

Mechanics of Machines Mechanical Vibration Module 6:

Tapan Kumar Mahanta, Ph.D. SMEC Chennai Campus







Mechanical vibration:

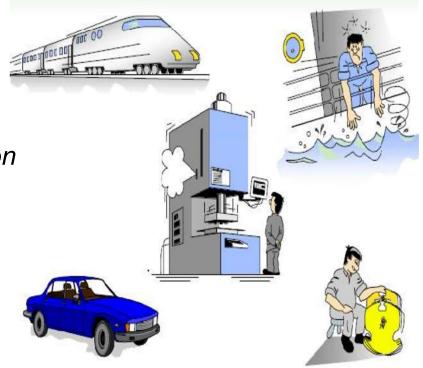
- Class Objective1: What is vibration?
- Class Objective2: Why vibration?
- Class objective3: Free vibration

Vibration:



- Vibrations are the oscillations of a structural system about the equilibrium position.
- Vibration system involves transfer of PE to KE, and KE to PE.

It is also an everyday phenomenon we meet on everyday life



Vibration:

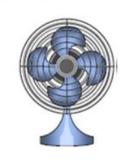


Useful Vibration





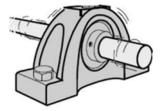
Harmful vibration



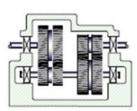
Noise



Destruction



Wear



Fatigue

Vibration definition:



- Mechanical vibration is the motion of a particle or body which oscillates about a position of equilibrium. Most vibrations in machines and structures are undesirable due to increased stresses and energy losses.
- Time interval required for a system to complete a full cycle of the motion is the period of the vibration.
- Number of cycles per unit time defines the frequency of the vibration.
- Maximum displacement of the system from the equilibrium position is the amplitude of the vibration.

Vibration definition:



- Free (or natural) vibrations: A vibration in which after the initial displacement, no external forces act and the motion is maintained by the internal elastic forces, is termed as free or natural vibration
- Forced vibration: These type of vibrations are caused when a periodic disturbing force is continuously applied to the body. The vibrations then has the same frequency as the applied force.
- Damping: It is the resistance to the motion of a vibrating body.
- Natural frequency: It is the frequency of free vibrations of a body vibrating of its own without the help of an external agency.

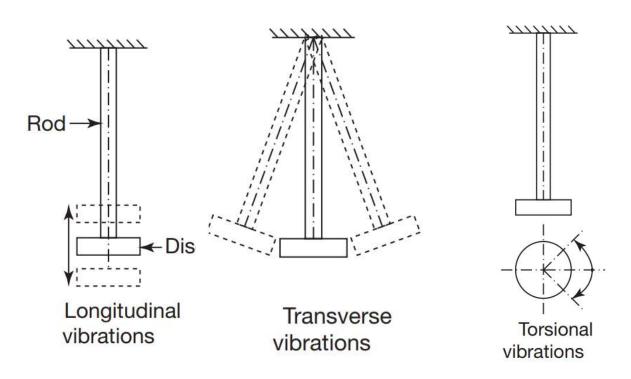
Vibration definition:



- Resonance: When the frequency of external excitation is equal to the natural frequency of a vibrating body.
- Degrees of freedom: The minimum number of independent coordinates required to specify the motion of a system.

Types of vibrations:

- Longitudinal vibrations
- Transverse vibrations
- Torsional vibrations



A vibrating system:

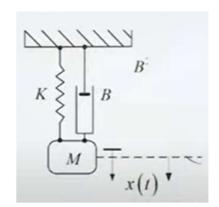


- 1. KE storing device (mass) or *Inertial elements*
- 2. PE storing device (spring) or Restoring elements
- 3. Friction (damper) or *Damping elements*
- 4. Unbalance force

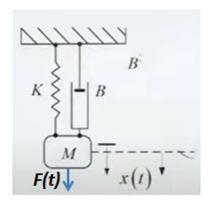
Free vibration system



Damped vibration system



Forced damped vibration system





Now the forces acting on the system are, applying D'Alembert's principle, we have

