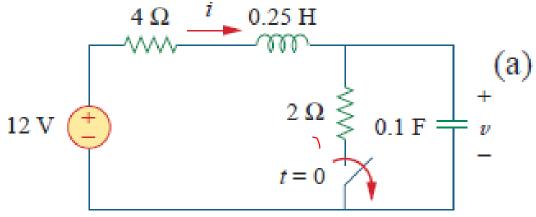
The switch in Fig. has been closed for a long time. It is open at t = 0. Find: (a) $i(0^+)$, $v(0^+)$, (b) $di(0^+)/dt$, $dv(0^+)/dt$, (c) $i(\infty)$, $v(\infty)$.



(a) If the switch is closed a long time before t = 0,

it means that the circuit has reached dc steady

state at t=0

At dc steady state, the inductor acts like a short circuit, while the capacitor acts like an open circuit

 $\begin{array}{c|c}
4 \Omega & \stackrel{i}{\longrightarrow} \\
& & \\
\end{array}$ $\begin{array}{c|c}
2 \Omega & \stackrel{\downarrow}{\geqslant} \nu \\
\end{array}$

at
$$t = 0^{-}$$

$$i(0^{-}) = \frac{12}{4+2} = 2 \text{ A},$$

$$v(0^-) = 2i(0^-) = 4 \text{ V}$$

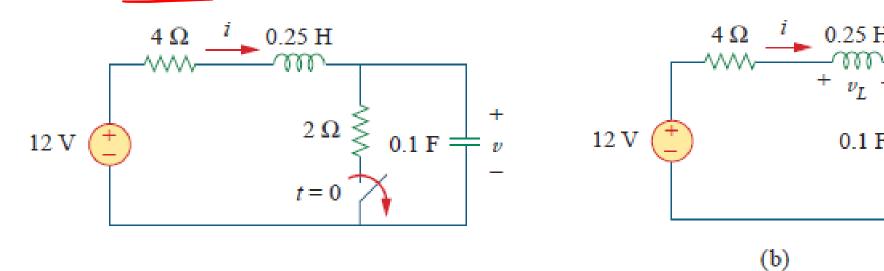
$$i(\bar{0}) = i(\bar{0}) = j(\bar{0})$$

 $V(\bar{0}) = V(\bar{0}) = V(\bar{0})$

As the inductor current and the capacitor voltage cannot change abruptly,

$$i(0^+) = i(0^-) = 2 \text{ A}, \quad v(0^+) = v(0^-) = 4 \text{ V}$$

(b) At $t = 0^+$, the switch is open;

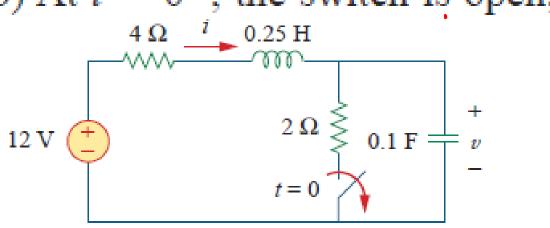


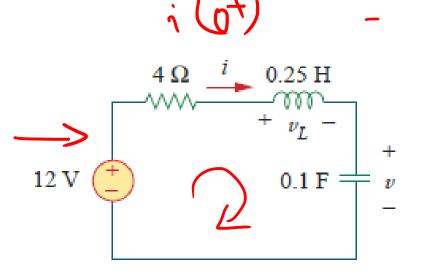
$$i_C(0^+) = i(0^+) = 2 \text{ A}$$

Since $C \frac{dv}{dt} = i_C$, $\frac{dv}{dt} = i_C/C$, and

$$\frac{dv(0^+)}{dt} = \frac{i_C(0^+)}{C} = \frac{2}{0.1} = 20 \text{ V/s}$$

(b) At $t = 0^+$, the switch is open;





Similarly, since $L di/dt = v_L$, $di/dt = v_L/L$. We now obtain v_L by applying KVL to the loop in Fig. 8.3(b). The result is

