#### 5.6 Circulator

#### Module:5 Microwave Passive components

Course: BECE305L – Antenna and Microwave Engineering

-Dr Richards Joe Stanislaus

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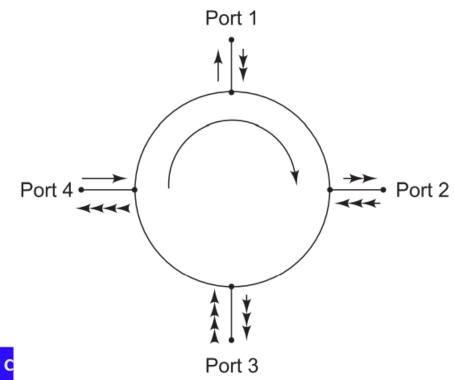
# Module:5 <u>Microwave Passive components</u> 6 hours

 Microwave Networks - ABCD, 'S' parameter and its properties. E-Plane Tee, H-Plane Tee, Magic Tee and Multi-hole directional coupler. Principle of Faraday rotation, isolator, circulator and phase shifter.

Source of the contents: Pozar

#### 6. Circulators

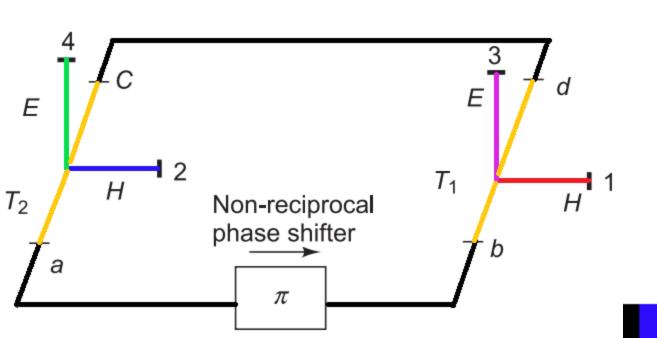
- Ferromagnetic materials (ferrite: Mg+Mn, Ni+Zn alloys) when placed in dc magntic field, electromagnetic wave propagation becomes non-reciprocal.
- This property is used for construction of circulators and isolators.
- Circulator: Multiport junction wave can travel from one port to the next immediate port in one direction only.
- Commonly used circulators
   Three port or
   Four port

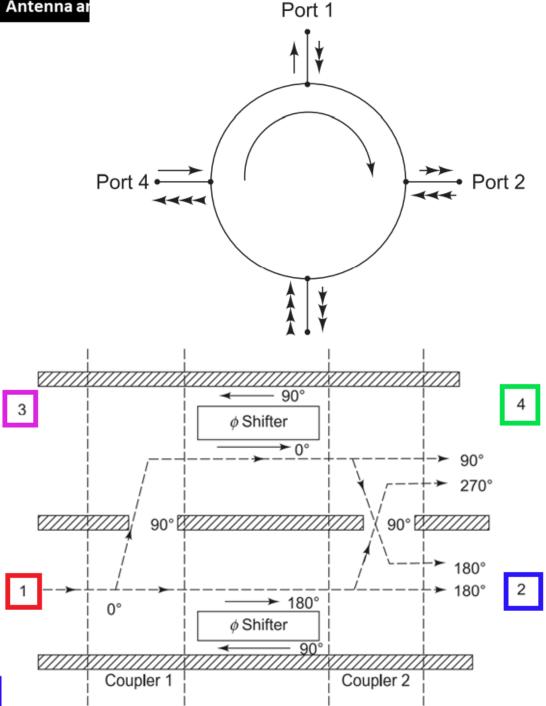


#### Antenna a

# 6.1 Four port Circulator

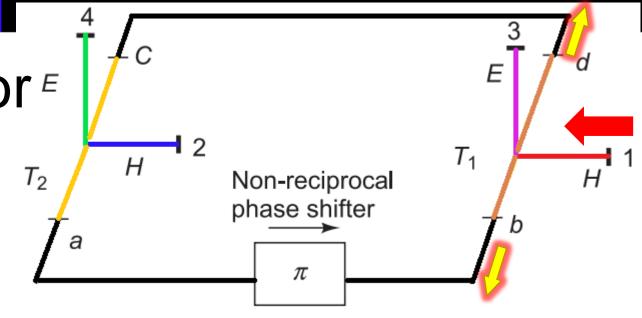
- Four port circulator can be constructed
  - 1) from two magic Ts and a non reciprocal 180° phase shifter or
  - 2) a combination of two 3dB side hole directional couplers with two non-reciprocal phase shifters