Upward force

$$=k(x+\delta_{st})$$

Downward force

$$= -m\ddot{x} + mg$$

For the equilibrium of the system, $-m\ddot{x} + mg = k(x + \delta_{st})$ $\therefore m\ddot{x} + kx = 0$

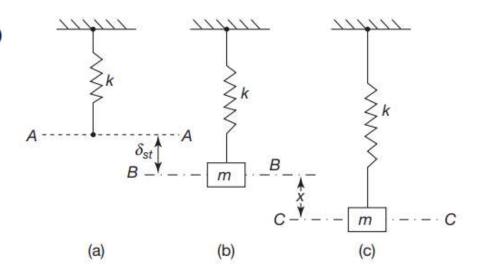
$$x(t) = A \sin \omega_n t + B \cos \omega_n t$$

$$\dot{x}(t) = \omega_n \left[A \cos \omega_n t - B \sin \omega_n t \right]$$

$$x(0) = x_o \quad \text{and} \quad \dot{x}(0) = v_o$$

$$x_o = B$$

$$v_o = \omega_n A$$



Stages in the extension of a spring

 $x(t) = X \sin \left(\omega_n t + \phi\right)$

$$x(t) = A \sin \omega_n t + B \cos \omega_n t$$

$$\dot{x}(t) = \omega_n \left[A \cos \omega_n t - B \sin \omega_n t \right]$$

$$x(0) = x_o \quad \text{and} \quad \dot{x}(0) = v_o$$

$$x_o = B$$

$$v_o = \omega_n A$$

$$A = \frac{v_o}{\omega_n}$$

$$x(t) = \left(\frac{v_o}{\omega_n} \right) \sin \omega_n t + x_o \cos \omega_n t$$

Stages in the extension of a spring



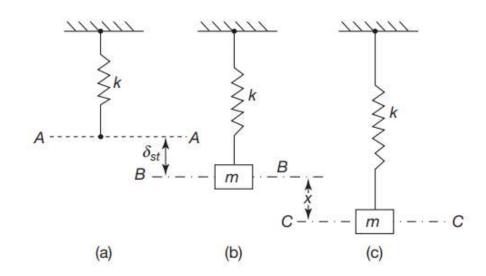
$$x(t) = X \sin (\omega_n t + \phi)$$

Velocity,
$$\dot{x}(t) = x \omega_n \cos(\omega_n t + \phi)$$

= $x \omega_n \sin\left[\frac{\pi}{2} + (\omega_n t + \phi)\right]$

Acceleration,
$$\ddot{x}(t) = -x \ \omega_n^2 \sin(\omega_n t + \phi)$$

= $x \ \omega_n^2 \sin\left[\pi + (\omega_n t + \phi)\right]$



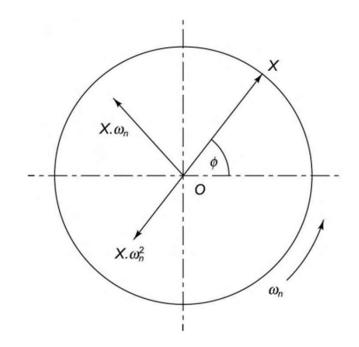
Stages in the extension of a spring



Acceleration,
$$\ddot{x}(t) = -x \omega_n^2 \sin(\omega_n t + \phi)$$

= $x \omega_n^2 \sin[\pi + (\omega_n t + \phi)]$

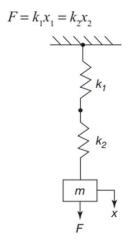
$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{g}{\delta_{st}}} \text{ rad/s}$$
 Time period, $T = \frac{2\pi}{\omega_n} = 2\pi \sqrt{\frac{m}{k}} \text{ s}$ Natural frequency, $f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}} \text{ Hz (Cycles/s)}$



