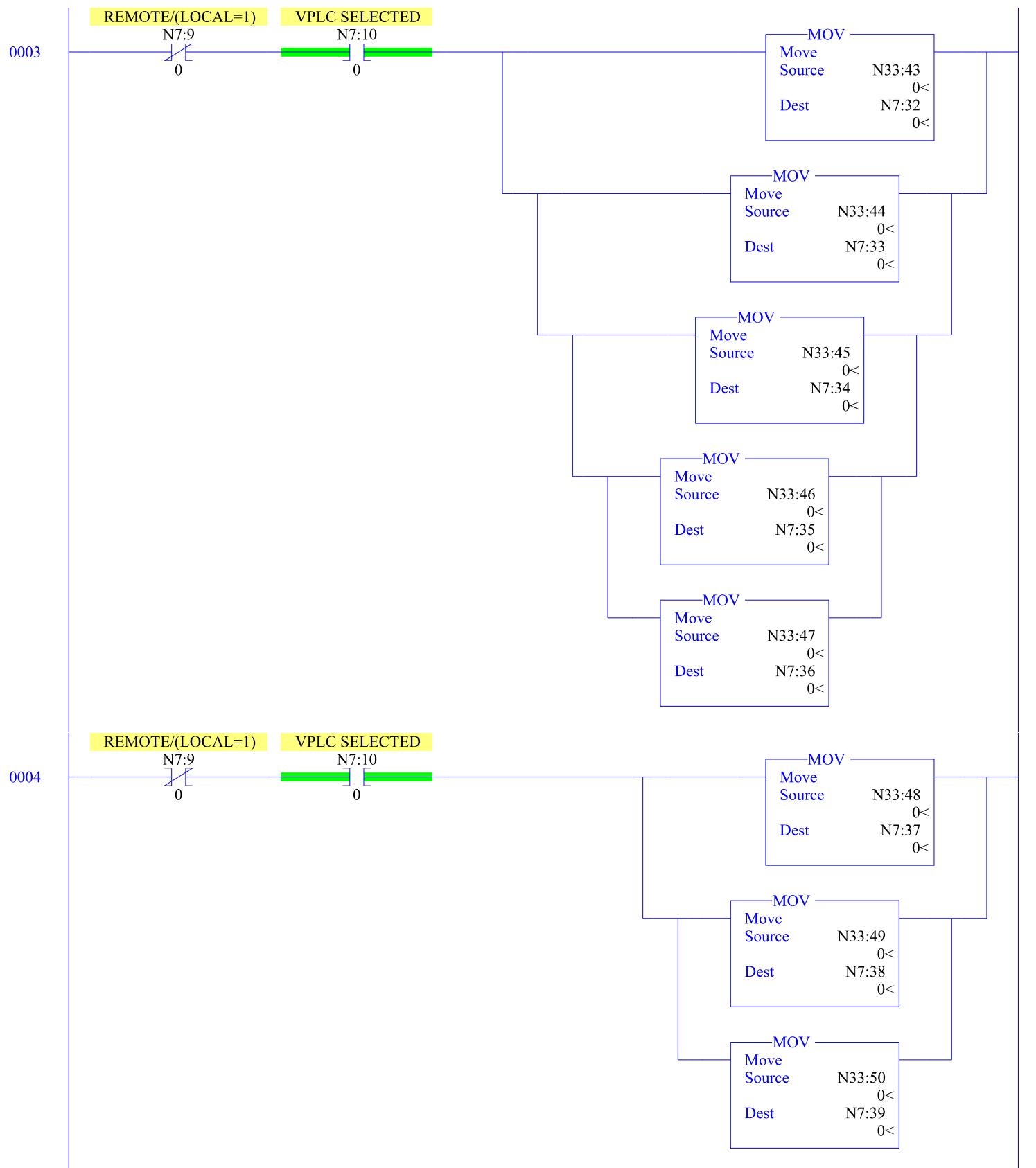


LAD 12 - --- Total Rungs in File = 14

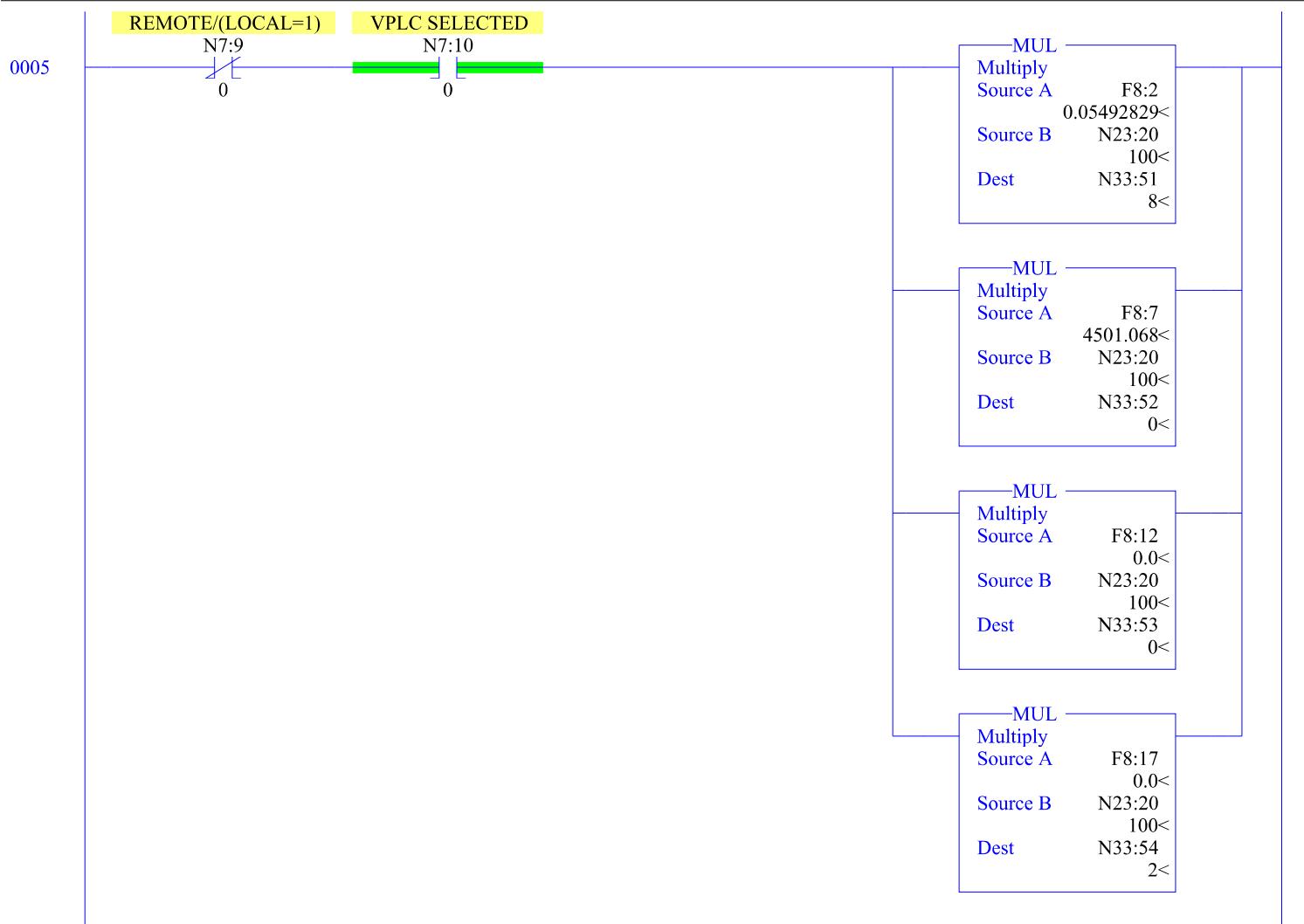




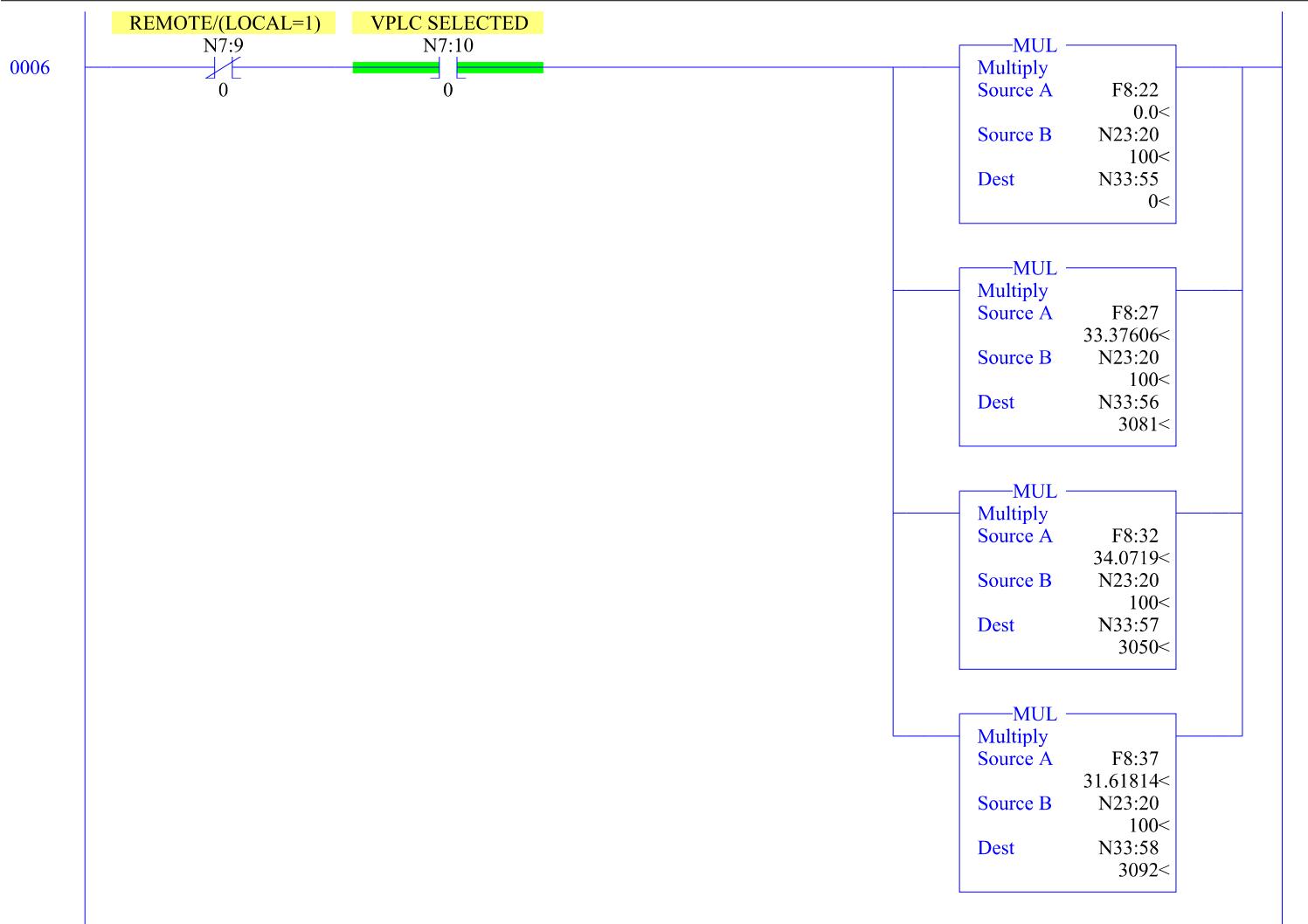
LAD 12 - --- Total Rungs in File = 14



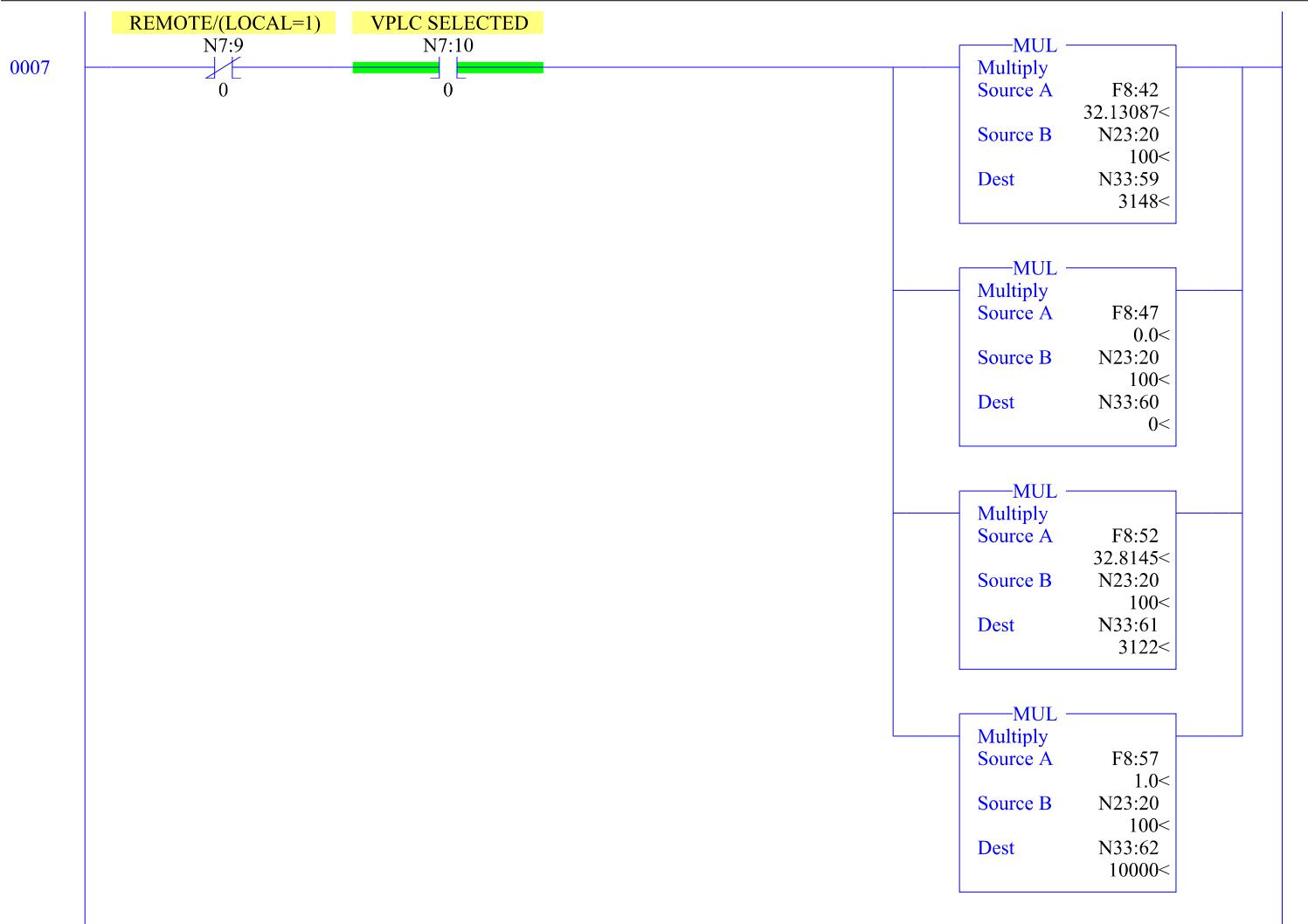
LAD 12 - --- Total Rungs in File = 14

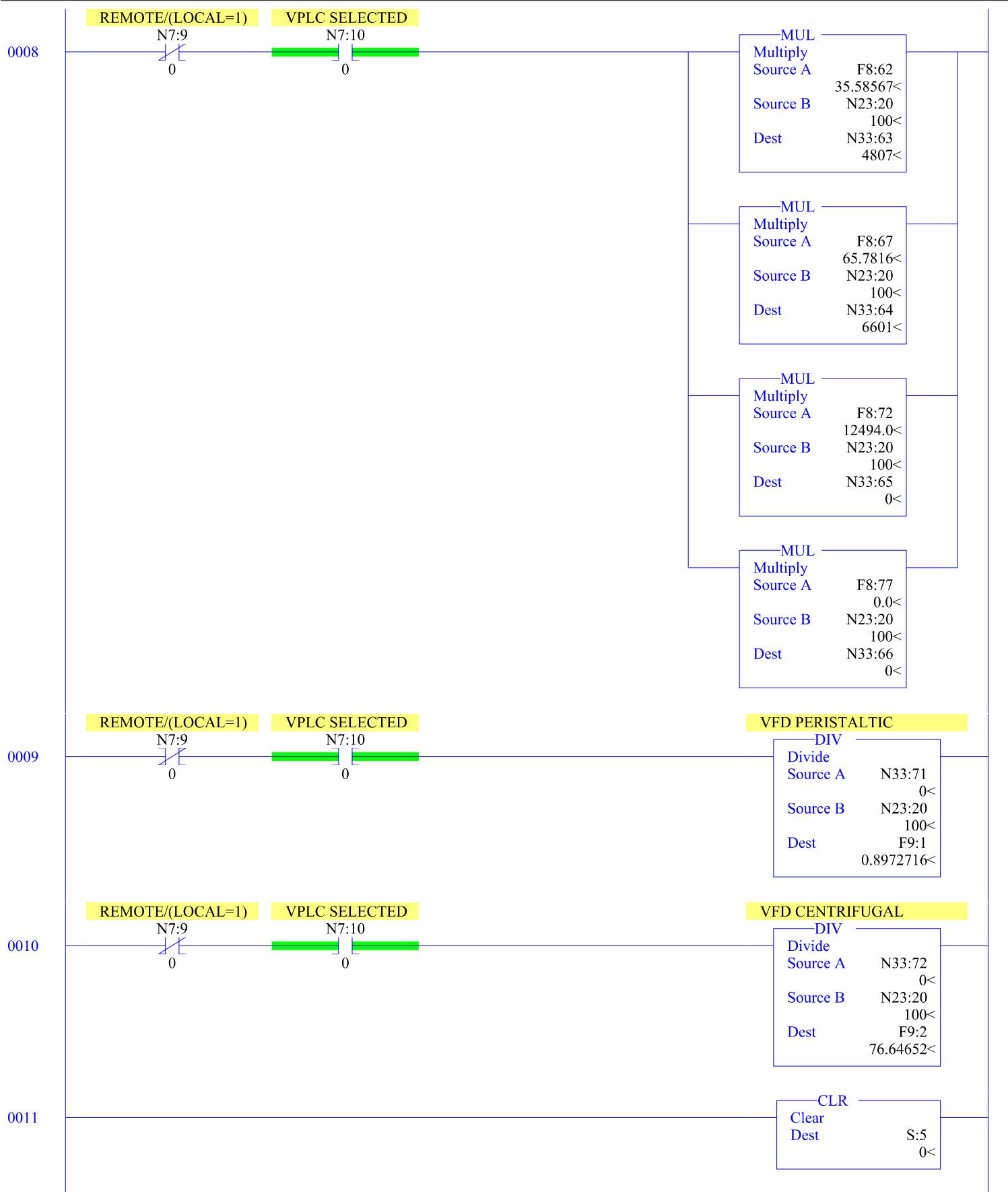


LAD 12 - --- Total Rungs in File = 14

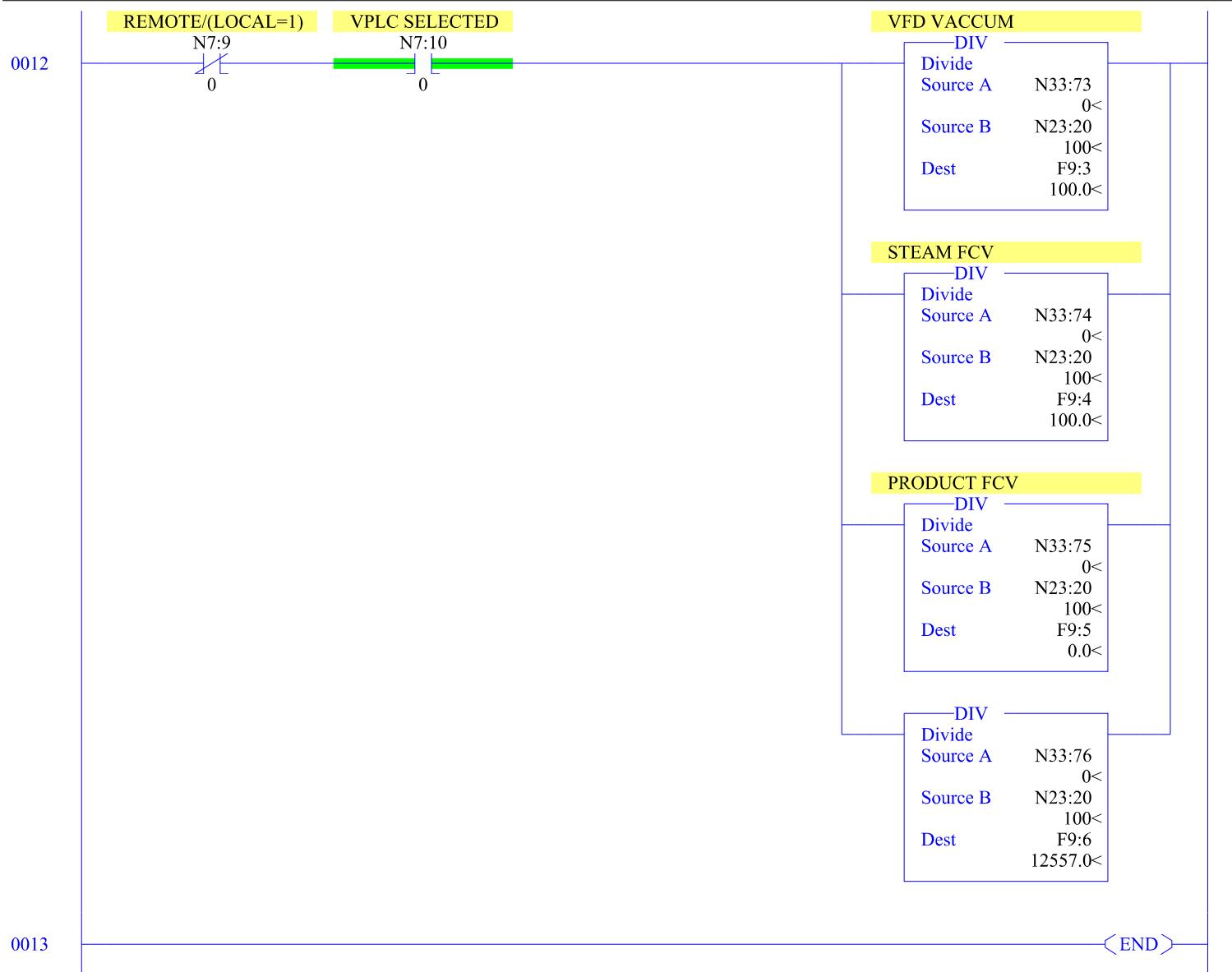


LAD 12 - --- Total Rungs in File = 14

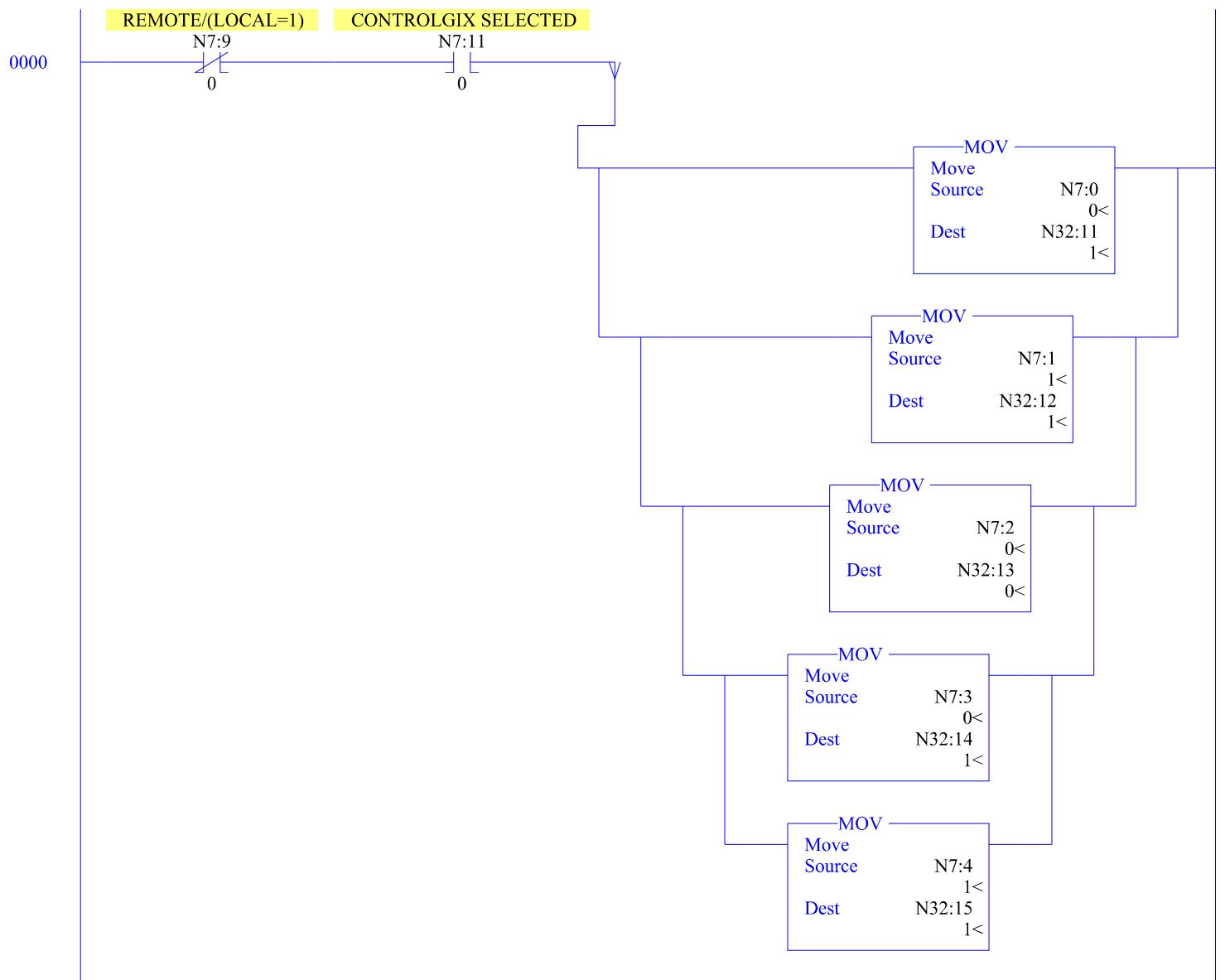




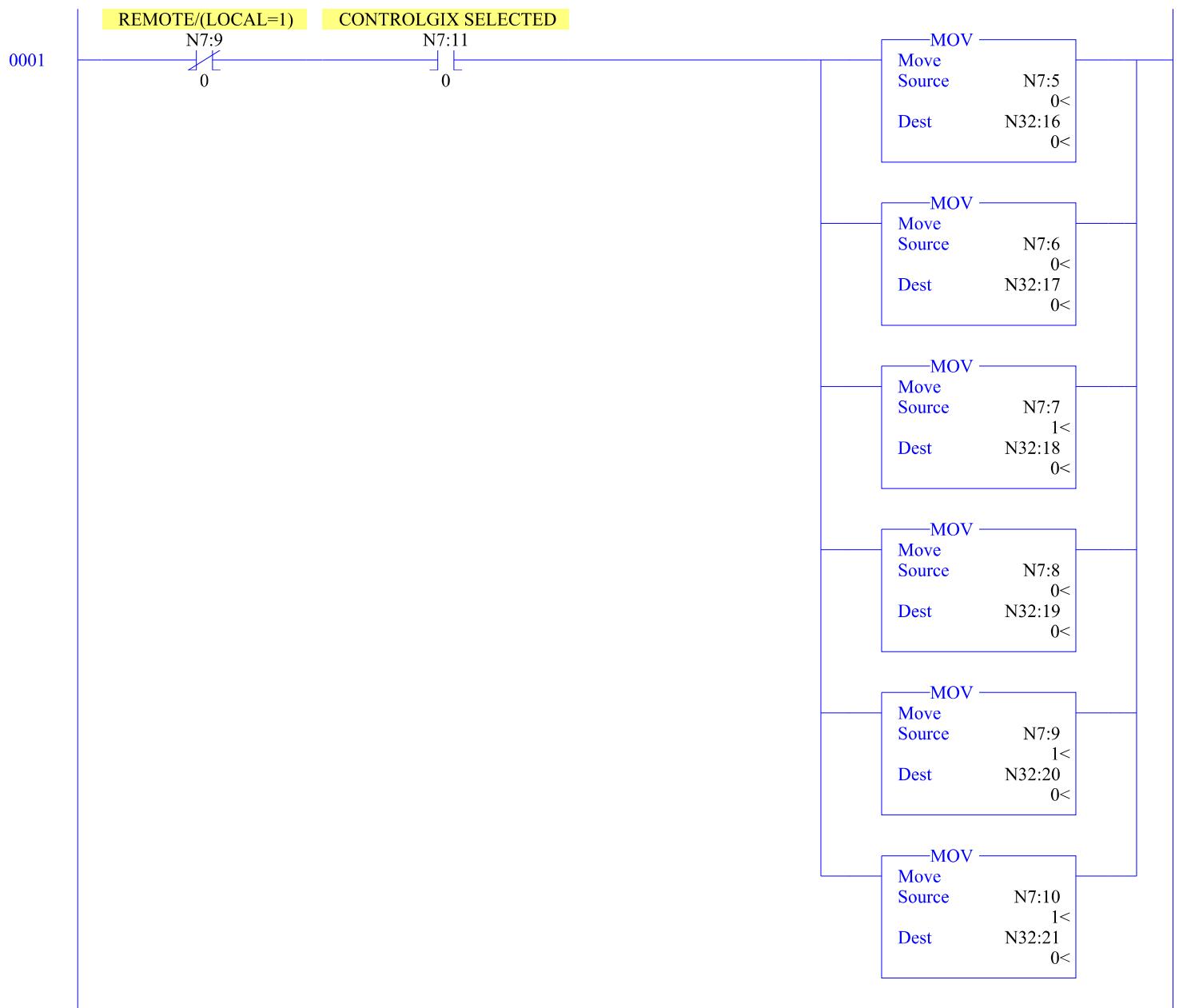
LAD 12 - --- Total Rungs in File = 14



LAD 13 - --- Total Rungs in File = 13



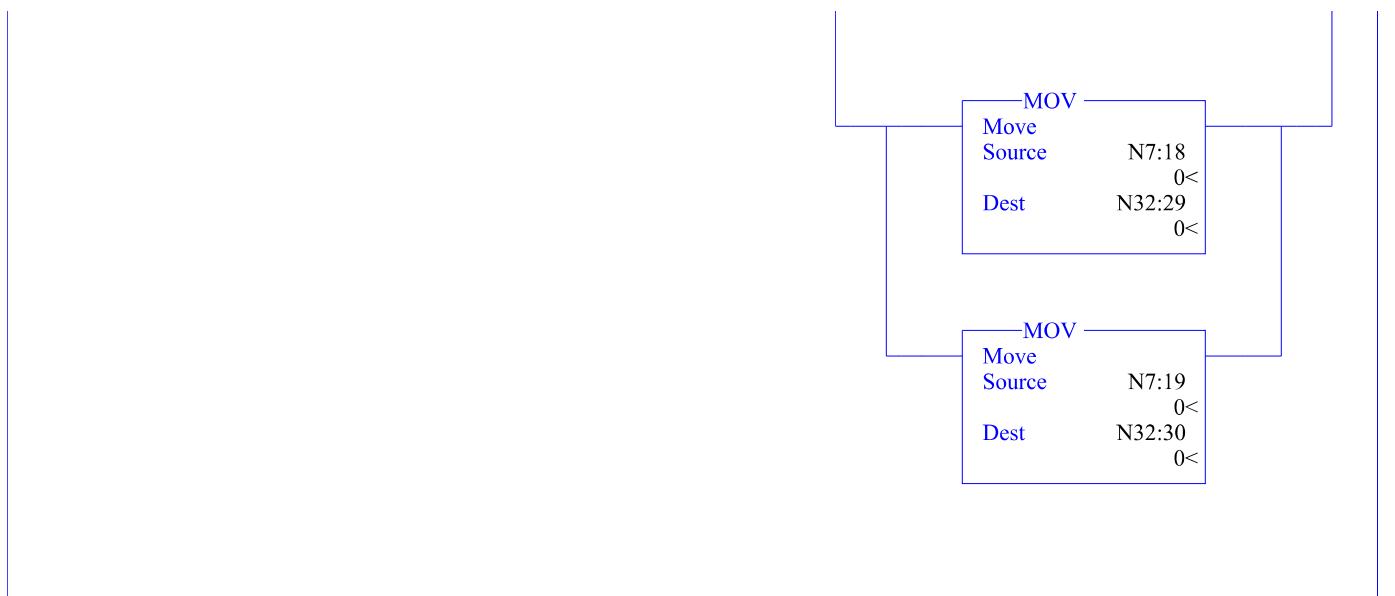
LAD 13 - --- Total Rungs in File = 13



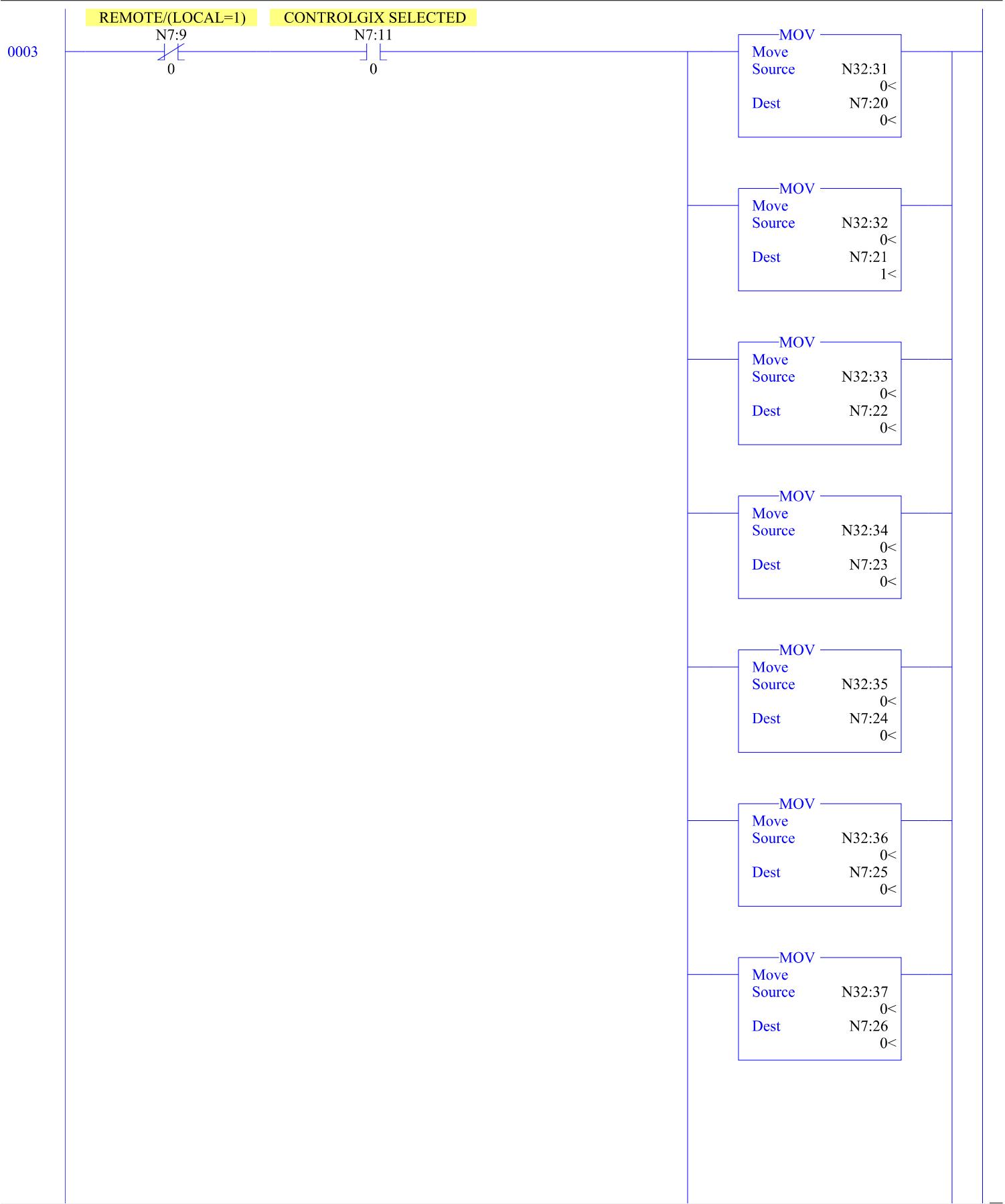
LAD 13 - --- Total Rungs in File = 13



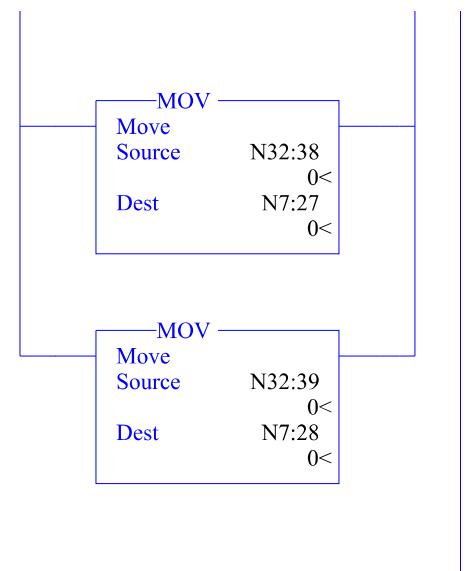
LAD 13 - --- Total Rungs in File = 13



LAD 13 - --- Total Rungs in File = 13



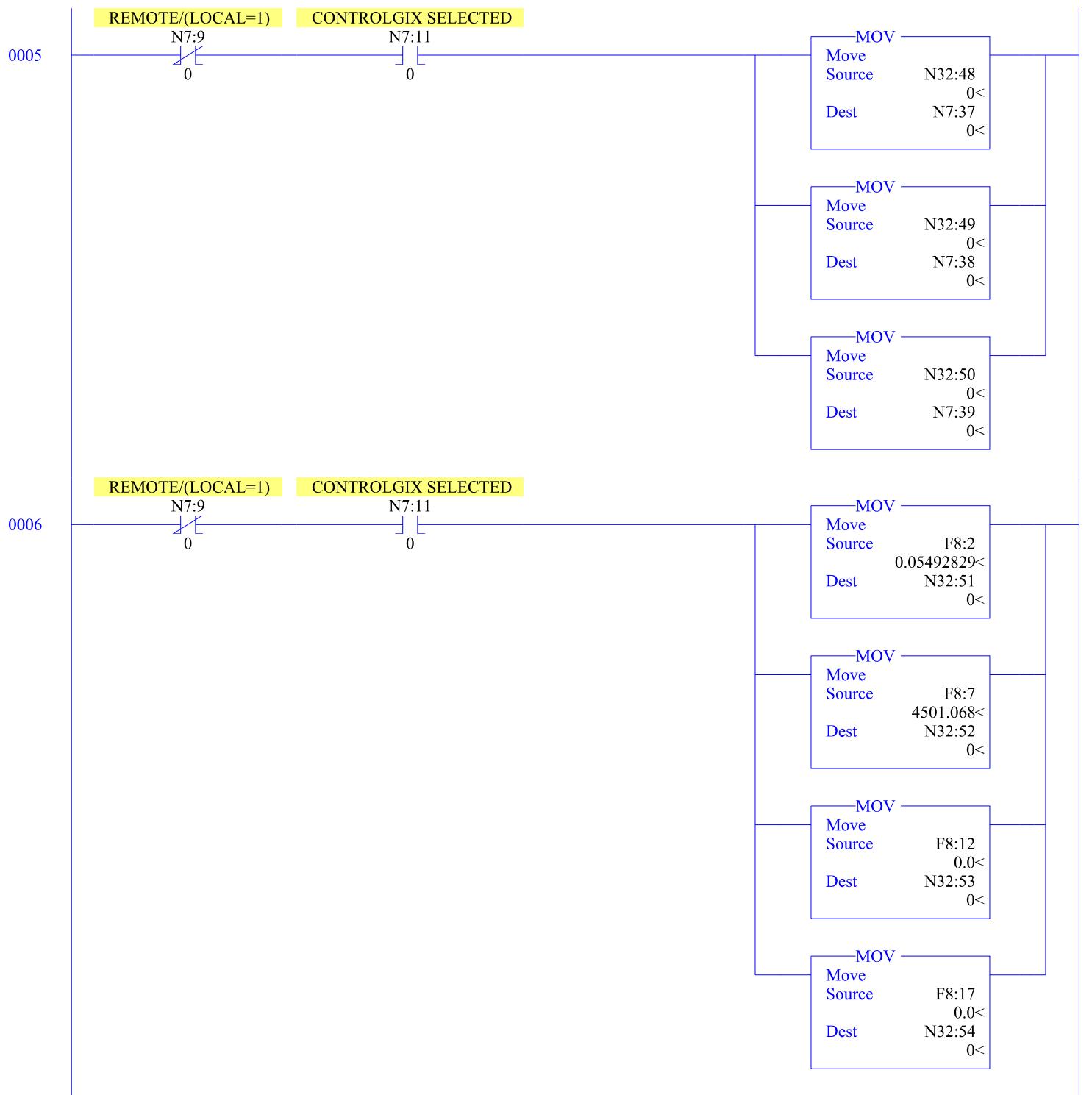
LAD 13 - --- Total Rungs in File = 13



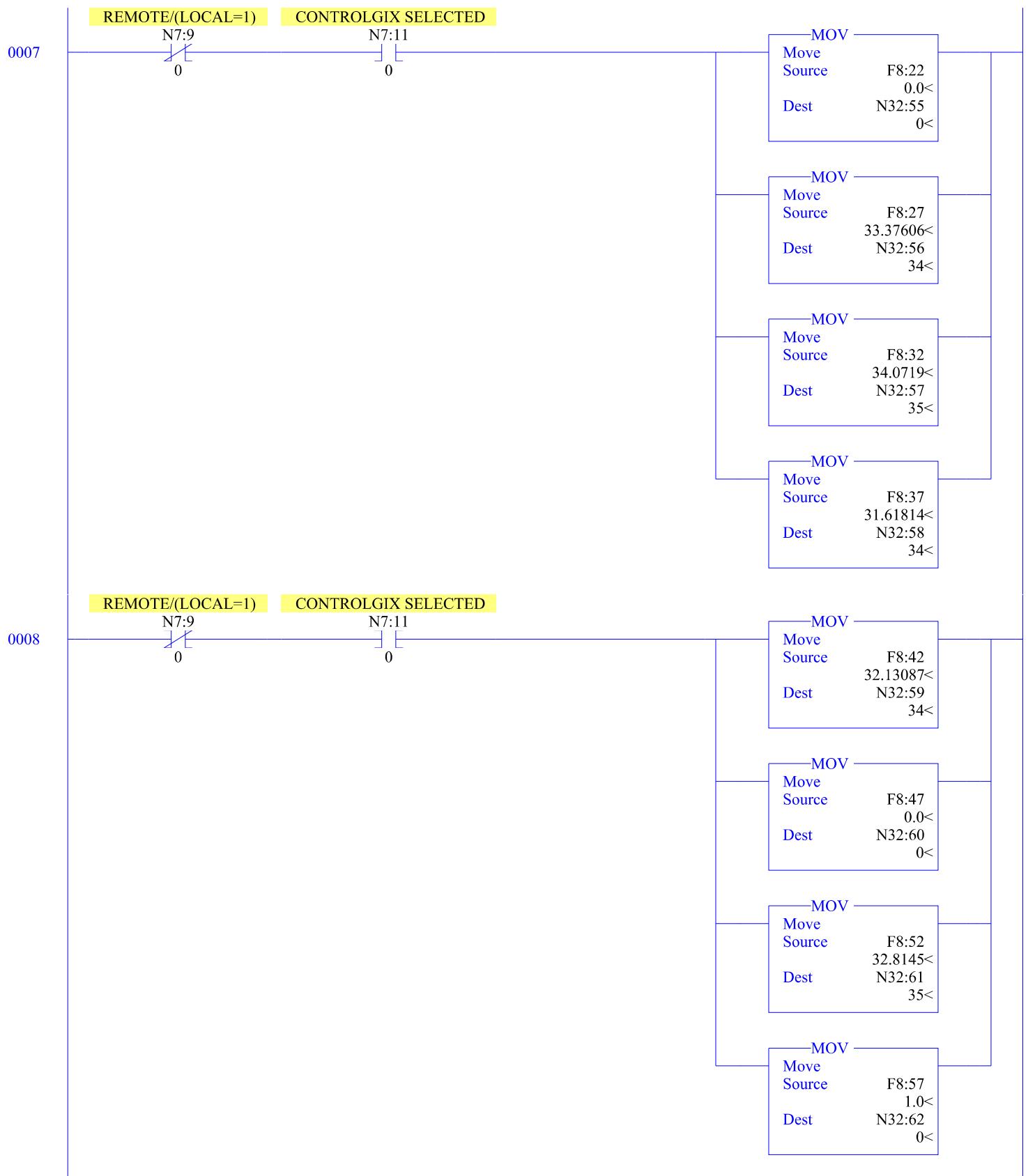
LAD 13 - --- Total Rungs in File = 13

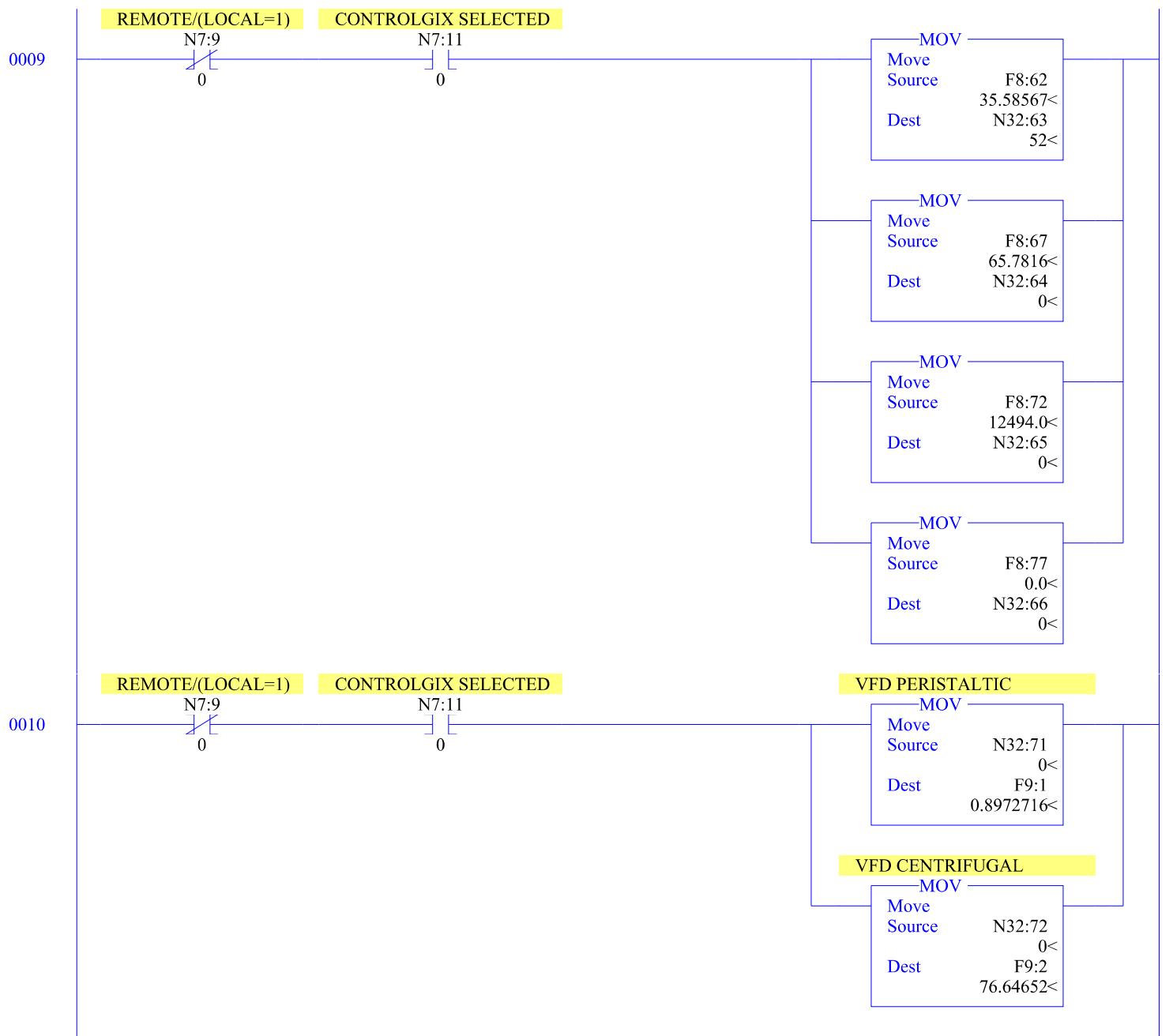


LAD 13 - --- Total Rungs in File = 13

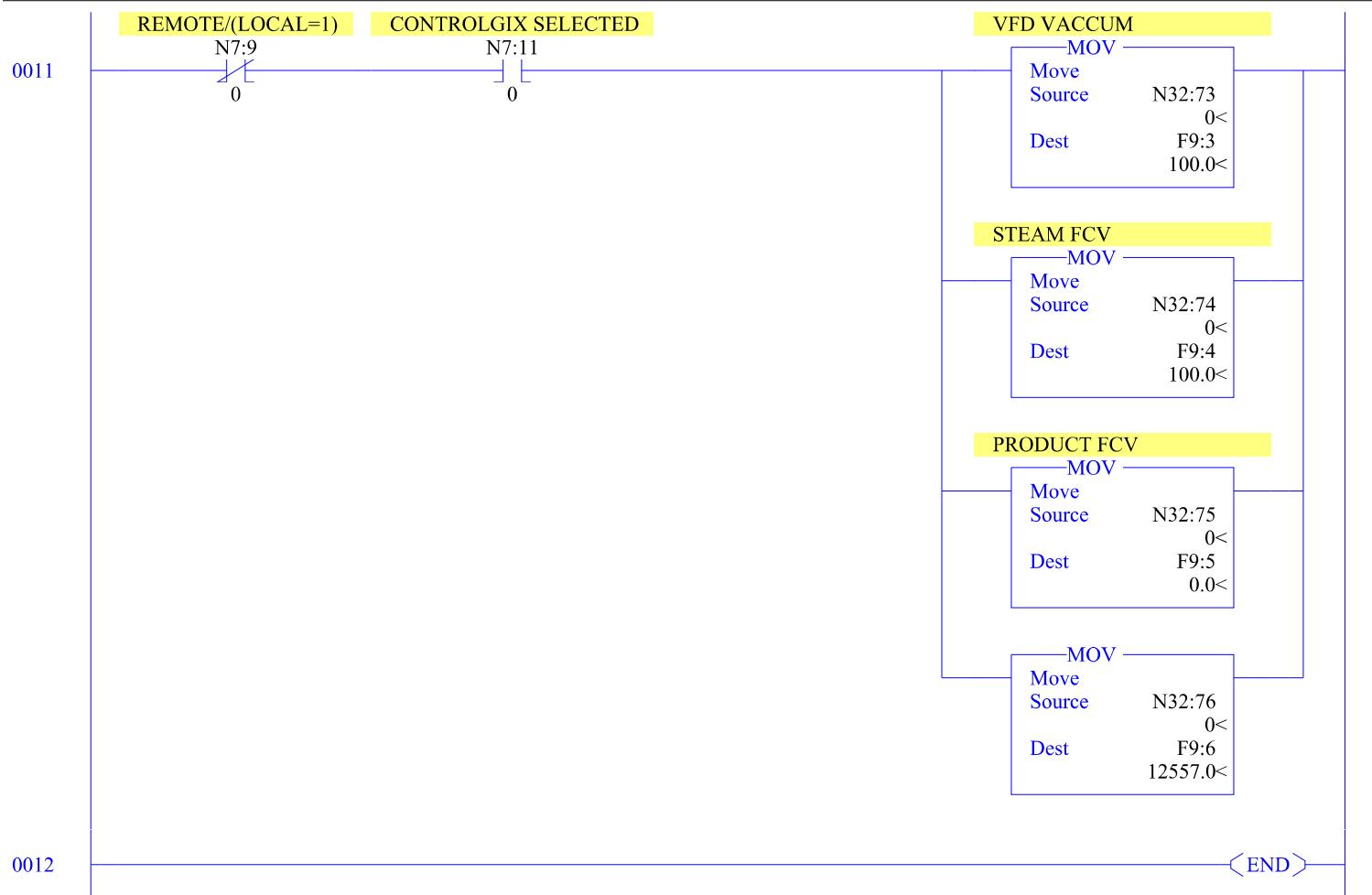


LAD 13 - --- Total Rungs in File = 13

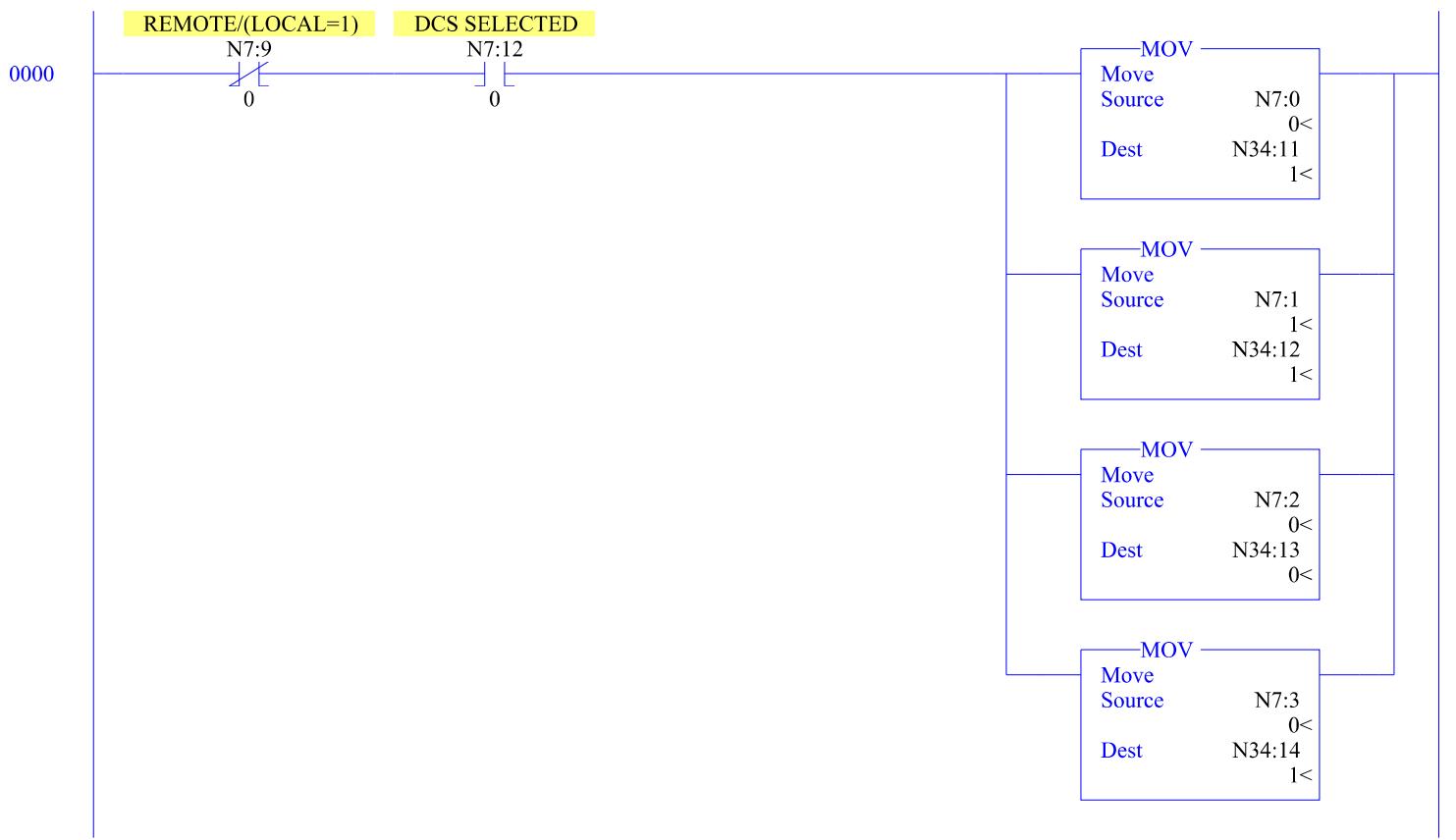




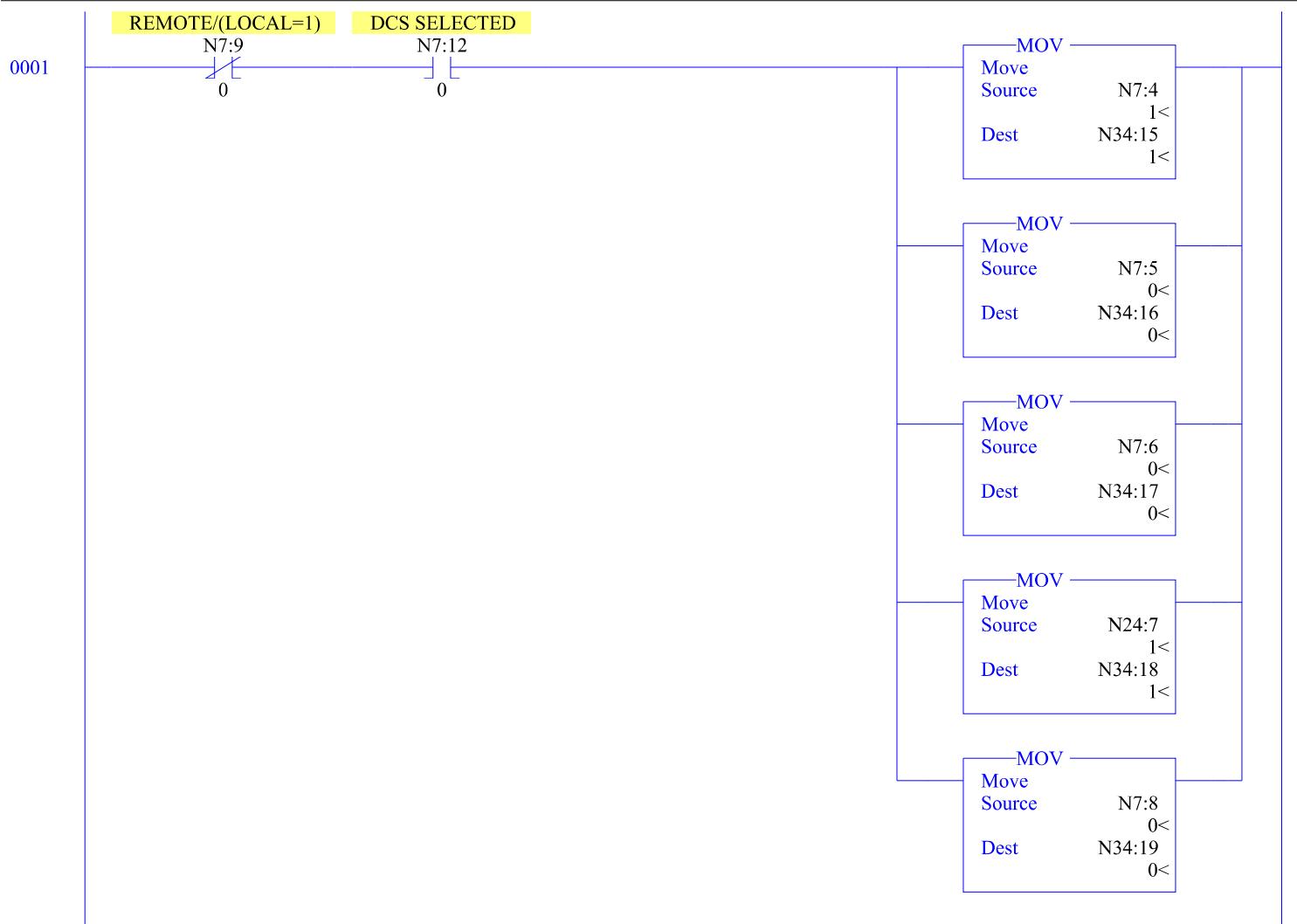
LAD 13 - --- Total Rungs in File = 13



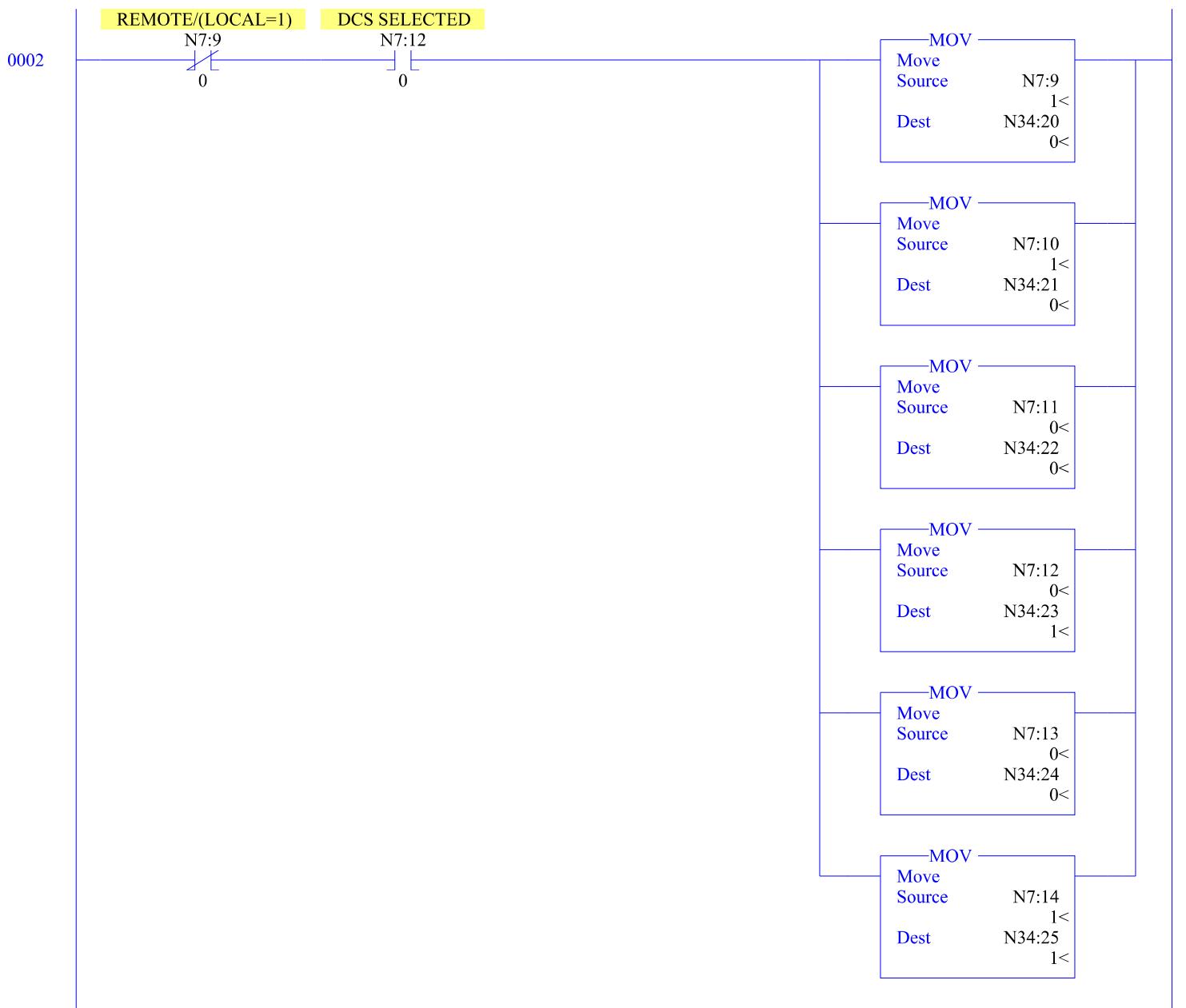
LAD 14 - --- Total Rungs in File = 15



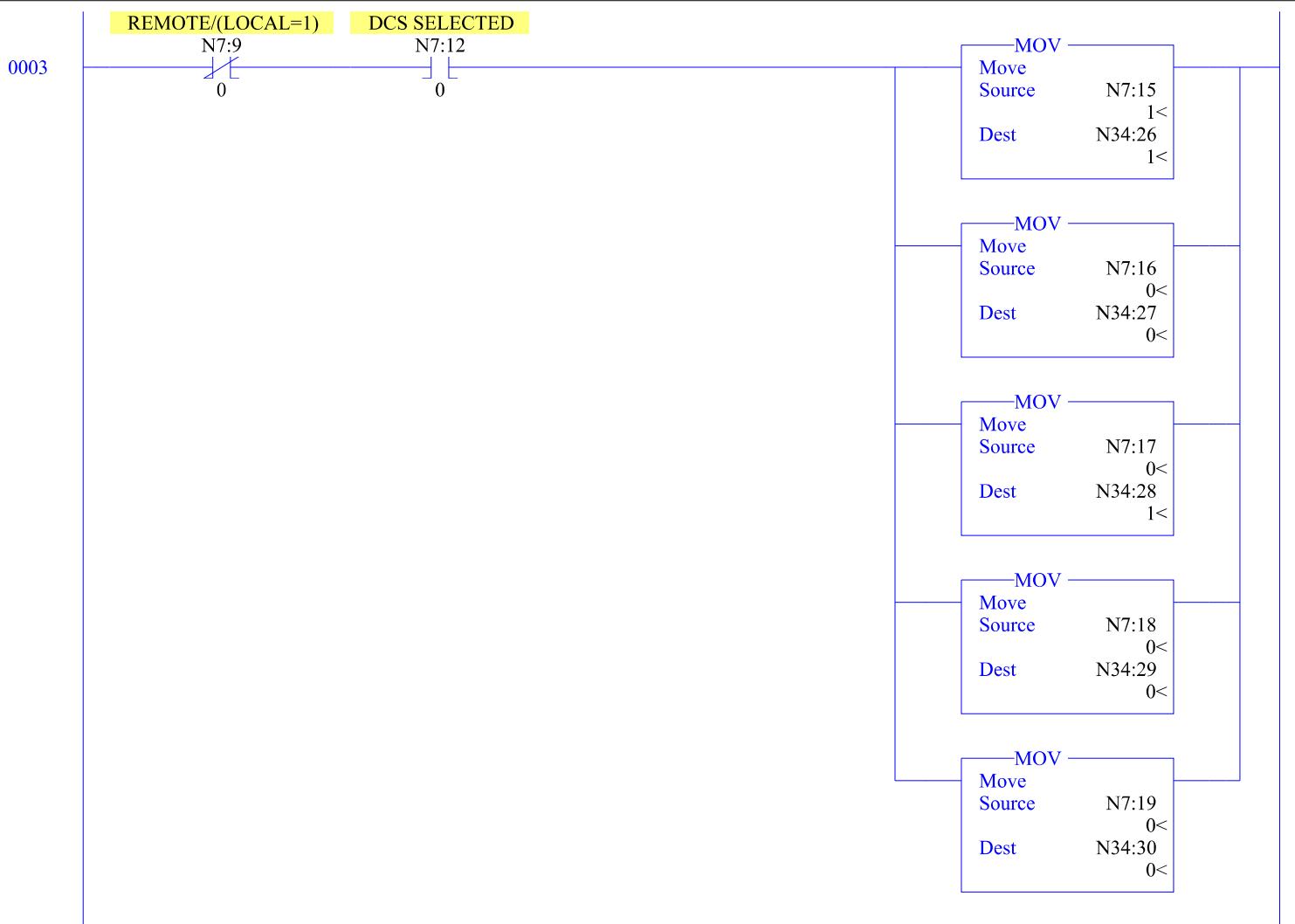
LAD 14 - --- Total Rungs in File = 15



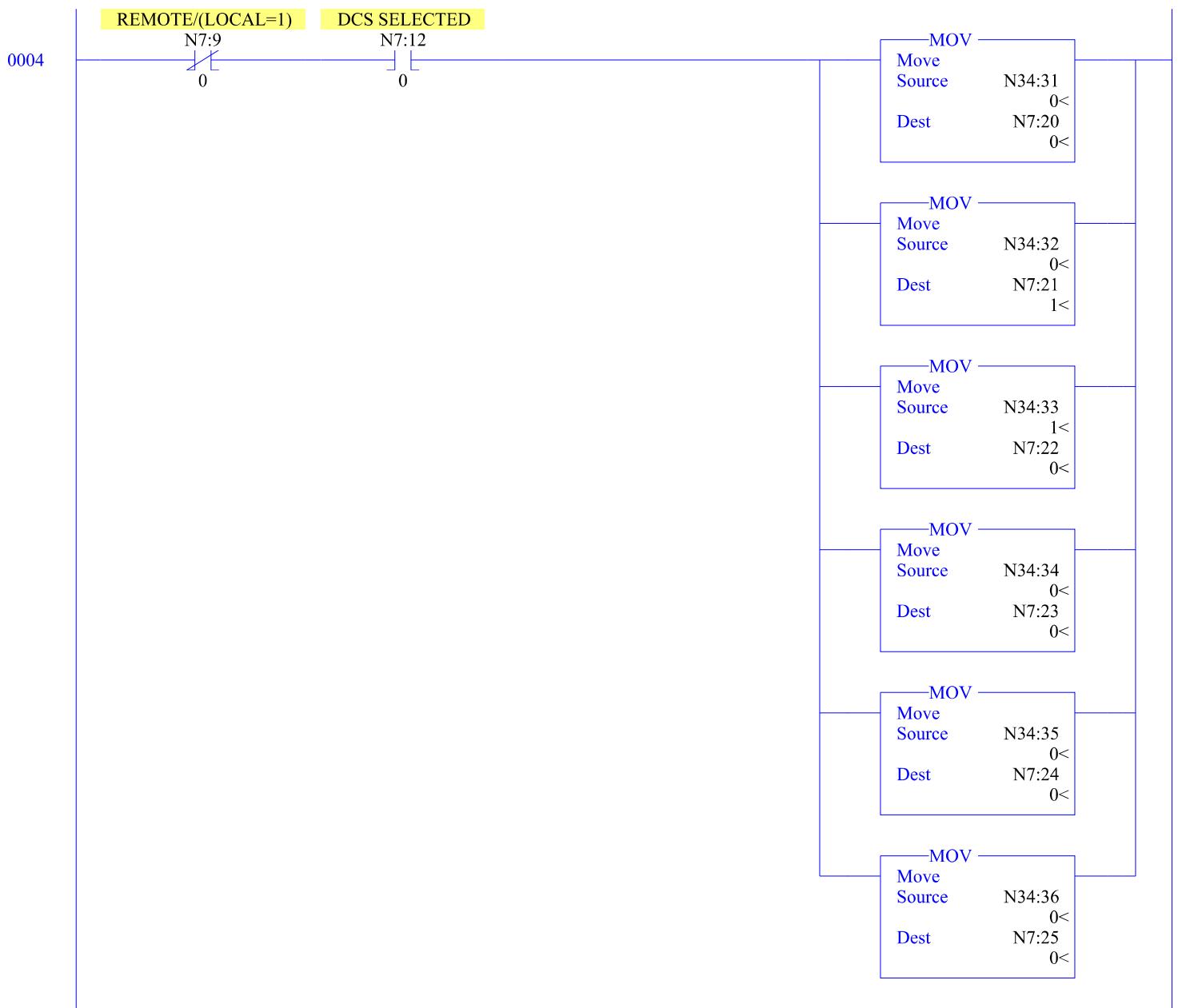
LAD 14 - --- Total Rungs in File = 15



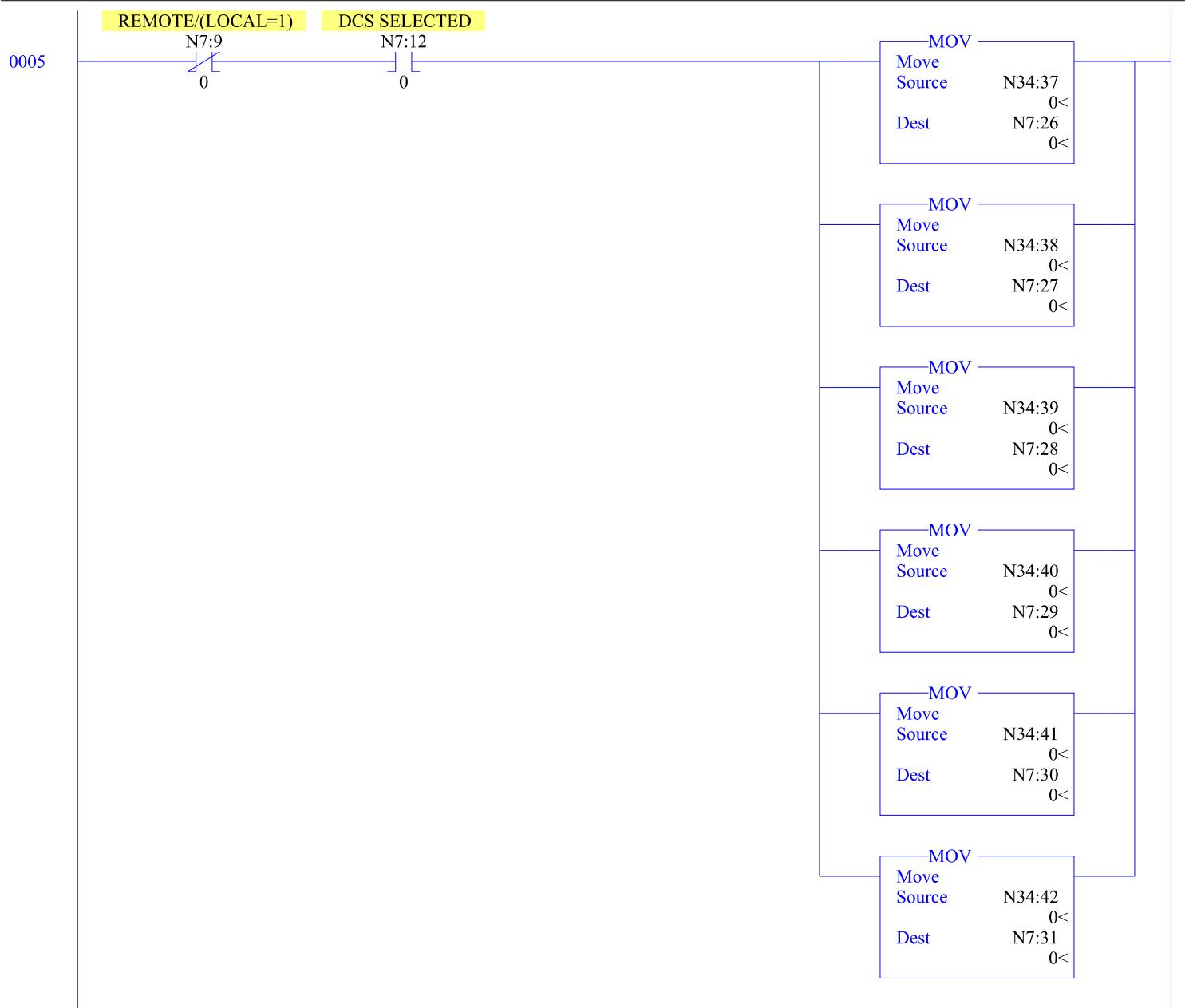
LAD 14 - --- Total Rungs in File = 15



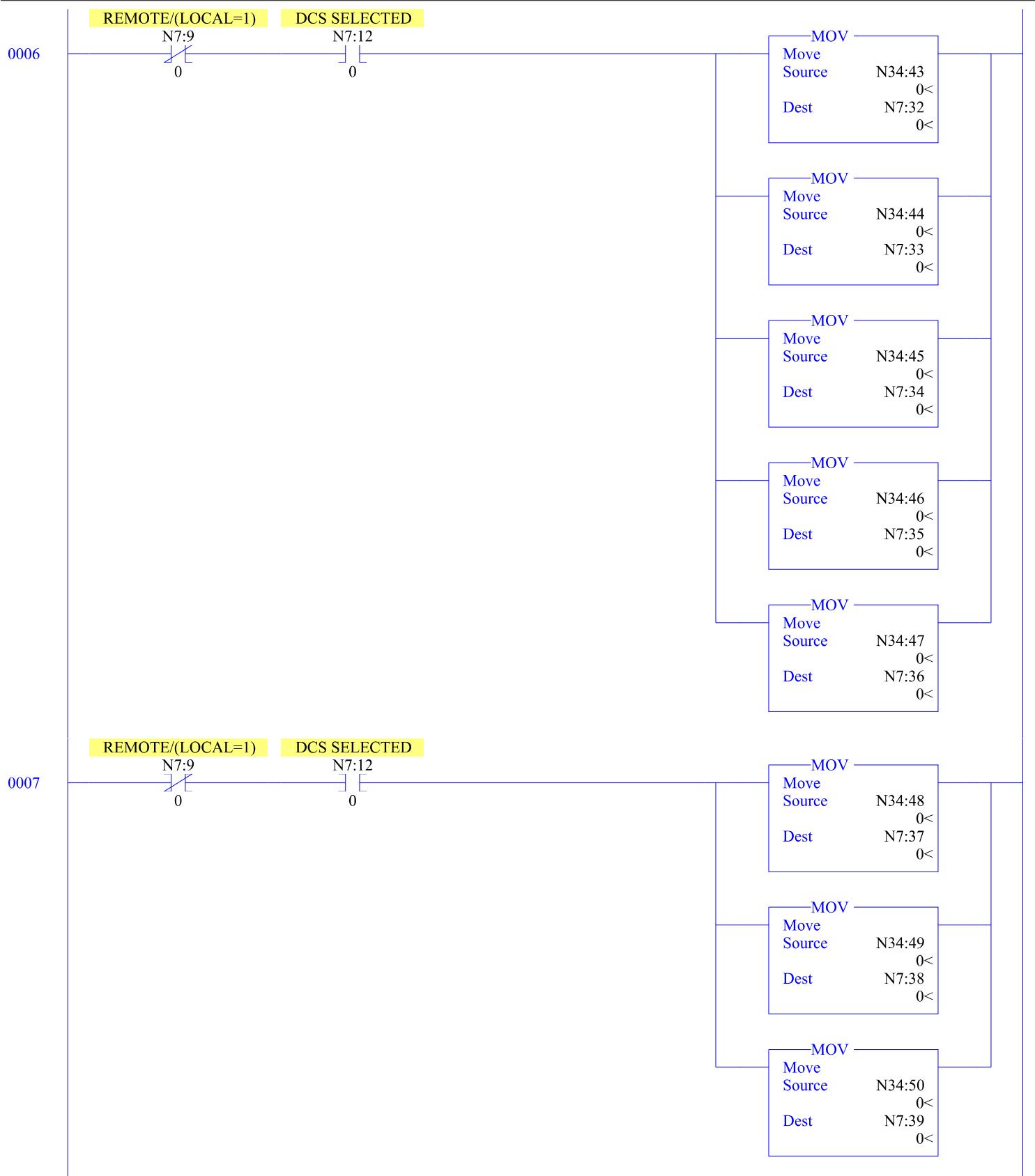
LAD 14 - --- Total Rungs in File = 15



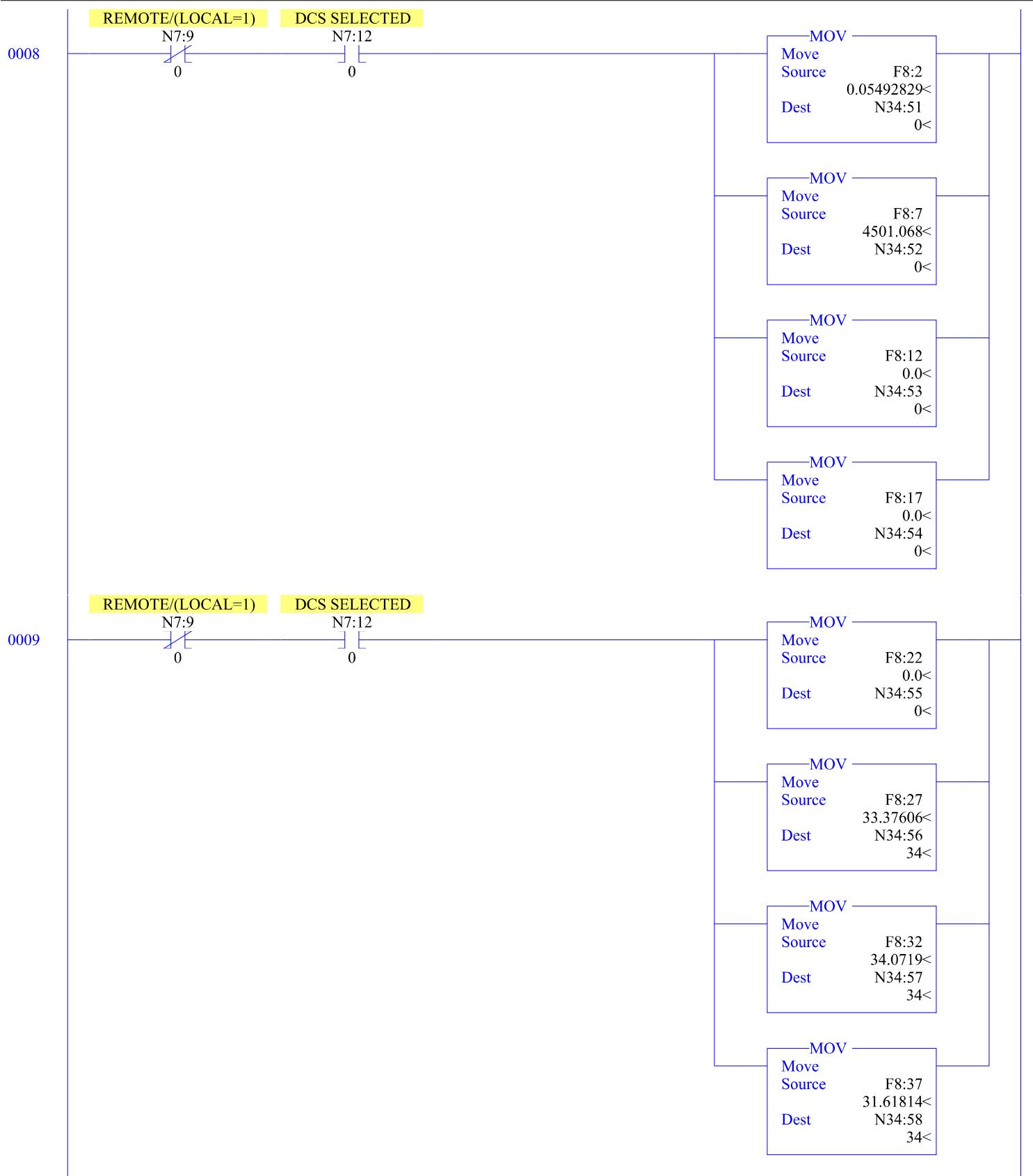
LAD 14 - --- Total Rungs in File = 15



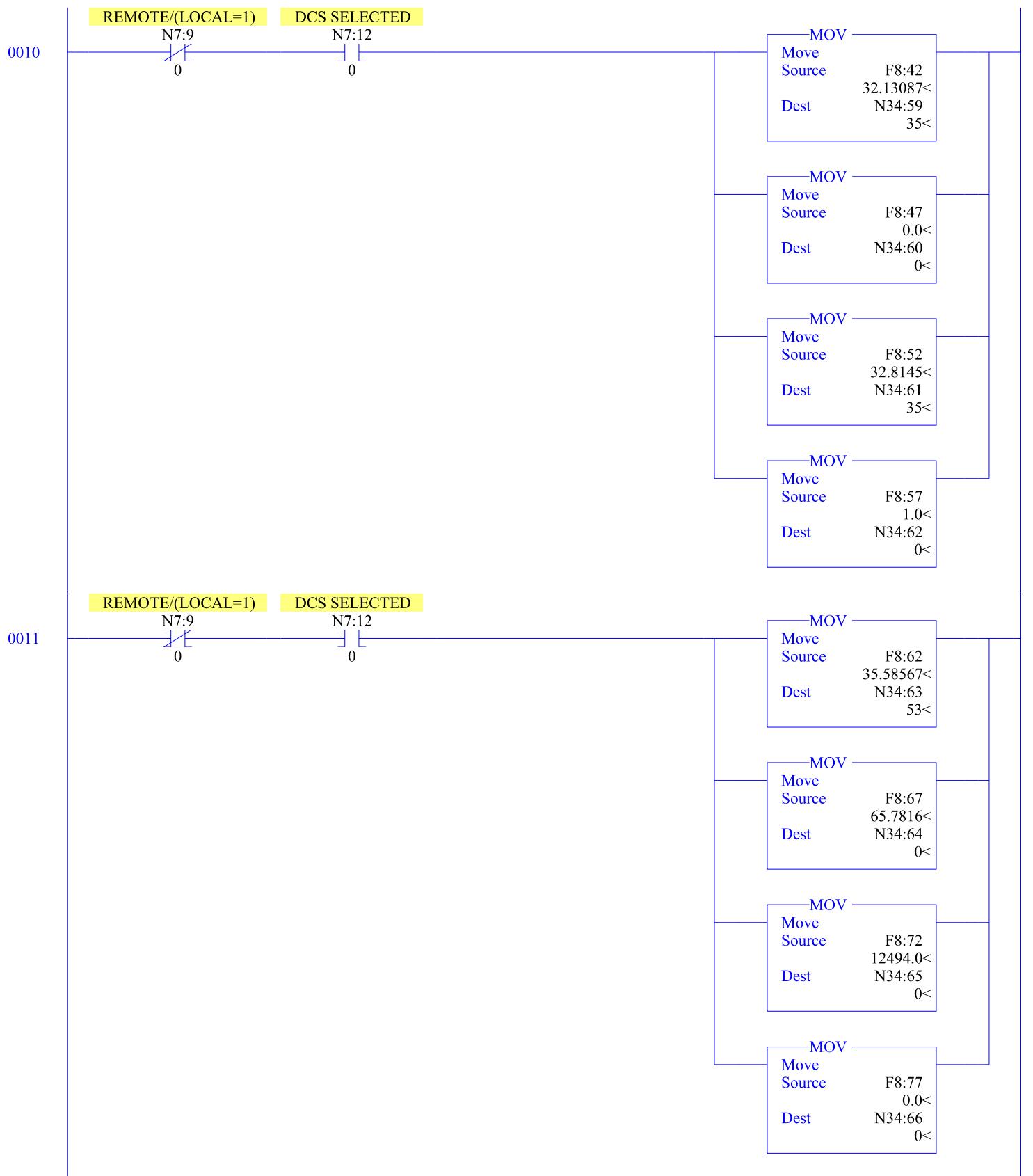
LAD 14 - --- Total Rungs in File = 15



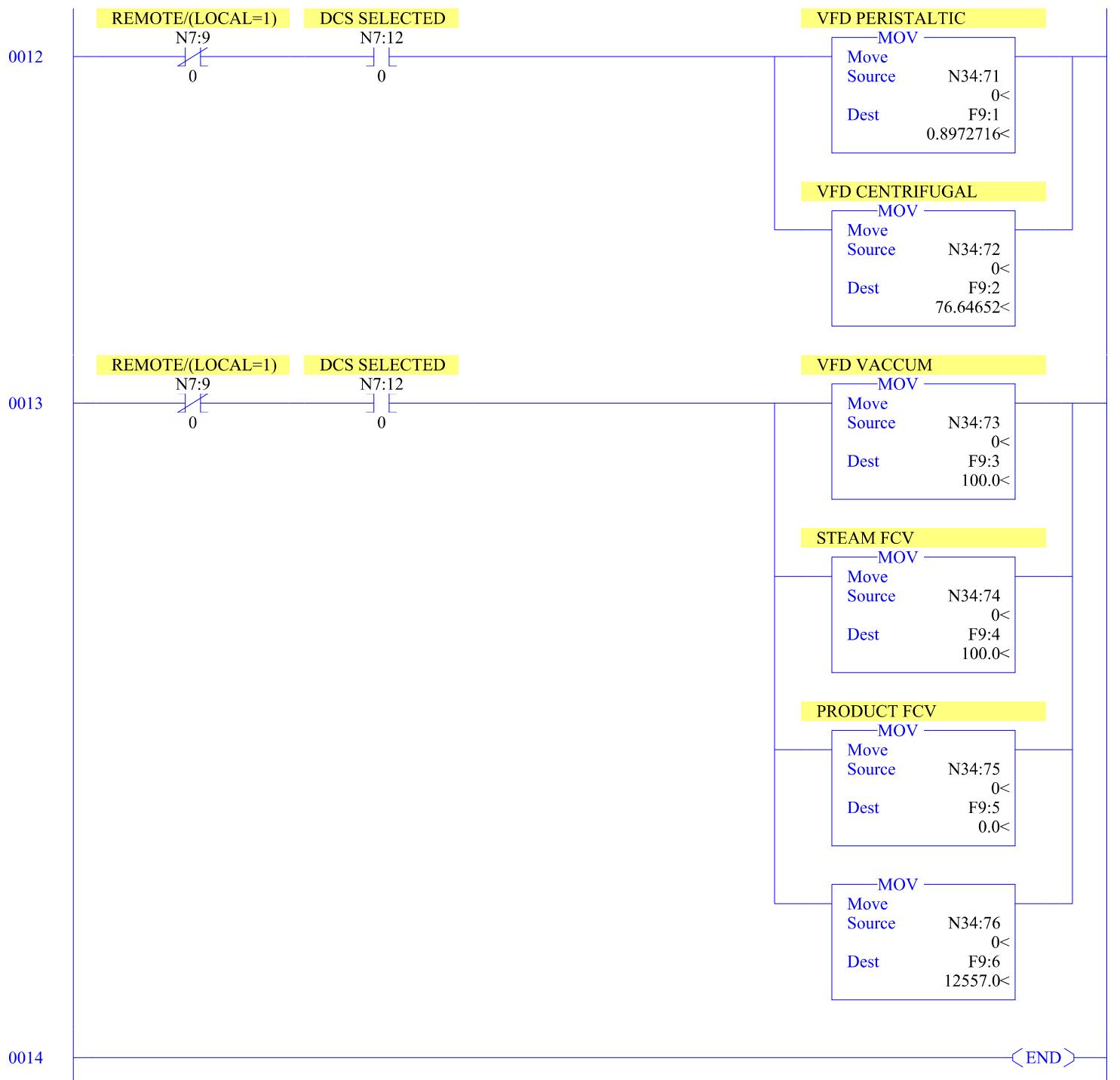
LAD 14 - --- Total Rungs in File = 15



LAD 14 - --- Total Rungs in File = 15



LAD 14 - --- Total Rungs in File = 15



## Data File 00 (bin) -- OUTPUT

Offset	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0			
