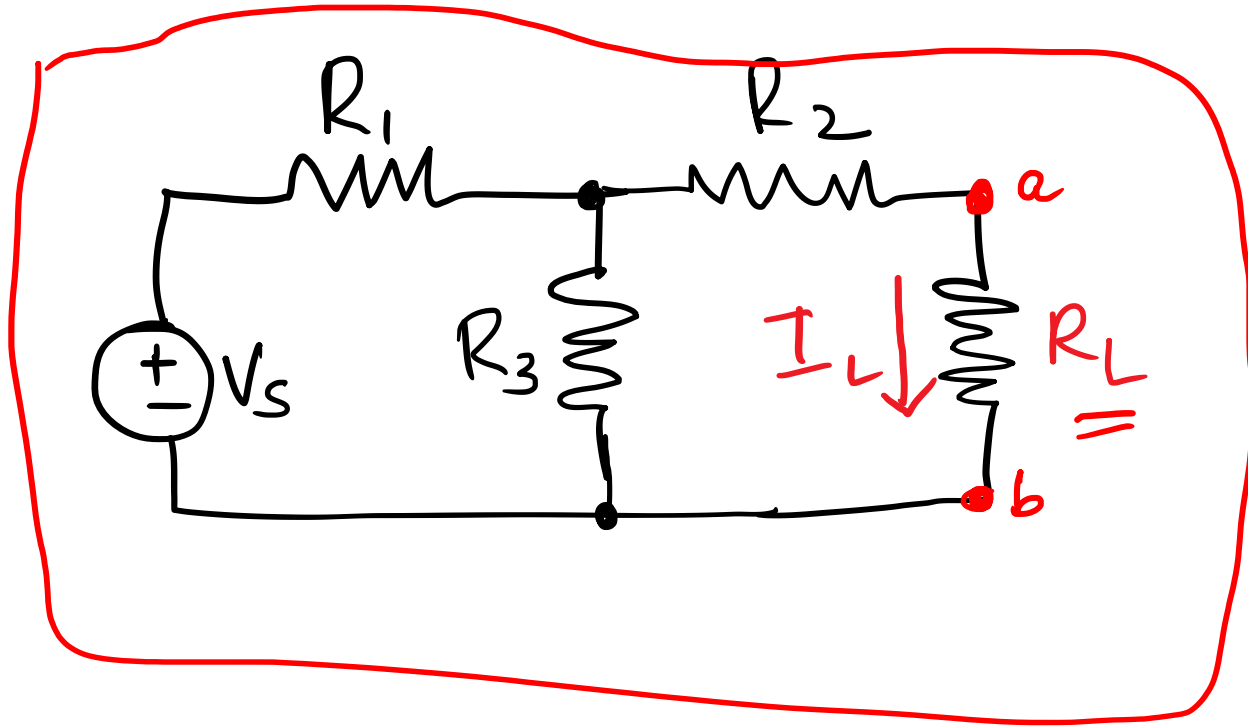


# Thevenin's Theorem

the Thevenin equivalent circuit, was developed in 1883 by M. Leon Thevenin (1857–1926), a French telegraph engineer.

DC ✓

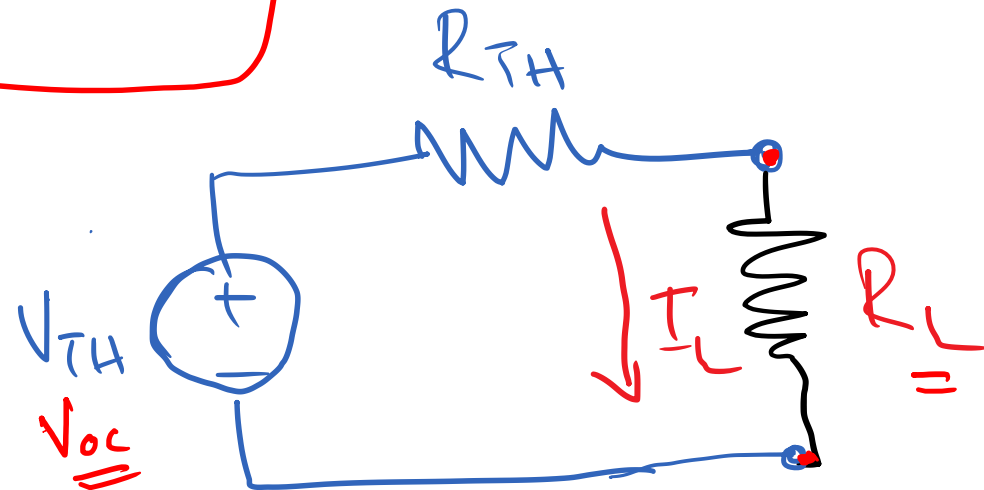
**Thevenin's theorem** states that a linear two-terminal circuit can be replaced by an equivalent circuit consisting of a voltage source  $V_{TH}$  in series with a resistor  $R_{TH}$ , where  $V_{TH}$  is the open-circuit voltage at the terminals and  $R_{TH}$  is the input or equivalent resistance at the terminals when the independent sources are turned off.

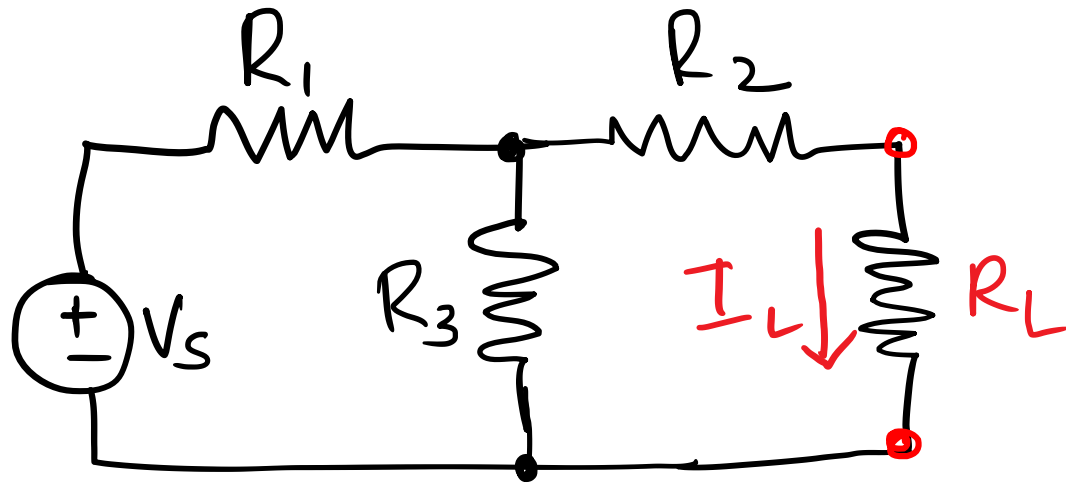


$R_L \rightarrow$  Load Resistance

$I_L \rightarrow$  Load Current

DC





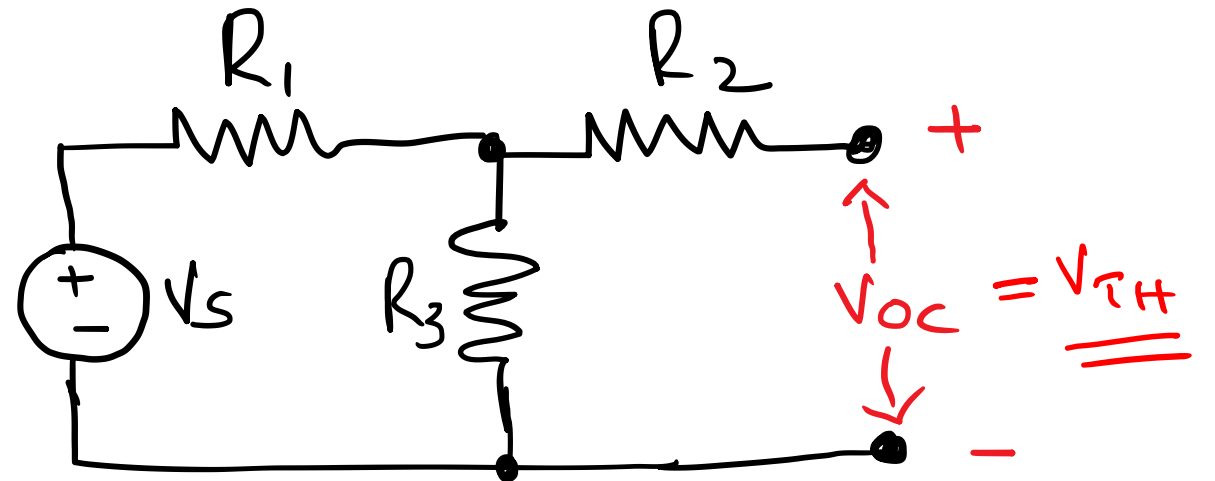
$R_L \rightarrow$  Load Resistance

$I_L \rightarrow$  Load Current

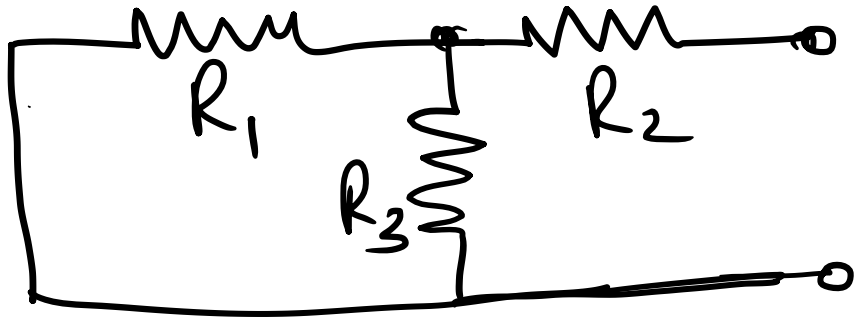
To find equivalent voltage source,  $R_L$  is removed

$$V_{oc} = I R_3$$

$$= \frac{V_s}{R_1 + R_3} \times R_3$$

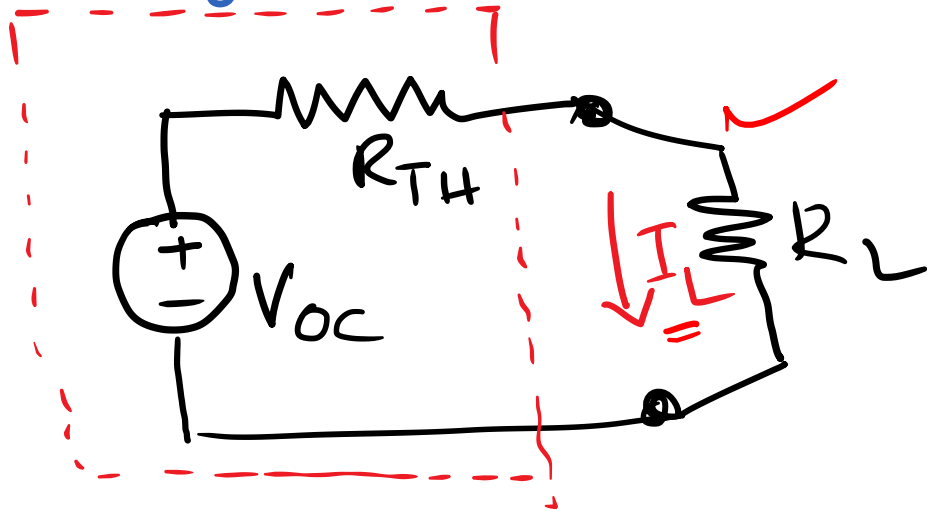


To find internal resistance of the network  
→ Thevenin resistance or equivalent resistance



$$R_{TH} = R_2 + \frac{R_1 R_3}{R_1 + R_3}$$

According to Thevenin theorem



$$I_L = \frac{V_{OC}}{R_{TH} + R_L}$$

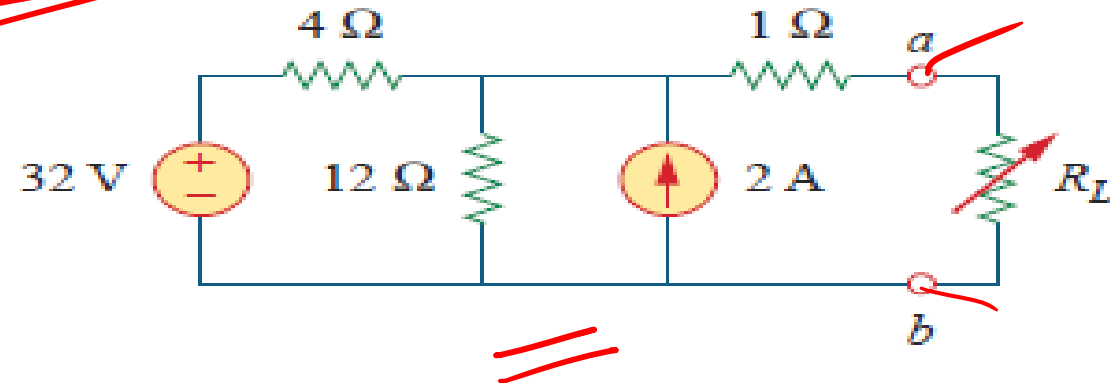
$$V_{OC} = V_{TH}$$

## Steps to find Thevenin's equivalent circuit

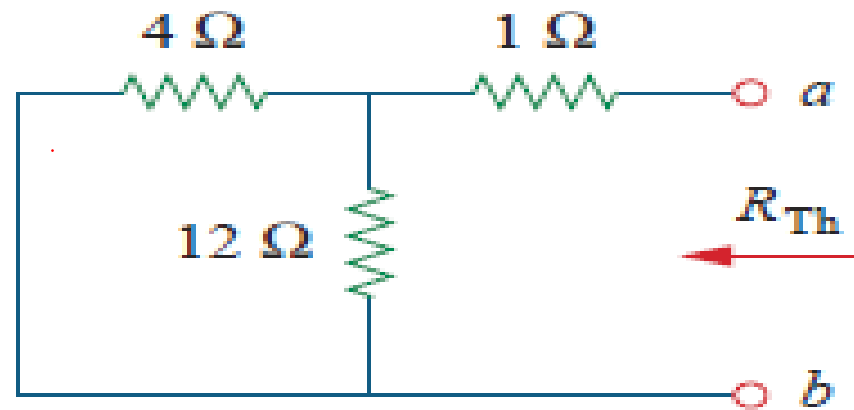
1. Identify the load terminals. ✓
2. Remove the load resistance from the circuit (if its is connected) ✓
3. Find the equivalent resistance ( $R_{Th}$ ) across the load terminal by replacing independent voltage source by short circuit and independent current source by open circuit
4. Find the open circuit voltage ( $V_{Th}$ ) using any of the circuit analysis techniques (mostly mesh/node methods)
5. Draw the Thevenin's equivalent circuit

## Example

DC



Find the Thevenin equivalent circuit of the circuit shown in Fig. to the left of the terminals  $a-b$ .  
Then find the current through  $R_L = 6, 16$ , and  $36 \Omega$ .