Equivalent Stiffness of Springs:



Springs in series:



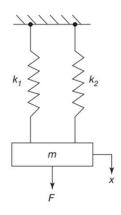
Total extension, $x = x_1 + x_2$

$$= F\left(\frac{1}{k_1} + \frac{1}{k_2}\right)$$

Equivalent stiffness, $k_e = \frac{F}{x} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}} = \frac{k_1 k_2}{k_1 + k_2}$

$$\frac{1}{k_e} = \frac{1}{k_1} + \frac{1}{k_2}$$

Springs in parallel:



$$F_1 = k_1 x$$
 and $F_2 = k_2 x$

$$F = F_1 + F_2$$
$$= (k_1 + k_2) x$$

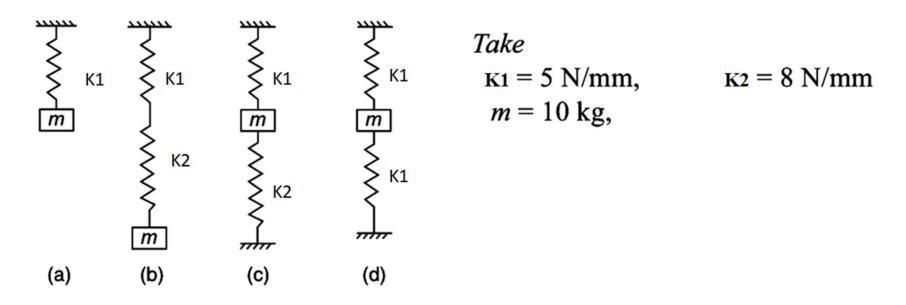
$$k_e = \frac{F}{x} = k_1 + k_2$$

Problem1:



Determine the equivalent spring stiffness and natural frequency of the following vibrating systems when

- (a) Mass is suspended to a spring
- (b) Mass is suspended at the bottom of the two springs in series.
- (c) Mass fixed in between two springs
- (d) Mass is fixed to the midpoint of a spring

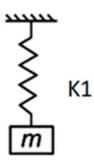




(a) Mass is suspended to a spring

$$f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$

= $\frac{1}{2\pi} \sqrt{\frac{5 \times 10^3}{10}} = 3.56 \text{ Hz}$

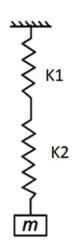


(b) Mass is suspended at the bottom of the two springs in series.

$$k_e = \frac{k_1 k_2}{k_1 + k_2}$$

$$f_n = \frac{1}{2\pi} \sqrt{\frac{\text{Keq}}{m}} = \frac{1}{2\pi} \sqrt{\frac{\text{K1 K2}}{(\text{K1+ K2})m}}$$

$$= \frac{1}{2\pi} \sqrt{\frac{(5 \times 10^3) \times (8 \times 10^3)}{(5+8) \times 10^3 \times 10}} = \underline{2.79 \text{ Hz}}$$





(c) Mass fixed in between two springs

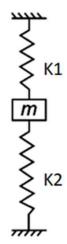
$$k_e = k_1 + k_2$$

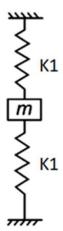
$$f_n = \frac{1}{2\pi} \sqrt{\frac{\text{Keq}}{m}} = \frac{1}{2\pi} \sqrt{\frac{13 \times 10^3}{10}} = \underline{5.74 \text{ Hz}}$$



Stiffness of spring on each side =
$$\frac{K1}{1/2} = 2 K1$$

$$f_n = \frac{1}{2\pi} \sqrt{\frac{4\text{K1}}{m}} = \frac{1}{2\pi} \sqrt{\frac{4 \times 5 \times 10^3}{10}} = \underline{7.12 \text{ Hz}}$$