O:0.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	Bul.1766	MicroLogix 1400 Series A	
O:0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Bul.1766	MicroLogix 1400 Series A	
O:0.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Bul.1766	MicroLogix 1400 Series A	
O:0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Bul.1766	MicroLogix 1400 Series A	
O:0.4	0	0	0	0	0	0	1	1	0	1	0	1	0	0	0	0	Bul.1766	MicroLogix 1400 Series A-Analog :	
O:0.5	0	0	0	0	1	1	0	1	0	0	0	1	1	1	0	0	Bul.1766	MicroLogix 1400 Series A-Analog :	
O:1.0										0	0	0	0	0	0	0	1762-OB8	- 8-Output (TRANS-SRC) 10/50 VDC	
O:5.0	0	0	1	1	1	1	0	0	0	1	1	1	1	0	1	0	1762-OF4	- 4-Channel Analog I/V Output Module	
O:5.1	0	0	1	1	1	1	0	0	0	1	1	1	1	0	1	0	1762-OF4	- 4-Channel Analog I/V Output Module	
O:5.2	0	0	0	0	1	1	0	0	0	0	0	1	1	0	0	0	1762-OF4	- 4-Channel Analog I/V Output Module	
O:5.3	0	0	0	0	1	1	0	0	1	0	0	0	0	1	1	1	1762-OF4	- 4-Channel Analog I/V Output Module	

## Data File I1 (bin) -- INPUT

Offset	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0			
I:0.0	1	1	0	0	0	1	1	0	0	1	0	1	0	0	1	0	Bul.1766	MicroLogix 1400 Series A	
I:0.1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	Bul.1766	MicroLogix 1400 Series A	
I:0.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Bul.1766	MicroLogix 1400 Series A	
I:0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Bul.1766	MicroLogix 1400 Series A	
I:0.4	0	0	0	0	0	0	1	1	0	0	1	1	1	0	0	1	Bul.1766	MicroLogix 1400 Series A-Analog	
I:0.5	0	0	0	0	1	0	0	0	1	1	1	1	0	0	0	1	Bul.1766	MicroLogix 1400 Series A-Analog	
I:0.6	0	0	0	0	0	0	1	1	0	0	1	1	0	0	1	1	Bul.1766	MicroLogix 1400 Series A-Analog	
I:0.7	0	0	0	0	0	0	1	1	0	0	1	1	0	0	1	1	Bul.1766	MicroLogix 1400 Series A-Analog	
I:2.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:2.1	0	0	0	0	1	0	1	0	1	0	1	0	1	1	1	0	1762-IF4	- Analog 4 Chan. Input	
I:2.2	0	0	0	0	1	0	1	0	1	1	1	0	0	1	1	1	1762-IF4	- Analog 4 Chan. Input	
I:2.3	0	0	0	0	1	0	1	0	0	0	1	0	0	1	0	0	1762-IF4	- Analog 4 Chan. Input	
I:2.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1762-IF4	- Analog 4 Chan. Input	
I:2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:2.6	1	0	1	0	1	1	0	0	1	1	0	0	1	0	1	1	1762-IF4	- Analog 4 Chan. Input	