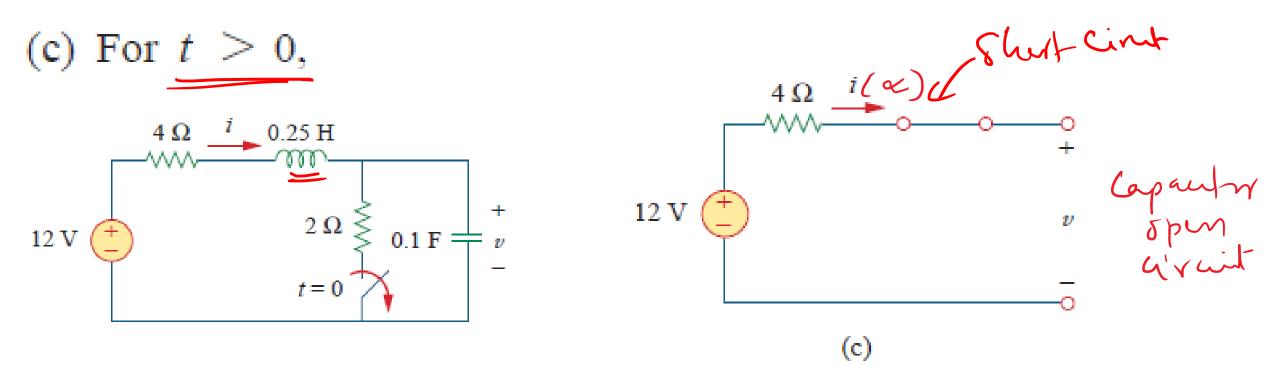
$$-12 + 4i(0^{+}) + v_{L}(0^{+}) + v(0^{+}) = 0$$

OI

$$v_L(0^+) = 12 - 8 - 4 = 0$$

Thus,

$$\frac{di(0^+)}{dt} = \frac{v_L(0^+)}{L} = \frac{0}{0.25} = 0 \text{ A/s}$$

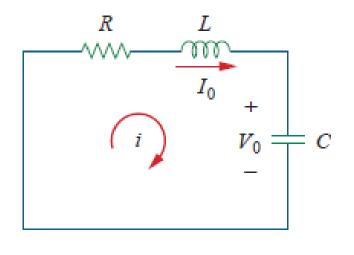


$$t \to \infty$$

The circuit reaches steady state again. The inductor acts like a short circuit and the capacitor like an open circuit,

$$i(\infty) = 0 \text{ A}, \qquad v(\infty) = 12 \text{ V}$$

In Fig. 8.8, $R = 40 \Omega$, L = 4 H, and C = 1/4 F. Calculate the characteristic roots of the circuit. Is the natural response overdamped, underdamped, or critically damped?



Solution:

We first calculate

The roots are

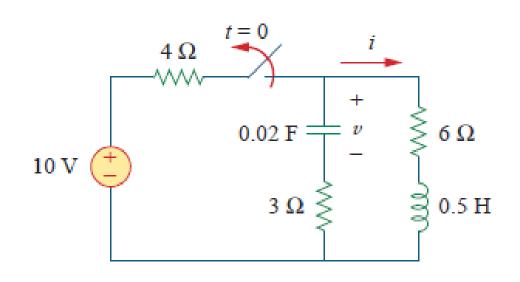
$$s_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2} = -5 \pm \sqrt{25 - 1}$$

OI

$$s_1 = -0.101, \qquad s_2 = -9.899$$

Since $\alpha \ge \omega_0$, we conclude that the response is overdamped. This is also evident from the fact that the roots are real and negative.

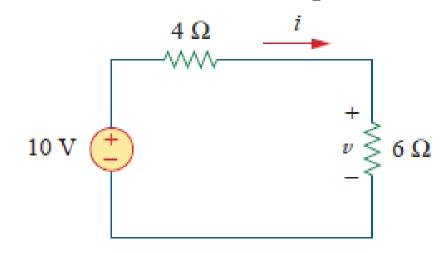
Find i(t) in the circuit of Fig. 8.10. Assume that the circuit has reached steady state at $t = 0^-$.



Thus, at t = 0,

For
$$t < 0$$
, the switch is closed.

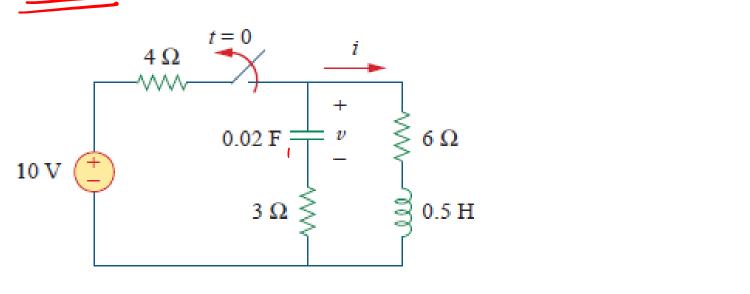
The capacitor acts like an open circuit while the inductor acts like a open circuit.



$$i(0) = \frac{10}{4+6} = 1 \text{ A}, \qquad v(0) = 6i(0) = 6 \text{ V}$$

where i(0) is the initial current through the inductor and v(0) is the initial voltage across the capacitor.