Damped vibration system:



$$m\ddot{x} + c\dot{x} + kx = 0$$

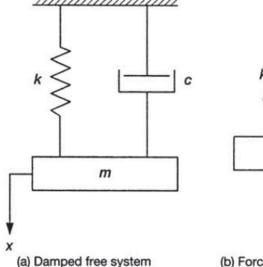
$$\ddot{x} + \left(\frac{c}{m}\right)\dot{x} + \left(\frac{k}{m}\right)x = 0$$

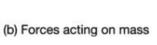
$$x = e^{\alpha t}$$

$$\alpha^2 + \frac{c}{m}\alpha + \frac{K}{m} = 0$$

$$\alpha_{1,2} = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \left(\frac{\kappa}{m}\right)}$$

$$x = A e^{\alpha_1 t} + B e^{\alpha_2 t}$$





mx

For critical damping, the term under the square root is zero



$$\alpha_{1,2} = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \left(\frac{\kappa}{m}\right)}$$

For critical damping, the term under the square root is zero, the damping coefficient is called the critical damping coefficient, $C_{c.}$

$$\left(\frac{c_c}{2m}\right)^2 - \frac{k}{m} = 0$$

$$\frac{c_c}{2m} = \left(\frac{k}{m}\right)^{1/2} = \omega_n$$

$$c_c = 2m\omega_n = 2(km)^{1/2}$$

$$c_c = 2m\omega_n = 2(km)^{1/2}$$

damping ratio,
$$\zeta = \frac{c}{c_c} = \frac{\text{damping coefficient}}{\text{critical damping coefficient}}$$



$$\ddot{x} + \left(\frac{c}{m}\right)\dot{x} + \left(\frac{k}{m}\right)x = 0$$

$$\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = 0$$

$$\alpha_{1,2} = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \left(\frac{K}{m}\right)}$$

$$\alpha_{1.2} = -\zeta \omega_n \pm \sqrt{\zeta^2 \omega_n^2 - \omega_n^2} = (-\zeta \pm \sqrt{\zeta^2 - 1})\omega_n$$

Over damped system ($\zeta > 1$)

Criticality damped system ($\zeta = 1$)

 $\frac{c}{2m} = \left(\frac{c}{c_c}\right) \left(\frac{c_c}{2m}\right) = \zeta \omega_n$

Under damped system ($\zeta < 1$)



Over damped system ($\zeta > 1$)

The roots of the auxiliary equation are real.

$$\alpha_{1.2} = (-\zeta \pm \sqrt{\zeta^2 - 1})\omega_n$$

Therefore, the solution is $x = Ae^{\alpha_1 t} + Be^{\alpha_2 t}$

$$x = Ae^{(-\zeta + \sqrt{\zeta^2 - 1})\omega_n t} + Be^{(-\zeta - \sqrt{\zeta^2 - 1})\omega_n t}$$

Constants A and B can be determined from the initial conditions. This is the equation of an aperiodic motion, i.e., the system cannot vibrate due to over-damping. The magnitude of the resultant displacement approaches zero with time.

Under damped system ($\zeta < 1$)



The roots of the auxiliary equation are imaginary. $\alpha_{1,2} = (-\zeta \pm i\sqrt{1-\zeta^2})\omega_n$

$$x = Ae^{(-\zeta + i\sqrt{1-\zeta^2})\omega_n t} + Be^{(-\zeta - i\sqrt{1-\zeta^2})\omega_n t}$$

$$= e^{-\zeta\omega_n t} \left[Ae^{(i\sqrt{1-\zeta^2})\omega_n t} + Be^{(-i\sqrt{1-\zeta^2})\omega_n t} \right]$$
Put $\sqrt{1-\zeta^2}\omega_n = \omega_d$

$$x = e^{-\zeta\omega_n t} [Ae^{i\omega_d t} + Be^{-i\omega_d t}]$$

$$= e^{-\zeta\omega_n t} [A(\cos\omega_d t + i\sin\omega_d t) + B(\cos\omega_d t - i\sin\omega_d t)]$$