I:3.0	0	0	0	0	1	0	1	0	0	1	0	0	1	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:3.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:3.2	0	0	0	0	1	0	1	0	1	0	0	0	0	0	0	1	1762-IF4	- Analog 4 Chan. Input	
I:3.3	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1762-IF4	- Analog 4 Chan. Input	
I:3.4	0	0	0	0	0	0	0	0	0	0	0	0	1	0	1	0	1762-IF4	- Analog 4 Chan. Input	
I:3.5	0	0	1	0	0	0	0	1	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:3.6	1	0	1	0	1	1	0	0	0	1	1	0	1	1	1	1	1762-IF4	- Analog 4 Chan. Input	
I:4.0	0	0	0	1	0	1	1	0	1	0	1	1	1	1	0	1	1762-IF4	- Analog 4 Chan. Input	
I:4.1	0	0	1	0	1	0	1	0	0	0	0	1	1	1	0	0	1762-IF4	- Analog 4 Chan. Input	
I:4.2	1	1	1	1	1	1	1	0	1	1	0	0	1	1	1	0	1762-IF4	- Analog 4 Chan. Input	
I:4.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:4.4	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	1762-IF4	- Analog 4 Chan. Input	
I:4.5	0	0	0	0	1	0	1	0	0	0	0	0	0	0	0	0	1762-IF4	- Analog 4 Chan. Input	
I:4.6	1	0	1	0	1	0	1	1	0	1	1	1	0	1	1	1	1762-IF4	- Analog 4 Chan. Input	
I:5.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1762-OF4 - 4-Channel Analog I/V Output Module
I:5.1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	1762-OF4 - 4-Channel Analog I/V Output Module

**Main**

Processor Mode S:1/0 - S:1/4 = Remote Run  
 On Power up Go To Run (Mode Behavior) S:1/12 = 0  
 First Pass S:1/15 = No  
 Free Running Clock S:4 = 0000-1110-0111-0000

**Proc**

OS Catalog Number S:57 = 1400	User Program Type S:63 = 9001h
OS Series S:58 = B	Compiler Revision Number S:64 =
OS FRS S:59 =	
Processor Catalog Number S:60 =	
Processor Series S:61 = B	
Processor FRN S:62 =	

**Scan Times**

Maximum (x10 ms) S:22 = 64  
 Watchdog (x10 ms) S:3 (high byte) = 10  
 Last 100 uSec Scan Time S:35 = 52  
 Scan Toggle Bit S:33/9 = 0

**Math**

Math Overflow Selected S:2/14 = 0	Math Register (lo word) S:13 = 0
Overflow Trap S:5/0 = 0	Math Register (high word) S:14-S:13 = 0
Carry S:0/0 = 0	Math Register (32 Bit) S:14-S:13 = 0
Overflow S:0/1 = 0	
Zero Bit S:0/2 = 1	
Sign Bit S:0/3 = 0	

**Chan 0**

Processor Mode S:1/0- S:1/4 = Remote Run	
Node Address S:15 (low byte) = 0	Outgoing Msg Cmd Pending S:33/2 = 0
Baud Rate S:15 (high byte) = ?	
