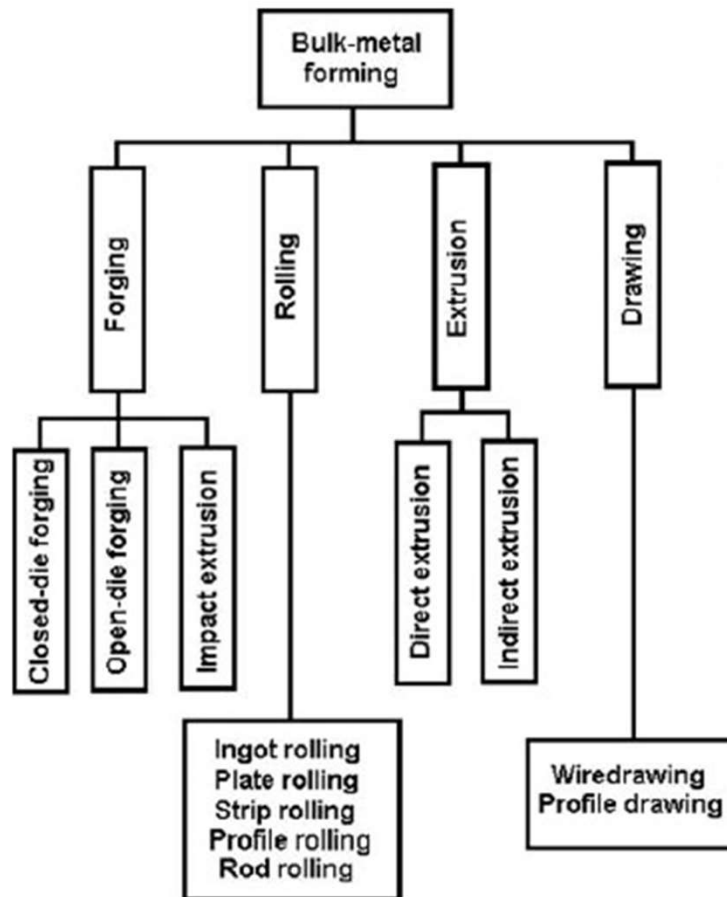




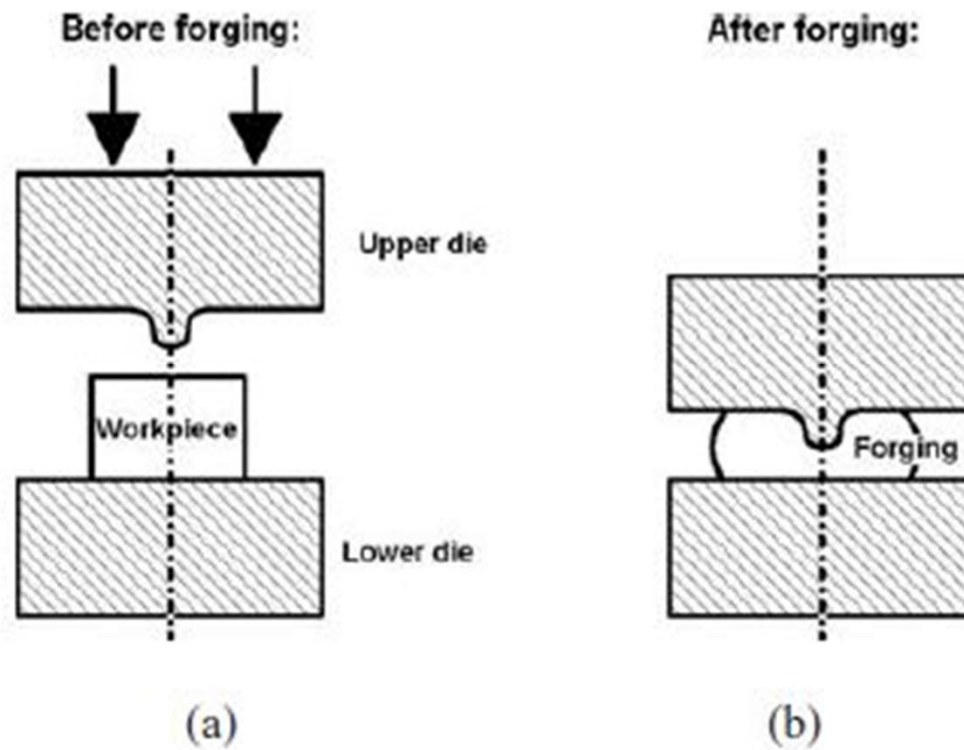
Tutorial 2

Forging

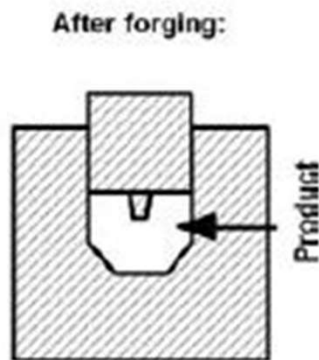