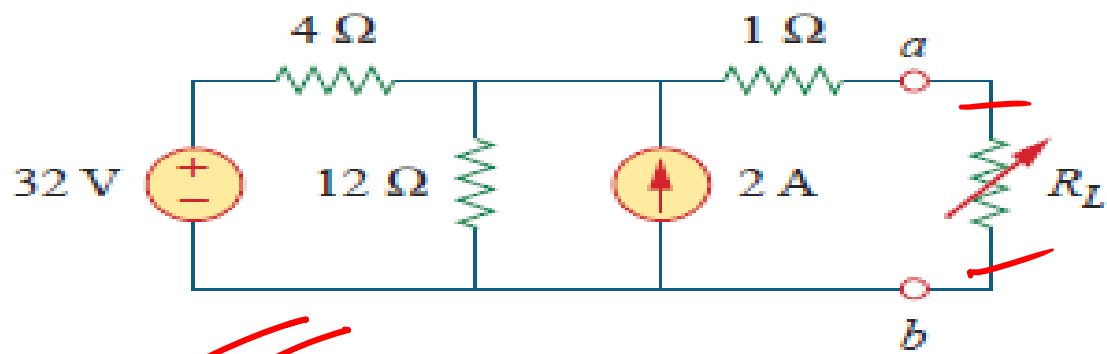


(a)

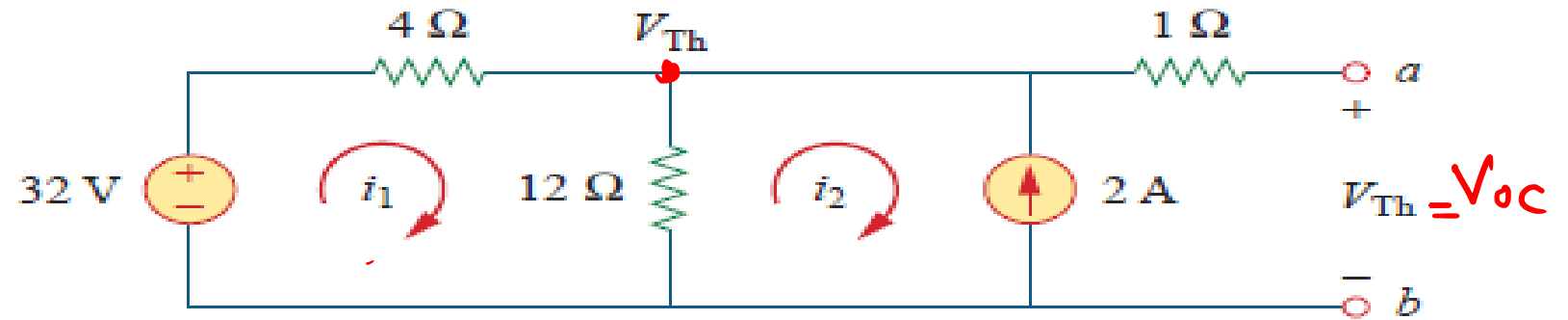
(a) finding  $R_{Th}$ .

$R_{Th} = ?$

$$R_{Th} = 4 \parallel 12 + 1 = \frac{4 \times 12}{16} + 1 = \underline{\underline{4 \Omega}}$$



Applying mesh analysis  
to the two loops, we obtain



(b)

(b) finding  $V_{Th}$ .

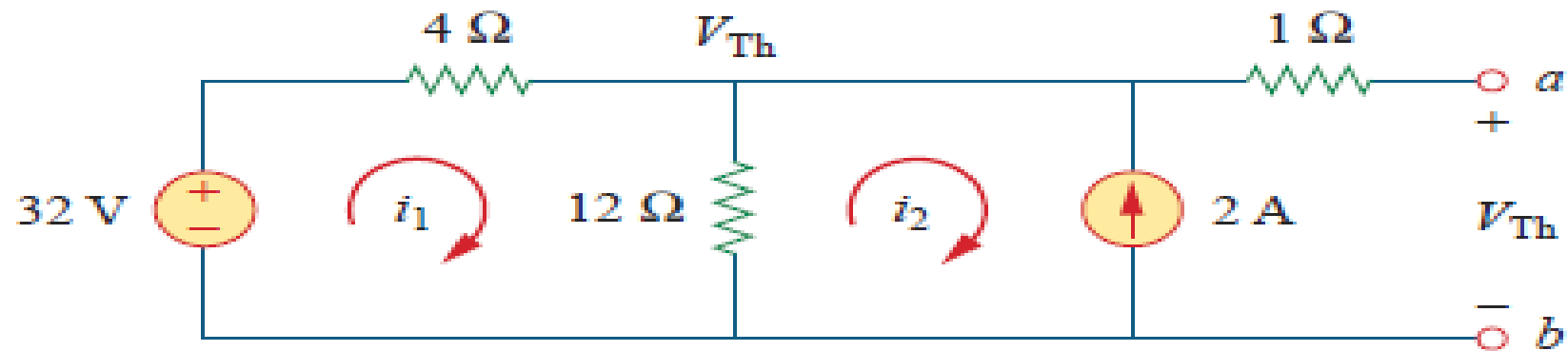
$$-32 + 4i_1 + 12(i_1 - i_2) = 0,$$

$$i_2 = -2 \text{ A}$$

$$V_{oc} = V_{Th} = 30 \text{ V}$$

Solving for  $i_1$ , we get  $i_1 = 0.5 \text{ A}$ . Thus,

$$V_{Th} = 12(i_1 - i_2) = 12(0.5 + 2.0) = 30 \text{ V}$$



(b)

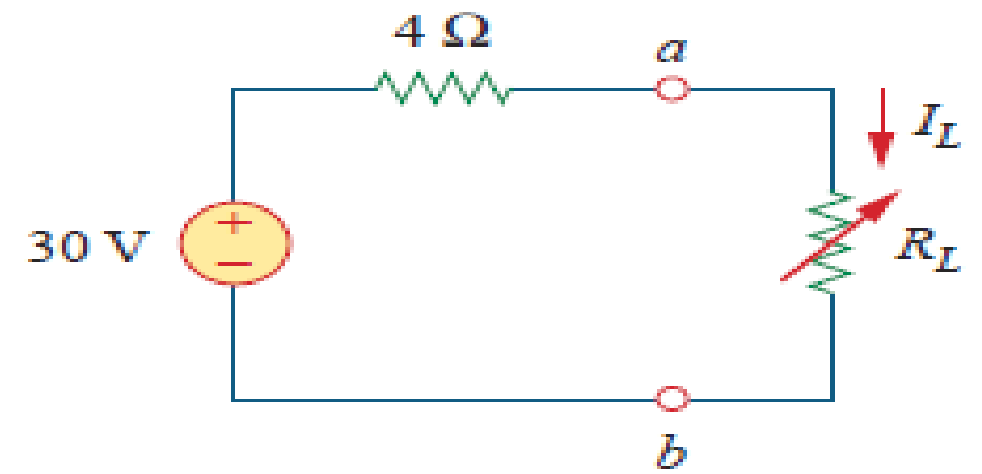
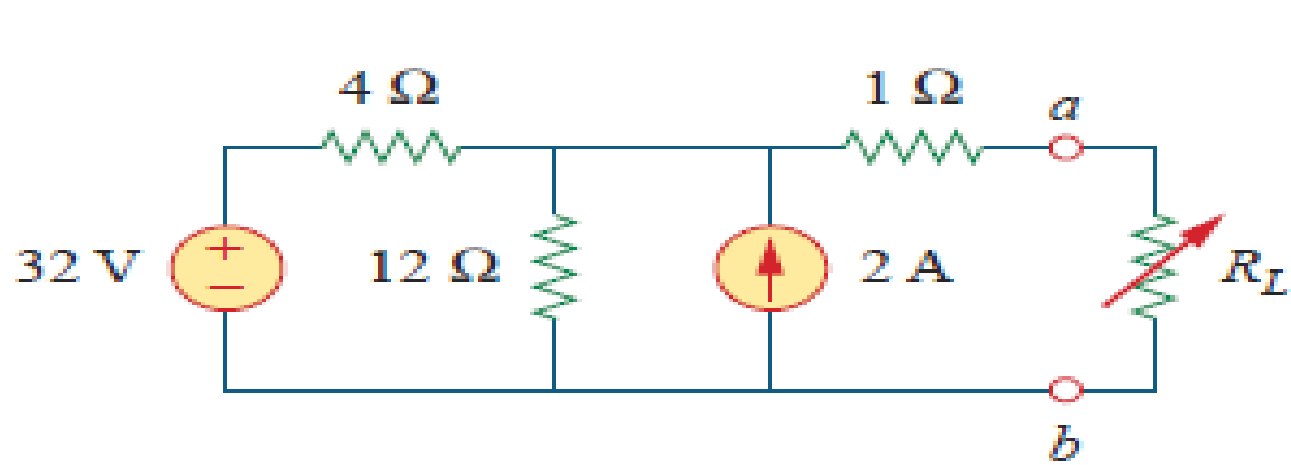
At the top node, KCL

We ignore the  $1\text{-}\Omega$  resistor since no current flows through it.

$$\frac{32 - V_{Th}}{4} + 2 = \frac{V_{Th}}{12}$$

$$96 - 3V_{Th} + 24 = V_{Th} \quad \Rightarrow \quad \underline{\underline{V_{Th} = 30\text{ V}}}$$





The Thevenin equivalent circuit

The current through  $R_L$  is

$$I_L = \frac{V_{Th}}{R_{Th} + R_L} = \frac{30}{4 + R_L}$$

$$\text{When } R_L = 6, \quad I_L = \frac{30}{10} = 3 \text{ A}$$

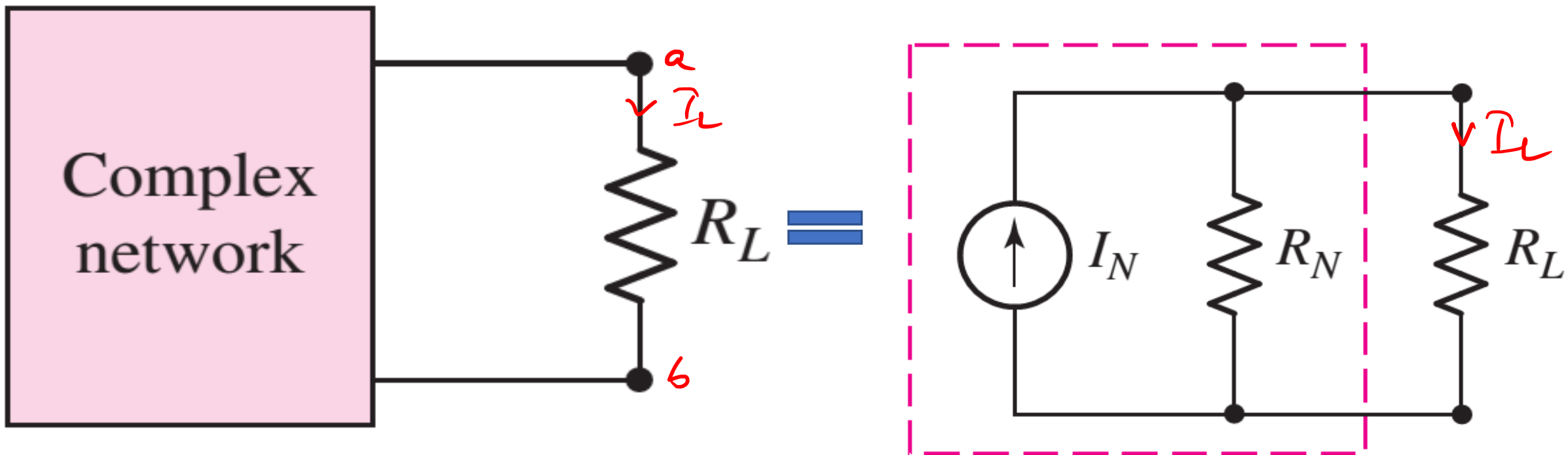
$$\text{When } R_L = 16, \quad I_L = \frac{30}{20} = 1.5 \text{ A}$$

$$\text{When } R_L = 36, \quad I_L = \frac{30}{40} = 0.75 \text{ A}$$

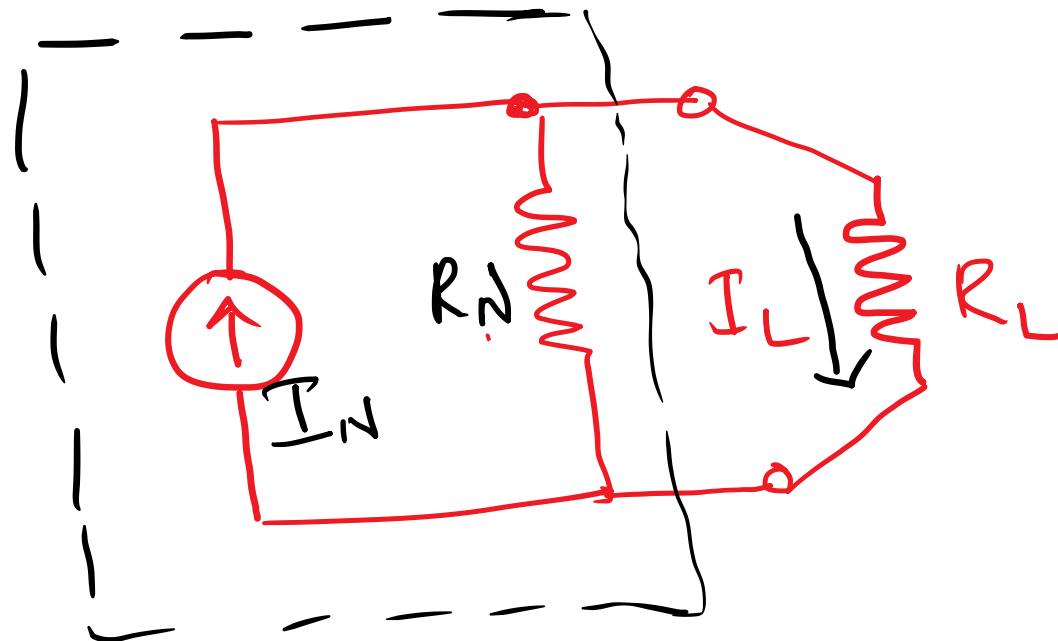
# Norton's Theorem

In 1926, about 43 years after Thevenin published his theorem, E. L. Norton, an American engineer at Bell Telephone Laboratories, proposed a similar theorem.