Configuration 1:

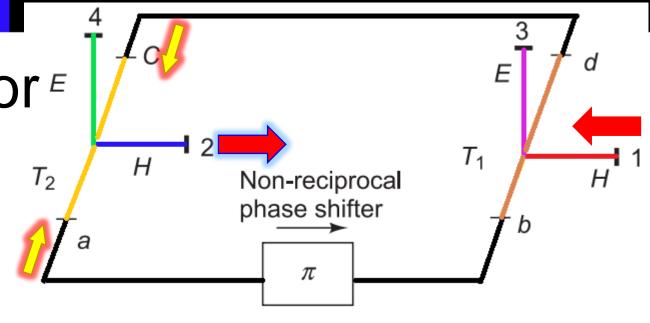
 Input signal at port 1 is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.



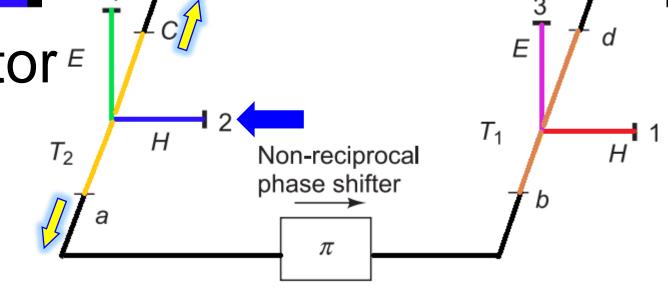
Configuration 1:

 Input signal at port 1 is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.

They enter in phase at ports a and c of magic tee T2, and are added at port 2.



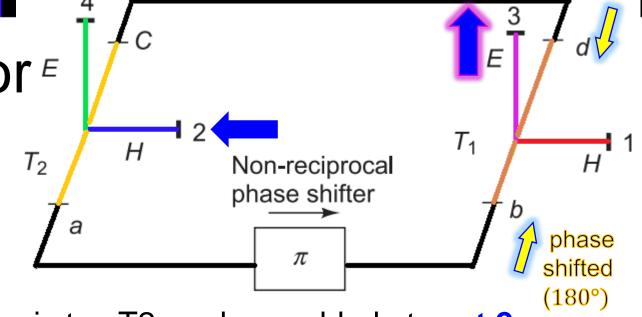
Configuration 1:
 Input signal at port 1 is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.



They enter in phase at ports a and c of magic tee T2, and are added at port 2.

• Input signal at port 2 is split into two in phase and equal amplitude waves in collinear arms a and c of magic tee T2.

Configuration 1:
 Input signal at port 1 is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.



They enter in phase at ports a and c of magic tee T2, and are added at port 2.

Input signal at port 2 is split into two in phase and equal amplitude waves in collinear arms a and c of magic tee T2.
 They enter out of phase at ports b and d of magic tee T1, and appear at port 3.

 Configuration 1: Input signal at port 1 is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.



 $T_2$ 

- Input signal at port 2 is split into two in phase and equal amplitude
  waves in collinear arms a and c of magic tee T2.
  They enter out of phase at ports b and d of magic tee T1, and appear at port 3.
- Input signal at port 3 is split into two out of phase and equal amplitude waves in collinear arms b and d of magic tee T1 and

Non-reciprocal

phase shifter

 $\pi$ 

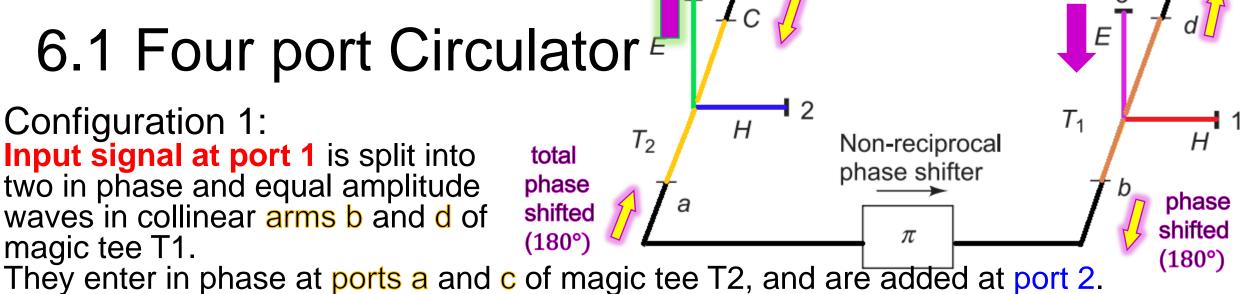
 $T_1$ 

phase

shifted

(180°)

 Configuration 1: **Input signal at port 1** is split into two in phase and equal amplitude waves in collinear arms b and d of magic tee T1.