$$= e^{-\zeta\omega_n t} [A(\cos\omega_d t + i\sin\omega_d t) + B(\cos\omega_d t - i\sin\omega_d t)]$$
where
$$= e^{-\zeta\omega_n t} [A(\cos\omega_d t + i(A - B)\sin\omega_d t)]$$

$$= e^{-\zeta\omega_n t} [C\cos\omega_d t + D\sin\omega_d t]$$

$$x = e^{-\zeta\omega_n t} (X\sin\varphi\cos\omega_d t + X\cos\varphi\sin\omega_d t)$$

$$= Xe^{-\zeta\omega_n t} \sin(\omega_d t + \varphi)$$

$$i(A - B) = X\cos\varphi$$

$$x = Xe^{-\zeta\omega_n t}\sin(\omega_d t + \varphi)$$



$$x = Xe^{-\zeta\omega_n t}\sin(\omega_d t + \varphi)$$

Constants X and φ are to be determined from initial conditions. This equation indicates that the system oscillates with frequency $\omega_d (= \sqrt{1 - \zeta^2} \omega_n)$. As ζ is less than 1, ω_d is always less than ω_n .

- X, which is constant
- $e^{-\zeta \omega_n t}$, which decreases with time and finally $e^{-\infty} = 0$
- $\sin(\omega_d t + \varphi)$ which represents a repetition of motion Thus, the resultant motion is oscillatory with decreasing amplitudes having a frequency of ω_d . Ultimately, the motion dies down with time. Also,

linear frequency,
$$f_d = \frac{\omega_d}{2\pi}$$

time period, $T_d = \frac{\omega_d}{2\pi}$

VIVIT

let X_0 = displacement at the start of motion when t = 0 X_1 = displacement at the end of first oscillation when $t = T_d$

$$= Xe^{-\zeta\omega_n T_d} \sin(\omega_d T_d + \varphi)$$

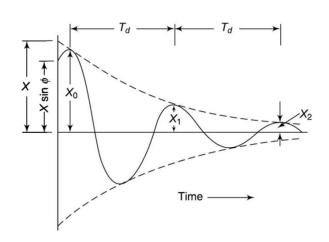
$$= Xe^{-\zeta\omega_n T_d} \sin\left(\omega_d \frac{2\pi}{\omega_d} + \varphi\right)$$

$$= Xe^{-\zeta\omega_n T_d} \sin\varphi$$

 X_2 = displacement at the end of second oscillation = $Xe^{-\zeta\omega_n\times 2T_d}\sin\varphi$

$$X_{n+1} = Xe^{-\zeta\omega_n \times (n+1)T_d} \sin \varphi$$

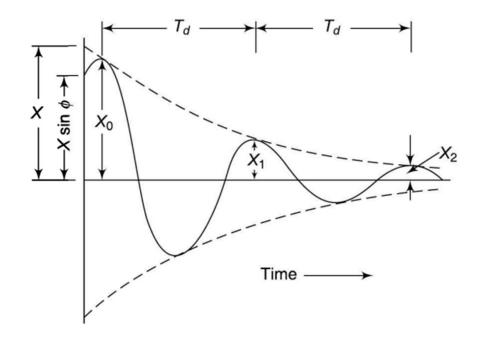
$$\frac{X_n}{X_{n+1}} = e^{\zeta \omega_n T_d} = \frac{X_0}{X_1} = \frac{X_1}{X_2} = \frac{X_2}{X_3} = \dots$$





$$\frac{X_n}{X_{n+1}} = e^{\zeta \omega_n T_d} = \frac{X_0}{X_1} = \frac{X_1}{X_2} = \frac{X_2}{X_3} = \dots$$

ratio of amplitudes of two successive oscillations is constant



Criticality damped system ($\zeta = 1$)



$$\alpha_{1.2} = (-\zeta \pm \sqrt{\zeta^2 - 1})\omega_n$$

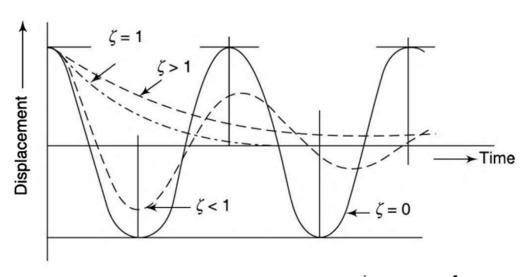
$$x = A e^{\alpha_1 t} + B e^{\alpha_2 t}$$