Norton's theorem states that a linear two-terminal circuit can be replaced by an equivalent circuit consisting of a current source  $I_N$  in parallel with a resistor  $R_N$ , where  $I_N$  is the short-circuit current through the terminals and  $R_N$  is the input or equivalent resistance at the terminals when the independent sources are turned off.



$$R_N = R_{TH}$$



$$I_L = I_N \times \frac{R_N}{R_N + R_L}$$

# Steps to find Norton's equivalent circuit

1. Identify the load terminals. ✓
2. Remove the load resistance from the circuit (if its is connected) ✓
3. Find the equivalent resistance ( $R_N$ ) across the load terminal by replacing independent voltage source by short circuit and independent current source by open circuit
4. Create a short circuit across the load terminals ✓
5. Find the short circuit current ( $I_N$ ) using any of the circuit analysis techniques (mostly mesh/node methods)
6. Draw the Norton's equivalent circuit

$$I_N = \underline{\underline{I_{sc}}}$$

$$R_{TH} = \underline{\underline{R_N}}$$

# Relationship between Thevenin's & Norton's Theorem

$$\underline{V_{OC} = V_{TH}}$$
$$I_N = I_{sc}$$

$$I_N = \frac{V_{Th}}{R_{Th}}$$

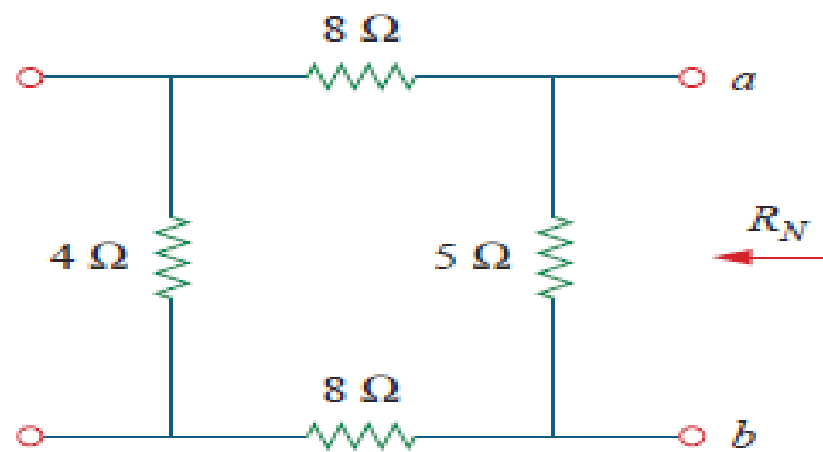
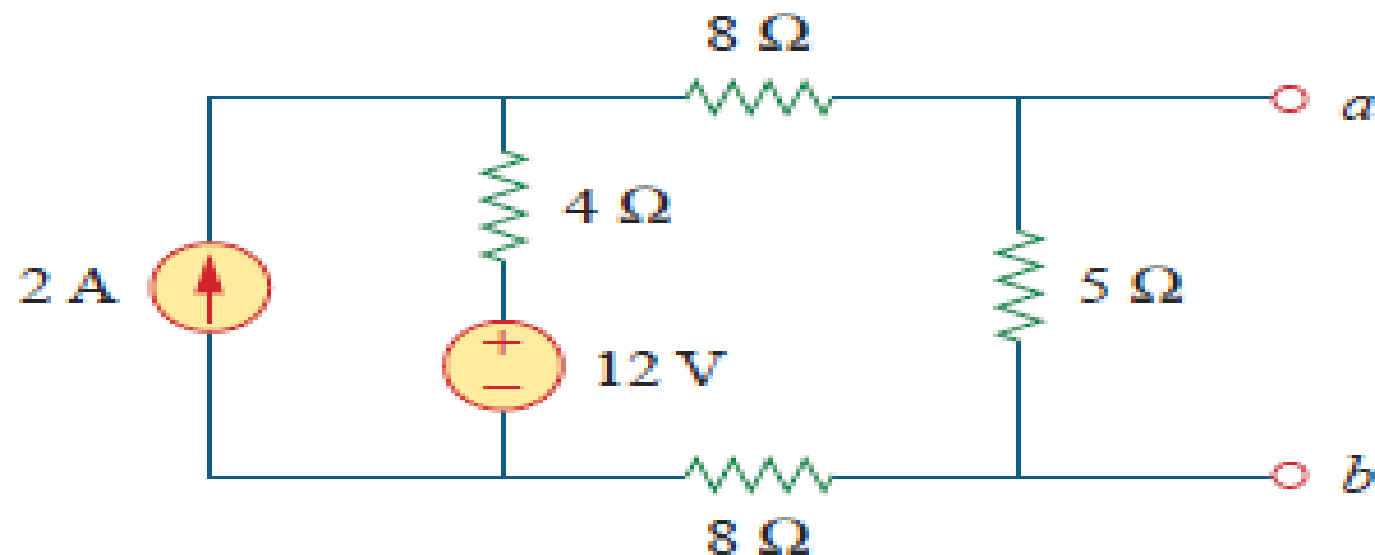
$$\underline{R_N} = R_{Th}$$

## Example

Find the Norton equivalent circuit of the circuit in Fig. terminals  $a$ - $b$ .

DC Source

$$R_N = R_{T4}$$

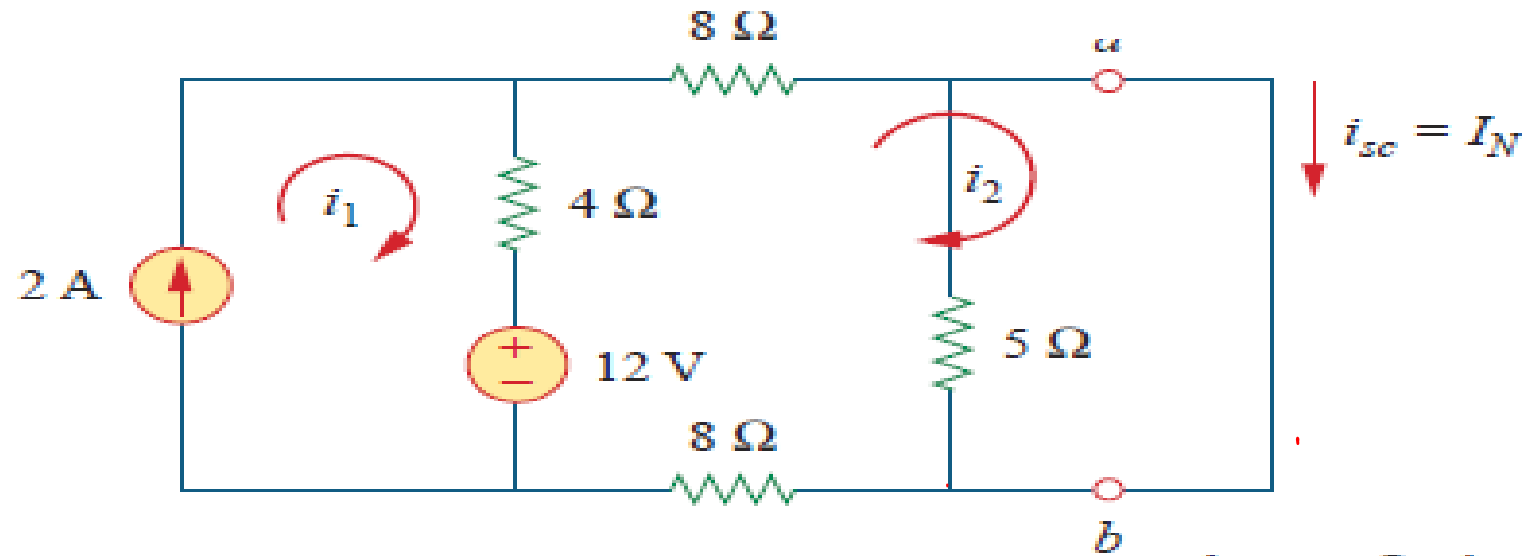
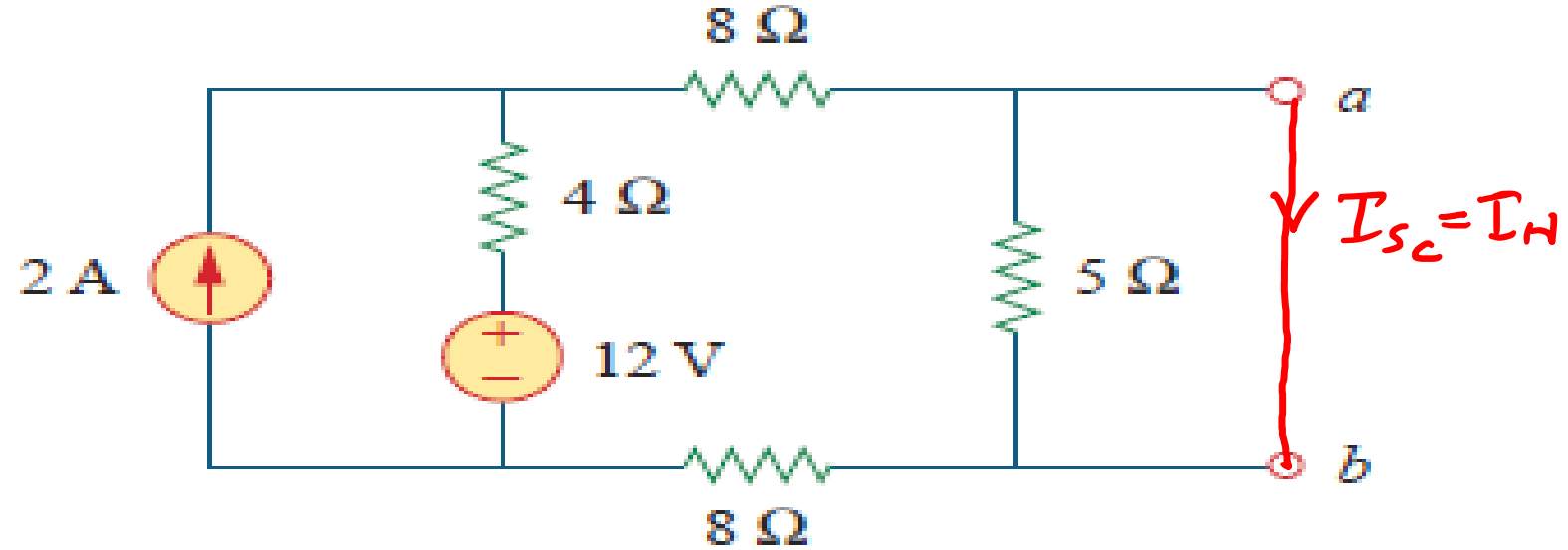


(a)

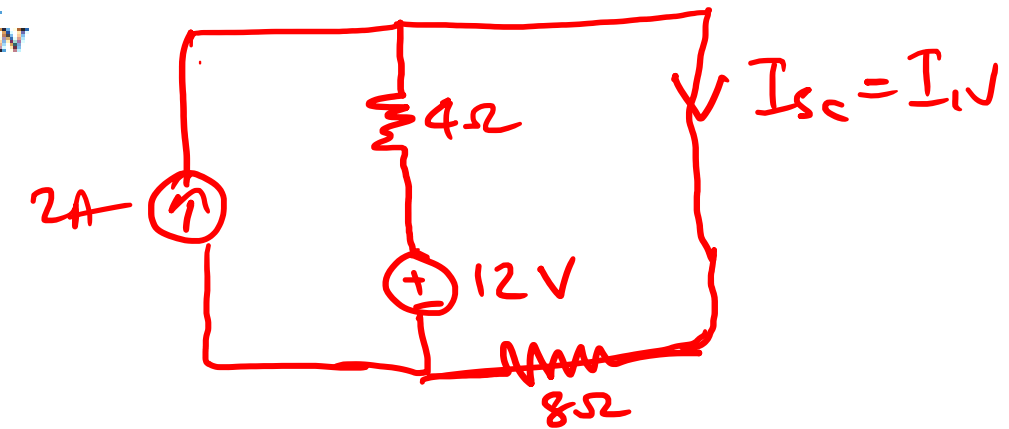


$$R_N = 5 \parallel (8 + 4 + 8) = 5 \parallel 20 = \frac{20 \times 5}{25} = 4 \Omega$$

We ignore the 5- $\Omega$  resistor because it has been short-circuited.  
Applying mesh analysis, we obtain



(b)



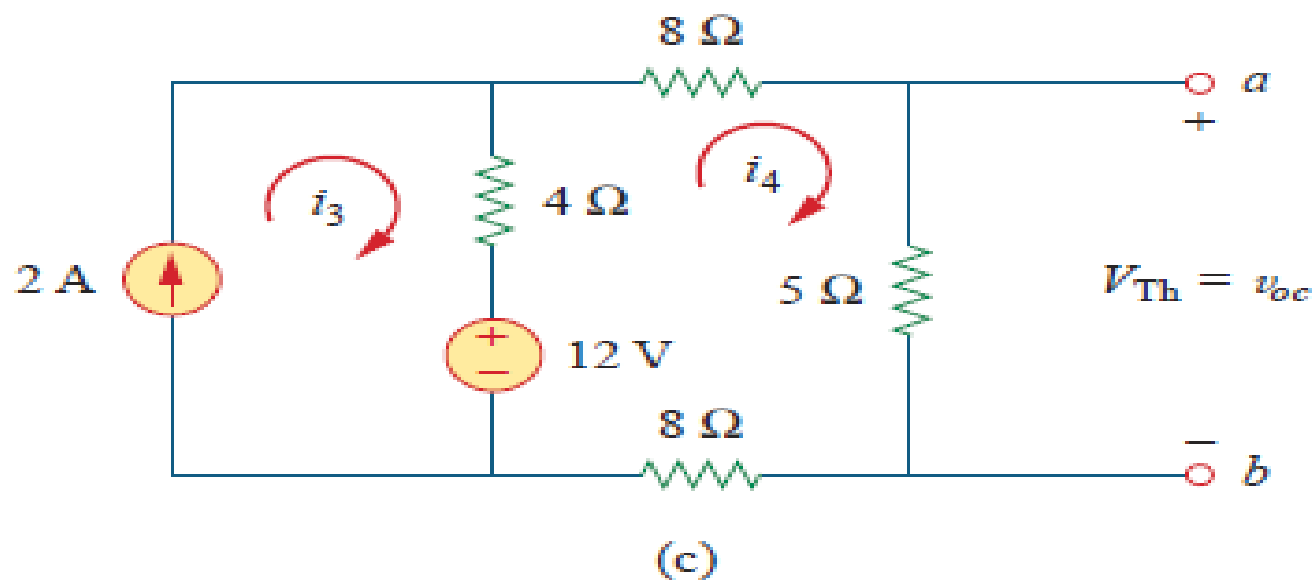
$$i_1 = 2 \text{ A},$$

$$20i_2 - 4i_1 - 12 = 0$$

$$i_2 = 1 \text{ A} = i_{sc} = I_N$$



Alternatively, we may determine  $I_N$  from  $V_{Th}/R_{Th}$ . We obtain  $V_{Th}$  as the open-circuit voltage across terminals  $a$  and  $b$  in