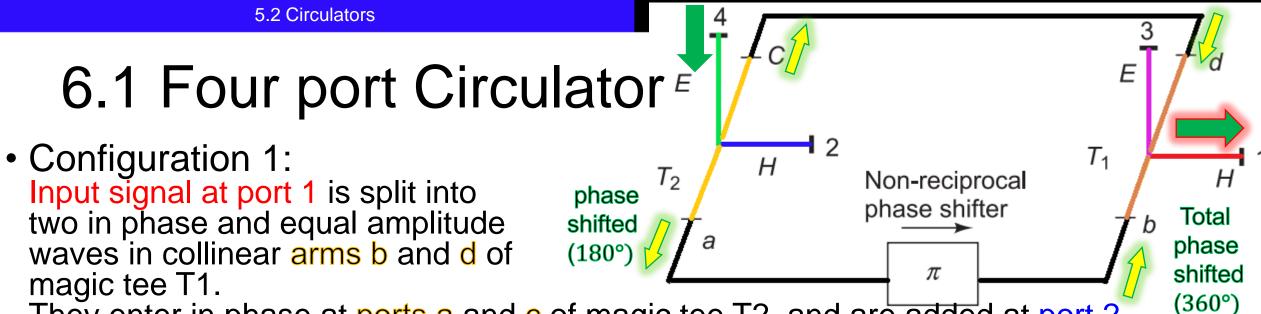


 Input signal at port 2 is split into two in phase and equal amplitude waves in collinear arms a and c of magic tee T2. They enter out of phase at ports b and d of magic tee T1, and appear at port 3.

 Input signal at port 3 is split into two out of phase and equal amplitude waves in collinear arms b and d of magic tee T1 and appear at Port 4 of T2

They enter in phase at ports a and c of magic tee T2, and are added at port 2.

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  waves in collinear arms a and c of magic tee T2.
  They enter out of phase at ports b and d of magic tee T1, and appear at port 3.
- Input signal at port 3 is split into two out of phase and equal amplitude waves in collinear arms b and d of magic tee T1 and appear at Port 4 of T2
- Input signal at port 4 is split into two out of phase and equal amplitude waves in collinear arms a and c of magic tee T2 and

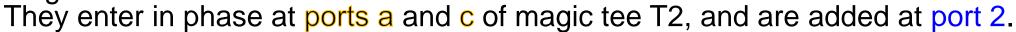


- They enter in phase at ports a and c of magic tee T2, and are added at port 2.

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- Input signal at port 4 is split into two out of phase and equal amplitude waves in collinear arms a and c of magic tee T2 and appear at Port 1 of T1
- Port 1 -> port 2; port 2 -> port 3; port 3-> Port 4; Port 4-> Port 1

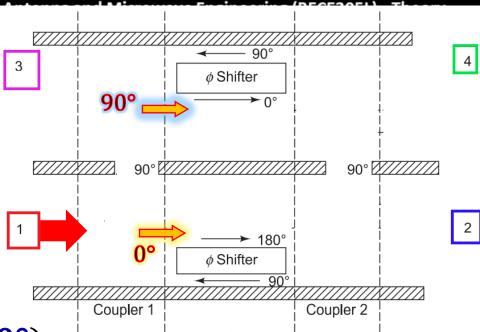
Non-reciprocal

phase shifter

 $\pi$ 

 $T_1$ 

- Configuration 2:
- Each 3dB coupler introduces 90° phase shift.
- Input signal in port 1, splits into two at coupler 1, one with 90° phase shift. (0°, 90°)



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  These signals split at the coupler 2 again, to give zero output (partly at 90° + partly at 270° = cancellation of signal) at port 4 and

φ Shifter

90°

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Output (partly at 180° and remaining at same 180°) at port 2. Summary: port 1-> port 2

 $\phi$  Shifter

180°

90°

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  Output (partly at 180° and remaining at same 180°) at port 2.
- Similarly, port 2-> port 3; port 3-> port 4; port 4->port 1