The roots of the auxiliary equation are equal, each being equal to $-\omega_n$ and the solution is $x = (A + Bt) e^{-\omega_n t}$

Since $e^-\omega_n^t$ approaches zero as $t\to\infty$, the motion is aperiodic. The displacement will be approaching to zero with time.

Comparison:





- (i) An undamped system ($\zeta = 0$) vibrates at its frequency which depends upon the static deflection under the weight of its mass ($\omega_n = \sqrt{g/\Delta}$).
- (ii) When the system is underdamped ($\zeta < 1$), the frequency of the system decreases to $\omega_d (= \sqrt{1 \zeta^2 \omega_n})$ and the time period increases to $T_d = 2 \pi/\omega_d$. The amplitudes of the vibrations decrease with time, the ratio of successive amplitudes being constant. The vibrations die down with time.
- (iii) At critical damping, $\zeta = 1$, $\omega_d = 0$ and $T_d = \infty$. The system does not vibrate and the mass m moves back slowly to the equilibrium position.
- (iv) For an overdamped system, $\zeta > 1$, the system behaves in the same manner as for critical damping.
- (v) ζ is the ratio of the existing damping in a system to that required for critical damping, i.e., $\zeta = c/c_c$.

Logarithmic Decrement



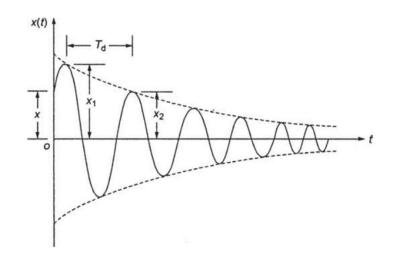
ratio of two successive oscillations is constant in an underdamped system.

Natural logarithm of this ratio is called logarithmic decrement and is denoted by $\delta = \ln \left(\frac{X_n}{X_{n+1}} \right)$

$$\delta = \ln e^{(\zeta \omega_n T_d)} = \zeta \omega_n T_d$$

$$\delta = \zeta \omega_n \frac{2\pi}{\omega_d} = \zeta \omega_n \frac{2\pi}{\sqrt{1 - \zeta^2} \omega_n} = \frac{2\pi \zeta}{\sqrt{1 - \zeta^2}}$$

$$\delta = \frac{2\pi \zeta}{\sqrt{1 - \zeta^2}}$$



$$\frac{X_n}{X_{n+1}} = e^{\zeta \omega_n T_d} = \frac{X_0}{X_1} = \frac{X_1}{X_2} = \frac{X_2}{X_3} = \dots$$

Problem 1:



A vibrating system consists of a mass of 50 kg, a spring with a stiffness of 30 kN/m and a damper. The damping provided is only 20% of the critical value.

Determine the

- (i) damping factor
- (ii) critical damping coefficient
- (iii) natural frequency of damped vibrations
- (iv) logarithmic decrement
- (v) ratio of two consecutive amplitudes



$$m = 50 \text{ kg}$$
 $s = 30 000 \text{ N/m}$ $c = 0.2 c_c$

(i)
$$\zeta = \frac{c}{c_c} = 0.2$$

(ii)
$$c_c = 2\sqrt{sm} = 2\sqrt{30\ 000 \times 50} = 2450\ \text{N/m/s}$$

= 2.45 N/mm/s

(iii)
$$\omega_d = \sqrt{1-\zeta^2}\omega_n$$

where

$$\omega_n = \sqrt{\frac{s}{m}} = \sqrt{\frac{30\ 000}{50}} = 24.5\ \text{rad/s}$$

$$\omega_d = \sqrt{1 - (0.2)^2} \times 24.5 = 24 \text{ rad/s}$$

(iv)
$$\delta = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}} = \frac{2\pi\times0.2}{\sqrt{1-(0.2)^2}} = \underline{1.28}$$