$$i_3 = 2 \text{ A}$$

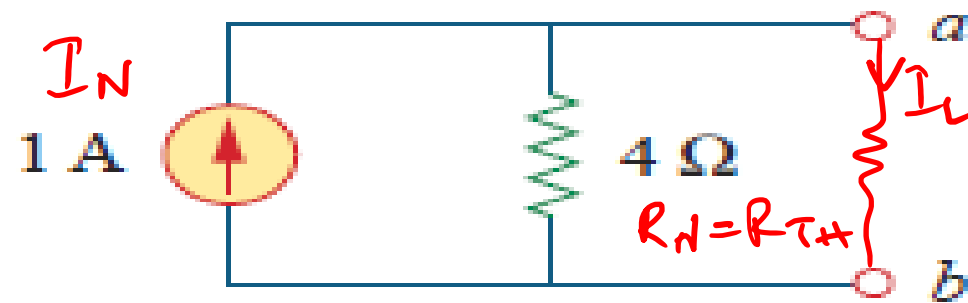
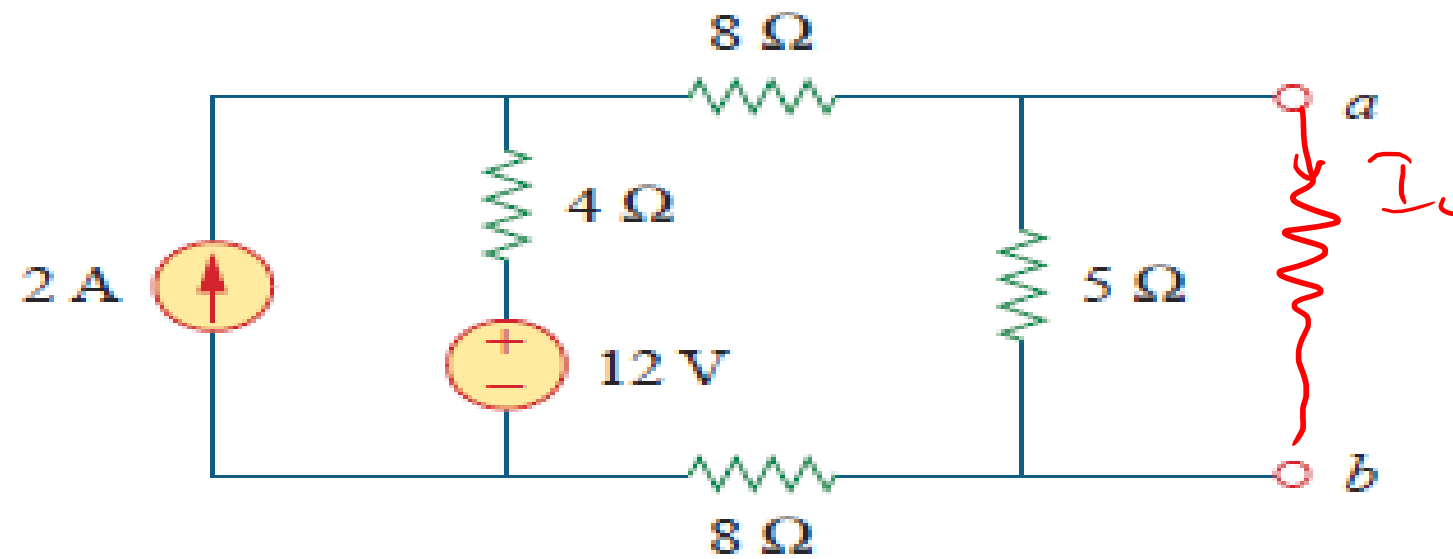
$$4i_3 - 12 = 0 \quad \Rightarrow \quad i_4 = 0.8 \text{ A}$$

and

$$v_{oc} = V_{Th} = 5i_4 = 4 \text{ V}$$

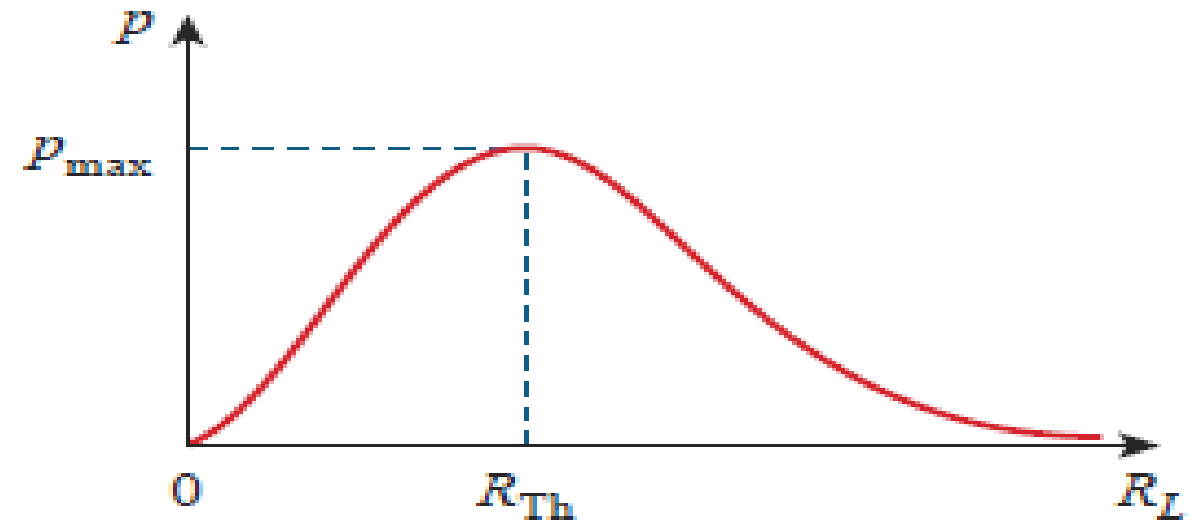
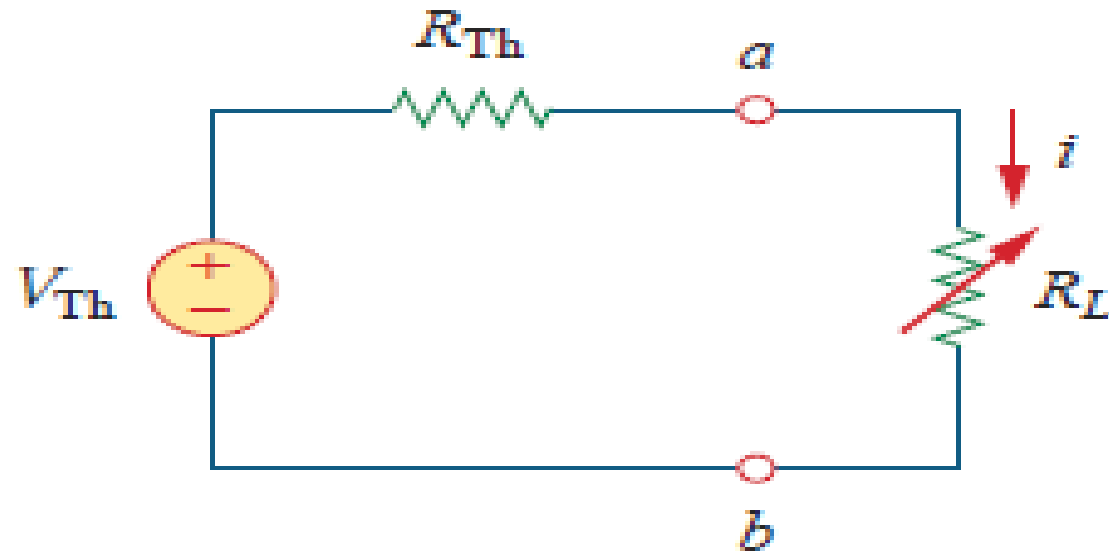
Hence,

$$I_N = \frac{V_{Th}}{R_{Th}} = \frac{4}{4} = 1 \text{ A}$$



Norton equivalent of the circuit

## Maximum Power Transfer



$$p = i^2 R_L = \left( \frac{V_{Th}}{R_{Th} + R_L} \right)^2 R_L$$

Maximum power is transferred to the load when the load resistance equals the Thevenin resistance as seen from the load ( $R_L = R_{Th}$ ).

$$p = i^2 R_L = \left( \frac{V_{\text{Th}}}{R_{\text{Th}} + R_L} \right)^2 R_L$$

$$\begin{aligned} \frac{dp}{dR_L} &= V_{\text{Th}}^2 \left[ \frac{(R_{\text{Th}} + R_L)^2 - 2R_L(R_{\text{Th}} + R_L)}{(R_{\text{Th}} + R_L)^4} \right] \\ &= V_{\text{Th}}^2 \left[ \frac{(R_{\text{Th}} + R_L - 2R_L)}{(R_{\text{Th}} + R_L)^3} \right] = 0 \end{aligned}$$

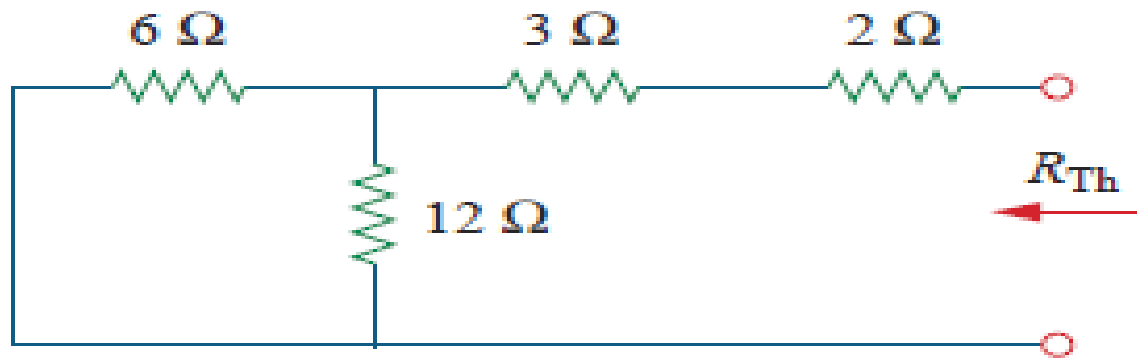
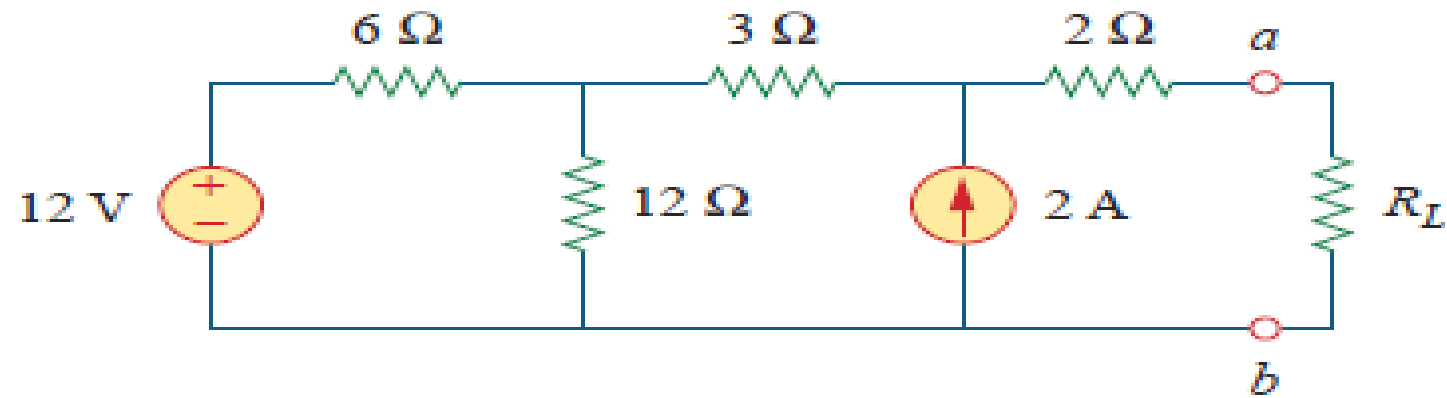
$$0 = (R_{\text{Th}} + R_L - 2R_L) = (R_{\text{Th}} - R_L)$$

$$R_L = R_{\text{Th}}$$

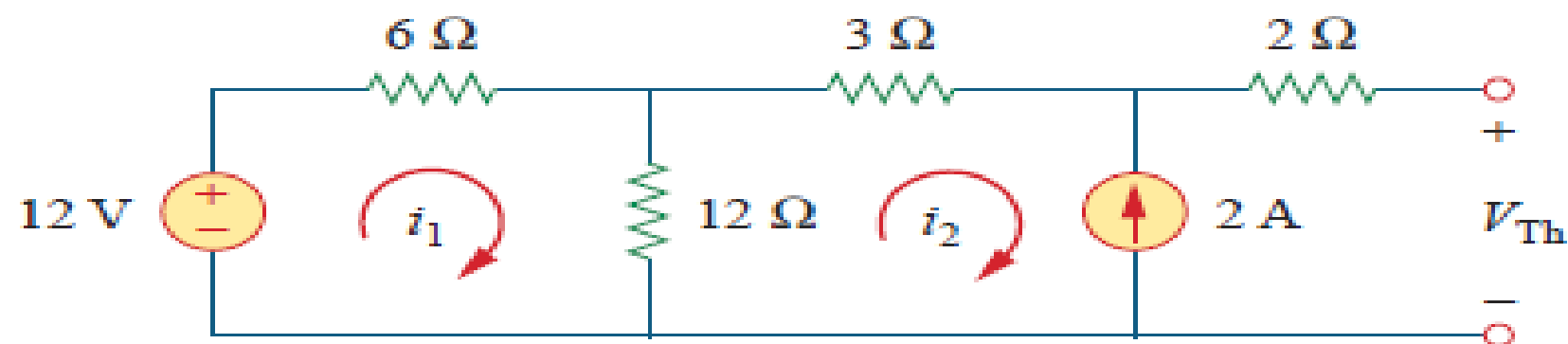
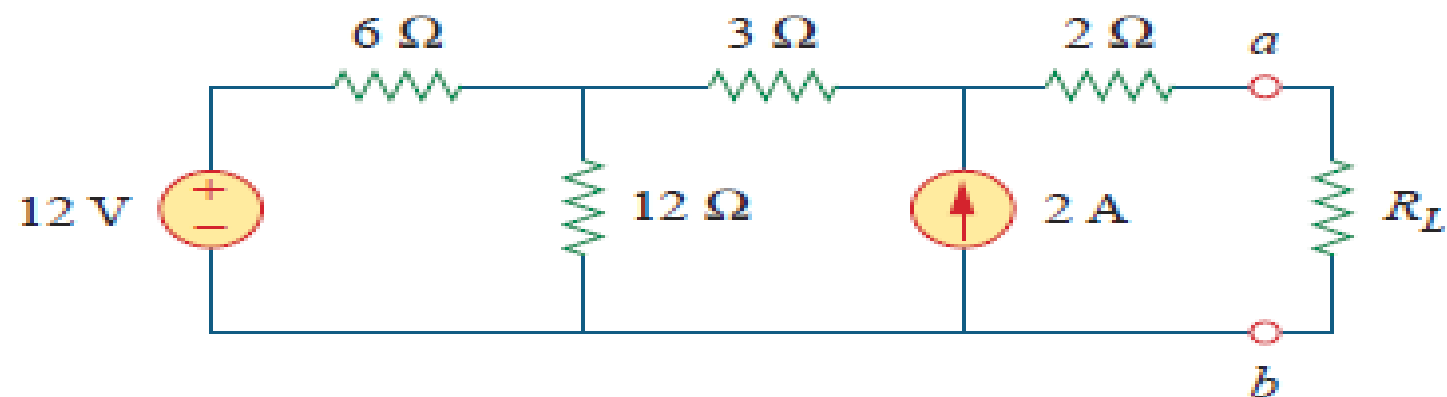
$$p_{\text{max}} = \frac{V_{\text{Th}}^2}{4R_{\text{Th}}}$$