Channel Mode S:33/3 = 0	
Comms Active S:33/4 = 0	
Incoming Cmd Pending S:33/0 = 0	
Msg Reply Pending S:33/1 = 0	

**Debug**

Suspend Code S:7 = 0  
 Suspend File S:8 = 0

**Errors**

Fault Override At Power Up S:1/8 = 0	Fault Routine S:29 = 0
Startup Protection Fault S:1/9 = 0	Major Error S:6 = 0h
Major Error Halt S:1/13 = 0	
Overflow Trap S:5/0 = 0	Error Description:
Control Register Error S:5/2 = 0	
Major Error Executing User	
Fault Rtn. S:5/3 = 0	
Battery Low S:5/11 = 0	
Input Filter Selection Modified S:5/13 = 0	
ASCII String Manipulation error S:5/15 = 0	

**Protection**

Deny Future Access S:1/14 = No  
 Data File Overwrite Protection Lost S:36/10 = False

**Mem Module**

Memory Module Loaded On Boot S:5/8 = 0  
 Password Mismatch S:5/9 = 0  
 Load Memory Module On Memory Error S:1/10 = 0  
 Load Memory Module Always S:1/11 = 0  
 On Power up Go To Run (Mode Behavior) S:1/12 = 0  
 Program Compare S:2/9 = 0  
 Data File Overwrite Protection Lost S:36/10 = 0

**Mem Module**

Memory Module Loaded On Boot S:5/8 = 0  
Password Mismatch S:5/9 = 0  
Load Memory Module On Memory Error S:1/10 = 0  
Load Memory Module Always S:1/11 = 0  
On Power up Go To Run (Mode Behavior) S:1/12 = 0  
Program Compare S:2/9 = 0  
Data File Overwrite Protection Lost S:36/10 = 0

**Forces**

Forces Enabled S:1/5 = Yes  
Forces Installed S:1/6 = No

Data File B3 (bin) -- BINARY

---

Offset	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	(Symbol)	Description
B3:0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	
B3:1	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	
B3:2	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	
B3:3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
B3:10	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0		
B3:11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
B3:19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		

Data File T4 -- TIMER

---

Offset	EN	TT	DN	BASE	PRE	ACC	(Symbol)	Description
T4:0	0	0	0	.01 sec	0	0		

Offset	CU	CD	DN	OV	UN	UA	PRE	ACC	(Symbol)	Description
C5:0	0	0	0	0	0	0	0	0		

Data File R6 -- CONTROL

---

Offset	EN	EU	DN	EM	ER	UL	IN	FD	LEN	POS	(Symbol)	Description
R6:0	0	0	0	0	0	0	0	0	0	0		