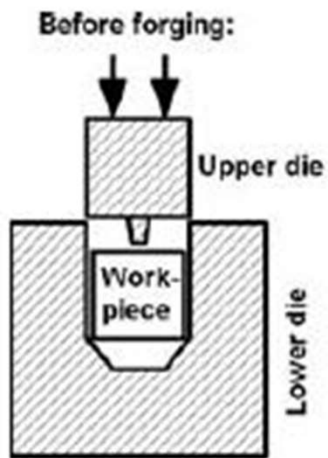
TYPES OF FORGING



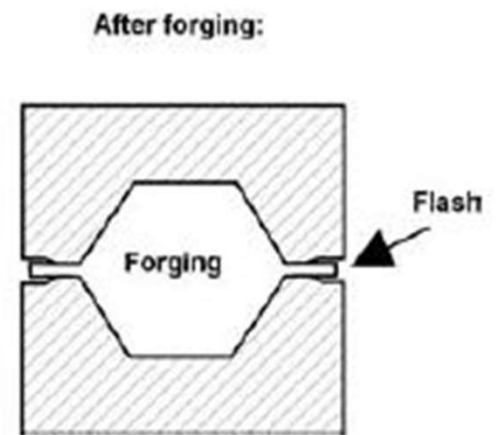
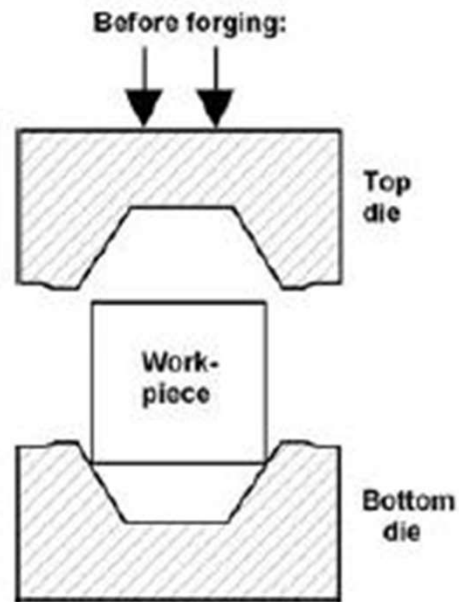
OPEN - DIE FORGING