Summary: port 1-> port 2

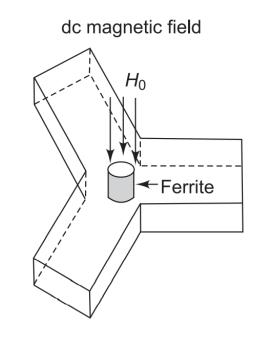
4

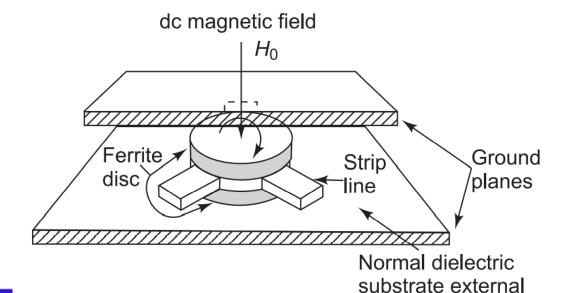
90° ///////

 A perfectly matched, lossless and non-reciprocal four port circulator has the S matrix:

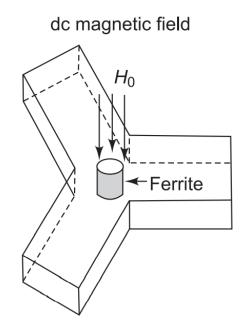
$$[S] = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$$

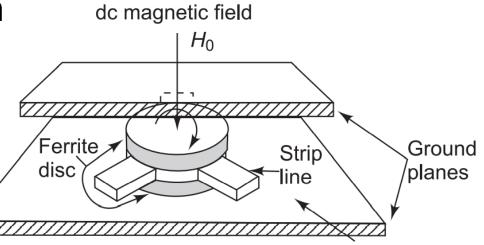
• A three port circulator is formed by a 120° H —plane waveguide or stripline symmetrical Y junction with a ferrite post or disc.





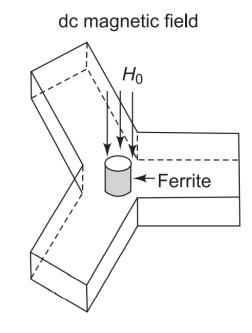
- A three port circulator is formed by a  $120^{\circ}$  H —plane waveguide or stripline symmetrical Y junction with a ferrite post or disc.
- A steady magnetic field H<sub>0</sub> is applied along the axis of the post/disc.
- Based on the polarization of incident wave and direction of  $H_0$ , microwave signal travels from one port to immediate next one only.

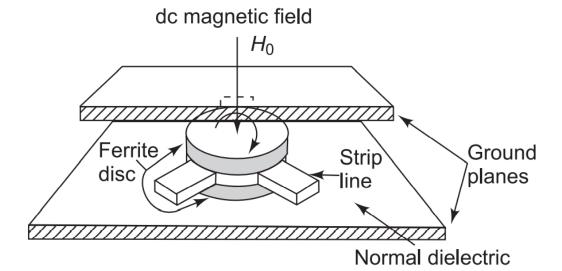




 A perfectly matched, lossless and nonreciprocal three port circulator has the S matrix:

$$[S] = \begin{bmatrix} 0 & 0 & S_{13} \\ S_{21} & 0 & 0 \\ 0 & S_{32} & 0 \end{bmatrix}$$





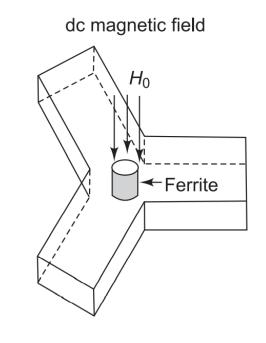
substrate external

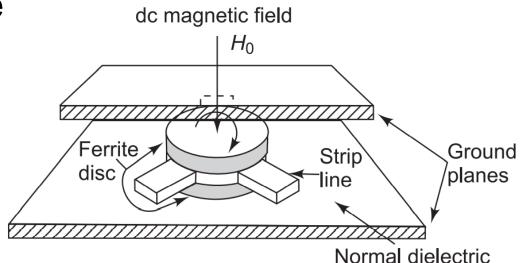
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• By proper choice of terminal planes, phase angles of  $S_{13}$ ,  $S_{21}$ ,  $S_{32}$  are made zero and