## Data File N7 (dec) -- INTEGER

Offset	0	1	2	3	4	5	6	7	8	9
N7:0	0	1	0	0	1	0	0	1	0	1
N7:10	1	0	0	0	1	1	0	0	0	0
N7:20	0	1	0	0	0	0	0	0	0	0
N7:30	0	0	0	0	0	0	0	0	0	0
N7:40	0	0	0	0	0	0	0	0	0	0
N7:50	0	10								

## Data File F8 -- FLOAT

Offset	0	1	2	3	4
F8:0	0	30	0.05492829	0	59.99992
F8:5	0	10000	4501.068	60	0
F8:10	0	100	0	0.02439024	0
F8:15	0	5	0	7.629395e-05	1.214525
F8:20	0	200	0	1.860828e-06	32.4971
F8:25	0	200	33.37606	0	32.37502
F8:30	0	200	34.0719	0	32.48489
F8:35	0	200	31.61814	0	31.97217
F8:40	0	200	32.13087	0	32.27736
F8:45	0	200	0	0	32.32619
F8:50	0	200	32.8145	100	31.44723
F8:55	0	1	1	0	0
F8:60	0	100	35.58567	0	0
F8:65	0	100	65.7816	0	0
F8:70	0	819	12494	0	0
F8:75	0	100	0	0	0
F8:80	100	0	0	0	0
F8:85	30	10	0	0	0

Data File F9

---

Offset	0	1	2	3	4
F9:0	0	0.8972716	76.64652	100	100
F9:5	0	12557	147	16383	16383
F9:10	0	0	0	0	0
F9:15	0	0	0	0	0
F9:20	0	0	0	0	0
F9:25	0	0	0	0	0

## Data File N10 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N10:0	60	1	60	60	250	10250	101	0	0	

## Data File PD11

Offset	TM	AM	CM	OL	RG	SC	TF	DA	DB	UL	LL	SP	PV	DN	EN	SPS	KC	Ti	TD	MAXS	MINS	ZCD
PD11:0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	4500	14	5	1	10000	0	0
PD11:1	0	0	1	0	0	0	0	0	0	0	0	0	1	1	1	8	14	5	1	10	0	0
PD11:2	0	0	0	0	0	0	0	0	0	1	0	0	0	1	1	40	18	5	1	200	0	0
PD11:3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	14	1	1	100	0	0
PD11:4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD11:5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD11:6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD11:7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD11:8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD11:9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Data File F12

---

Offset	0	1	2	3	4
F12:0	0	0	0	0	0
F12:5	0	0	0		

## Data File PD16

Offset	TM	AM	CM	OL	RG	SC	TF	DA	DB	UL	LL	SP	PV	DN	EN	SPS	KC	Ti	TD	MAXS	MINS	ZCD
PD16:0	0	0	0	0	0	0	0	0	1	0	0	0	0	1	1	35	50	1	2	100	0	0
PD16:1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	29	14	1	1	100	0	0
PD16:2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PD16:9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

## Data File N23 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N23:0	0	0	0	0	0	0	0	0	0	0
N23:10	0	0	0	0	0	0	0	0	0	0
N23:20	100	60	0							

## Data File N24 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N24:0	1	0	0	0	1	0	0	1	0	1
N24:10	1	0	0	0	0	1	0	0	0	0
N24:20	0	0	0	0	0	0	0	0	0	0
N24:30	0	0	0	0	0	0	0	0	0	0

## Data File N29 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N29:0	0	16383	0	16383	20479	16383	0	0	2688	16383
N29:10	7409	12508	0	0	5833	16383	147	100	0	0
N29:20	1	0	0	0	0	0	0	0	0	0

## Data File N30 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N30:0	0	0	0	0	0	0	0	0	0	0
N30:10	0	0	0							

## Data File N31 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N31:0	0									

## Data File N32 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N32:0	0	0	0	0	0	0	0	0	0	0
N32:10	0	1	1	0	1	1	0	0	0	0
N32:20	0	0	1	0	0	1	1	0	1	0
N32:30	0	0	0	0	0	0	0	0	0	0
N32:40	0	0	0	0	0	0	0	0	0	0
N32:50	0	0	0	0	0	0	34	35	34	34
N32:60	0	35	0	52	0	0	0	0	0	0
N32:70	0	0	0	0	0	0	0	0	0	0

## Data File N33 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N33:0	0	0	0	0	0	0	0	0	0	0
N33:10	0	0	1	0	0	1	0	0	1	0
N33:20	1	1	0	0	0	1	1	0	1	0
N33:30	0	0	0	0	0	0	0	0	0	0
N33:40	0	0	0	0	0	0	0	0	0	0
N33:50	0	8	0	0	2	0	3081	3050	3092	3148
N33:60	0	3122	10000	4807	6601	0	0	0	0	0
N33:70	0	0	0	0	0	0	0	0	0	0
N33:80	0	0	0	0	0	0	0	0	0	0
N33:90	0	0	0	0	0	0	0	0	0	0

## Data File N34 (dec)

Offset	0	1	2	3	4	5	6	7	8	9
N34:0	0	0	0	0	0	0	0	0	0	0
N34:10	0	1	1	0	1	1	0	0	1	0
N34:20	0	0	0	1	0	1	1	0	1	0
N34:30	0	0	0	1	0	0	0	0	0	0
N34:40	0	0	0	0	0	0	0	0	0	0
N34:50	0	0	0	0	0	0	34	34	34	35
N34:60	0	35	0	53	0	0	0	0	0	0
N34:70	0	0	0	0	0	0	0	0	0	0
N34:80	0	0	0	0	0	0	0	0	0	0
N34:90	0	0	0	0	0	0	0	0	0	0

## Appendix F

# Contrologix Programming Boiler & Heat Exchanger

<b>General</b>			
Vendor:	Allen-Bradley	Mode:	Remote Run
Revision:	16.3	Key Switch Position:	REM
Chassis Type:	1756-A10 10-Slot ControlLogix Chassis	Created:	10/9/2013 7:12:06 PM
Slot:	0	Edited:	6/23/2014 3:54:38 PM
<b>Serial Port</b>			
Mode:	System	Control Line:	No Handshake
Baud Rate:	19200	RTS Send Delay:	0 (x20 ms)
Date Bits:	8	RTS Off Delay:	0 (x20 ms)
Parity:	None	DCD Wait Delay:	0 (x1 sec)
Stop Bits:	1		
<b>System Protocol - DF1 Master</b>			
Station Address:	0	Polling Mode:	Message Based (slave can initiate messages)
Transmit Retries:	3	Error Detection:	BCC
ACK Timeout:	50 (x20 ms)	Enable Duplicate Detection:	Yes
Relay Message Wait:	5 (x20 ms)		
<b>System Protocol - DF1 Point to Point (Current)</b>			
Station Address:	0	Embedded Responses:	Autodetect
NAK Receive Limit:	3	Error Detection:	BCC
ENQ Transmit Limit:	3	Enable Duplicate Detection:	Yes
ACK Timeout:	50 (x20 ms)		
<b>System Protocol - DF1 Radio Modem</b>			
Station Address:	0	Error Detection:	BCC
Store and Forward:	No		
<b>System Protocol - DF1 Slave</b>			
Station Address:	0	EOT Suppression:	No
Transmit Retries:	3	Error Detection:	BCC
Slave Poll Timeout:	3000 (x20 ms)	Enable Duplicate Detection:	Yes
<b>System Protocol - DH485</b>			
Station Address:	0	Token Hold Factor:	1
Max Station Address:	31	Error Detection:	CRC
<b>User Protocol - ASCII</b>			
Read/Write Buffer Size:	82 bytes	Append Character 2:	'\$I'
Termination Character 1:	'\$r'	XON/XOFF:	No
Termination Character 2:	'\$FF'	Echo Mode:	No
Append Character 1:	'\$r'	Delete Mode:	Ignore
<b>Date/Time</b>			
Date and Time:	1/2/1998 6:58:42 PM		
Time Zone:	(GMT+00:00)		
Daylight Saving (+01:00):	No		
CST Master:	No		
Is Master:	Off	Duplicate Master Detected:	Off
Synchronized with Master:	Off	Timer Hardware Faulted:	Off
<b>Advanced</b>			
Controller Fault Handler:	<none>	Security:	No Protection
Power-Up Handler:	<none>	Match Project To Controller:	No
System Overhead Time Slice:	20 %	Serial Number:	00356A6C
During unused System Overhead Time Slice:	Run Continuous Task		
<b>SFC Execution</b>			
Execution Control:	Execute current active steps only	Last Scan of Active Step:	Don't scan
Restart Position:	Restart at most recently executed step		
<b>Nonvolatile Memory</b>			
<Empty>			
<b>Memory</b>			
Memory Option:	1756-L60M03SE/A		
I/O Memory			
Total Memory:	505,856 bytes	Max Used:	37,616 bytes
Free Memory:	468,240 bytes	Largest Block Free:	466,072 bytes
Used Memory:	37,616 bytes		
Data and Logic Memory			

Total Memory:	768,000 bytes	Max Used:	89,500 bytes
Free Memory:	679,140 bytes	Largest Block Free:	678,344 bytes
Used Memory:	88,860 bytes		

Name	Value	Data Type	Scope
<b>AI</b>		REAL[13]	cpu
AI[0] - MainProgram/COMMUNICATION - *0(MSG)			
AI[0] - MainProgram/IOINTERFACE - 0(MOV)			
AI[10] - MainProgram/IOINTERFACE - 10(MOV)			
AI[11] - MainProgram/IOINTERFACE - 11(MOV)			
AI[1] - MainProgram/IOINTERFACE - 1(MOV)			
AI[2] - MainProgram/IOINTERFACE - 2(MOV)			
AI[3] - MainProgram/IOINTERFACE - 3(MOV)			
AI[4] - MainProgram/IOINTERFACE - 4(MOV)			
AI[5] - MainProgram/IOINTERFACE - 5(MOV)			
AI[6] - MainProgram/IOINTERFACE - 6(MOV)			
AI[7] - MainProgram/IOINTERFACE - 7(MOV)			
AI[8] - MainProgram/IOINTERFACE - 8(MOV)			
AI[9] - MainProgram/IOINTERFACE - 9(MOV)			
<b>AM</b>	1	BOOL	cpu
AM - MainProgram/MainRoutine - *4(OTE)			
<b>AO1</b>		REAL[10]	cpu
AO1[0] - MainProgram/COMMUNICATION - 1(MSG)			
AO1[0] - MainProgram/IOINTERFACE - *12(MOV)			
AO1[1] - MainProgram/IOINTERFACE - *13(MOV)			
AO1[2] - MainProgram/IOINTERFACE - *14(MOV)			
AO1[3] - MainProgram/IOINTERFACE - *15(MOV)			
AO1[4] - MainProgram/IOINTERFACE - *16(MOV)			
AO1[5] - MainProgram/IOINTERFACE - *17(MOV)			
<b>AS</b>	0	BOOL	cpu
AS - MainProgram/MAINLOGIC - *18(ONS)			
<b>AUTO</b>	0	BOOL	cpu
AUTO - MainProgram/MainRoutine - 3(XIC)			
<b>CLDPSTRT</b>	0	BOOL	cpu
CLDPSTRT - MainProgram/MAINLOGIC - *14(OTE), 15(XIC), 17(XIC)			
<b>COLD</b>	30.0	REAL	cpu
COLD - MainProgram/MAINLOGIC - 16(MOV)			
<b>CONTROLOSEL</b>	0	BOOL	cpu
CONTROLOSEL - MainProgram/IOINTERFACE - *33(OTE)			
<b>DCSSEL</b>	1	BOOL	cpu
DCSSEL - MainProgram/IOINTERFACE - *32(OTE)			
<b>DI</b>		INT[32]	cpu
DI[0] - MainProgram/COMMUNICATION - *2(MSG)			
DI[0].0 - MainProgram/IOINTERFACE - 18(XIC)			
DI[10].0 - MainProgram/IOINTERFACE - 28(XIC)			
DI[11].0 - MainProgram/IOINTERFACE - 29(XIC)			
DI[12].0 - MainProgram/IOINTERFACE - 30(XIC)			
DI[13].0 - MainProgram/IOINTERFACE - 31(XIC)			
DI[14].0 - MainProgram/IOINTERFACE - 32(XIC)			
DI[15].0 - MainProgram/IOINTERFACE - 33(XIC)			
DI[16].0 - MainProgram/IOINTERFACE - 34(XIC)			
DI[1].0 - MainProgram/IOINTERFACE - 19(XIC)			
DI[2].0 - MainProgram/IOINTERFACE - 20(XIC)			
DI[3].0 - MainProgram/IOINTERFACE - 21(XIC)			
DI[4].0 - MainProgram/IOINTERFACE - 22(XIC)			
DI[5].0 - MainProgram/IOINTERFACE - 23(XIC)			
DI[6].0 - MainProgram/IOINTERFACE - 24(XIC)			
DI[7].0 - MainProgram/IOINTERFACE - 25(XIC)			

**DI (Continued)**

DI[8].0 - MainProgram/IOINTERFACE - 26(XIC)  
DI[9].0 - MainProgram/IOINTERFACE - 27(XIC)

**DISPLAY** 0 BOOL cpu  
DISPLAY - MainProgram/MAINLOGIC - 0(XIO), 1(XIO), 10(XIO), 11(XIO), 12(XIO), 13(XIO), 14(XIO), 15(XIO), 16(XIO), 17(XIO), 18(XIO), 19(XIO), 2(XIO), 20(XIO), 3(XIO), 4(XIO), 5(XIO), 6(XIC), 7(XIO), 8(XIO), 9(XIO)  
DISPLAY - MainProgram/MainRoutine - \*3(OTE), 4(XIO), 5(XIC), 6(XIO), 7(XIO), 8(XIO), 9(XIO)

**DO1** INT[10] cpu  
DO1[0] - MainProgram/COMMUNICATION - 3(MSG)  
DO1[0].0 - MainProgram/IOINTERFACE - \*35(OTE)  
DO1[1].0 - MainProgram/IOINTERFACE - \*36(OTE)  
DO1[2].0 - MainProgram/IOINTERFACE - \*37(OTE)  
DO1[3].0 - MainProgram/IOINTERFACE - \*38(OTE)  
DO1[4].0 - MainProgram/IOINTERFACE - \*39(OTE)

**FCV1** 0.0 REAL cpu  
FCV1 - MainProgram/HEAT\_EXCHANGER\_TEMP\_CONTROL - \*0(PID)  
FCV1 - MainProgram/IOINTERFACE - 17(MOV)  
FCV1 - MainProgram/MAINLOGIC - \*1(MOV), \*20(MOV)

**fic1** PID cpu  
fic1 - MainProgram/LEVELCONTROL - \*5(PID)  
fic1.OUT - MainProgram/LEVELCONTROL - 6(MOV)  
fic1.SP - MainProgram/LEVELCONTROL - \*4(MOV)

**FRT** 0 BOOL cpu  
FRT - MainProgram/MAINLOGIC - \*6(OTE)

**fsp** 0.0 REAL MainProgram  
fsp - MainProgram/LEVELCONTROL - \*3(DIV), 4(MOV)

**FT1** 0.0 REAL cpu  
FT1 - MainProgram/IOINTERFACE - \*10(MOV)  
FT1 - MainProgram/LEVELCONTROL - 5(PID)  
FT1 - MainProgram/PID\_test - 1-B1(IREF,FT1), 1-B1(PIDE,PIDE\_01.PV)  
FT1 - MainProgram/pidsqyare - 0(PID)

**FT2** 0.0 REAL cpu  
FT2 - MainProgram/IOINTERFACE - \*9(MOV)

**FT3** 0.0 REAL cpu  
FT3 - MainProgram/IOINTERFACE - \*8(MOV)  
FT3 - MainProgram/LEVELCONTROL - 0(MOV)

**HEATER** 0 BOOL cpu  
HEATER - MainProgram/IOINTERFACE - 37(XIC)  
HEATER - MainProgram/MAINLOGIC - \*13(OTE)

**HETRSCADA** 0 BOOL cpu  
HETRSCADA - MainProgram/MAINLOGIC - 13(XIC)

**HOOTER** 0 BOOL cpu  
HOOTER - MainProgram/IOINTERFACE - 39(XIC)

**HOOTERACK** 0 BOOL cpu  
HOOTERACK - MainProgram/IOINTERFACE - \*34(OTE)

**hr** 0 BOOL cpu  
hr - MainProgram/MAINLOGIC - \*8(OSF)

**HXT** PID cpu

**HXT (Continued)**

*HXT - MainProgram/HEAT\_EXCHANGER\_TEMP\_CONTROL - \*0(PID)*

<b>J</b>	0	BOOL	cpu
	<i>J - MainProgram/MAINLOGIC - *0(OSR)</i>		
<b>le</b>	0	BOOL	cpu
	<i>le - MainProgram/MAINLOGIC - *4(OTE), 7(XIC)</i>		
<b>level</b>		PID	cpu
	<i>level - MainProgram/LEVELCONTROL - *2(PID)</i>		
	<i>level - MainProgram/pidsqyare - *3(PID)</i>		
	<i>level.BIAS - MainProgram/LEVELCONTROL - *1(MOV)</i>		
	<i>level.OUT - MainProgram/LEVELCONTROL - *2(PID), 3(DIV)</i>		
<b>levltune</b>	0	BOOL	cpu
	<i>levltune - MainProgram/pidsqyare - 0(XIC), 1(XIC), 2(XIC)</i>		
<b>LSH201</b>	1	BOOL	cpu
	<i>LSH201 - MainProgram/IOINTERFACE - *22(OTE)</i>		
<b>LSH301</b>	0	BOOL	cpu
	<i>LSH301 - MainProgram/IOINTERFACE - *24(OTE)</i>		
<b>LSL101</b>	0	BOOL	cpu
	<i>LSL101 - MainProgram/IOINTERFACE - *21(OTE)</i>		
	<i>LSL101 - MainProgram/MAINLOGIC - 3(XIO)</i>		
<b>LSL201</b>	0	BOOL	cpu
	<i>LSL201 - MainProgram/IOINTERFACE - *23(OTE)</i>		
<b>LSL301</b>	0	BOOL	cpu
	<i>LSL301 - MainProgram/IOINTERFACE - *25(OTE)</i>		
<b>LSL401</b>	0	BOOL	cpu
	<i>LSL401 - MainProgram/IOINTERFACE - *18(OTE)</i>		
	<i>LSL401 - MainProgram/MAINLOGIC - 13(XIO)</i>		
<b>LT1</b>	86.39443	REAL	cpu
	<i>LT1 - MainProgram/IOINTERFACE - *0(MOV)</i>		
	<i>LT1 - MainProgram/LEVELCONTROL - 2(PID), 7(PID)</i>		
	<i>LT1 - MainProgram/MAINLOGIC - 12(GRT), 4(GRT)</i>		
	<i>LT1 - MainProgram/pidsqyare - 3(PID)</i>		
<b>msg_ai</b>		MESSAGE	cpu
	<i>msg_ai - MainProgram/COMMUNICATION - *0(MSG)</i>		
<b>msg_ao</b>		MESSAGE	cpu
	<i>msg_ao - MainProgram/COMMUNICATION - *1(MSG)</i>		
<b>msg_D0</b>		MESSAGE	cpu
	<i>msg_D0 - MainProgram/COMMUNICATION - *3(MSG)</i>		
<b>msg_DI</b>		MESSAGE	cpu
	<i>msg_DI - MainProgram/COMMUNICATION - *2(MSG)</i>		
<b>msg_spai</b>		MESSAGE	cpu
	<i>msg_spai - MainProgram/SprayDryerTest - *0(MSG)</i>		
<b>MSV1</b>	0.0	REAL	cpu
	<i>MSV1 - MainProgram/IOINTERFACE - 15(MOV)</i>		
<b>MSV2</b>	0.0	REAL	cpu