CLOSED - DIE FORGING

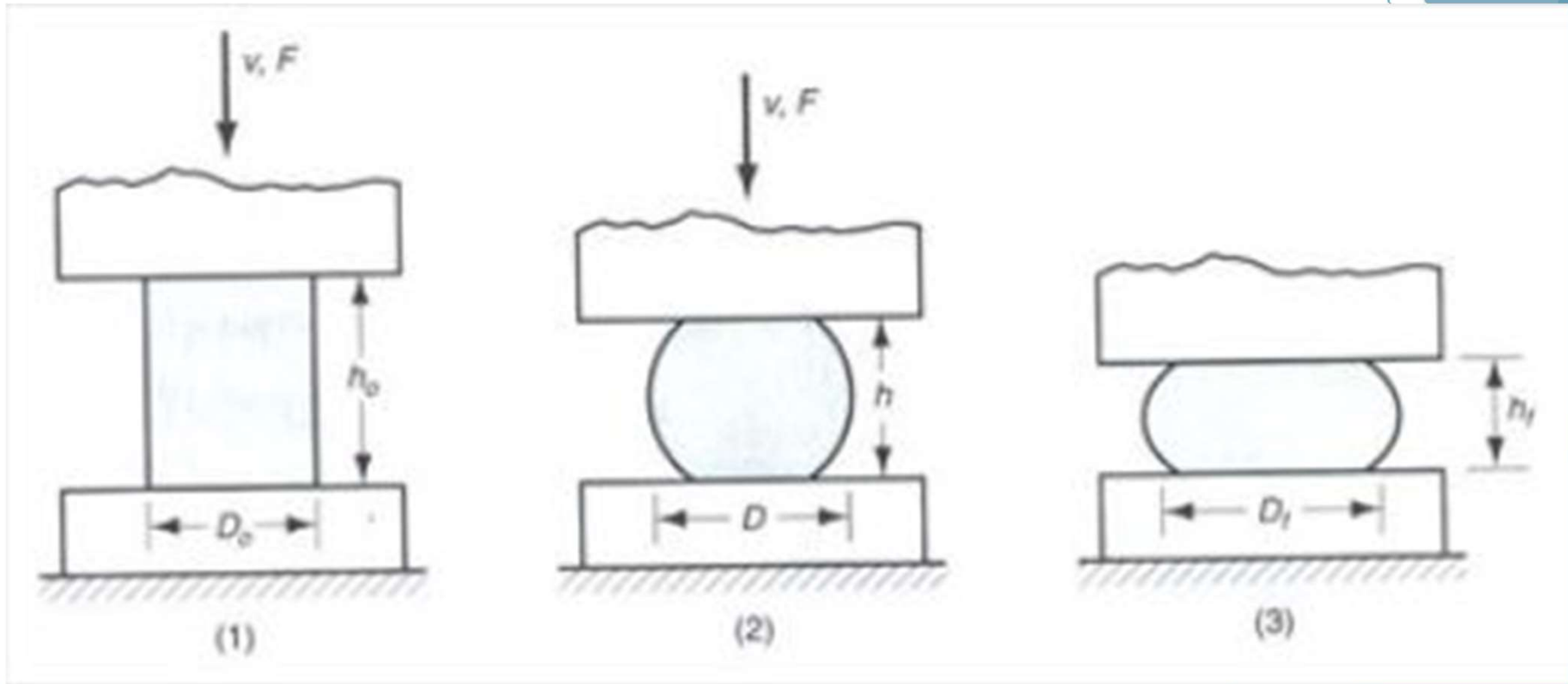


(a)



(b)

CASE 1: UPSET FORGING OF CYLINDRICAL BILLET



initial height, h_0

final deformed height, h_f

true strain, $\epsilon = \ln\left(\frac{h_0}{h_f}\right)$

Forging force, $F = YA$

Here, by volume constancy,

$$A \cdot h = A_0 h_0$$

$$\Rightarrow A = \frac{A_0 h_0}{h}$$

Let γ be flow stress,

average flow stress,

$$\bar{\gamma} = \frac{k \epsilon^n}{n+1}$$

where,

k - strengthening factor

n - strain-hardening exponent

$$\Rightarrow \text{Forging Force, } F = \bar{\gamma} \cdot A$$

Practical case includes
assumption of barreling.

∴ for non-homogenous upsetting,

$$F = k_f \bar{Y} A,$$

$$\text{where, } k_f = 1 + \frac{0.4 \mu d}{h},$$

k_f - forging shape factor

PROBLEM 1

Cold upset forging of a cylindrical billet of initial height 60 mm and initial diameter 30 mm, results in a final reduced height of 40 mm. The material of the billet has flow stress given by the expression $= 300 \varepsilon^{0.2}$ MPa. The coefficient of friction between the billet and die surfaces can be assumed to be 0.1. What is the forging force required at the reduced height?

Given :

$$h_o = 60 \text{ mm}$$

$$d_o = 30 \text{ mm}$$

$$h_f = 40 \text{ mm}$$

$$Y = 300 \epsilon^{0.2} \text{ MPa} ; k = 300, n = 0.2$$

$$\mu = 0.1$$

$$F = k_f \bar{Y} A$$

(i) Finding A_f

$$A_f = \frac{A_o h_o}{h_f}$$

$$= \frac{\frac{\pi}{4} d_o^2 h_o}{h_f}$$

$$= \frac{\frac{\pi}{4} (30)^2 (60)}{40}$$

$$= 1060.29 \text{ mm}^2$$

$$A_f = \frac{\pi}{4} d_f^2$$

$$\begin{aligned} d_f &= \left(\frac{4}{\pi} A_f \right)^{1/2} \\ &= \left[\frac{4}{\pi} \times 1060.29 \right]^{1/2} \\ &= 36.74 \text{ mm} \end{aligned}$$