For t > 0 the switch is opened and the voltage source is disconnected.



$$\alpha = \frac{R}{2L} = \frac{9}{2(\frac{1}{2})} = 9, \quad \omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{\frac{1}{2} \times \frac{1}{50}}} = 10$$

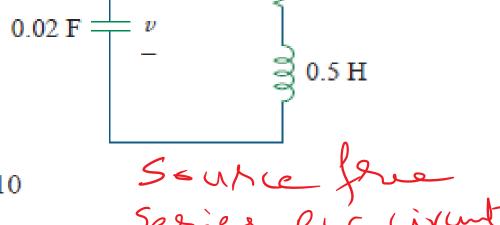
$$S \leq Uh ce free for the series RLC Cival$$

$$s_{1.2} = -9 \pm j4.359$$

 $s_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2} = -9 \pm \sqrt{81 - 100}$

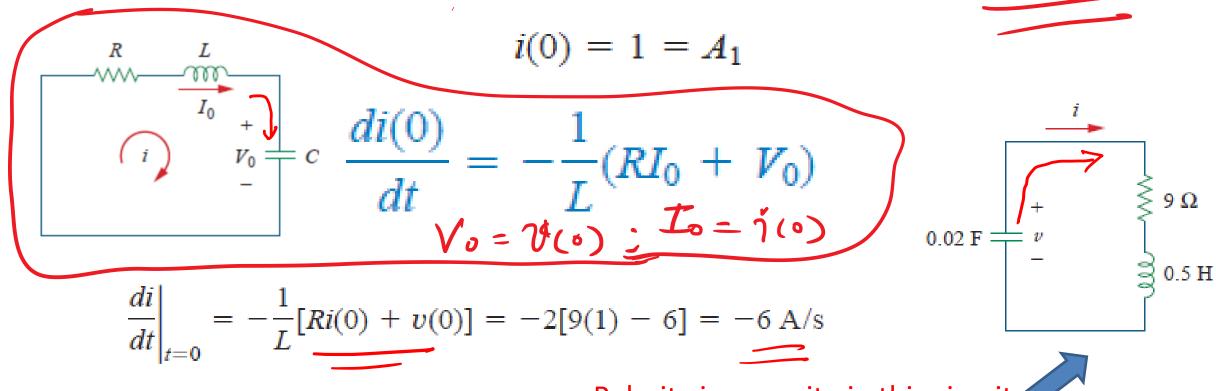
Hence, the response is underdamped ($\alpha \leq \omega$); that is,

$$i(t) = e^{-9t} (A_1 \cos 4.359t + A_2 \sin 4.359t)$$



$$i(t) = e^{-9t} (A_1 \cos 4.359t + A_2 \sin 4.359t)$$

We now obtain A_1 and A_2 using the initial conditions. At t = 0,



Polarity is opposite in this circuit

Hence Note that $v(0) = V_0 = -6 \text{ V}$

$$\frac{di}{dt} = -9e^{-9t}(A_1\cos 4.359t + A_2\sin 4.359t) + e^{-9t}(4.359)(-A_1\sin 4.359t + A_2\cos 4.359t)$$

Imposing the condition in Eq. (8.4.3) at t = 0 gives

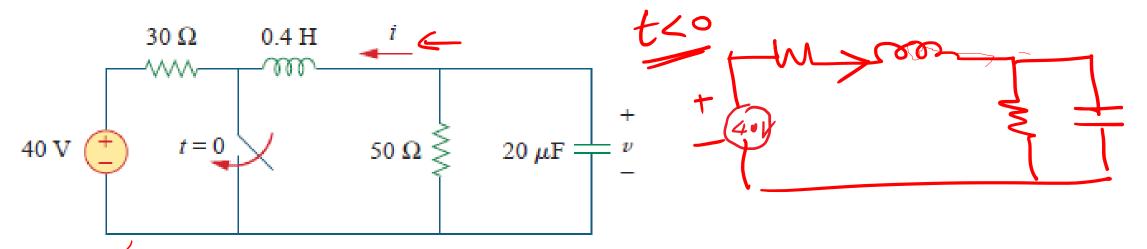
$$-6 = -9(A_1 + 0) + 4.359(-0 + A_2)$$

But $A_1 = 1$ from Eq. (8.4.2). Then

$$-6 = -9 + 4.359A_2 \implies A_2 = 0.6882$$

$$i(t) = e^{-9t}(\cos 4.359t + 0.6882 \sin 4.359t)$$
 A

Find v(t) for t > 0 in the *RLC* circuit of Fig.