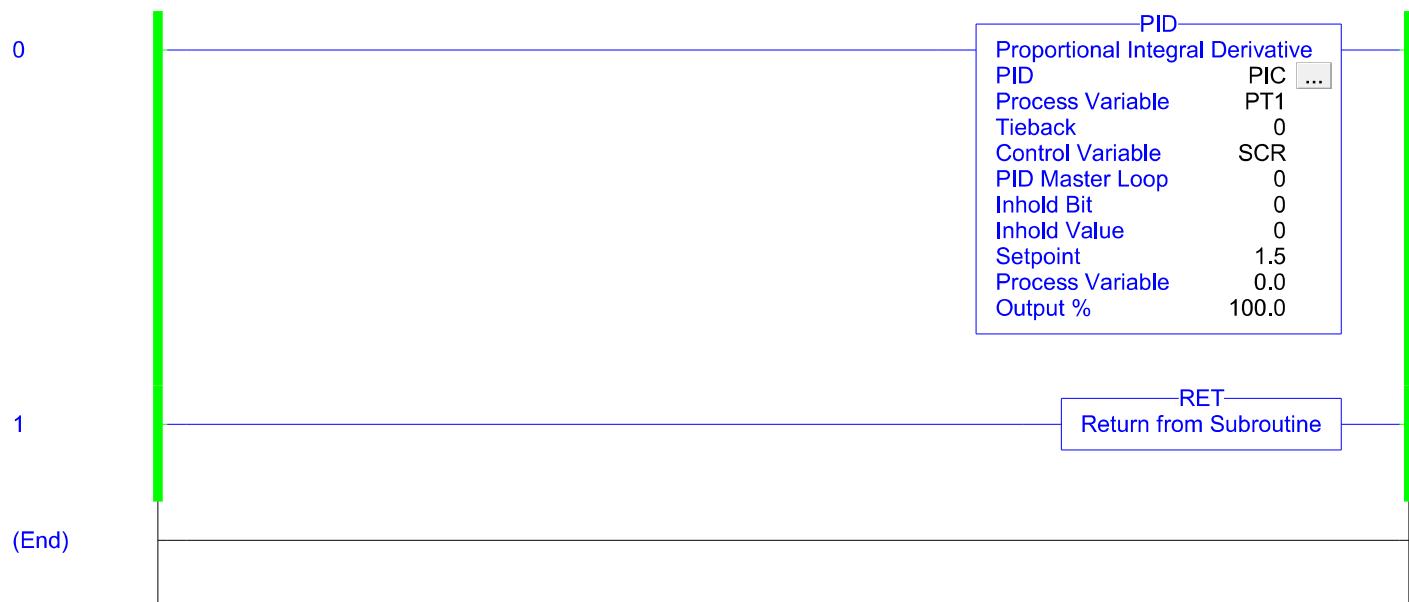
**MSV2 (Continued)**

*MSV2 - MainProgram/IOINTERFACE - 16(MOV)*

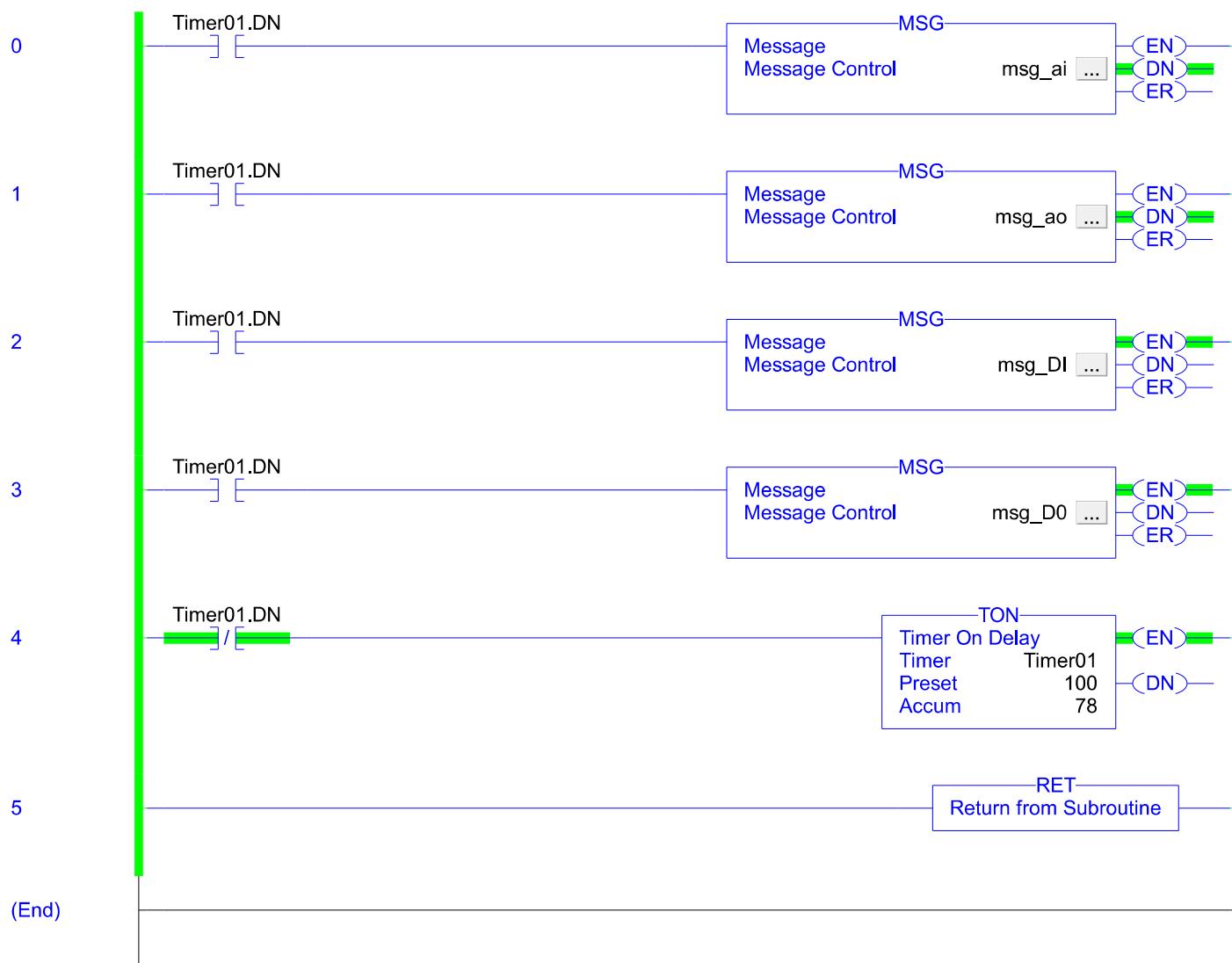
<b>onecontrol</b>	0	PID	cpu
<i>onecontrol - MainProgram/LEVELCONTROL - *7(PID)</i>			
<i>onecontrol.OUT - MainProgram/LEVELCONTROL - 8(MOV)</i>			
<b>out</b>	0	DINT	cpu
<i>out - MainProgram/pidsqyare - 1(MOV)</i>			
<i>out - MainProgram/square_wav - *1(MOV), *3(MOV)</i>			
<b>P101</b>	0	BOOL	cpu
<i>P101 - MainProgram/IOINTERFACE - 35(XIC)</i>			
<i>P101 - MainProgram/MAINLOGIC - *3(OTE)</i>			
<b>P101R</b>	0	BOOL	cpu
<i>P101R - MainProgram/IOINTERFACE - *26(OTE)</i>			
<b>p101scada</b>	0	BOOL	cpu
<i>p101scada - MainProgram/MAINLOGIC - 3(XIC)</i>			
<b>P101T</b>	0	BOOL	cpu
<i>P101T - MainProgram/IOINTERFACE - *27(OTE)</i>			
<b>P301</b>	0	BOOL	cpu
<i>P301 - MainProgram/IOINTERFACE - 36(XIC)</i>			
<i>P301 - MainProgram/MAINLOGIC - *15(OTE), 16(XIC)</i>			
<b>P301R</b>	0	BOOL	cpu
<i>P301R - MainProgram/IOINTERFACE - *28(OTE)</i>			
<b>P301T</b>	0	BOOL	cpu
<i>P301T - MainProgram/IOINTERFACE - *29(OTE)</i>			
<b>PEM</b>	0.024415553	REAL	cpu
<i>PEM - MainProgram/IOINTERFACE - *11(MOV)</i>			
<b>PHTEX</b>	0	BOOL	cpu
<i>PHTEX - MainProgram/MAINLOGIC - *17(OTE), 18(XIC)</i>			
<b>PIC</b>	0	PID	cpu
<i>PIC - MainProgram/BOILER_PRESSURE - *0(PID)</i>			
<b>PIDE_01</b>		PID_ENHANCED	MainProgram
<i>PIDE_01 - MainProgram/PID_test - *1-A2(IREF,SP), *1-B1(IREF,FTI), *1-B1(PIDE,PIDE_01), *1-C1(OREF,VFD101)</i>			
<b>PIDHX</b>	0	BOOL	cpu
<i>PIDHX - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(XIC)</i>			
<i>PIDHX - MainProgram/MAINLOGIC - *18(OTL), *19(OTU)</i>			
<b>pidsq</b>	0	PID	cpu
<i>pidsq - MainProgram/pidsqyare - *0(PID)</i>			
<i>pidsq.OUT - MainProgram/pidsqyare - 2(MOV)</i>			
<i>pidsq.SP - MainProgram/pidsqyare - *1(MOV)</i>			
<b>PS</b>	0	BOOL	cpu
<i>PS - MainProgram/LEVELCONTROL - 7(XIC), 8(XIC)</i>			
<i>PS - MainProgram/MAINLOGIC - *2(OTL), *9(OTU), 12(XIC), 14(XIC), 17(XIC), 3(XIC)</i>			
<b>PSH401</b>	0	BOOL	cpu
<i>PSH401 - MainProgram/IOINTERFACE - *20(OTE)</i>			
<i>PSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			

<b>PT1</b>	0.0	REAL	cpu
	<i>PT1 - MainProgram/BOILER_PRESSURE - 0(PID)</i>		
	<i>PT1 - MainProgram/IOINTERFACE - *1(MOV)</i>		
	<i>PT1 - MainProgram/MAINLOGIC - 14(GRT), 17(GRT)</i>		
<b>ref</b>	87.0	REAL	cpu
	<i>ref - MainProgram/MAINLOGIC - 4(GRT)</i>		
<b>REMOTELOCAL</b>	0	BOOL	cpu
	<i>REMOTELOCAL - MainProgram/IOINTERFACE - *30(OTE)</i>		
<b>reslt</b>	0.0	REAL	MainProgram
	<i>reslt - MainProgram/LEVELCONTROL - *0(MOV), 1(MOV)</i>		
<b>SCR</b>	100.0	REAL	cpu
	<i>SCR - MainProgram/BOILER_PRESSURE - *0(PID)</i>		
	<i>SCR - MainProgram/IOINTERFACE - 14(MOV)</i>		
<b>SOV201</b>	0	BOOL	cpu
	<i>SOV201 - MainProgram/IOINTERFACE - 38(XIC)</i>		
<b>SP</b>	0.0	REAL	cpu
	<i>SP - MainProgram/PID_test - 1-A2(IREF,SP), 1-B1(PIDE,PIDE_01.SPProg)</i>		
<b>SPAI</b>		REAL[20]	cpu
	<i>SPAI[0] - MainProgram/SprayDryerTest - *0(MSG)</i>		
<b>STARTHEATER</b>	0	BOOL	cpu
	<i>STARTHEATER - MainProgram/MAINLOGIC - *12(OTE), 13(XIC)</i>		
<b>stp</b>	0	BOOL	cpu
	<i>stp - MainProgram/MAINLOGIC - *8(OSF), 10(XIC), 19(XIC), 20(XIC), 9(XIC)</i>		
<b>STPING</b>	0	BOOL	cpu
	<i>STPING - MainProgram/MAINLOGIC - *10(OTL), *11(OTU), 15(XIC)</i>		
<b>STRT</b>	0	BOOL	cpu
	<i>STRT - MainProgram/MAINLOGIC - 0(XIC), 8(XIC)</i>		
<b>STRTRISE</b>	0	BOOL	cpu
	<i>STRTRISE - MainProgram/MAINLOGIC - *0(OSR), 1(XIC), 11(XIC), 2(XIC)</i>		
<b>t1</b>		TIMER	MainProgram
	<i>t1 - MainProgram/squar_wav - *0(TON)</i>		
	<i>t1.DN - MainProgram/squar_wav - 2(XIC)</i>		
	<i>t1.TT - MainProgram/squar_wav - 1(XIC)</i>		
<b>t123</b>		TIMER	cpu
	<i>t123 - MainProgram/MainRoutine - *5(TON)</i>		
	<i>t123.DN - MainProgram/MainRoutine - 2(XIO)</i>		
<b>t2</b>		TIMER	MainProgram
	<i>t2 - MainProgram/squar_wav - *2(TON)</i>		
	<i>t2.DN - MainProgram/squar_wav - 0(XIO)</i>		
	<i>t2.TT - MainProgram/squar_wav - 3(XIC)</i>		
<b>te</b>	0	BOOL	cpu
	<i>te - MainProgram/MAINLOGIC - *5(OTE), 7(XIC)</i>		
<b>threeelement</b>	0	BOOL	cpu
	<i>threeelement - MainProgram/LEVELCONTROL - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIC), 5(XIC), 6(XIC), 7(XIO), 8(XIO)</i>		
	<i>threeelement - MainProgram/MAINLOGIC - *7(OTE)</i>		

<b>Timer01</b>		TIMER	cpu
<i>Timer01 - MainProgram/COMMUNICATION - *4(TON)</i>			
<i>Timer01 - MainProgram/SprayDryerTest - *1(TON)</i>			
<i>Timer01.DN - MainProgram/COMMUNICATION - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIO)</i>			
<i>Timer01.DN - MainProgram/SprayDryerTest - 0(XIC), 1(XIO)</i>			
<b>TRE</b>	0	BOOL	cpu
<i>TRE - MainProgram/MAINLOGIC - *6(ONS)</i>			
<b>TSH401</b>	0	BOOL	cpu
<i>TSH401 - MainProgram/IOINTERFACE - *19(OTE)</i>			
<i>TSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>TT1</b>	41.079166	REAL	cpu
<i>TT1 - MainProgram/IOINTERFACE - *2(MOV)</i>			
<i>TT1 - MainProgram/MAINLOGIC - 5(GRT)</i>			
<b>TT2</b>	28.639442	REAL	cpu
<i>TT2 - MainProgram/IOINTERFACE - *3(MOV)</i>			
<b>TT3</b>	27.45529	REAL	cpu
<i>TT3 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(PID)</i>			
<i>TT3 - MainProgram/IOINTERFACE - *4(MOV)</i>			
<b>TT4</b>	27	DINT	cpu
<i>TT4 - MainProgram/IOINTERFACE - *5(MOV)</i>			
<b>TT5</b>	27.50412	REAL	cpu
<i>TT5 - MainProgram/IOINTERFACE - *6(MOV)</i>			
<b>TT6</b>	27.601782	REAL	cpu
<i>TT6 - MainProgram/IOINTERFACE - *7(MOV)</i>			
<b>VFD101</b>	0.0	REAL	cpu
<i>VFD101 - MainProgram/IOINTERFACE - 12(MOV)</i>			
<i>VFD101 - MainProgram/LEVELCONTROL - *5(PID), *6(MOV), *7(PID), *8(MOV)</i>			
<i>VFD101 - MainProgram/PID_test - *1-C1(OREF,VFD101), 1-B1(PIDE,PIDE_01.CVEU)</i>			
<i>VFD101 - MainProgram/pidsqyare - *0(PID), *2(MOV), *3(PID)</i>			
<b>VFD301</b>	0.0	REAL	cpu
<i>VFD301 - MainProgram/IOINTERFACE - 13(MOV)</i>			
<i>VFD301 - MainProgram/MAINLOGIC - *16(MOV)</i>			
<b>VPLCSEL</b>	0	BOOL	cpu
<i>VPLCSEL - MainProgram/IOINTERFACE - *31(OTE)</i>			



Name	Value	Data Type	Scope
PIC		PID	cpu
	PIC - MainProgram/BOILER_PRESSURE - *0(PID)		
PT1	0.0	REAL	cpu
	PT1 - MainProgram/BOILER_PRESSURE - 0(PID)		
	PT1 - MainProgram/IΟINTERFACE - *1(MOV)		
	PT1 - MainProgram/MΑΙΝLOGIC - 14(GRT), 17(GRT)		
SCR	100.0	REAL	cpu
	SCR - MainProgram/BOILER_PRESSURE - *0(PID)		
	SCR - MainProgram/IΟINTERFACE - 14(MOV)		



Name	Value	Data Type	Scope
AI	AI[0] - MainProgram/COMMUNICATION - *0(MSG) AI[0] - MainProgram/IOINTERFACE - 0(MOV) AI[10] - MainProgram/IOINTERFACE - 10(MOV) AI[11] - MainProgram/IOINTERFACE - 11(MOV) AI[1] - MainProgram/IOINTERFACE - 1(MOV) AI[2] - MainProgram/IOINTERFACE - 2(MOV) AI[3] - MainProgram/IOINTERFACE - 3(MOV) AI[4] - MainProgram/IOINTERFACE - 4(MOV) AI[5] - MainProgram/IOINTERFACE - 5(MOV) AI[6] - MainProgram/IOINTERFACE - 6(MOV) AI[7] - MainProgram/IOINTERFACE - 7(MOV) AI[8] - MainProgram/IOINTERFACE - 8(MOV) AI[9] - MainProgram/IOINTERFACE - 9(MOV)	REAL[13]	cpu
AO1	AO1[0] - MainProgram/COMMUNICATION - 1(MSG) AO1[0] - MainProgram/IOINTERFACE - *12(MOV) AO1[1] - MainProgram/IOINTERFACE - *13(MOV) AO1[2] - MainProgram/IOINTERFACE - *14(MOV) AO1[3] - MainProgram/IOINTERFACE - *15(MOV) AO1[4] - MainProgram/IOINTERFACE - *16(MOV) AO1[5] - MainProgram/IOINTERFACE - *17(MOV)	REAL[10]	cpu
DI	DI[0] - MainProgram/COMMUNICATION - *2(MSG) DI[0].0 - MainProgram/IOINTERFACE - 18(XIC) DI[10].0 - MainProgram/IOINTERFACE - 28(XIC) DI[11].0 - MainProgram/IOINTERFACE - 29(XIC) DI[12].0 - MainProgram/IOINTERFACE - 30(XIC) DI[13].0 - MainProgram/IOINTERFACE - 31(XIC) DI[14].0 - MainProgram/IOINTERFACE - 32(XIC) DI[15].0 - MainProgram/IOINTERFACE - 33(XIC) DI[16].0 - MainProgram/IOINTERFACE - 34(XIC) DI[1].0 - MainProgram/IOINTERFACE - 19(XIC) DI[2].0 - MainProgram/IOINTERFACE - 20(XIC) DI[3].0 - MainProgram/IOINTERFACE - 21(XIC) DI[4].0 - MainProgram/IOINTERFACE - 22(XIC) DI[5].0 - MainProgram/IOINTERFACE - 23(XIC) DI[6].0 - MainProgram/IOINTERFACE - 24(XIC) DI[7].0 - MainProgram/IOINTERFACE - 25(XIC) DI[8].0 - MainProgram/IOINTERFACE - 26(XIC) DI[9].0 - MainProgram/IOINTERFACE - 27(XIC)	INT[32]	cpu
DO1	DO1[0] - MainProgram/COMMUNICATION - 3(MSG) DO1[0].0 - MainProgram/IOINTERFACE - *35(OTE) DO1[1].0 - MainProgram/IOINTERFACE - *36(OTE) DO1[2].0 - MainProgram/IOINTERFACE - *37(OTE) DO1[3].0 - MainProgram/IOINTERFACE - *38(OTE) DO1[4].0 - MainProgram/IOINTERFACE - *39(OTE)	INT[10]	cpu
msg_ai	msg_ai - MainProgram/COMMUNICATION - *0(MSG)	MESSAGE	cpu
msg_ao	msg_ao - MainProgram/COMMUNICATION - *1(MSG)	MESSAGE	cpu
msg_D0	msg_D0 - MainProgram/COMMUNICATION - *3(MSG)	MESSAGE	cpu
msg_DI		MESSAGE	cpu

**msg\_DI (Continued)***msg\_DI - MainProgram/COMMUNICATION - \*2(MSG)***Timer01**

TIMER

cpu

*Timer01 - MainProgram/COMMUNICATION - \*4(TON)**Timer01 - MainProgram/SprayDryerTest - \*1(TON)**Timer01.DN - MainProgram/COMMUNICATION - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIO)**Timer01.DN - MainProgram/SprayDryerTest - 0(XIC), 1(XIO)*



Name	Value	Data Type	Scope
FCV1	0.0	REAL	cpu
	<i>FCV1 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - *0(PID)</i>		
	<i>FCV1 - MainProgram/IOINTERFACE - 17(MOV)</i>		
	<i>FCV1 - MainProgram/MAINLOGIC - *1(MOV), *20(MOV)</i>		
HXT		PID	cpu
	<i>HXT - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - *0(PID)</i>		
PIDHX	0	BOOL	cpu
	<i>PIDHX - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(XIC)</i>		
	<i>PIDHX - MainProgram/MAINLOGIC - *18(OTL), *19(OTU)</i>		
TT3	27.45529	REAL	cpu
	<i>TT3 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(PID)</i>		
	<i>TT3 - MainProgram/IOINTERFACE - *4(MOV)</i>		









Name	Value	Data Type	Scope
<b>AI</b>		REAL[13]	cpu
AI[0] - MainProgram/COMMUNICATION - *0(MSG)			
AI[0] - MainProgram/IOINTERFACE - 0(MOV)			
AI[10] - MainProgram/IOINTERFACE - 10(MOV)			
AI[11] - MainProgram/IOINTERFACE - 11(MOV)			
AI[1] - MainProgram/IOINTERFACE - 1(MOV)			
AI[2] - MainProgram/IOINTERFACE - 2(MOV)			
AI[3] - MainProgram/IOINTERFACE - 3(MOV)			
AI[4] - MainProgram/IOINTERFACE - 4(MOV)			
AI[5] - MainProgram/IOINTERFACE - 5(MOV)			
AI[6] - MainProgram/IOINTERFACE - 6(MOV)			
AI[7] - MainProgram/IOINTERFACE - 7(MOV)			
AI[8] - MainProgram/IOINTERFACE - 8(MOV)			
AI[9] - MainProgram/IOINTERFACE - 9(MOV)			
<b>AO1</b>		REAL[10]	cpu
AO1[0] - MainProgram/COMMUNICATION - 1(MSG)			
AO1[0] - MainProgram/IOINTERFACE - *12(MOV)			
AO1[1] - MainProgram/IOINTERFACE - *13(MOV)			
AO1[2] - MainProgram/IOINTERFACE - *14(MOV)			
AO1[3] - MainProgram/IOINTERFACE - *15(MOV)			
AO1[4] - MainProgram/IOINTERFACE - *16(MOV)			
AO1[5] - MainProgram/IOINTERFACE - *17(MOV)			
<b>CONTROLOSEL</b>	0	BOOL	cpu
CONTROLOSEL - MainProgram/IOINTERFACE - *33(OTE)			
<b>DCSSEL</b>	1	BOOL	cpu
DCSSEL - MainProgram/IOINTERFACE - *32(OTE)			
<b>DI</b>		INT[32]	cpu
DI[0] - MainProgram/COMMUNICATION - *2(MSG)			
DI[0].0 - MainProgram/IOINTERFACE - 18(XIC)			
DI[10].0 - MainProgram/IOINTERFACE - 28(XIC)			
DI[11].0 - MainProgram/IOINTERFACE - 29(XIC)			
DI[12].0 - MainProgram/IOINTERFACE - 30(XIC)			
DI[13].0 - MainProgram/IOINTERFACE - 31(XIC)			
DI[14].0 - MainProgram/IOINTERFACE - 32(XIC)			
DI[15].0 - MainProgram/IOINTERFACE - 33(XIC)			
DI[16].0 - MainProgram/IOINTERFACE - 34(XIC)			
DI[1].0 - MainProgram/IOINTERFACE - 19(XIC)			
DI[2].0 - MainProgram/IOINTERFACE - 20(XIC)			
DI[3].0 - MainProgram/IOINTERFACE - 21(XIC)			
DI[4].0 - MainProgram/IOINTERFACE - 22(XIC)			
DI[5].0 - MainProgram/IOINTERFACE - 23(XIC)			
DI[6].0 - MainProgram/IOINTERFACE - 24(XIC)			
DI[7].0 - MainProgram/IOINTERFACE - 25(XIC)			
DI[8].0 - MainProgram/IOINTERFACE - 26(XIC)			
DI[9].0 - MainProgram/IOINTERFACE - 27(XIC)			
<b>DO1</b>		INT[10]	cpu
DO1[0] - MainProgram/COMMUNICATION - 3(MSG)			
DO1[0].0 - MainProgram/IOINTERFACE - *35(OTE)			
DO1[1].0 - MainProgram/IOINTERFACE - *36(OTE)			
DO1[2].0 - MainProgram/IOINTERFACE - *37(OTE)			
DO1[3].0 - MainProgram/IOINTERFACE - *38(OTE)			
DO1[4].0 - MainProgram/IOINTERFACE - *39(OTE)			
<b>FCV1</b>	0.0	REAL	cpu
FCV1 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - *0(PID)			
FCV1 - MainProgram/IOINTERFACE - 17(MOV)			
FCV1 - MainProgram/MAINLOGIC - *1(MOV), *20(MOV)			

<b>FT1</b>	0.0	REAL	cpu
<i>FT1 - MainProgram/IOINTERFACE - *10(MOV)</i>			
<i>FT1 - MainProgram/LEVELCONTROL - 5(PID)</i>			
<i>FT1 - MainProgram/PID_test - 1-B1(IREF,FT1), 1-B1(PIDE,PIDE_01.PV)</i>			
<i>FT1 - MainProgram/pidsqyare - 0(PID)</i>			
<b>FT2</b>	0.0	REAL	cpu
<i>FT2 - MainProgram/IOINTERFACE - *9(MOV)</i>			
<b>FT3</b>	0.0	REAL	cpu
<i>FT3 - MainProgram/IOINTERFACE - *8(MOV)</i>			
<i>FT3 - MainProgram/LEVELCONTROL - 0(MOV)</i>			
<b>HEATER</b>	0	BOOL	cpu
<i>HEATER - MainProgram/IOINTERFACE - 37(XIC)</i>			
<i>HEATER - MainProgram/MAINLOGIC - *13(OTE)</i>			
<b>HOOTER</b>	0	BOOL	cpu
<i>HOOTER - MainProgram/IOINTERFACE - 39(XIC)</i>			
<b>HOOTERACK</b>	0	BOOL	cpu
<i>HOOTERACK - MainProgram/IOINTERFACE - *34(OTE)</i>			
<b>LSH201</b>	1	BOOL	cpu
<i>LSH201 - MainProgram/IOINTERFACE - *22(OTE)</i>			
<b>LSH301</b>	0	BOOL	cpu
<i>LSH301 - MainProgram/IOINTERFACE - *24(OTE)</i>			
<b>LSL101</b>	0	BOOL	cpu
<i>LSL101 - MainProgram/IOINTERFACE - *21(OTE)</i>			
<i>LSL101 - MainProgram/MAINLOGIC - 3(XIO)</i>			
<b>LSL201</b>	0	BOOL	cpu
<i>LSL201 - MainProgram/IOINTERFACE - *23(OTE)</i>			
<b>LSL301</b>	0	BOOL	cpu
<i>LSL301 - MainProgram/IOINTERFACE - *25(OTE)</i>			
<b>LSL401</b>	0	BOOL	cpu
<i>LSL401 - MainProgram/IOINTERFACE - *18(OTE)</i>			
<i>LSL401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>LT1</b>	86.39443	REAL	cpu
<i>LT1 - MainProgram/IOINTERFACE - *0(MOV)</i>			
<i>LT1 - MainProgram/LEVELCONTROL - 2(PID), 7(PID)</i>			
<i>LT1 - MainProgram/MAINLOGIC - 12(GRT), 4(GRT)</i>			
<i>LT1 - MainProgram/pidsqyare - 3(PID)</i>			
<b>MSV1</b>	0.0	REAL	cpu
<i>MSV1 - MainProgram/IOINTERFACE - 15(MOV)</i>			
<b>MSV2</b>	0.0	REAL	cpu
<i>MSV2 - MainProgram/IOINTERFACE - 16(MOV)</i>			
<b>P101</b>	0	BOOL	cpu
<i>P101 - MainProgram/IOINTERFACE - 35(XIC)</i>			
<i>P101 - MainProgram/MAINLOGIC - *3(OTE)</i>			
<b>P101R</b>	0	BOOL	cpu
<i>P101R - MainProgram/IOINTERFACE - *26(OTE)</i>			
<b>P101T</b>	0	BOOL	cpu