(v)
$$\frac{X_n}{X_{n+1}} = e^{\delta} = e^{1.28} = \underline{3.6}$$

Problem 2:



Determine the time in which the mass in a damped vibrating system would settle down to 1/50 th of its initial deflection for the following data: m = 200 kg $\zeta = 0.22$ Also, find the number of oscillations completed to reach this value of deflection.

$$\frac{X_0}{X_N} = e^{\zeta \omega_n N T_d}$$

$$\omega_n = \sqrt{\frac{s}{m}} = \sqrt{\frac{40 \times 10^3}{200}} = 14.14 \text{ rad/s}$$

$$50 = e^{0.22 \times 14.14 NT_d}$$

. 50 – e

or

Total time $NT_d = \underline{1.26 \text{ s}}$

$$T_d = \frac{2\pi}{\sqrt{1 - \zeta^2 \omega_n}}$$

$$= \frac{2\pi}{(\sqrt{1 - (0.22)^2}) \times 14.14} = 0.455 \text{ s}$$

Number of oscillations completed = $\frac{1.26}{0.455} = \frac{2.76}{0.455}$

Problem 3:



In a single-degree damped vibrating system, a suspended mass of 8 kg makes 30 oscillations in 18 seconds. The amplitude decreases to 0.25 of the initial value after 5 oscillations. Determine the

- (i) stiffness of the spring
- (ii) logarithmic decrement
- (iii) damping factor, and
- (iv) damping coefficient

$$m = 8 \text{ kg}, N = 30, t = 18\text{s}$$

 $f_n = \frac{30}{18} = 1.67 \text{ Hz}$
 $\omega_n = 2\pi f_n = 2\pi \times 1.67 = 10.47 \text{ rad/s}$

(i)
$$\omega_n = \sqrt{\frac{s}{m}}$$

$$10.47 = \sqrt{\frac{s}{8}}$$

$$\therefore s = 877 \text{ N/m}$$

or

0.877 N/mm

(ii)
$$\frac{X_0}{X_5} = \frac{X_0}{X_1} \times \frac{X_1}{X_2} \times \frac{X_2}{X_3} \times \frac{X_3}{X_4} \times \frac{X_4}{X_5}$$
$$= \left(\frac{X_0}{X_1}\right)^5 \cdots \left(\frac{X_0}{X_1} = \frac{X_1}{X_2} = \frac{X_2}{X_3} = \frac{X_3}{X_4} = \frac{X_4}{X_5}\right)$$

$$\therefore \left(\frac{X_0}{X_1}\right) = \left(\frac{X_0}{X_5}\right)^{1/5} = \left(\frac{1}{0.25}\right)^{1/5} = 1.32$$

$$\delta = \ln\left(\frac{X_0}{X_5}\right) = \ln 1.32 = 0.278$$



(iii)
$$\frac{2\pi\zeta}{\sqrt{1-\zeta^2}} = 0.278$$
or
$$\sqrt{1-\zeta^2} = 22.6\zeta$$

$$1-\zeta^2 = 510.82\zeta^2$$

$$\zeta^2 = 0.00195$$

$$\zeta = 0.0442$$
(iv) $c = 2 m \omega_n \zeta$

= 7.4 N/m/s

 $= 2 \times 8 \times 10.47 \times 0.0442$

Problem 4:



The measurements on a mechanical vibrating system show that it has a mass of 8 kg and that the springs can be combined to give an equivalent spring of stiffness 5.4 N/mm. If the vibrating system have a dashpot attached which exerts a force of 40 N when the mass has a velocity of 1 m/s, find: 1. critical damping coefficient, 2. damping factor, 3. logarithmic decrement, and 4. ratio of two consecutive amplitudes.