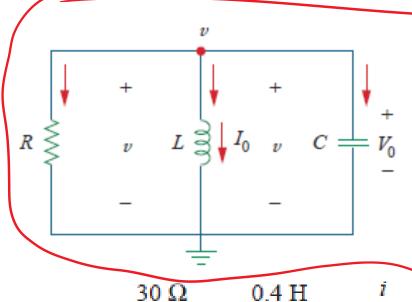
When t < 0, the switch is open; the inductor acts like a short circuit while the capacitor behaves like an open circuit. The initial voltage across the capacitor is the same as the voltage across the 50- Ω resistor; that is,

$$v(0) = \frac{50}{30 + 50}(40) = \frac{5}{8} \times 40 = 25 \text{ V}$$

The initial current through the inductor is

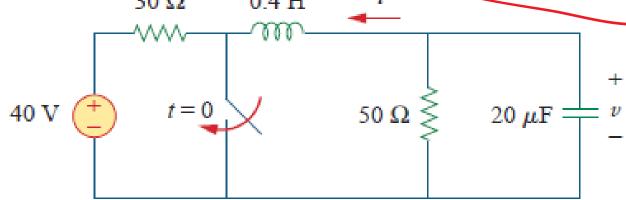
$$\rightarrow i(0) = -\frac{40}{30 + 50} = -0.5 \,\text{A}$$
 (when is opposite)

•



$$\frac{dv(0)}{dt} = -\frac{(V_0 + RI_0)}{RC}$$

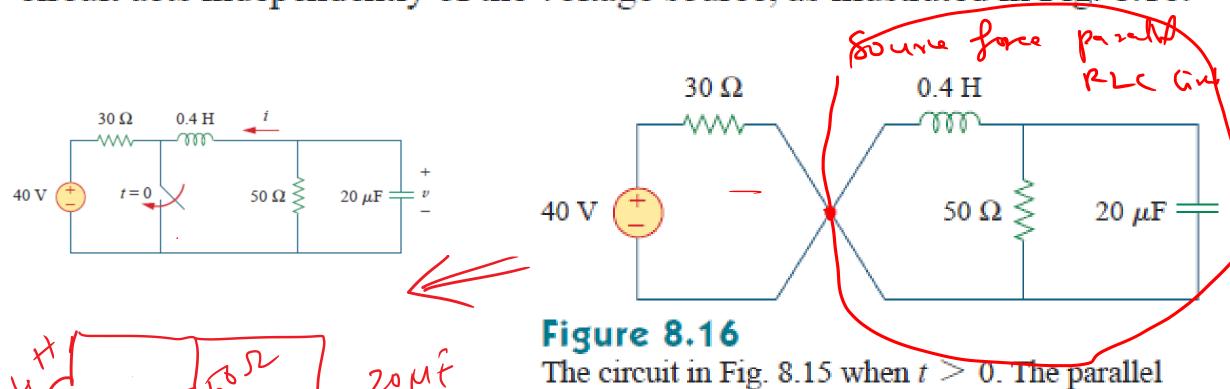
The direction of i is as to conform with the direction of I_0 which is in agreement with the convention that current flows into the positive terminal of an inductor



Here directions of went

$$\frac{dv(0)}{dt} = -\frac{v(0) + Ri(0)}{RC} = -\frac{25 - 50 \times 0.5}{50 \times 20 \times 10^{-6}} = 0$$

When t > 0, the switch is closed. The voltage source along with the 30- Ω resistor is separated from the rest of the circuit. The parallel *RLC* circuit acts independently of the voltage source, as illustrated in Fig. 8.16.



The circuit in Fig. 8.15 when t > 0. The parallel *RLC* circuit on the right-hand side acts independently of the circuit on the left-hand side of the junction.

source flee parallel RLC Circui

$$\alpha = \frac{1}{2RC} = \frac{1}{2 \times 50 \times 20 \times 10^{-6}} = 500$$

$$\omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{0.4 \times 20 \times 10^{-6}}} = 354$$

$$s_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

$$= -500 \pm \sqrt{250,000 - 124,997.6} = -500 \pm 354$$

$$s_1 = -854, \qquad s_2 = -146$$

Since $\alpha > \omega_0$, we have the overdamped response

$$v(t) = A_1 e^{-854t} + A_2 e^{-146t}$$

At t = 0, we impose the condition in Eq. (8.6.1),

$$v(0) = 25 = A_1 + A_2 \implies A_2 = 25 - A_1$$

Taking the derivative of v(t) in Eq. (8.6.3),

$$\frac{dv}{dt} = -854A_1e^{-854t} - 146A_2e^{-146t}$$

Imposing the condition in Eq. (8.6.2),

$$\frac{dv(0)}{dt} = 0 = -854A_1 - 146A_2$$

$$\frac{dv(0)}{dt} = 0 = -854A_1 - 146A_2$$

or

$$0 = 854A_1 + 146A_2$$

Solving Eqs. (8.6.4) and (8.6.5) gives

$$A_1 = -5.156, \qquad A_2 = 30.16$$

Thus, the complete solution in Eq. (8.6.3) becomes

$$v(t) = -5.156e^{-854t} + 30.16e^{-146t} V$$