$$S_{13} = S_{21} = S_{32} = 1$$
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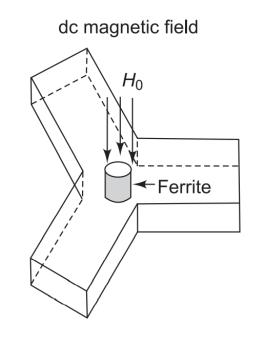
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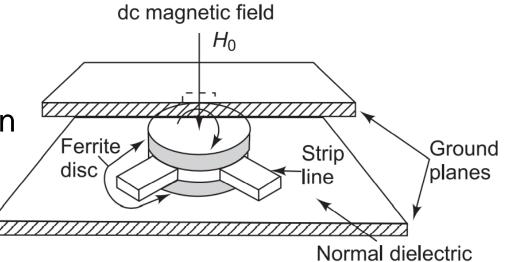
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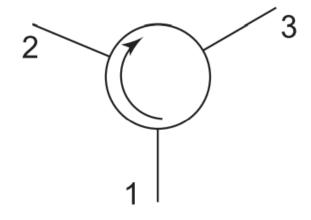
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Practically, finite isolation Insertion loss <1dB Isolation≈30-40dB VSWR<1.5

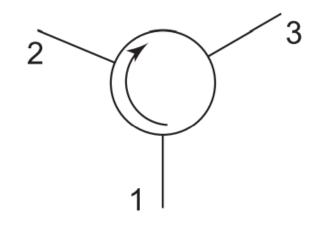




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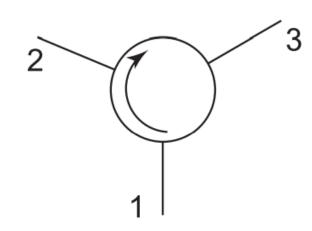


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$$[S] = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{32} & S_{33} \end{bmatrix}$$
 S matrix of 3 port circulator



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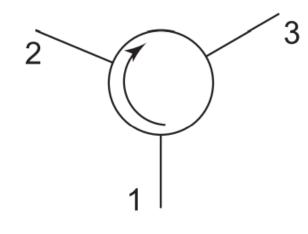
• Insertion loss=1dB= $-20 \log_{10} |S_{21}|$  $|S_{21}| = 10^{-1/20} = 0.89$ 



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Same insertion loss between ports (1,2), and (2,3) and (3,1)  $|S_{21}| = |S_{32}| = |S_{13}| = 0.89$ 

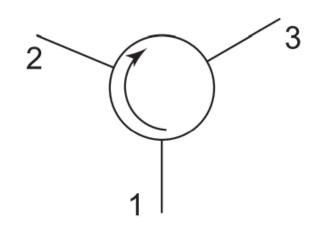


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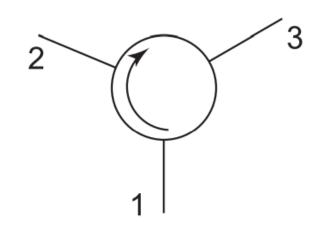


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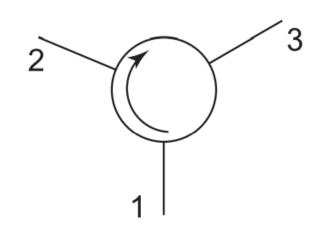
• Isolation between ports is  $30dB = -20 \log_{10} |S_{31}|$  $|S_{31}| = 10^{-30/20} = 10^{-1.5} = 0.032 = |S_{23}| = |S_{12}|$ 



6.3 Problem: A three port circulator has an insertion loss of 1dB, Isolation 30dB and VSWR 1.5. Find the S matrix.  $\begin{bmatrix} S_{11} & S_{12} & S_{13} \end{bmatrix}$ 

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 S matrix of 3 port circulator

- Insertion loss=1dB=-20  $\log_{10}|S_{21}|$  $|S_{21}| = 10^{-1/20} = 0.89$
- Same insertion loss between ports (1,2), and (2,3) and (3,1)  $|S_{21}| = |S_{32}| = |S_{13}| = 0.89$
- Isolation between ports is  $30dB = -20 \log_{10} |S_{31}|$   $|S_{31}| = 10^{-30/20} = 10^{-1.5} = 0.032 = |S_{23}| = |S_{12}|$
- VSWR = 1.5, reflection coefficient  $|\Gamma| = \frac{S-1}{S+1} = \frac{1.5-1}{1.5+1} = \frac{1.5-1}{1.5+1}$



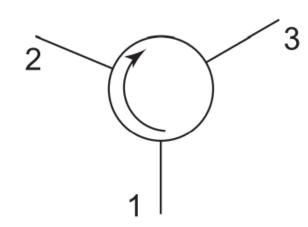
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 S matrix of 3 port circulator

