

Weld Design										
Problem Statement & Executive Summary					The weld profile to be used within the attachment of both the diagonal beam to the baseplate and the vertical end beam is a butt weld.					
<p>The following spreadsheet encompasses the investigation of a suitable weld and reasoning upon selected weld, attaching the two diagonal beams that connect to rear of the vertical beams and the horizontal base plate.</p> <p>The beam selected is based through restrictions upon the volumetric dimensions highlighted in the technical drawing and design of the food shredder. The beam material for welding, welding frame and the baseplate is AISI 304 structural steel. Furthermore, the shredder plate and frame plate are also of same steel material.</p> <p>This investigation will include the justification of the selected beam to minimise various undesirable effects of loads and ensure security while balancing cost and manufacturing process through a method of analysis. The specific final values will include a weld profile and specifications.</p>					<p>The weld leg length for the beam being attached to both the baseplate and the vertical end beam is to be a 14mm weld.</p> <p>The maximum convexity of the weld is to be approximately 4.5mm.</p>					
Requirements & Specifications										
<p>The following section denotes the requirements of this investigation concerning the design of the weld profile:</p> <ul style="list-style-type: none">> Steel AISI 304 Beam Material (Both Vertical & Diagonal Welded Frame).> Wide: 100mm, Length: 80mm, Height: 100mm, Thickness: 20mm> Beam is connecting to the Baseplate and Vertical Beams.> Centre of Area (C of A) superimposed with the coordinate system outside of the vertical beam.> Selection & justification of weld profile.> Selection & justification of suitable weld size.										
Assumptions & Load										
<p>Loads applied on the system include:</p> <ul style="list-style-type: none">> 100N Downward Vertical Force> 1000N Tangential Force										
Compiled Data & Calculations										
Notes	Description	Property	Value	Unit	Symbol	Expression	Reference	Citations		
Downward Direction	End Beam Size	End Beam Height	800	mm	eb_h	-	Defined	-	-	
		End Beam Width	100	-	eb_w	-	-	-	-	
		End Beam Thickness	20	-	eb_t	-	-	-	-	
	Base Plate Size	Base Plate Height	1500	mm	bp_h	-	Defined	-	-	
		Base Plate Width	1500	-	bp_w	-	-	-	-	
		Base Plate Thickness	15	-	bp_t	-	-	-	-	
	Specified FOS	Length of Beam	80	mm	l_b	-	Defined	-	-	
		Factor of Safety	2	-	FOS	-	-	-	-	
	Force Y - Direction	Hole A Force	1943.10	N	F	$SQR((F_{pl1}+F_{pl2}+F_{pl3})^2+(F_{pl4}+F_{pl5})^2)$	Calculated	-	-	
	Offset - Figure 7	Hole A	Offset Distance	300	mm	offset_d	-	Calculated	-	-
Diameter			30	-	dia_b	-	Defined	-	-	
Mass			Plate 1	49.46	kg	m_pl1	-	Bolt Design	-	-
		Plate 2	7.07	-	m_pl2	-	-	-	-	
Shredder Unit			45.45	-	m_shrd	-	-	-	-	
		Tension Bolt	1000.00	N	F_b	-	Defined	-	-	
		X Component	461.75	-	F_bx	$F_b \sin(\text{ang_rads})$	Calculated	-	-	
		Y Component	887.01	-	F_by	$F_b \cos(\text{ang_rads})$	Calculated	-	-	
Angle		Bolt - Degrees	27.5	theta	ang_deg	$\text{PI}/(180)$	Defined	-	-	
		Bolt - Rads	0.48	theta	ang_rads	-	Calculated	-	-	
	Shredder Unit	45.45	-	m_shrd	-	-	-	-		
Acceleration due to Gravity	Rectangular Hollow Beam	Plate 1	485.20	-	F_pl1	$m_{pl1} \cdot g$	Calculated	-	-	
		Plate 2	69.36	-	F_pl2	$m_{pl2} \cdot g$	-	-	-	
		Shredder Unit	445.86	-	F_shrd	$m_{shrd} \cdot g$	-	-	-	
	Gravity Constant		9.81	m/s ²	g	-	Researched	[1]	-	
		Rectangular Hollow Beam	Beam Height	100	mm	b_h	-	Defined	-	-
		Diagonal - Welded Frame	Beam Width	100	-	b_w	-	-	-	-
	AISI 304 Steel Beam Material	Beam Thickness	20	-	b_t	-	-	-	-	
		Tensile Strength	505	N/mm ²	Su	-	Datasheet	[3]	-	
		Weld Shear Stress Factor	3	-	weld_f	-	Researcher	[2]	-	
	Formula from Lectures	Allowable Shear Stress	119.03	MPa	t_all	$Su \cdot \text{weld_f}$	Calculated	Lectures	-	
	Calculations - End Beam									
Acting upon each mm	Beam to Base Plate Bending	Moment	38861.92	Nmm	M	$F_{pl1} \cdot \text{eb_h}_1$	Calculated	[1]	-	
		Moment of Inertia	3533.33	-	Z_w	$(b_w \cdot h_w^3)/(12)$	-	-	-	
		Component due to Bending	11.00	N/mm	F_bnd	M/Z_w	-	-	-	
	Shear	Assumption of Width	1.00	mm	w	$(b_w \cdot h_w)/(2 \cdot \text{eb_h}_1)$	Assumption	Lectures	-	