## Example 4

Find the value of  $R_L$  for maximum power transfer in the circuit



$$R_{Th} = 2 + 3 + 6 \parallel 12 = 5 + \frac{6 \times 12}{18} = 9\ \Omega$$



$$-12 + 18i_1 - 12i_2 = 0, \quad i_2 = -2 \text{ A}$$

Solving for  $i_1$ , we get  $i_1 = -2/3$ .

$$-12 + 6i_1 + 3i_2 + 2(0) + V_{\text{Th}} = 0 \quad \Rightarrow \quad V_{\text{Th}} = 22 \text{ V}$$

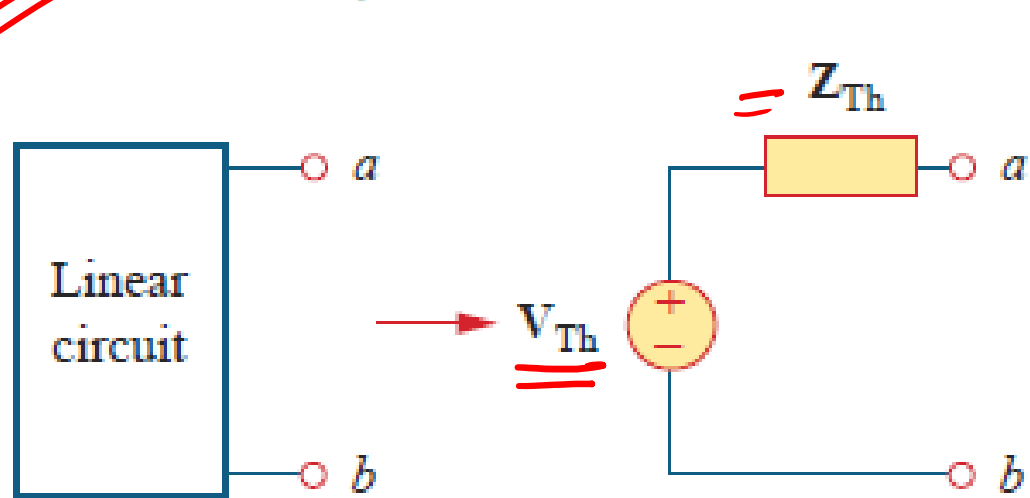
$$R_L = R_{\text{Th}} = 9 \, \Omega$$

$$p_{\text{max}} = \frac{V_{\text{Th}}^2}{4R_L} = \frac{22^2}{4 \times 9} = 13.44 \, \text{W}$$

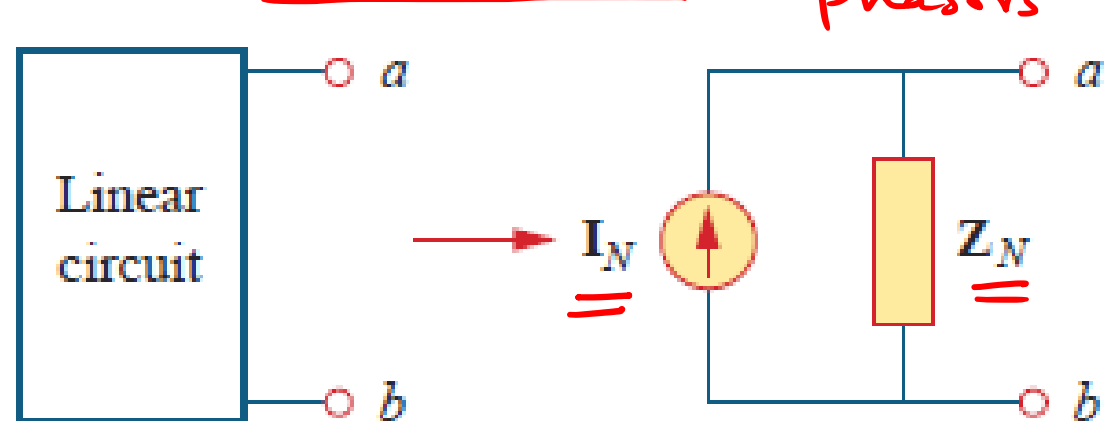
## 10.6

Thevenin and Norton  
Equivalent Circuits

Sinusoidal voltage sources & current.  
(AC with constant  $\omega$  or Sinusoidal)  
Phasors



Thevenin equivalent



Norton equivalent

$$V_{Th} = Z_N I_N, \quad Z_{Th} = Z_N$$

$V_{Th}$  → Thevenin voltage (open circuit voltage)

$Z_{Th}$  → Thevenin equivalent impedance

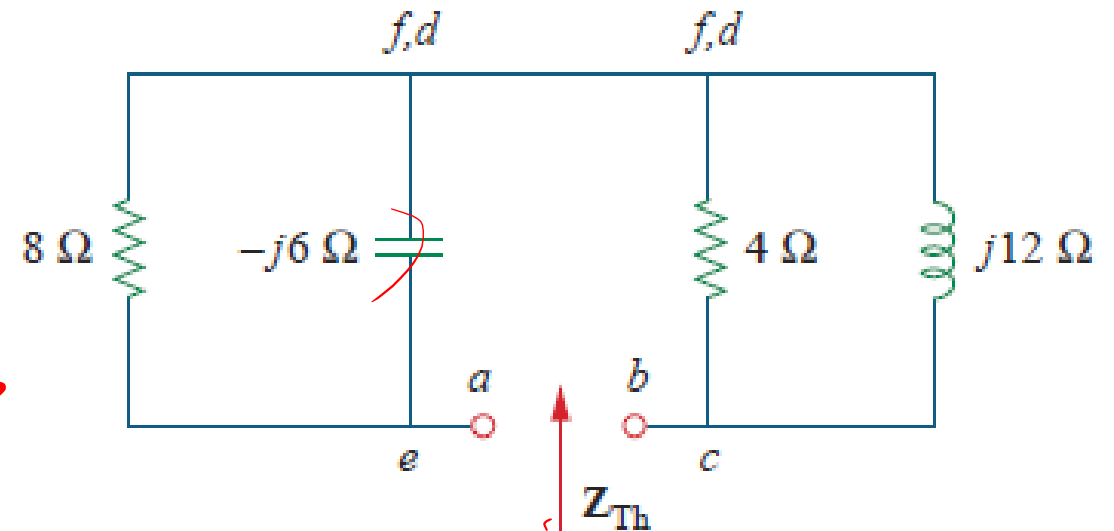
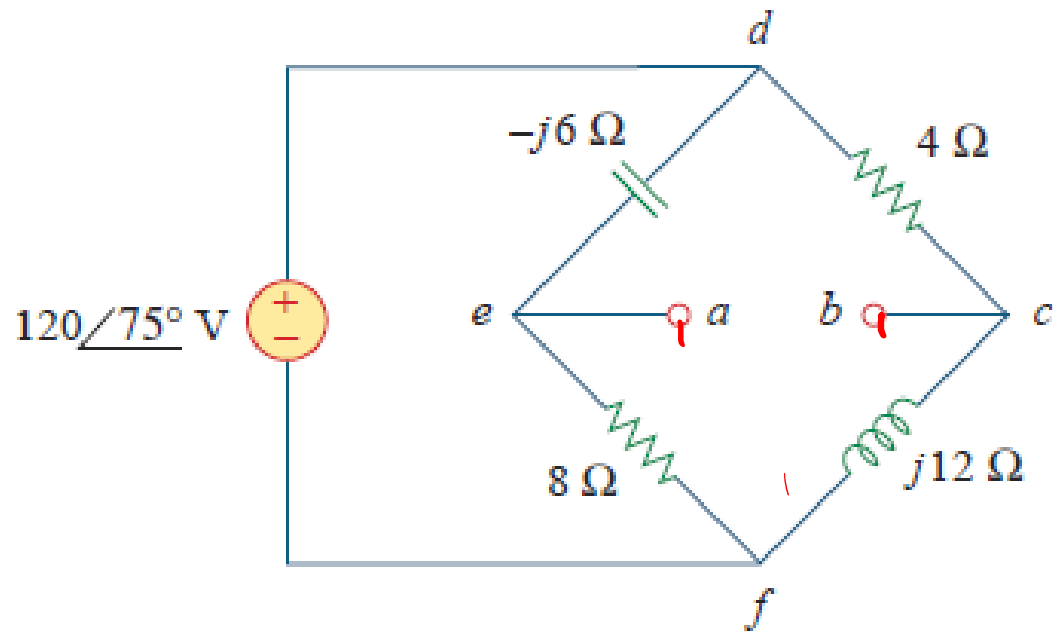
$I_N$  → Norton current (short-circuit current)

$Z_N$  → Norton equivalent impedance



## Example 10.8

Obtain the Thevenin equivalent at terminals  $a-b$  of the circuit in Fig.

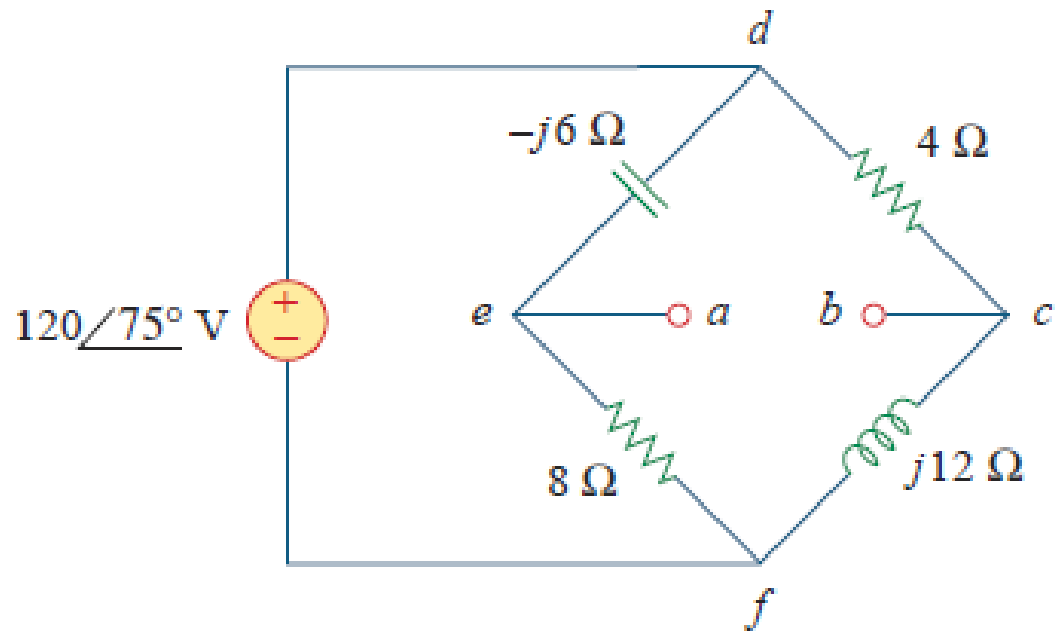


(a)

$$\mathbf{Z}_1 = -j6 \parallel 8 = \frac{-j6 \times 8}{8 - j6} = 2.88 - j3$$

$$\mathbf{Z}_2 = 4 \parallel j12 = \frac{j12 \times 4}{4 + j12} = 3.6 + j1.2 \, \Omega$$

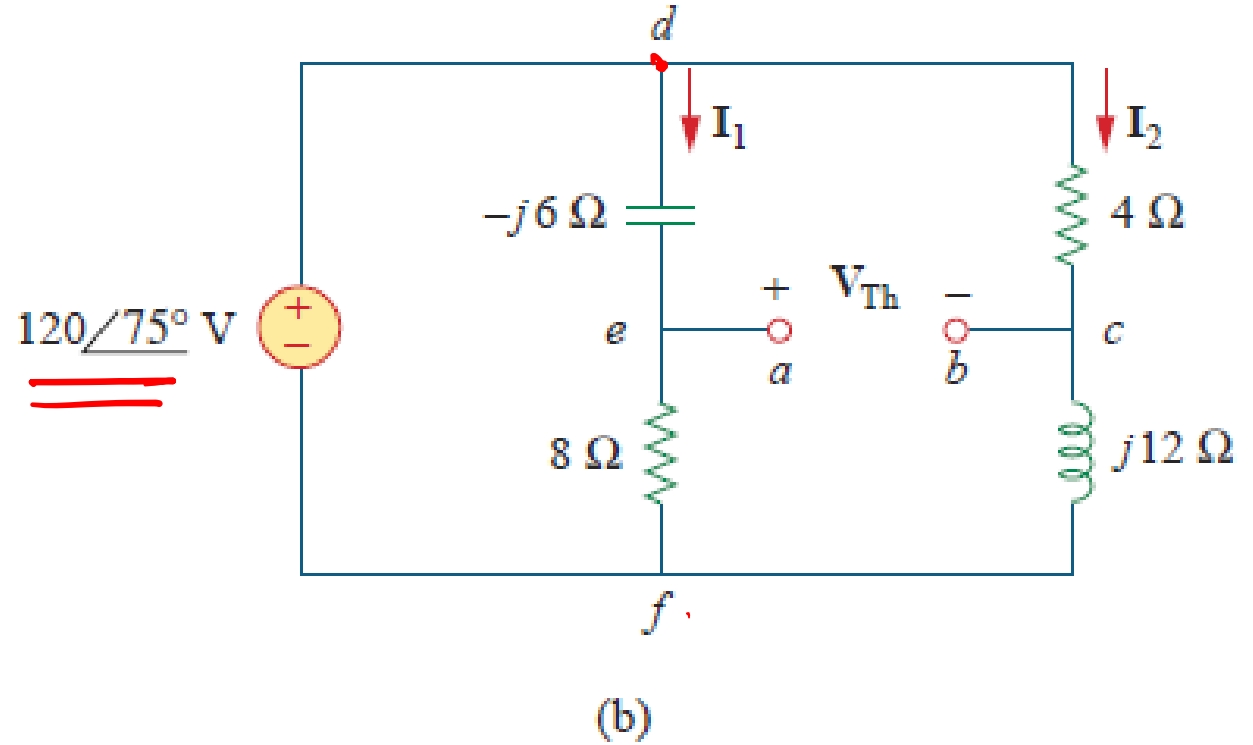
$$\begin{aligned} \mathbf{Z}_{Th} &= \mathbf{Z}_1 + \mathbf{Z}_2 \\ &= (6.48 - j2.64) \, \Omega \end{aligned}$$