**P101T (Continued)***P101T - MainProgram/IOINTERFACE - \*27(OTE)*

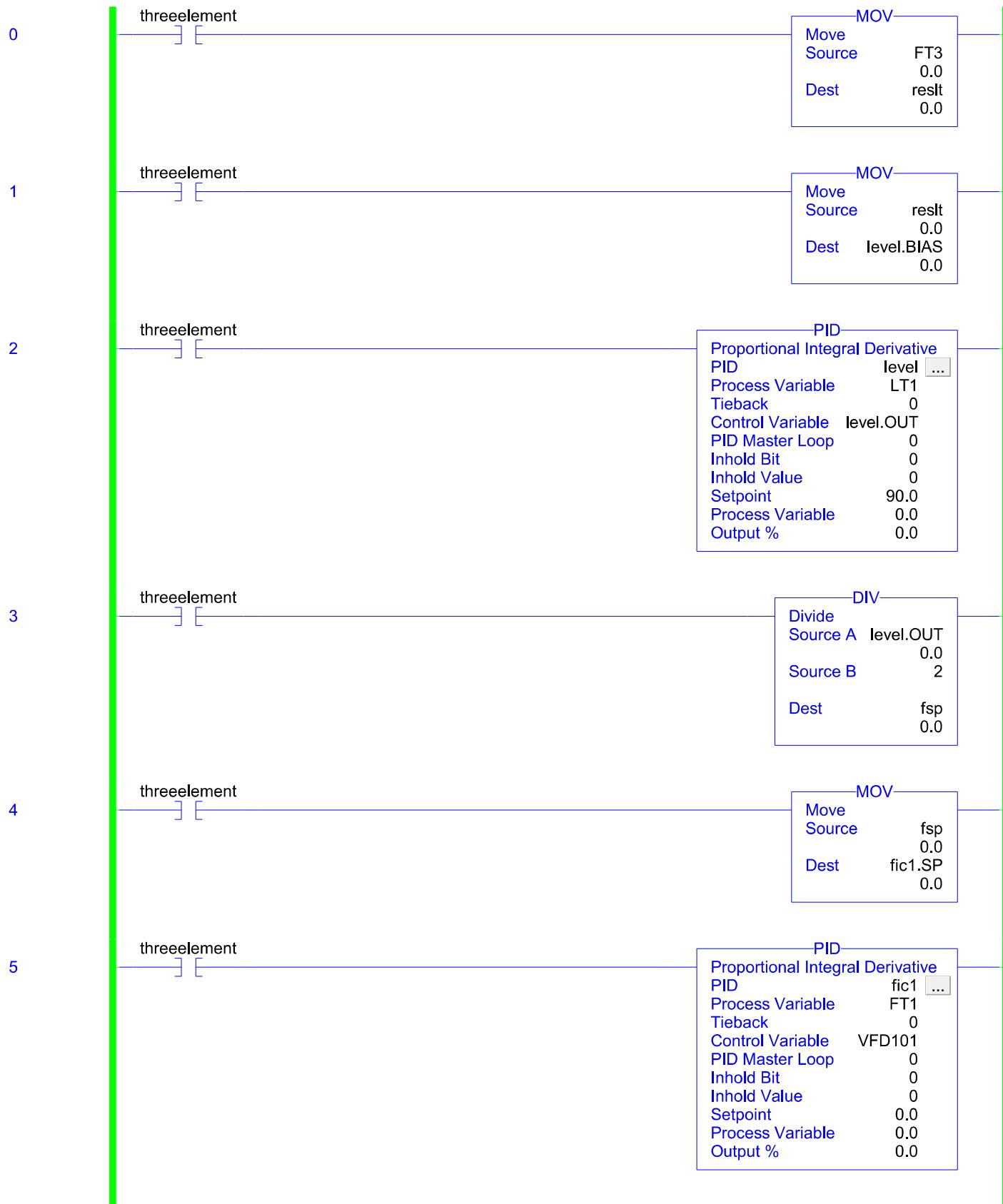
<b>P301</b>	0	BOOL	cpu
<i>P301 - MainProgram/IOINTERFACE - 36(XIC)</i>			
<i>P301 - MainProgram/MAINLOGIC - *15(OTE), 16(XIC)</i>			
<b>P301R</b>	0	BOOL	cpu
<i>P301R - MainProgram/IOINTERFACE - *28(OTE)</i>			
<b>P301T</b>	0	BOOL	cpu
<i>P301T - MainProgram/IOINTERFACE - *29(OTE)</i>			
<b>PEM</b>	0.024415553	REAL	cpu
<i>PEM - MainProgram/IOINTERFACE - *11(MOV)</i>			
<b>PSH401</b>	0	BOOL	cpu
<i>PSH401 - MainProgram/IOINTERFACE - *20(OTE)</i>			
<i>PSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>PT1</b>	0.0	REAL	cpu
<i>PT1 - MainProgram/BOILER_PRESSURE - 0(PID)</i>			
<i>PT1 - MainProgram/IOINTERFACE - *1(MOV)</i>			
<i>PT1 - MainProgram/MAINLOGIC - 14(GRT), 17(GRT)</i>			
<b>REMOTELOCAL</b>	0	BOOL	cpu
<i>REMOTELOCAL - MainProgram/IOINTERFACE - *30(OTE)</i>			
<b>SCR</b>	100.0	REAL	cpu
<i>SCR - MainProgram/BOILER_PRESSURE - *0(PID)</i>			
<i>SCR - MainProgram/IOINTERFACE - 14(MOV)</i>			
<b>SOV201</b>	0	BOOL	cpu
<i>SOV201 - MainProgram/IOINTERFACE - 38(XIC)</i>			
<b>TSH401</b>	0	BOOL	cpu
<i>TSH401 - MainProgram/IOINTERFACE - *19(OTE)</i>			
<i>TSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>TT1</b>	41.079166	REAL	cpu
<i>TT1 - MainProgram/IOINTERFACE - *2(MOV)</i>			
<i>TT1 - MainProgram/MAINLOGIC - 5(GRT)</i>			
<b>TT2</b>	28.639442	REAL	cpu
<i>TT2 - MainProgram/IOINTERFACE - *3(MOV)</i>			
<b>TT3</b>	27.45529	REAL	cpu
<i>TT3 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(PID)</i>			
<i>TT3 - MainProgram/IOINTERFACE - *4(MOV)</i>			
<b>TT4</b>	27	DINT	cpu
<i>TT4 - MainProgram/IOINTERFACE - *5(MOV)</i>			
<b>TT5</b>	27.50412	REAL	cpu
<i>TT5 - MainProgram/IOINTERFACE - *6(MOV)</i>			
<b>TT6</b>	27.601782	REAL	cpu
<i>TT6 - MainProgram/IOINTERFACE - *7(MOV)</i>			
<b>VFD101</b>	0.0	REAL	cpu
<i>VFD101 - MainProgram/IOINTERFACE - 12(MOV)</i>			
<i>VFD101 - MainProgram/LEVELCONTROL - *5(PID), *6(MOV), *7(PID), *8(MOV)</i>			
<i>VFD101 - MainProgram/PID_test - *1-C1(OREF,VFD101), 1-B1(PIDE,PIDE_01.CVEU)</i>			

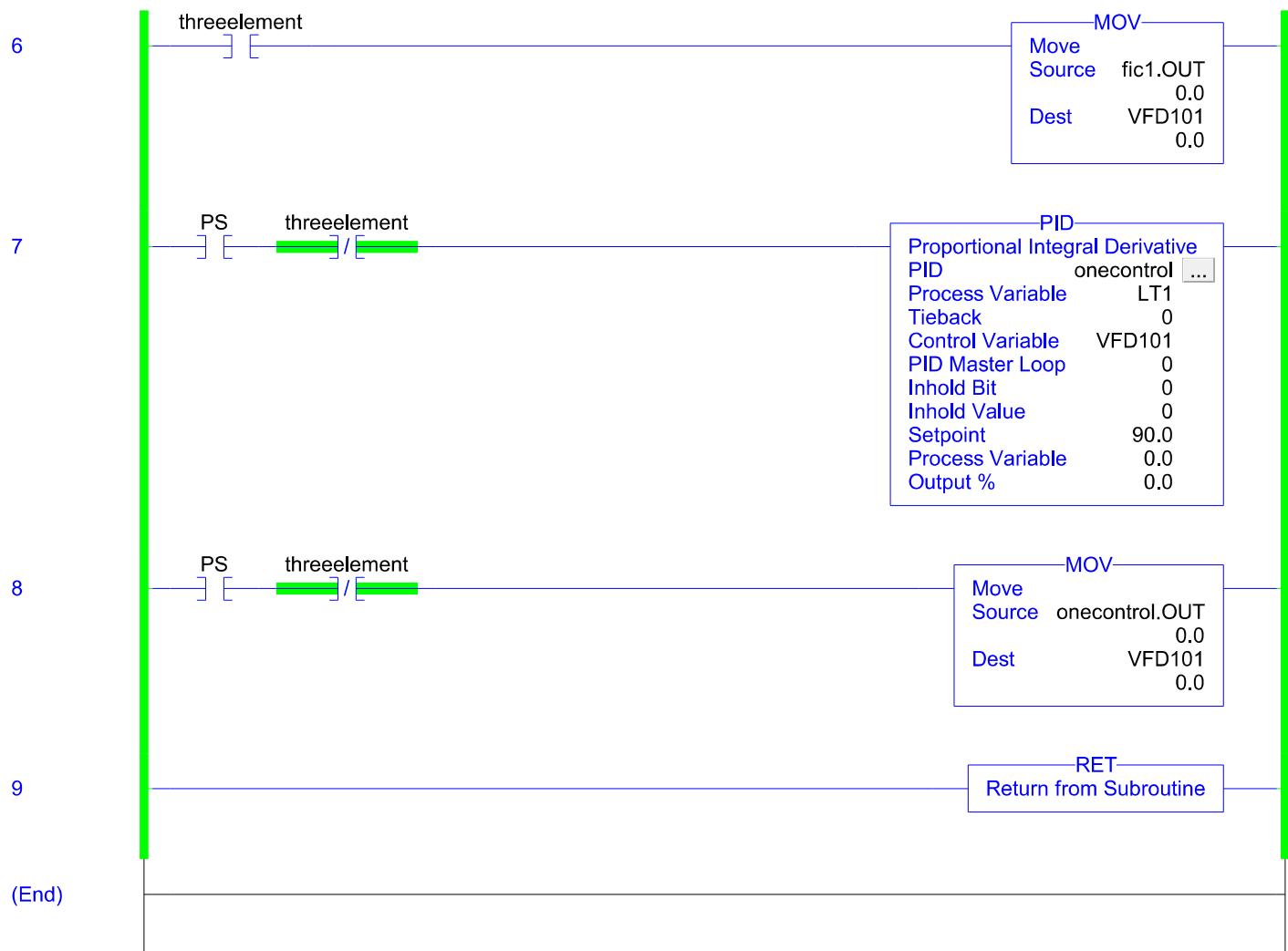
**VFD101 (Continued)**

*VFD101 - MainProgram/pidsqyare - \*0(PID), \*2(MOV), \*3(PID)*

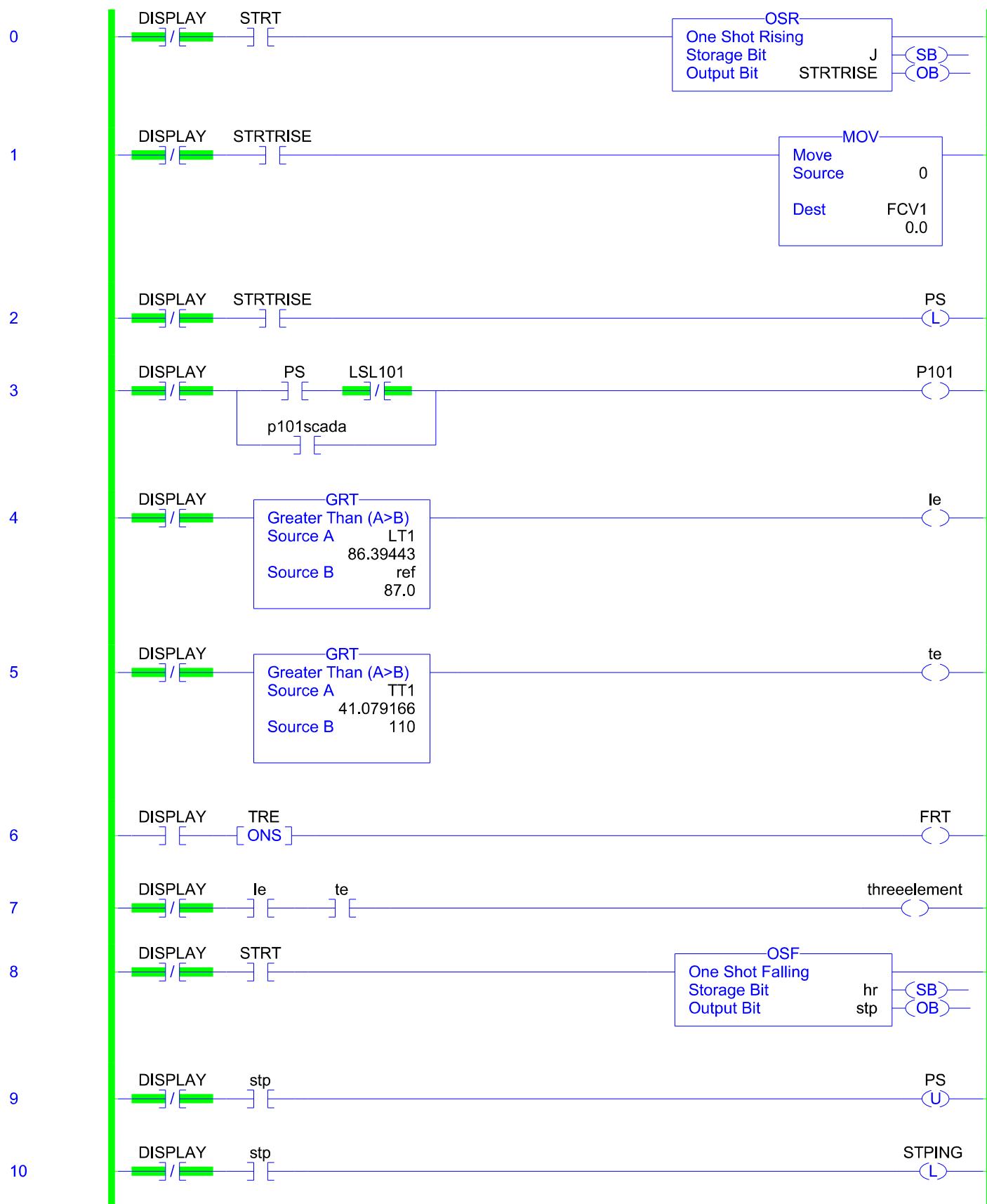
**VFD301** 0.0 REAL cpu  
*VFD301 - MainProgram/IOINTERFACE - 13(MOV)*  
*VFD301 - MainProgram/MAINLOGIC - \*16(MOV)*

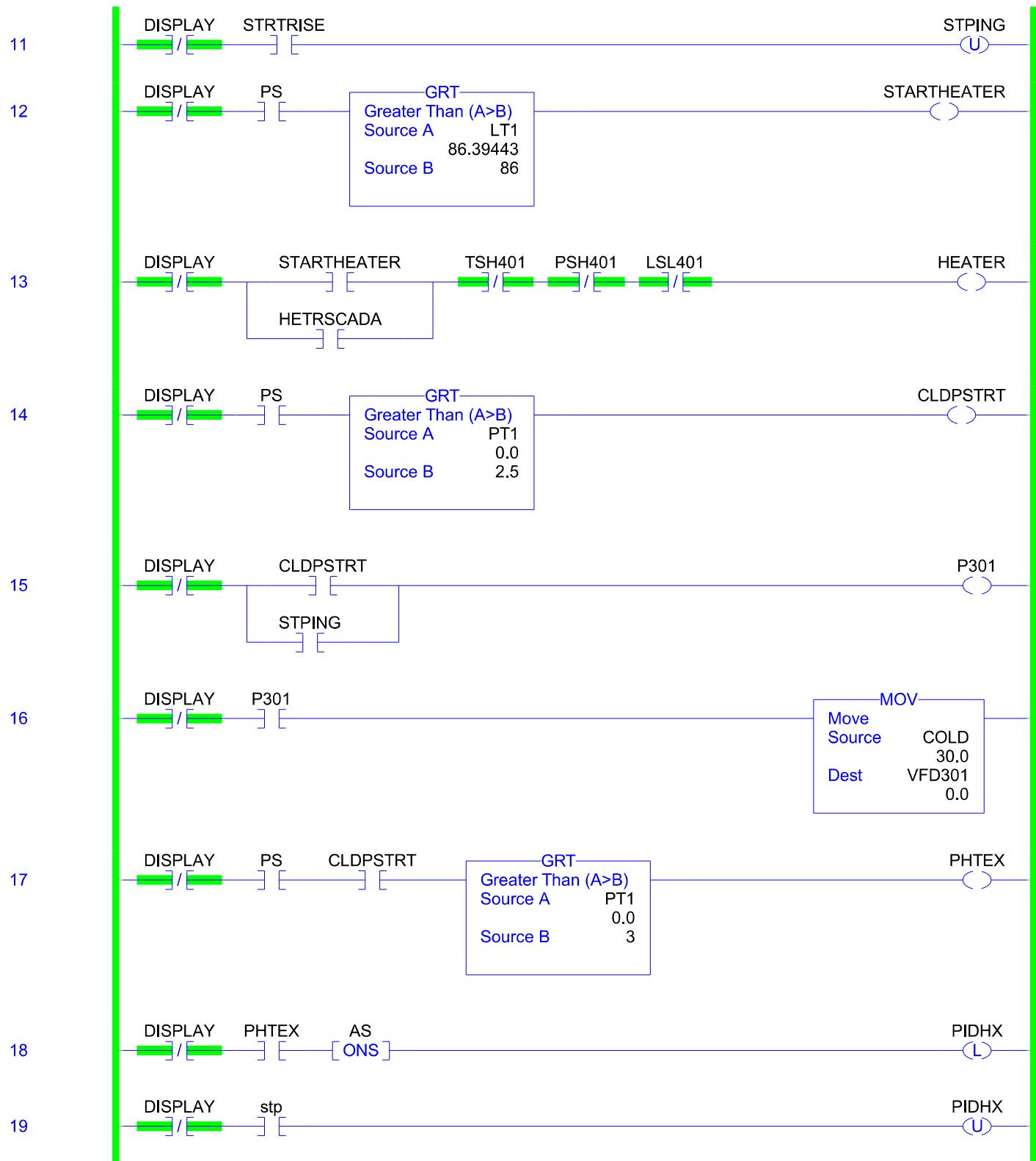
**VPLCSEL** 0 BOOL cpu  
*VPLCSEL - MainProgram/IOINTERFACE - \*31(OTE)*





Name	Value	Data Type	Scope
<b>fic1</b>		PID	cpu
	<i>fic1 - MainProgram/LEVELCONTROL - *5(PID)</i>		
	<i>fic1.OUT - MainProgram/LEVELCONTROL - 6(MOV)</i>		
	<i>fic1.SP - MainProgram/LEVELCONTROL - *4(MOV)</i>		
<b>fsp</b>	0.0	REAL	MainProgram
	<i>fsp - MainProgram/LEVELCONTROL - *3(DIV), 4(MOV)</i>		
<b>FT1</b>	0.0	REAL	cpu
	<i>FT1 - MainProgram/IΟINTERFACE - *10(MOV)</i>		
	<i>FT1 - MainProgram/LEVELCONTROL - 5(PID)</i>		
	<i>FT1 - MainProgram/PID_test - 1-B1(IREF,FT1), 1-B1(PIDE,PIDE_01.PV)</i>		
	<i>FT1 - MainProgram/pidsqyare - 0(PID)</i>		
<b>FT3</b>	0.0	REAL	cpu
	<i>FT3 - MainProgram/IΟINTERFACE - *8(MOV)</i>		
	<i>FT3 - MainProgram/LEVELCONTROL - 0(MOV)</i>		
<b>level</b>		PID	cpu
	<i>level - MainProgram/LEVELCONTROL - *2(PID)</i>		
	<i>level - MainProgram/pidsqyare - *3(PID)</i>		
	<i>level.BIAS - MainProgram/LEVELCONTROL - *1(MOV)</i>		
	<i>level.OUT - MainProgram/LEVELCONTROL - *2(PID), 3(DIV)</i>		
<b>LT1</b>	86.39443	REAL	cpu
	<i>LT1 - MainProgram/IΟINTERFACE - *0(MOV)</i>		
	<i>LT1 - MainProgram/LEVELCONTROL - 2(PID), 7(PID)</i>		
	<i>LT1 - MainProgram/MΑΙΝLOGIC - 12(GRT), 4(GRT)</i>		
	<i>LT1 - MainProgram/pidsqyare - 3(PID)</i>		
<b>onecontrol</b>		PID	cpu
	<i>onecontrol - MainProgram/LEVELCONTROL - *7(PID)</i>		
	<i>onecontrol.OUT - MainProgram/LEVELCONTROL - 8(MOV)</i>		
<b>PS</b>	0	BOOL	cpu
	<i>PS - MainProgram/LEVELCONTROL - 7(XIC), 8(XIC)</i>		
	<i>PS - MainProgram/MΑΙΝLOGIC - *2(OTL), *9(OTU), 12(XIC), 14(XIC), 17(XIC), 3(XIC)</i>		
<b>reslt</b>	0.0	REAL	MainProgram
	<i>reslt - MainProgram/LEVELCONTROL - *0(MOV), 1(MOV)</i>		
<b>threeelement</b>	0	BOOL	cpu
	<i>threeelement - MainProgram/LEVELCONTROL - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIC), 5(XIC), 6(XIC), 7(XIO), 8(XIO)</i>		
	<i>threeelement - MainProgram/MΑΙΝLOGIC - *7(OTE)</i>		
<b>VFD101</b>	0.0	REAL	cpu
	<i>VFD101 - MainProgram/IΟINTERFACE - 12(MOV)</i>		
	<i>VFD101 - MainProgram/LEVELCONTROL - *5(PID), *6(MOV), *7(PID), *8(MOV)</i>		
	<i>VFD101 - MainProgram/PID_test - *1-C1(OREF,VFD101), 1-B1(PIDE,PIDE_01.CVEU)</i>		
	<i>VFD101 - MainProgram/pidsqyare - *0(PID), *2(MOV), *3(PID)</i>		