1. critical damping coefficient:



$$c_c = 2m.\omega_n = 2 \times 8 \sqrt{\frac{5400}{8}} = 416 \text{ N/m/s}$$

2. damping factor:

$$\zeta = \frac{c}{c_c} = \frac{40}{416} = 0.096$$

3. logarithmic decrement:

$$\delta = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}} = 0.6$$

4. ratio of two consecutive amplitudes.

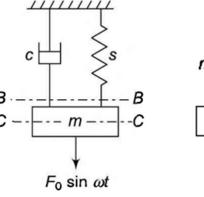
$$\delta = \log_e \left[\frac{x_n}{x_{n+1}} \right]$$
 $\frac{x_n}{x_{n+1}} = e^{\delta} = (2.7)^{0.6} = 1.82$

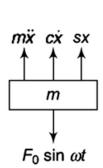
Forced damped Vibrations:



$$m\ddot{x} + c\dot{x} + sx - F_0 \sin\omega t = 0$$

$$m\ddot{x} + c\dot{x} + sx = F_0 \sin\omega t$$





Complete solution of this equation consists of two parts, the complementary function (CF) and the particular integral (PI).

$$CF = Xe^{-\zeta\omega_n t} \sin(\omega_d t + \varphi_1)$$

To obtain the PI, let

$$\frac{c}{m} = a, \frac{s}{m} = b, \text{ and } \frac{F_0}{m} = d$$

Then, using the operator D, the equation becomes

$$(D^2 + aD + b) x = d \sin \omega t$$



$$PI = \frac{d \sin \omega t}{D^2 + aD + b}$$

$$= \frac{d \sin \omega t}{-\omega^2 + aD + b}$$

$$= \frac{1}{(b - \omega^2) + aD} \times \frac{(b - \omega^2) - aD}{(b - \omega^2) - aD} d \sin \omega t$$

$$= d \left[\frac{\sin \omega t (b - \omega^2) - aD \sin \omega t}{(b - \omega^2)^2 - a^2 D^2} \right]$$

$$= d \left[\frac{\sin \omega t (b - \omega^2) - a\omega \cos \omega t}{(b - \omega^2)^2 + (a\omega)^2} \right]$$

Take $(b - \omega^2) = R \cos \varphi$ and $a \omega = R \sin \varphi$ Constants R and φ are given by

$$R = \sqrt{(b - \omega^2)^2 + (a\omega)^2} \quad \text{and} \quad \varphi = \tan^{-1} \frac{a}{b - \omega^2}$$

$$PI = \frac{dR(\sin \omega t \cos \varphi - \cos \omega t \sin \varphi)}{(b - \omega^2)^2 + (a\omega)^2}$$

$$= \frac{d\sqrt{(b - \omega^2)^2 + (a\omega)^2}}{(b - \omega^2) + (a\omega)^2} \sin(\omega t - \varphi)$$

$$= \frac{d}{\sqrt{(b - \omega^2)^2 + (a\omega)^2}} \sin(\omega t - \varphi)$$

$$= \frac{F_0 / m}{\sqrt{\left(\frac{s}{m} - \omega^2\right)^2 + \left(\frac{c}{m}\omega\right)^2}} \sin(\omega t - \varphi)$$

$$= \frac{F_0}{\sqrt{(s - m\omega^2)^2 + (c\omega)^2}} \sin(\omega t - \varphi)$$



$$x = CF + PI$$

$$Xe^{-\zeta\omega_n t} \sin(\omega_d t - \varphi_1) + \frac{F_0}{\sqrt{(s - m\omega^2)^2 + (c\omega)^2}} \sin(\omega t - \varphi)$$