Voltage applied between d & f  
is same as voltage applied betn

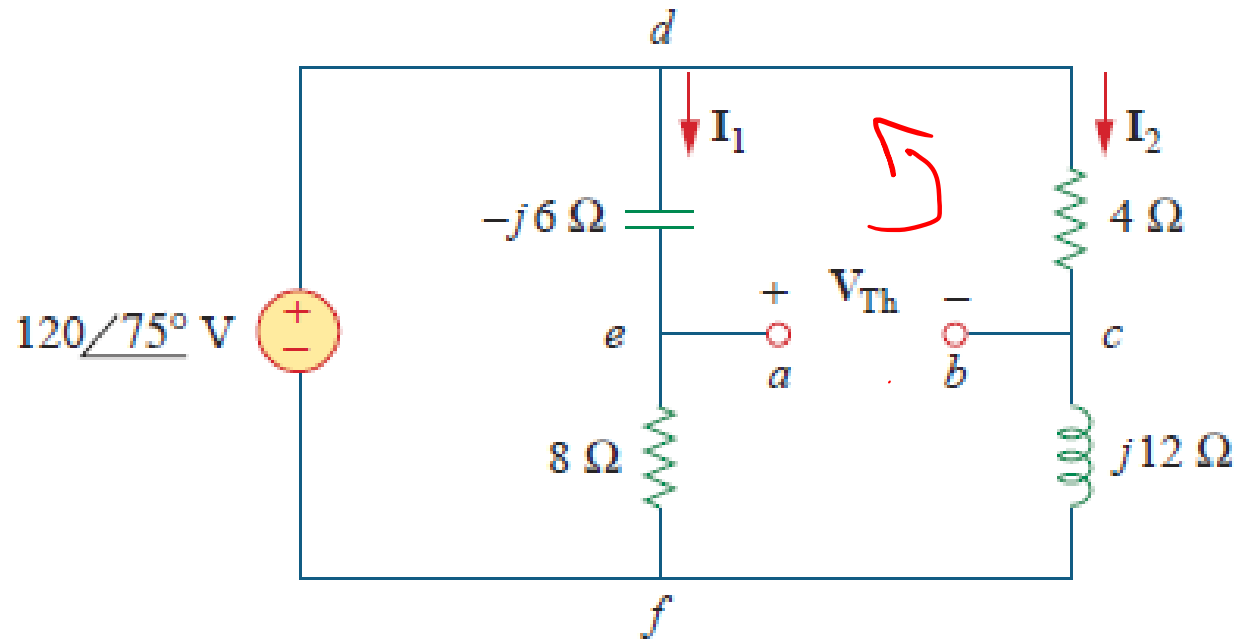
$$\underline{\underline{I_1 = \frac{120 \angle 75^\circ}{8 - j6} \text{ A}}}$$

$$\underline{\underline{I_2 = \frac{120 \angle 75^\circ}{4 + j12} \text{ A}}}$$



The Thevenin impedance is the series combination of  $\mathbf{Z}_1$  and  $\mathbf{Z}_2$ ; that is,

$$\mathbf{Z}_{Th} = \underline{\mathbf{Z}_1} + \underline{\mathbf{Z}_2} = 6.48 - j2.64 \Omega$$



(b)

$$\checkmark V_{Th} = \underline{\underline{-28.936 - j24.55}}$$

$$= \underline{\underline{37.95 \angle 220.31^\circ \text{ V}}}$$

$$\underline{\underline{bcdeab}} \Rightarrow \underline{\underline{KVL}}$$

Using  $\mathbf{I}_1$  &  $\mathbf{I}_2 \Rightarrow$

$$V_{Th} - 4I_2 + (-j6I_1) = 0$$

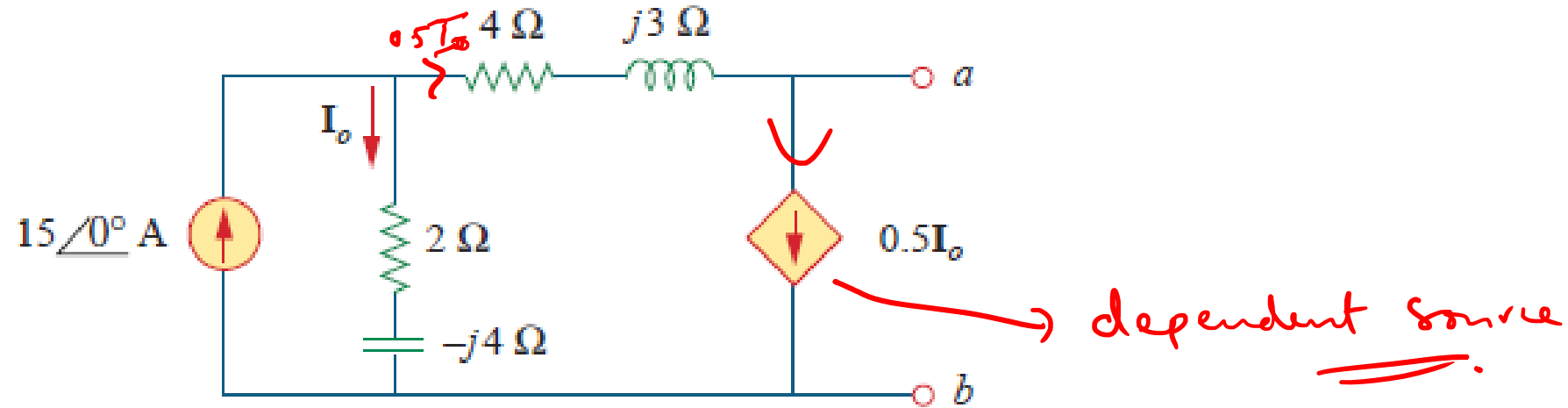
$$V_{Th} = \underline{\underline{4I_2 + j6I_1}}$$

$$\mathbf{V_{Th}} - 4\mathbf{I_2} + (-j6)\mathbf{I_1} = 0$$

$$\begin{aligned}\mathbf{V_{Th}} = 4\mathbf{I_2} + j6\mathbf{I_1} &= \frac{480\angle 75^\circ}{4 + j12} + \frac{720\angle 75^\circ + 90^\circ}{8 - j6} \\ &= 37.95\angle 3.43^\circ + 72\angle 201.87^\circ \\ &= -28.936 - j24.55 = \underline{\underline{37.95\angle 220.31^\circ \text{ V}}}\end{aligned}$$

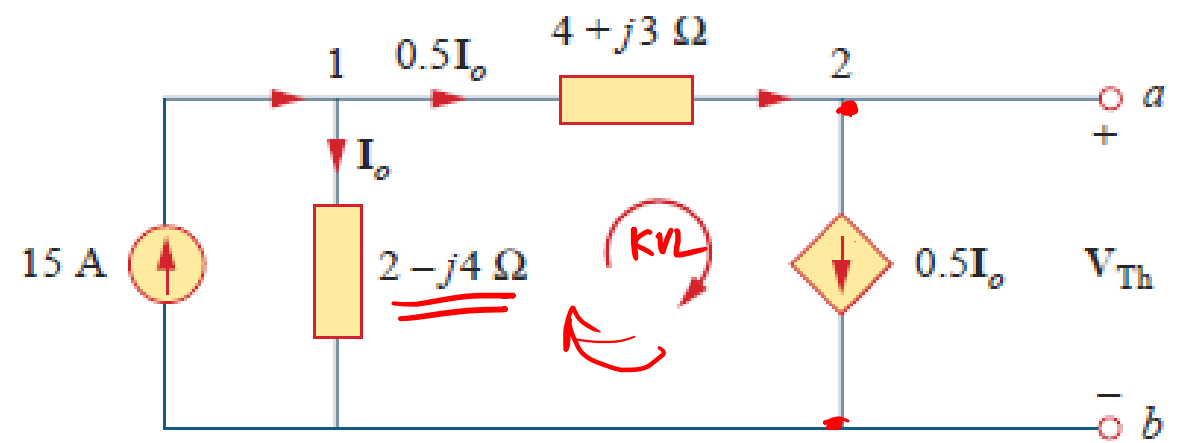
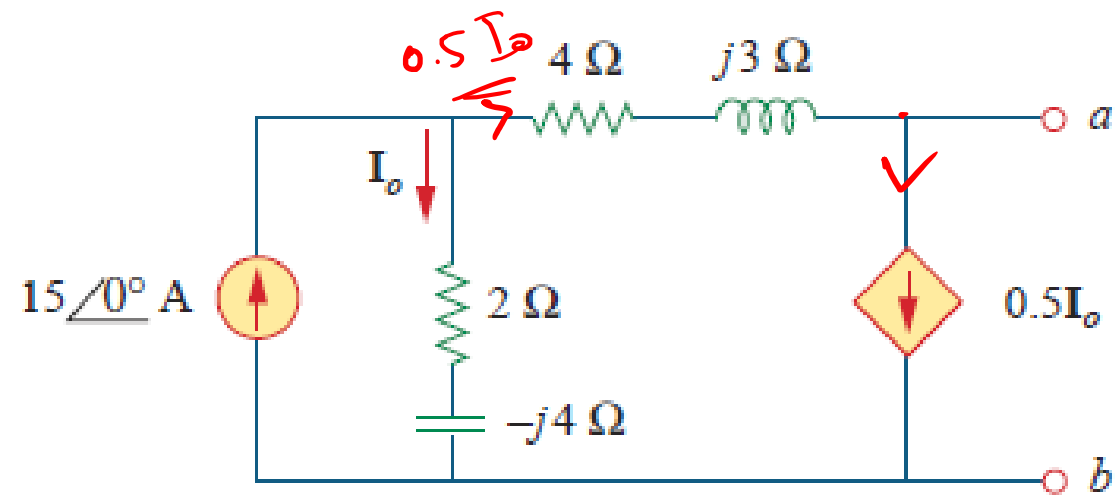
## Example 10.9

Find the Thevenin equivalent of the circuit in Fig.



To find  $V_{Th}$ , we apply KCL at node 1 in Fig.

$$\underline{15 = I_o + 0.5I_o} \Rightarrow \underline{I_o = 10 \text{ A}}$$



(a)

Applying KVL to the loop on the right-hand side in Fig.

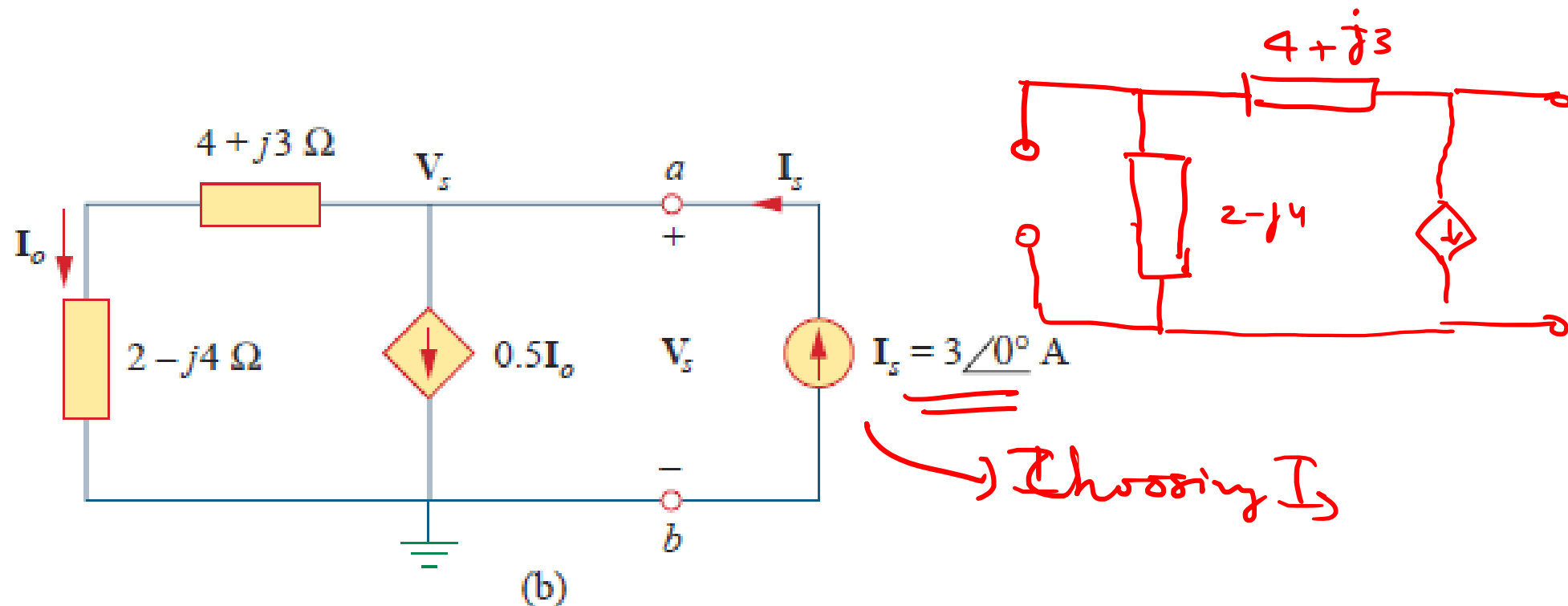
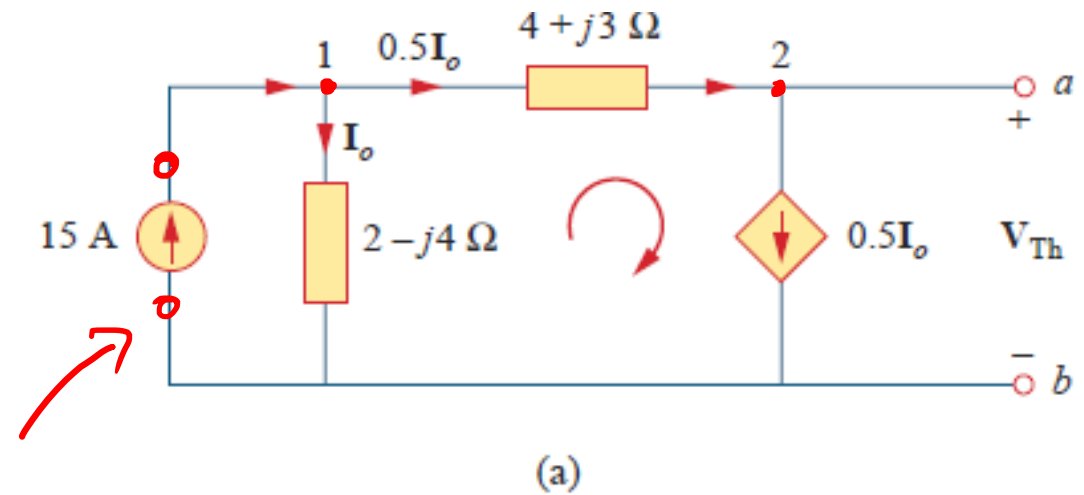
$$-\mathbf{I}_o(2 - j4) + 0.5\mathbf{I}_o(4 + j3) + \mathbf{V}_{Th} = 0$$