ii) Finding \bar{Y}

$$\bar{Y} = \frac{k \epsilon^n}{n+1} = \frac{Y}{n+1}$$

$$\begin{aligned} \epsilon &= \ln \left[\frac{h_0}{h_f} \right] \\ &= \ln \left[\frac{60}{40} \right] \\ &= 0.405 \end{aligned}$$

$$\bar{Y} = \frac{300 (0.405)^{0.2}}{0.2 + 1}$$

$$= 208.65 \text{ MPa}$$

iii) Finding k_f

$$k_f = 1 + \frac{0.4 \mu d_f}{h_f}$$

$$= 1 + \frac{(0.4)(0.1)(36.74)}{40}$$

$$= 1.037$$

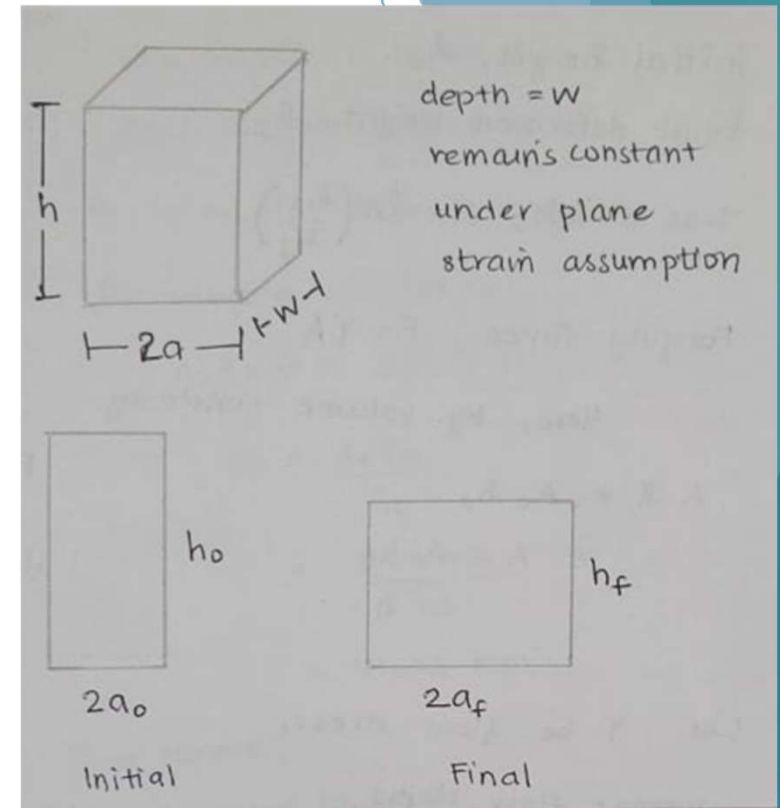
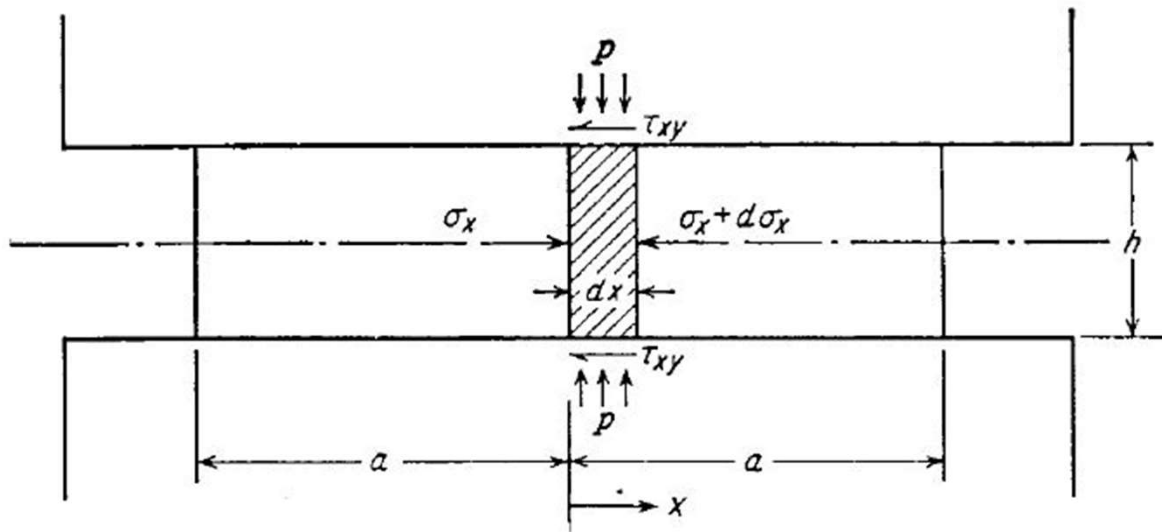
$$\Rightarrow F = k_f \bar{Y} A_f$$