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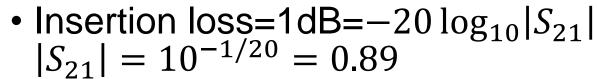
Same insertion loss between ports (1,2), and (2,3) and (3,1)  $|S_{21}| = |S_{32}| = |S_{13}| = 0.89$ 

- Isolation between ports is  $30dB = -20 \log_{10} |S_{31}|$   $|S_{31}| = 10^{-30/20} = 10^{-1.5} = 0.032 = |S_{23}| = |S_{12}|$
- VSWR = 1.5, reflection coefficient  $|\Gamma| = \frac{S-1}{S+1} = \frac{1.5-1}{1.5+1} = 0.2 = |S_{11}| = |S_{22}| = |S_{33}|$

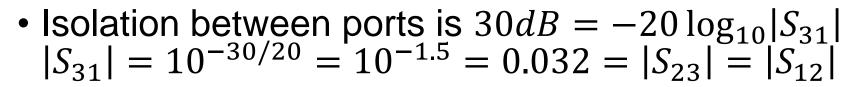


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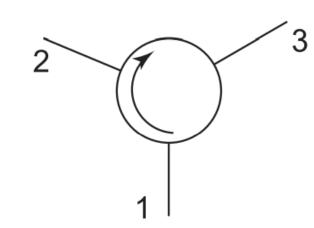
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Same insertion loss between ports (1,2), and (2,3) and (3,1)  $|S_{21}| = |S_{32}| = |S_{13}| = 0.89$ 

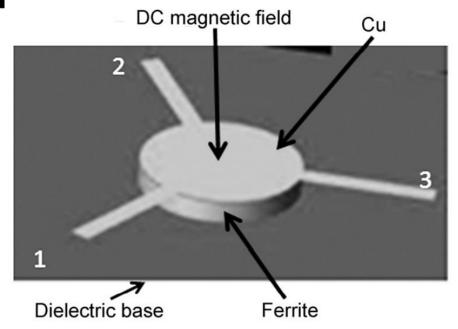


• 
$$VSWR = 1.5$$
, reflection coefficient  $|\Gamma| = \frac{S-1}{S+1} = \frac{1.5-1}{1.5+1} = 0.2 = |S_{11}| = |S_{22}| = |S_{33}|$ 



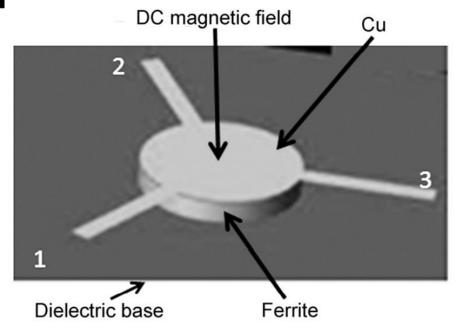
$$[S] = \begin{bmatrix} 0.2 & 0.032 & 0.89 \\ 0.89 & 0.2 & 0.032 \\ 0.032 & 0.89 & 0.2 \end{bmatrix}$$

- Remove top ground plane in stripline
- Basic design criteria:
   Selection of radius R of ferrite disc
   Calculation of radius R of magnet cylinder for the whole ferrite substrate



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$$R = \frac{1.84}{\omega_0 \sqrt{\varepsilon_0 \varepsilon_r \mu_0 \mu_{eff}}}$$

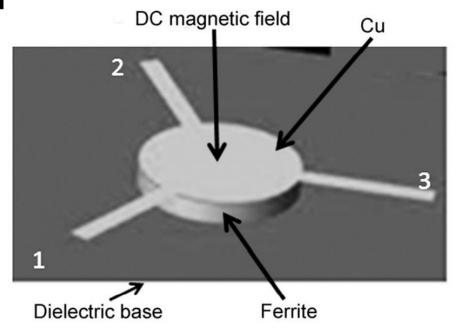


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 $\omega_0$  =Center angular frequency

 $\varepsilon_0$ ,  $\mu_0$ : Free space permittivity and permeability



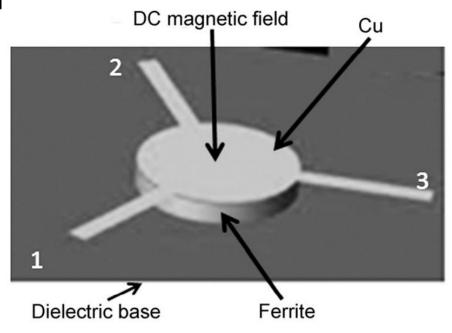
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$$\mu_{eff} = \frac{(\mu^2 - K^2)}{\mu}$$
 =scalar effective permeability