$$\mathbf{V}_{Th} = 10(2 - j4) - 5(4 + j3) = -j55$$

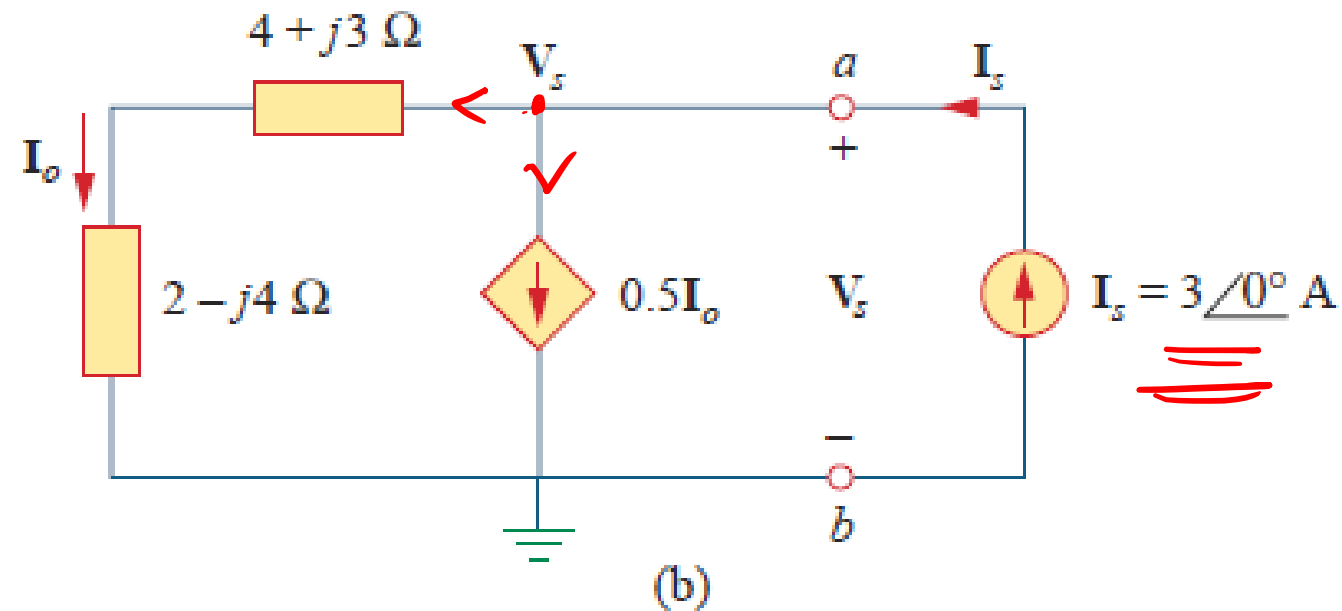
$$\mathbf{V}_{Th} = 55 \angle -90^\circ \text{ V}$$

To obtain  $\underline{Z}_{Th}$ , we remove the independent source.

- Due to the presence of the dependent current source, we connect a 3-A current source (3 is an arbitrary value chosen for convenience here, a number divisible by the sum of currents leaving the node) to terminals  $a-b$



- At the node, KCL gives



$$3 = \mathbf{I_o} + 0.5\mathbf{I_o} \quad \Rightarrow \quad \mathbf{I_o} = \underline{\underline{2 \text{ A}}}$$

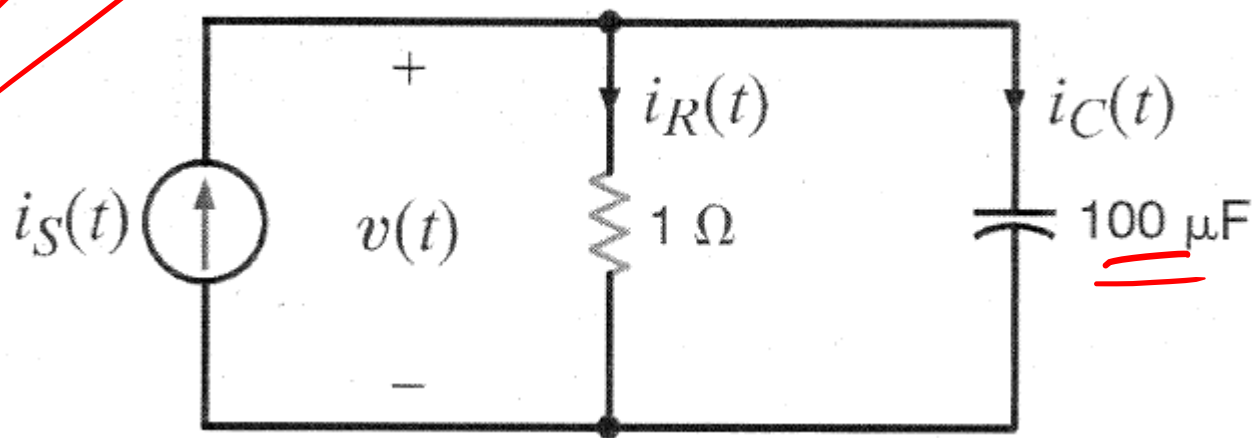
Applying KVL to the outer loop in Fig. 10.26(b) gives

$$\underline{\underline{\mathbf{V_s}}} = \mathbf{I_o}(4 + j3 + 2 - j4) = 2(6 - j)$$

The Thevenin impedance is

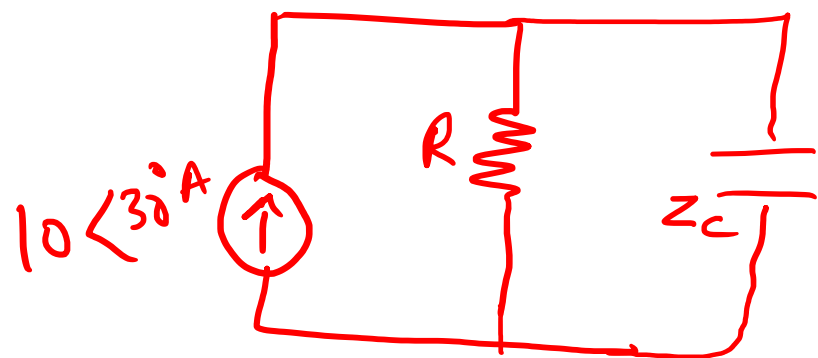
$$\underline{\underline{\mathbf{Z_{Th}}}} = \frac{\mathbf{V_s}}{\mathbf{I_s}} = \frac{2(6 - j)}{3} = \underline{\underline{4 - j0.6667 \Omega}}$$





Draw the frequency domain circuit and calculate  $v(t)$   
 $i_S(t) = 10 \cos(377t + 30^\circ) \text{ A}$   
 $\phi = 30^\circ$

$$\omega = 377 \text{ rad/sec.}$$



$$Z_C = \frac{1}{j\omega C}$$

$$R = 1 \Omega$$

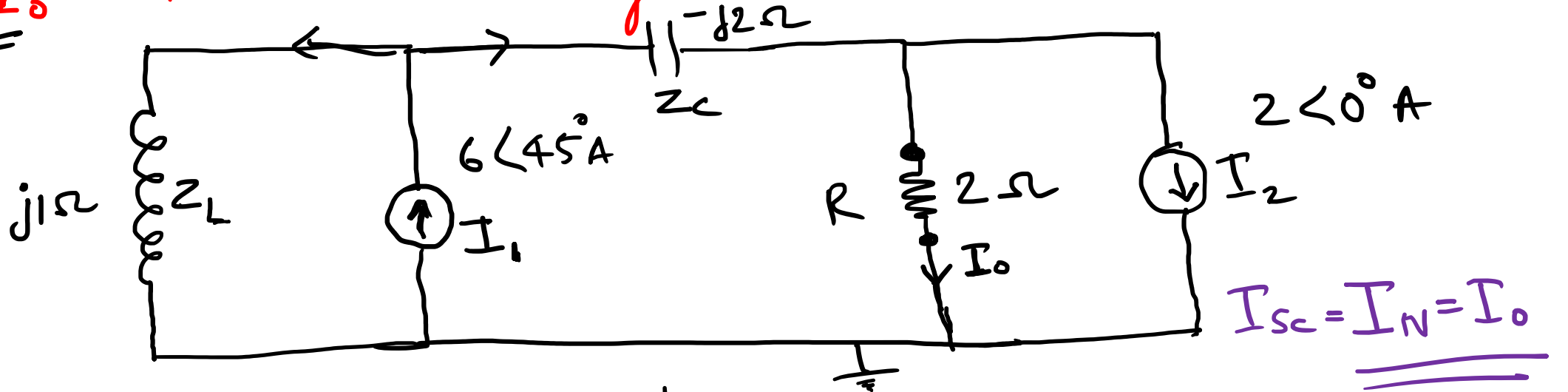
$$\frac{V}{Z} = I$$

$$V = I Z$$

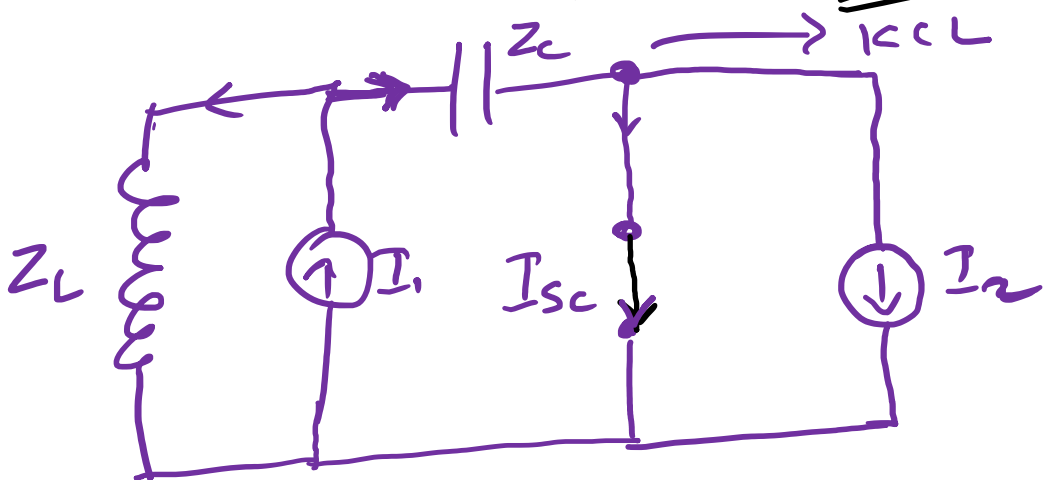
$$= 10 \angle 30^\circ \left( \frac{R Z_C}{R + Z_C} \right)$$

$$v(t) = 9.99 \cos(377t + 27.8^\circ)$$

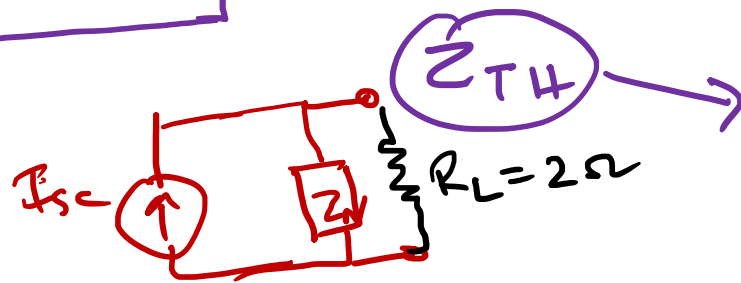
Find  $I_o$  in the network using Norton's theorem



The current through the  $2\Omega$  resistor (Load)

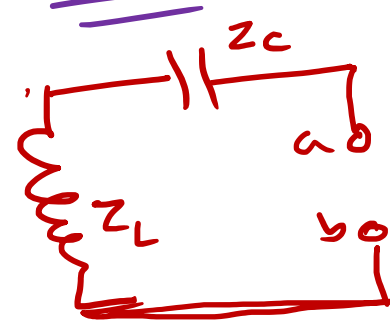


Eg. Girul



$$I_{sc} + I_2 - I_1 \frac{Z_L}{Z_L + Z_C} = 0 \quad \underline{\underline{(k(L))}}$$