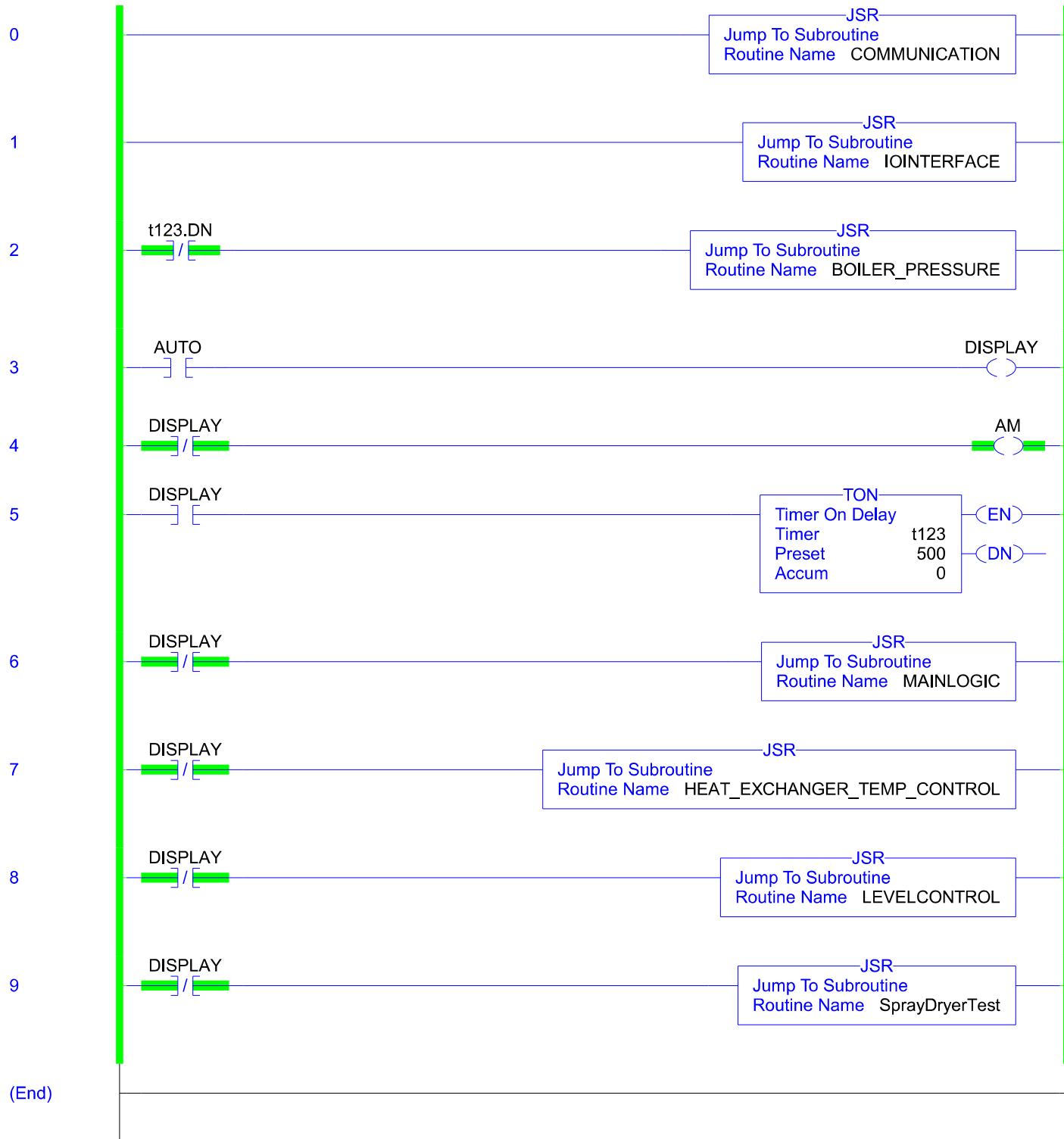




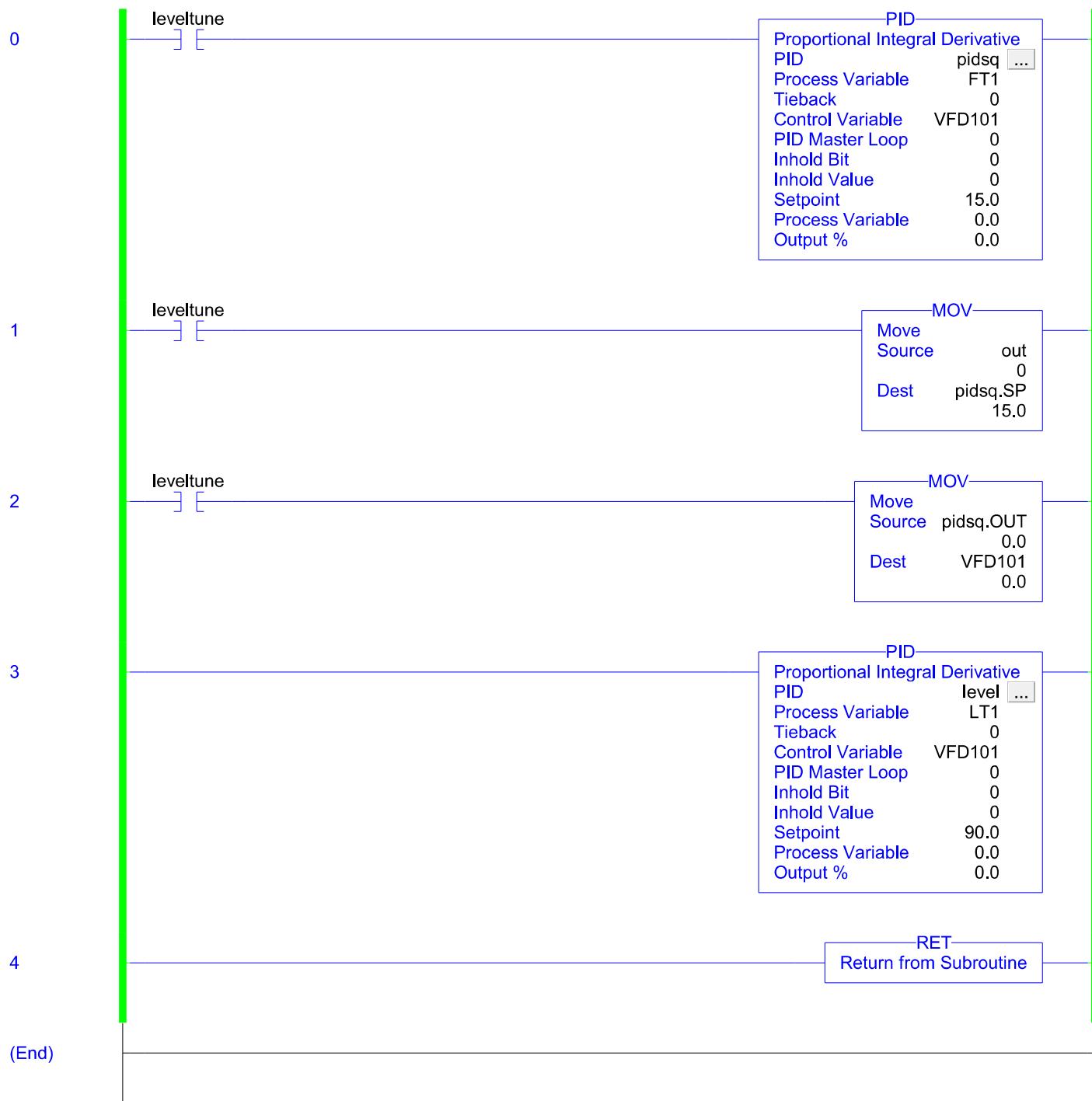


Name	Value	Data Type	Scope
AS	0	BOOL	cpu
	<i>AS - MainProgram/MAINLOGIC - *18(ONS)</i>		
CLDPSTRT	0	BOOL	cpu
	<i>CLDPSTRT - MainProgram/MAINLOGIC - *14(OTE), 15(XIC), 17(XIC)</i>		
COLD	30.0	REAL	cpu
	<i>COLD - MainProgram/MAINLOGIC - 16(MOV)</i>		
DISPLAY	0	BOOL	cpu
	<i>DISPLAY - MainProgram/MAINLOGIC - 0(XIO), 1(XIO), 10(XIO), 11(XIO), 12(XIO), 13(XIO), 14(XIO), 15(XIO), 16(XIO), 17(XIO), 18(XIO), 19(XIO), 2(XIO), 20(XIO), 3(XIO), 4(XIO), 5(XIO), 6(XIC), 7(XIO), 8(XIO), 9(XIO)</i>		
	<i>DISPLAY - MainProgram/MainRoutine - *3(OTE), 4(XIO), 5(XIC), 6(XIO), 7(XIO), 8(XIO), 9(XIO)</i>		
FCV1	0.0	REAL	cpu
	<i>FCV1 - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - *0(PID)</i>		
	<i>FCV1 - MainProgram/IOINTERFACE - 17(MOV)</i>		
	<i>FCV1 - MainProgram/MAINLOGIC - *1(MOV), *20(MOV)</i>		
FRT	0	BOOL	cpu
	<i>FRT - MainProgram/MAINLOGIC - *6(OTE)</i>		
HEATER	0	BOOL	cpu
	<i>HEATER - MainProgram/IOINTERFACE - 37(XIC)</i>		
	<i>HEATER - MainProgram/MAINLOGIC - *13(OTE)</i>		
HETRSCADA	0	BOOL	cpu
	<i>HETRSCADA - MainProgram/MAINLOGIC - 13(XIC)</i>		
hr	0	BOOL	cpu
	<i>hr - MainProgram/MAINLOGIC - *8(OSF)</i>		
J	0	BOOL	cpu
	<i>J - MainProgram/MAINLOGIC - *0(OSR)</i>		
le	0	BOOL	cpu
	<i>le - MainProgram/MAINLOGIC - *4(OTE), 7(XIC)</i>		
LSL101	0	BOOL	cpu
	<i>LSL101 - MainProgram/IOINTERFACE - *21(OTE)</i>		
	<i>LSL101 - MainProgram/MAINLOGIC - 3(XIO)</i>		
LSL401	0	BOOL	cpu
	<i>LSL401 - MainProgram/IOINTERFACE - *18(OTE)</i>		
	<i>LSL401 - MainProgram/MAINLOGIC - 13(XIO)</i>		
LT1	86.39443	REAL	cpu
	<i>LT1 - MainProgram/IOINTERFACE - *0(MOV)</i>		
	<i>LT1 - MainProgram/LEVELCONTROL - 2(PID), 7(PID)</i>		
	<i>LT1 - MainProgram/MAINLOGIC - 12(GRT), 4(GRT)</i>		
	<i>LT1 - MainProgram/pidsqyare - 3(PID)</i>		
P101	0	BOOL	cpu
	<i>P101 - MainProgram/IOINTERFACE - 35(XIC)</i>		
	<i>P101 - MainProgram/MAINLOGIC - *3(OTE)</i>		
p101scada	0	BOOL	cpu
	<i>p101scada - MainProgram/MAINLOGIC - 3(XIC)</i>		
P301	0	BOOL	cpu
	<i>P301 - MainProgram/IOINTERFACE - 36(XIC)</i>		
	<i>P301 - MainProgram/MAINLOGIC - *15(OTE), 16(XIC)</i>		

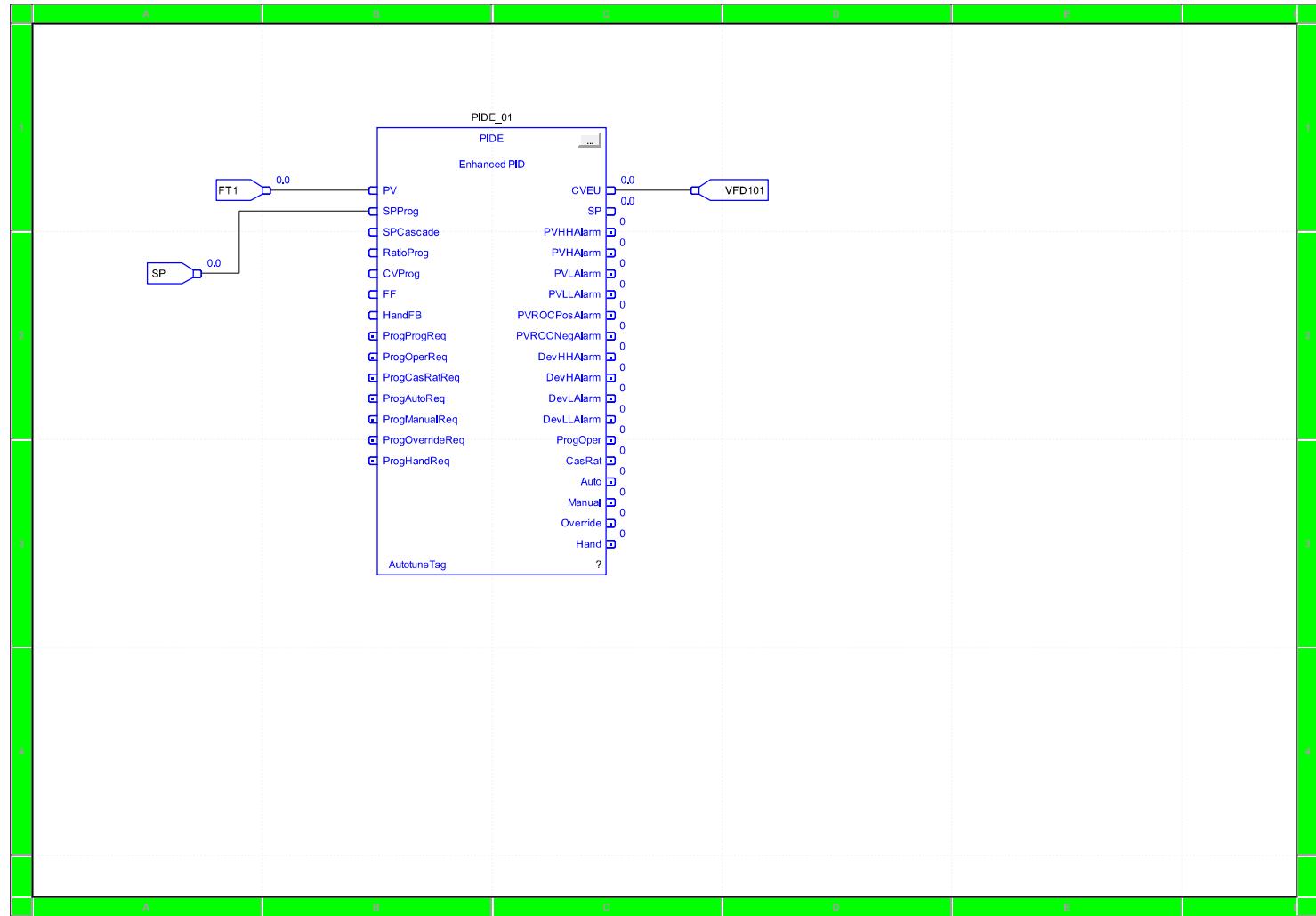
<b>PHTEX</b>	0	BOOL	cpu
<i>PHTEX - MainProgram/MAINLOGIC - *17(OTE), 18(XIC)</i>			
<b>PIDHX</b>	0	BOOL	cpu
<i>PIDHX - MainProgram/HEAT_EXCHANGER_TEMP_CONTROL - 0(XIC)</i>			
<i>PIDHX - MainProgram/MAINLOGIC - *18(OTL), *19(OTU)</i>			
<b>PS</b>	0	BOOL	cpu
<i>PS - MainProgram/LEVELCONTROL - 7(XIC), 8(XIC)</i>			
<i>PS - MainProgram/MAINLOGIC - *2(OTL), *9(OTU), 12(XIC), 14(XIC), 17(XIC), 3(XIC)</i>			
<b>PSH401</b>	0	BOOL	cpu
<i>PSH401 - MainProgram/IOINTERFACE - *20(OTE)</i>			
<i>PSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>PT1</b>	0.0	REAL	cpu
<i>PT1 - MainProgram/BOILER_PRESSURE - 0(PID)</i>			
<i>PT1 - MainProgram/IOINTERFACE - *1(MOV)</i>			
<i>PT1 - MainProgram/MAINLOGIC - 14(GRT), 17(GRT)</i>			
<b>ref</b>	87.0	REAL	cpu
<i>ref - MainProgram/MAINLOGIC - 4(GRT)</i>			
<b>STARTHEATER</b>	0	BOOL	cpu
<i>STARTHEATER - MainProgram/MAINLOGIC - *12(OTE), 13(XIC)</i>			
<b>stp</b>	0	BOOL	cpu
<i>stp - MainProgram/MAINLOGIC - *8(OSF), 10(XIC), 19(XIC), 20(XIC), 9(XIC)</i>			
<b>STPING</b>	0	BOOL	cpu
<i>STPING - MainProgram/MAINLOGIC - *10(OTL), *11(OTU), 15(XIC)</i>			
<b>STRT</b>	0	BOOL	cpu
<i>STRT - MainProgram/MAINLOGIC - 0(XIC), 8(XIC)</i>			
<b>STRTRISE</b>	0	BOOL	cpu
<i>STRTRISE - MainProgram/MAINLOGIC - *0(OSR), 1(XIC), 11(XIC), 2(XIC)</i>			
<b>te</b>	0	BOOL	cpu
<i>te - MainProgram/MAINLOGIC - *5(OTE), 7(XIC)</i>			
<b>threelement</b>	0	BOOL	cpu
<i>threelement - MainProgram/LEVELCONTROL - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIC), 5(XIC), 6(XIC), 7(XIC), 8(XIO)</i>			
<i>threelement - MainProgram/MAINLOGIC - *7(OTE)</i>			
<b>TRE</b>	0	BOOL	cpu
<i>TRE - MainProgram/MAINLOGIC - *6(ONS)</i>			
<b>TSH401</b>	0	BOOL	cpu
<i>TSH401 - MainProgram/IOINTERFACE - *19(OTE)</i>			
<i>TSH401 - MainProgram/MAINLOGIC - 13(XIO)</i>			
<b>TT1</b>	41.079166	REAL	cpu
<i>TT1 - MainProgram/IOINTERFACE - *2(MOV)</i>			
<i>TT1 - MainProgram/MAINLOGIC - 5(GRT)</i>			
<b>VFD301</b>	0.0	REAL	cpu
<i>VFD301 - MainProgram/IOINTERFACE - 13(MOV)</i>			
<i>VFD301 - MainProgram/MAINLOGIC - *16(MOV)</i>			



Name	Value	Data Type	Scope
AM	1	BOOL	cpu
	<i>AM - MainProgram/MainRoutine - *4(OTE)</i>		
AUTO	0	BOOL	cpu
	<i>AUTO - MainProgram/MainRoutine - 3(XIC)</i>		
DISPLAY	0	BOOL	cpu
	<i>DISPLAY - MainProgram/MANLOGIC - 0(XIO), 1(XIO), 10(XIO), 11(XIO), 12(XIO), 13(XIO), 14(XIO), 15(XIO), 16(XIO), 17(XIO), 18(XIO), 19(XIO), 2(XIO), 20(XIO), 3(XIO), 4(XIO), 5(XIO), 6(XIC), 7(XIO), 8(XIO), 9(XIO)</i>		
	<i>DISPLAY - MainProgram/MainRoutine - *3(OTE), 4(XIO), 5(XIC), 6(XIO), 7(XIO), 8(XIO), 9(XIO)</i>		
t123		TIMER	cpu
	<i>t123 - MainProgram/MainRoutine - *5(TON)</i>		
	<i>t123.DN - MainProgram/MainRoutine - 2(XIO)</i>		



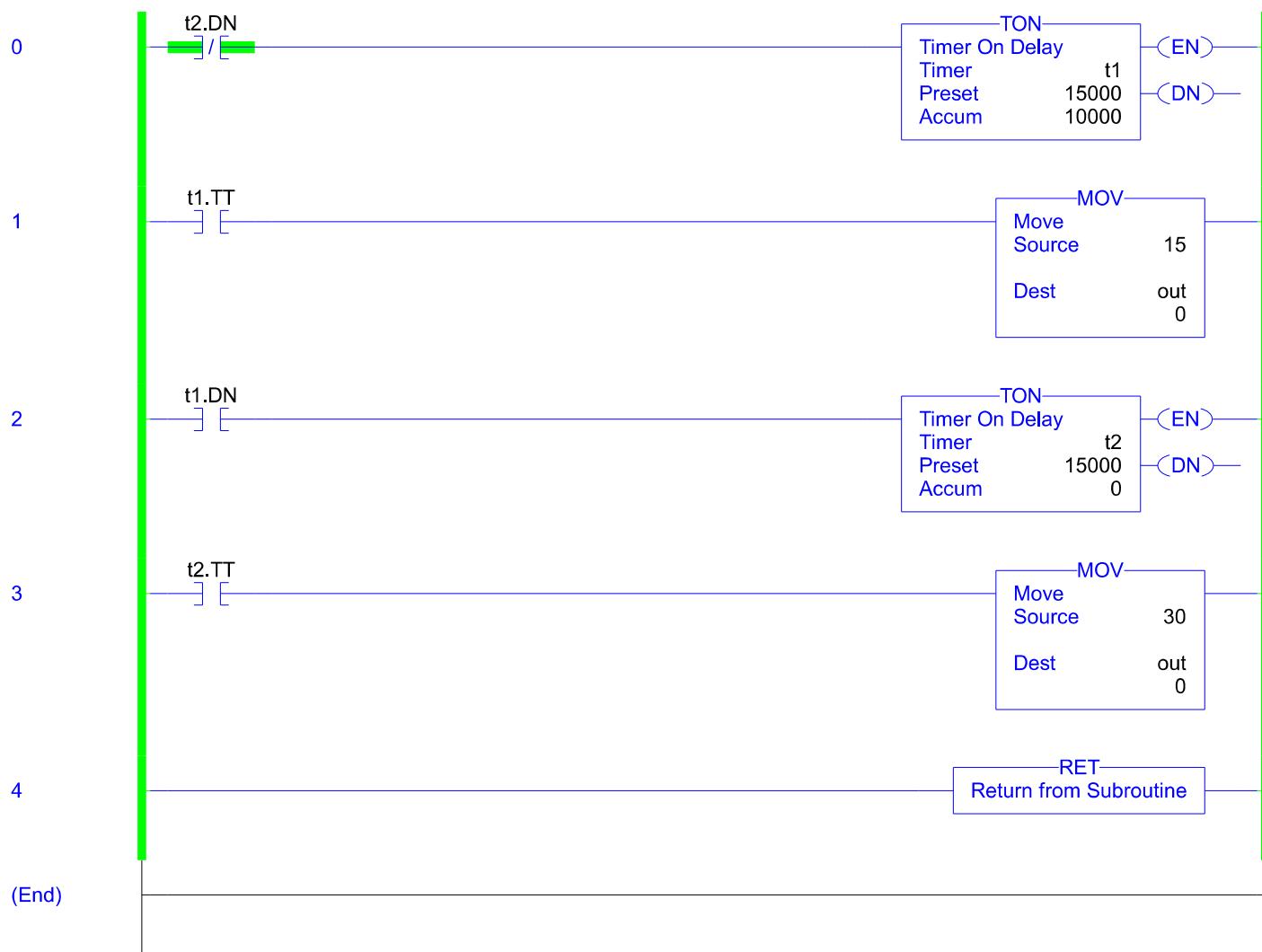
Name	Value	Data Type	Scope
<b>FT1</b>	0.0	REAL	cpu
	<i>FT1 - MainProgram/IOINTERFACE - *10(MOV)</i>		
	<i>FT1 - MainProgram/LEVELCONTROL - 5(PID)</i>		
	<i>FT1 - MainProgram/PID_test - 1-B1(IREF,FT1), 1-B1(PIDE,PIDE_01.PV)</i>		
	<i>FT1 - MainProgram/pidsqyare - 0(PID)</i>		
<b>level</b>		PID	cpu
	<i>level - MainProgram/LEVELCONTROL - *2(PID)</i>		
	<i>level - MainProgram/pidsqyare - *3(PID)</i>		
	<i>level.BIAS - MainProgram/LEVELCONTROL - *1(MOV)</i>		
	<i>level.OUT - MainProgram/LEVELCONTROL - *2(PID), 3(DIV)</i>		
<b>levltune</b>	0	BOOL	cpu
	<i>levltune - MainProgram/pidsqyare - 0(XIC), 1(XIC), 2(XIC)</i>		
<b>LT1</b>	86.39443	REAL	cpu
	<i>LT1 - MainProgram/IOINTERFACE - *0(MOV)</i>		
	<i>LT1 - MainProgram/LEVELCONTROL - 2(PID), 7(PID)</i>		
	<i>LT1 - MainProgram/MAINLOGIC - 12(GRT), 4(GRT)</i>		
	<i>LT1 - MainProgram/pidsqyare - 3(PID)</i>		
<b>out</b>	0	DINT	cpu
	<i>out - MainProgram/pidsqyare - 1(MOV)</i>		
	<i>out - MainProgram/square_wav - *1(MOV), *3(MOV)</i>		
<b>pidsq</b>		PID	cpu
	<i>pidsq - MainProgram/pidsqyare - *0(PID)</i>		
	<i>pidsq.OUT - MainProgram/pidsqyare - 2(MOV)</i>		
	<i>pidsq.SP - MainProgram/pidsqyare - *1(MOV)</i>		
<b>VFD101</b>	0.0	REAL	cpu
	<i>VFD101 - MainProgram/IOINTERFACE - 12(MOV)</i>		
	<i>VFD101 - MainProgram/LEVELCONTROL - *5(PID), *6(MOV), *7(PID), *8(MOV)</i>		
	<i>VFD101 - MainProgram/PID_test - *1-C1(OREF,VFD101), 1-B1(PIDE,PIDE_01.CVEU)</i>		
	<i>VFD101 - MainProgram/pidsqyare - *0(PID), *2(MOV), *3(PID)</i>		



Name	Value	Data Type	Scope
FT1	0.0	REAL	cpu
	<i>FT1 - MainProgram/IOINTERFACE - *10(MOV)</i>		
	<i>FT1 - MainProgram/LEVELCONTROL - 5(PID)</i>		
	<i>FT1 - MainProgram/PID_test - 1-B1(IREF,FT1), 1-B1(PIDE,PIDE_01.PV)</i>		
	<i>FT1 - MainProgram/pidsqyare - 0(PID)</i>		
PIDE_01		PID_ENHANCED	MainProgram
	<i>PIDE_01 - MainProgram/PID_test - *1-A2(IREF,SP), *1-B1(IREF,FT1), *1-B1(PIDE,PIDE_01), *1-C1(OREF,VFD101)</i>		
SP	0.0	REAL	cpu
	<i>SP - MainProgram/PID_test - 1-A2(IREF,SP), 1-B1(PIDE,PIDE_01.SPProg)</i>		
VFD101	0.0	REAL	cpu
	<i>VFD101 - MainProgram/IOINTERFACE - 12(MOV)</i>		
	<i>VFD101 - MainProgram/LEVELCONTROL - *5(PID), *6(MOV), *7(PID), *8(MOV)</i>		
	<i>VFD101 - MainProgram/PID_test - *1-C1(OREF,VFD101), 1-B1(PIDE,PIDE_01.CVEU)</i>		
	<i>VFD101 - MainProgram/pidsqyare - *0(PID), *2(MOV), *3(PID)</i>		



Name	Value	Data Type	Scope
msg_spai	<i>msg_spai - MainProgram/SprayDryerTest - *0(MSG)</i>	MESSAGE	cpu
SPAI	<i>SPAI[0] - MainProgram/SprayDryerTest - *0(MSG)</i>	REAL[20]	cpu
Timer01	<i>Timer01 - MainProgram/COMMUNICATION - *4(TON) Timer01 - MainProgram/SprayDryerTest - *1(TON) Timer01.DN - MainProgram/COMMUNICATION - 0(XIC), 1(XIC), 2(XIC), 3(XIC), 4(XIO) Timer01.DN - MainProgram/SprayDryerTest - 0(XIC), 1(XIO)</i>	TIMER	cpu



Name	Value	Data Type	Scope
<b>out</b>	0	DINT	cpu
	<i>out - MainProgram/pidsqyare - 1(MOV)</i>		
	<i>out - MainProgram/square_wav - *1(MOV), *3(MOV)</i>		
<b>t1</b>		TIMER	MainProgram
	<i>t1 - MainProgram/square_wav - *0(TON)</i>		
	<i>t1.DN - MainProgram/square_wav - 2(XIC)</i>		
	<i>t1.TT - MainProgram/square_wav - 1(XIC)</i>		
<b>t2</b>		TIMER	MainProgram
	<i>t2 - MainProgram/square_wav - *2(TON)</i>		
	<i>t2.DN - MainProgram/square_wav - 0(XIO)</i>		
	<i>t2.TT - MainProgram/square_wav - 3(XIC)</i>		

Data type Name: STRING

Description:

Size 88 byte(s)

Name	Data Type	Style	Description
LEN	DINT	Decimal	
DATA	SINT[82]	ASCII	

# Appendix G

## References

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