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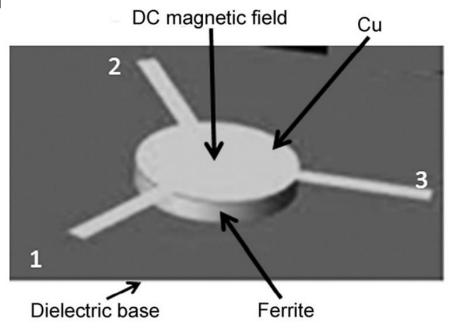
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$$\mu_{eff}=rac{(\mu^2-K^2)}{\mu}=$$
 scalar effective permeability  $\mu=1-rac{p\sigma}{1-\sigma^2}$   $K=rac{p}{1-\sigma^2}$ 

$$\mu = 1 - \frac{p\sigma}{1 - \sigma^2} \qquad K = \frac{p}{1 - \sigma^2}$$



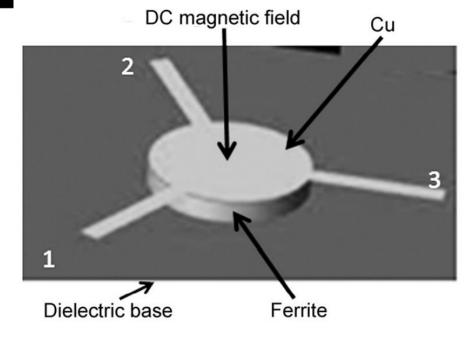
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 $\omega_0$  =Center angular frequency

 $\varepsilon_0$ ,  $\mu_0$ : Free space permittivity and permeability

$$\mu_{eff} = \frac{(\mu^2 - K^2)}{\mu}$$
 =scalar effective permeability  $\mu = 1 - \frac{p\sigma}{1 - \sigma^2}$   $K = \frac{p}{1 - \sigma^2}$ 



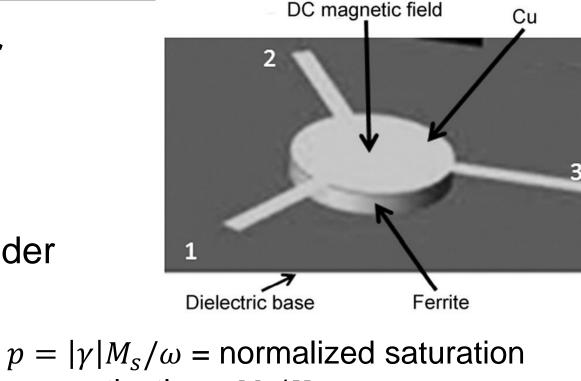
$$p = |\gamma| M_s/\omega$$
 = normalized saturation magnetization = $M_s/H_0$ 

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$$R = \frac{1.84}{\omega_0 \sqrt{\varepsilon_0 \varepsilon_r \mu_0 \mu_{eff}}}$$

 $\omega_0$  =Center angular frequency

 $\varepsilon_0$ ,  $\mu_0$ : Free space permittivity and permeability magnetic field=  $H_{dc}/H_0$  $\varepsilon_r$ : Relative permittivity of ferrite  $\mu_{eff}=\frac{(\mu^2-K^2)}{\mu}=$  scalar effective permeability  $\mu=1-\frac{p\sigma}{1-\sigma^2}$   $K=\frac{p}{1-\sigma^2}$ 



$$p = |\gamma| M_s/\omega = \text{normalized saturation}$$
  
magnetization  $=M_s/H_0$   
 $\sigma = |\gamma| H_0/\omega = \text{normalized biasing}$ 

- Remove top ground plane in stripline
- Basic design criteria: Selection of radius R of ferrite disc Calculation of radius R of magnet cylinder for the whole ferrite substrate

• 
$$R = \frac{1.84}{\omega_0 \sqrt{\varepsilon_0 \varepsilon_r \mu_0 \mu_{eff}}}$$