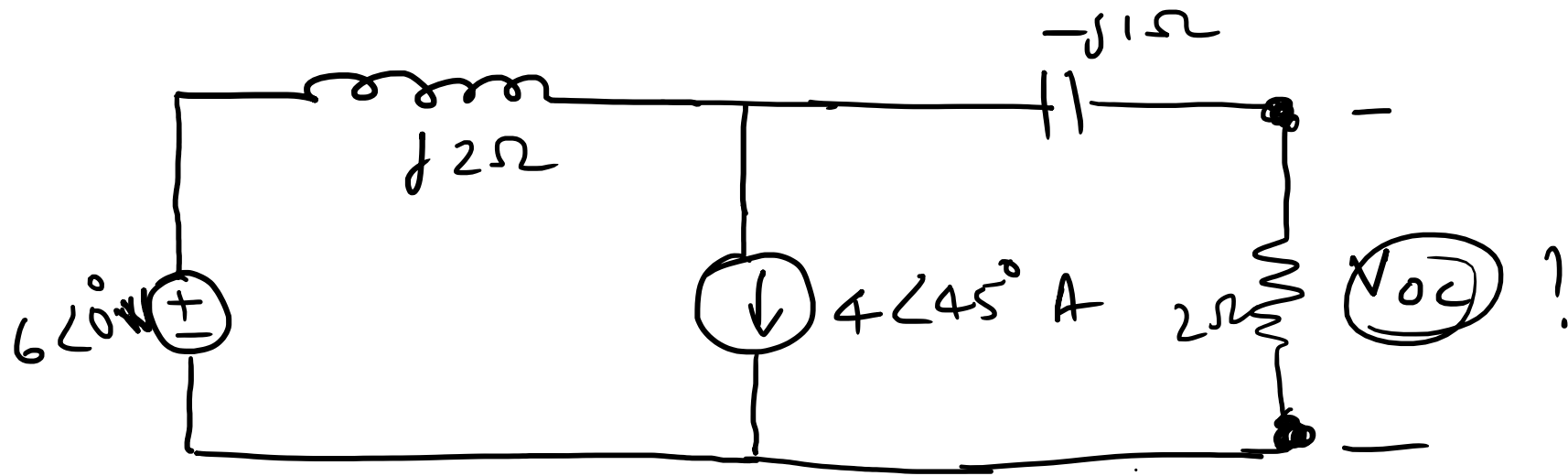
$I_{sc} = 9$  → Superpoint



$$Z_{TH} = Z_L + Z_C$$

$$= j1\Omega - j2\Omega$$

$$= -j1\Omega$$

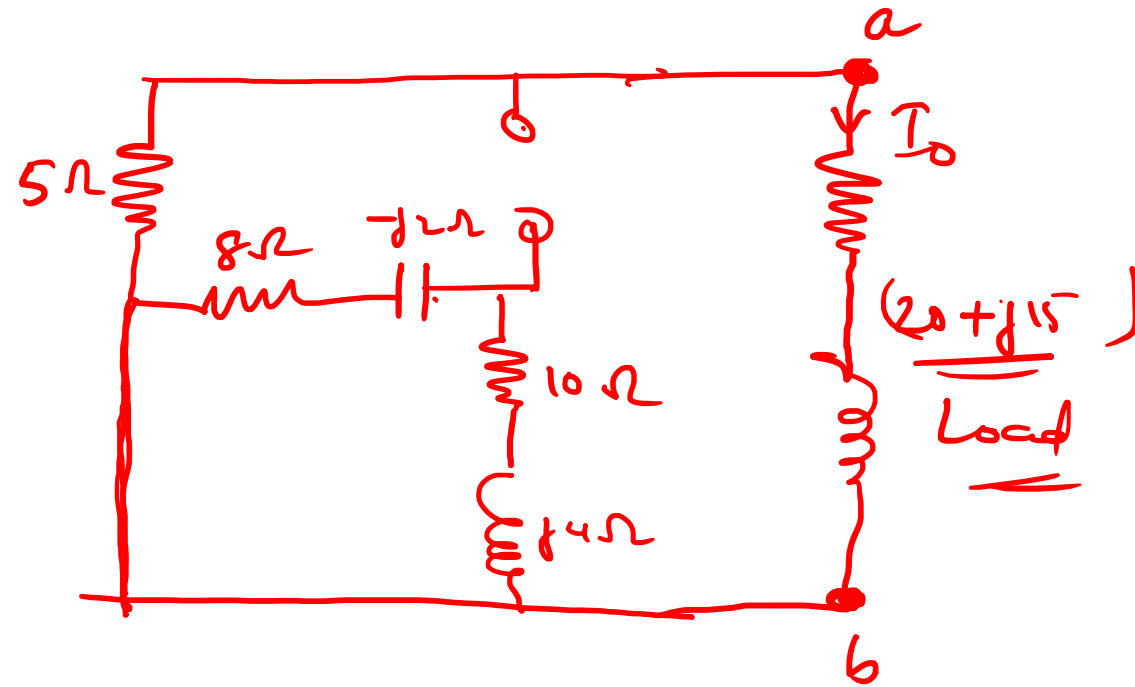
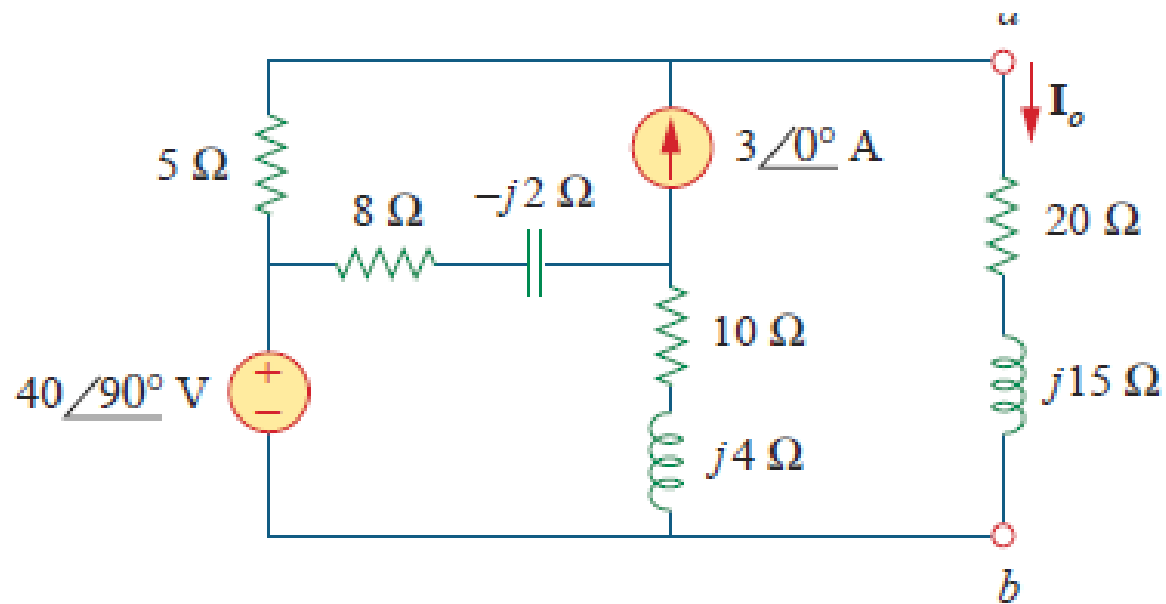


$$R_L = 2\Omega$$

$V_{TH}$  and  $Z_{TH}$  ?  
 =

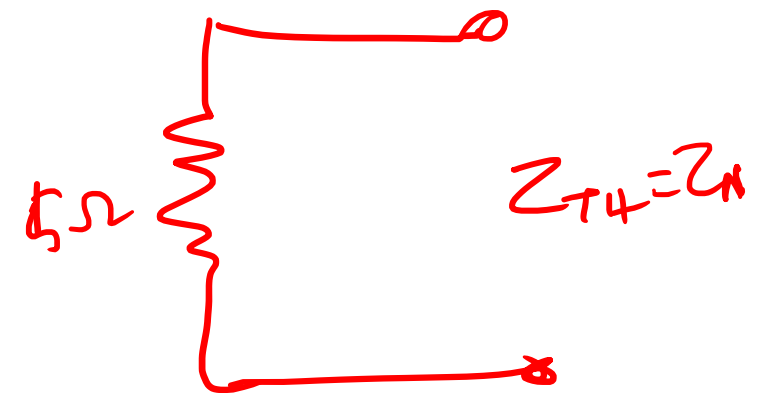
## Example 10.10

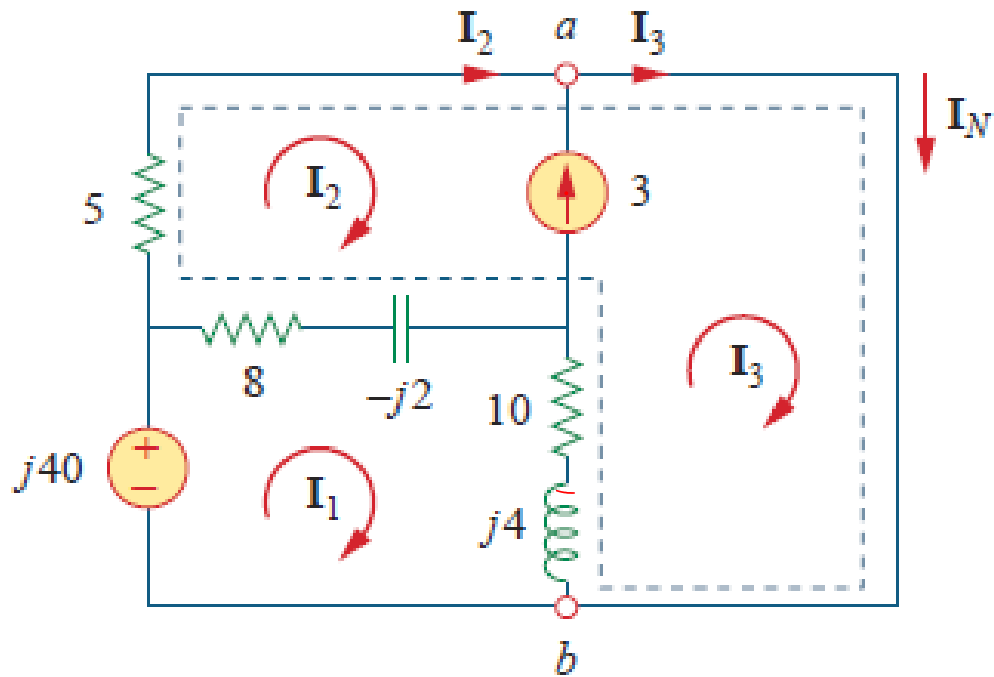
Obtain current  $I_o$  in Fig. using Norton's theorem.



As evident from the figure, the  $(8 - j2)$  and  $(10 + j4)$  impedances are short-circuited, so that

$$Z_{Th} = Z_N = \underline{\underline{5 \Omega}}$$



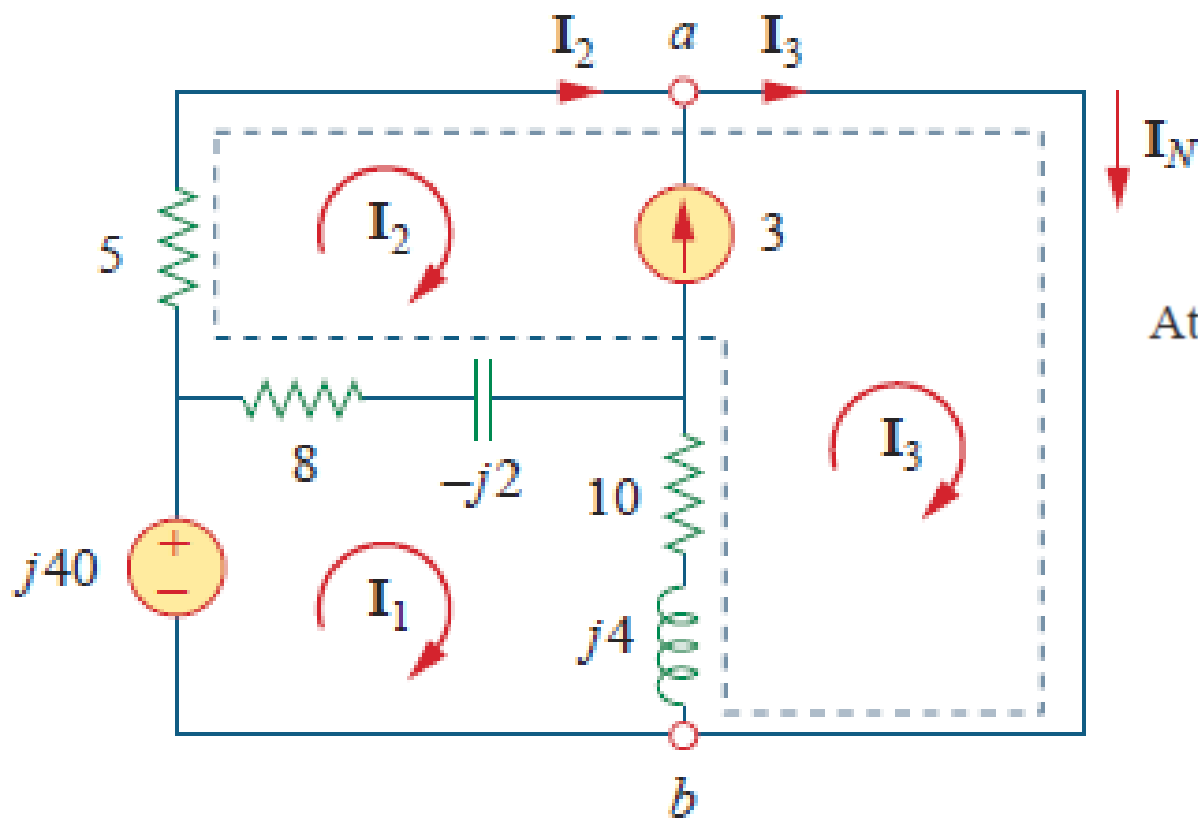


Notice that meshes 2 and 3 form a supermesh because of the current source linking them. For mesh 1,

$$-j40 + (18 + j2)\mathbf{I}_1 - (8 - j2)\mathbf{I}_2 - (10 + j4)\mathbf{I}_3 = 0 \quad \leftarrow$$

For the supermesh,

$$\rightarrow (13 - j2)\mathbf{I}_2 + (10 + j4)\mathbf{I}_3 - (18 + j2)\mathbf{I}_1 = 0$$



At node  $a$ , due to the current source between meshes 2 and 3,

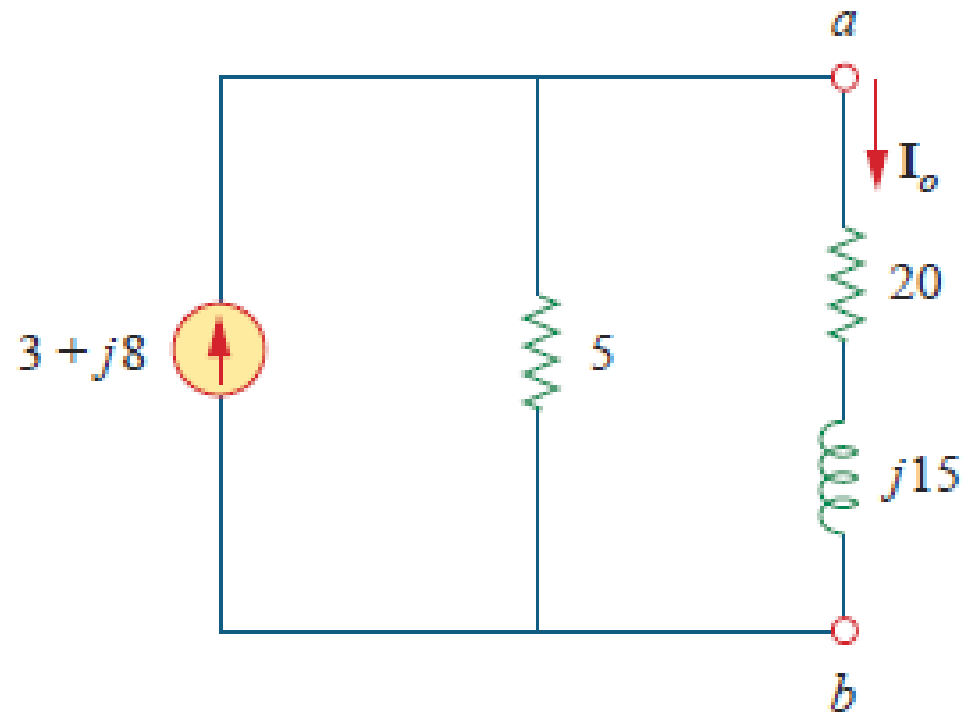
$$\mathbf{I}_3 = \mathbf{I}_2 + 3$$

$$-j40 + 5\mathbf{I}_2 = 0 \quad \Rightarrow \quad \mathbf{I}_2 = j8$$

The Norton current is

$$\mathbf{I}_N = \mathbf{I}_3 = (3 + j8) \text{ A}$$

The Norton equivalent circuit along with the impedance at terminals  $a$ - $b$ .



(c)

$$\mathbf{I}_o = \frac{5}{5 + 20 + j15} \mathbf{I}_N = \frac{3 + j8}{5 + j3} = 1.465 \angle 38.48^\circ \text{ A}$$