		Perimetre of Beam	400.00	-	p	-	Calculated	-	-	
		Area of Weld	400.00	mm ²	A_w	$w \cdot p$	Defined	-	-	
	Force due to Shear	Force	1943.095797	N	F	$F_{pl1} + F_{pl2} + F_{pl3}$	Calculated	-	-	
		Force due to Shear	4.86	N/mm	F_s	F/A_w	Calculated	[1]	-	
		Torsion	Torque	291443.70	Pa	T	$F_{pl1} \cdot \text{eb_h}_1$	-	[1]	-
	Beam Angles	Radius of Beam	70.71	mm	r_b	$SQR((b_w/2)^2 + (b_w/2)^2)$	-	-	-	
Twisting Moment of Inertia		133333.33	Pa	J_w	$(b_w \cdot h_w^3)/6$	-	-	-		
theta		1.11	radians	angB_rads	$ATAN(b_w/2 / b_w/2)$	-	-	-		
		63.43	degrees	angB_deg	$ATAN(b_w/2 / b_w/2) \cdot (180/\text{PI})$	-	-	-		
Force Components Torsion	Force due to Torsion	Force due to Torsion	154.57	N/mm	F_j	$(T \cdot r_b)/J_w$	-	-	-	
		Force due to Torsion Y-Axis	138.25	-	F_jy	$F_j \sin(\text{angB_rads})$	-	-	-	
		Force due to Torsion Z-Axis	69.13	-	F_jz	$F_j \cos(\text{angB_rads})$	-	-	-	
	Summing Vectorial	Force acting on Component	159.31	-	F_comp	$SQR((F_{bnd})^2 + (F_{s+T})^2)$	-	-	-	
	Weld	Weld Leg Length	2.68	mm	w_l	$(F_{comp} \cdot \text{FOS})/t_{all}$	-	Lectures	-	
		Advisable Weld Factor	0.67	-	w_fac	-	-	-	-	
		Advisable Weld Length	13.4	mm	w_ad	$b \cdot w_{fac}$	-	-	-	
	Researcher Value									
Calculations - Baseplate										
Acting upon each mm	Beam to End Plate Bending	Moment	29146.44	Nmm	M_bp	$F_{pl1} \cdot \text{eb_h}_1$	Calculated	[1]	-	
		Component due to Bending	8.25	N/mm	f_bnd_bp	M_{bp}/Z_w	-	-	-	
	Shear	Assumption of Width	1.00	mm	w_bp	-	Assumption	Lectures	-	
		Torque	194309.58	Pa	T_bp	$F_{pl1} \cdot \text{eb_h}_1$	Calculated	[1]	-	
	Force Components Torsion	Force due to Torsion	10.30	N/mm	F_j_bp	$(T_{bp} \cdot r_{bp})/J_{w_bp}$	-	-	-	
		Force due to Torsion Y-Axis	9.22	-	F_jy_bp	$F_{j_bp} \sin(\text{angB_rads})$	-	-	-	
		Force due to Torsion Z-Axis	4.61	-	F_jz_bp	$F_{j_bp} \cos(\text{angB_rads})$	-	-	-	
	Summing Vectorial Components	Force acting on Component	16.95	-	F_bp	$SQR((f_{bnd_bp})^2 + (f_{s+T_bp})^2)$	-	-	-	
Weld	Weld	Weld Leg Length	0.28	mm	w_l_bp	$(F_{bp} \cdot \text{FOS})/t_{all}$	-	Lectures	-	
		Advisable Weld Length	13.4	mm	w_ad_bp	-	-	-	-	
Results & Comments										
<p>The factor of safety for the end plate of the beam weld has denoted an appropriate value with the thinnest section of the beam at 20mm.</p> <p>Generally, it is advisable to use a weld that is no smaller than 0.67mm, the thickness of the beam material. Therefore, through this investigation the result is a value of 2mm to the nearest common weld leg length. Through the investigation however, the advisable weld leg length should be of a higher value as mentioned with the advisable factor consideration.</p> <p>Therefore, the final weld leg length is to be a length of 14mm to the nearest common weld leg length.</p> <p>This concludes the minimum required weld leg length of a value between 2 to 5mm for the beam to the end beam and the weld leg length hence, of recommended suitability to this weld falls within the expected range of approximately 10 to 15mm.</p> <p>As expected the weld of the beam to the base plate is a lower value than that of the weld of the beam to the end beam (or vertical beam). The results show the weld of the beam to the base plate to have a minimum required weld leg length of 0.28mm. Therefore, the weld leg length recommended must follow the advisable leg length for safety and fall at approximately 14mm for similar reasons mentioned prior.</p> <p>The size of the weld to the vertical end beam is expected to be larger due to the larger bending component involved.</p> <p>The weld profile suitable for this investigation and system would be a J or even potentially a corner joint with double bevel, J or fillet. For this investigation and prioritisation of labour and cost, it would be recommended to employ a double bevel for the balance for support and welding process. To save further on the weld cost a butt weld can also be used as illustrated in figure 7.</p> <p>The maximum convexity, C, of the weld has been referenced and researched to be an acceptable value of 5/16 of the width for welds with widths less than 8mm. Therefore, the weld should have a C of approximately 4.5mm.</p>										
References										
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