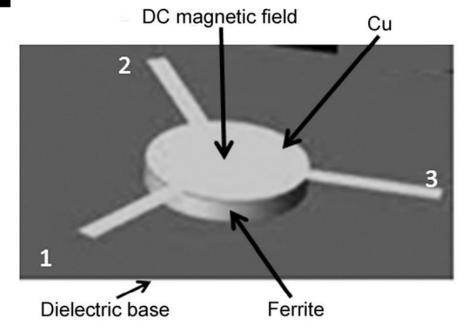
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 $\varepsilon_r$ : Relative permittivity of ferrite

$$\mu_{eff}=rac{(\mu^2-K^2)}{\mu}=$$
 scalar effective permeability resonance in infinite ferrite medium.  $\mu=1-rac{p\sigma}{1-\sigma^2}$   $K=rac{p}{1-\sigma^2}$ 

$$\mu = 1 - \frac{p\sigma}{1 - \sigma^2} \qquad K = \frac{p}{1 - \sigma^2}$$



 $p = |\gamma| M_s/\omega$  = normalized saturation magnetization = $M_s/H_0$ 

 $\sigma = |\gamma| H_0/\omega$ =normalized biasing

 $H_0 = \frac{\omega}{|\nu|}$  = field required for gyromagnetic

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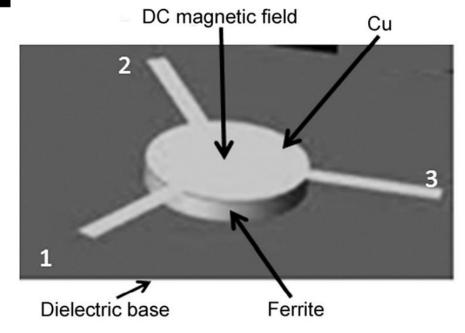
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$$\mu_{eff} = \frac{(\mu^2 - K^2)}{\mu}$$
 =scalar effective permeability

$$\mu = 1 - \frac{p\sigma}{1 - \sigma^2} \qquad K = \frac{p}{1 - \sigma^2}$$



 $p = |\gamma| M_s/\omega$  = normalized saturation magnetization = $M_s/H_0$ 

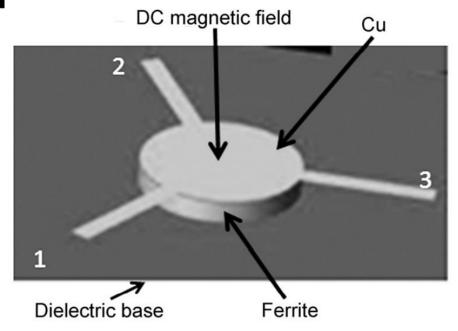
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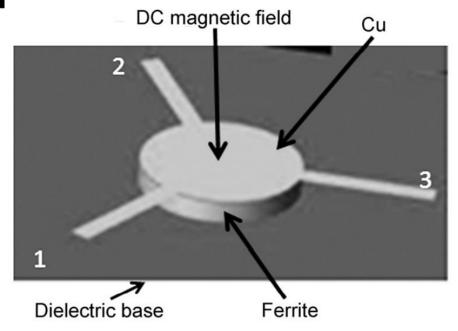
resonance in infinite ferrite medium.

Low magnetic loss: ferrite  $\frac{\gamma 4\pi M_S}{} = 0.6$ 

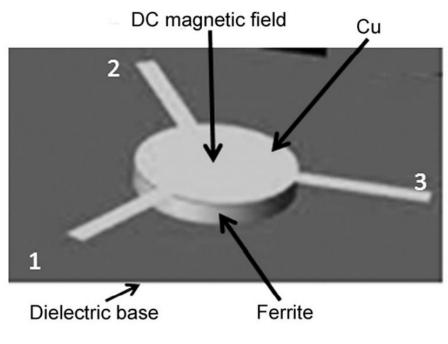
- Insertion loss between coupled ports:
  - 1) Copper loss of strip and ground plane
  - 2) Dielectric loss of input/output strips
  - 3) Magnetic loss of ferrite disc



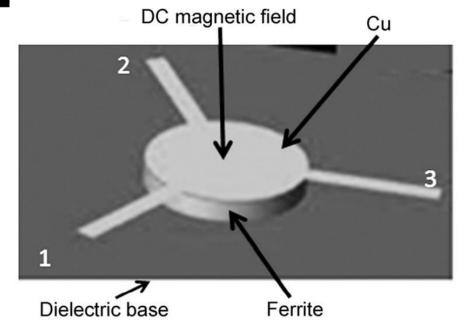
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- **YIG** (Yttrium Iron Garnet ) substrate of thickness h=0.055": Isolation>20dB, VSWR<1.2, Insertion loss IL<0.8dB, Power handling of 60W over frequency range of 8.5-9.9GHz

- Power handling capability of such device can be increased by
  - 1) Lowering the impedance or increasing intrinsic line width.
  - 2) Increasing substrate thickness h
  - 3) Decreasing  $4\pi M_S$  of the material by substituting Al ions in YIG material.