$$= 1.037 \times 208.65 \times 1060.29$$

$$= 229415. \text{ N}$$

$$= 229.42 \text{ kN}$$

CASE 2: UPSET FORGING OF RECTANGULAR BILLET



Stresses acting on a
plate forged in plane strain,

$$\frac{d\sigma_x}{dx} = -\frac{2\tau_{xy}}{h}$$

von-Mises yield criterion
for plane strain condition:

$$\sigma_1 - \sigma_3 = \frac{2}{\sqrt{3}} \bar{\gamma} = \bar{\gamma}$$

$$\text{Here, } \sigma_1 - \sigma_3 = \bar{\gamma} = p - \sigma_x$$

$\bar{\gamma}$ doesn't vary w.r.t x .

$$\Rightarrow \frac{dp}{dx} = \frac{d\sigma_x}{dx}$$

$$\Rightarrow \frac{dp}{dx} = -\frac{2\tau_{xy}}{h}$$

By Coulumb's law of sliding friction,

$$\tau_{xy} = \mu p$$

$$\Rightarrow \frac{dp}{p} = -\frac{2\mu}{h} dx$$

Integrating on both sides,
using first two terms of
expansion series to resolve,

$$P = \bar{Y} \left[1 + \frac{2\mu(a-x)}{h} \right]$$

Mean Forging pressure,

$$\bar{P} = \int_0^a p \frac{dx}{a}$$

$$\bar{P} = \frac{\bar{Y}}{\frac{2\mu a}{h}} \left(e^{\frac{2\mu a}{h}} - 1 \right)$$

Total Forging Load,

$$\begin{aligned} F &= \bar{P} A \\ &= \bar{P} (2a) w \end{aligned}$$

PROBLEM 2

A rectangular block of height 40 mm, width 100 mm and depth 30 mm is subjected to upset forging under sliding friction condition, with a friction coefficient of 0.2. The material of the billet has flow stress expressed as: $Y = 300 e^{0.2}$. Calculate the forging load required at the height reduction of 30%, assuming plane strain compression.

Given:

$$h_o = 40 \text{ mm}$$

$$2a_o = 100 \text{ mm} \Rightarrow a_o = 50 \text{ mm}$$

$$W = 30 \text{ mm} = \text{depth}$$

30% height reduction.

$$\Rightarrow h_f = (1 - 0.3) h_o = 28 \text{ mm}$$

By volume constancy,

$$2a_o h_o W = 2a_f h_f W$$

$$\Rightarrow a_f = \frac{a_o h_o}{h_f}$$

$$= \frac{50 \times 40}{28}$$

$$= 71.43 \text{ mm}$$

True strain,

$$\epsilon = \ln \left(\frac{h_0}{h_f} \right).$$

$$= \ln \left(\frac{40}{28} \right)$$

$$= 0.357$$

Flow stress, $\bar{Y} = 300 \epsilon^{0.2}$

$$\Rightarrow K = 300, n = 0.2$$

$$\bar{Y} = \frac{K \epsilon^n}{n+1} = 203.4 \text{ MPa}$$

$$\frac{2\mu a_f}{h_f} = \frac{2 \times 0.2 \times 71.43}{28} = 1.02$$

$$\bar{P} = \frac{\bar{Y}}{\frac{2\mu a_f}{h_f}} (e^{\frac{2\mu a_f}{h_f}} - 1)$$

$$= \frac{203.4}{1.02} (e^{1.02} - 1)$$

$$= 353.59 \text{ MPa}$$

Total forging Load,

$$F = \bar{P} (2a) w$$

$$= 353.59 \times (2 \times 71.43) \times 30$$

$$= 1515.42 \text{ kN}$$



THANK YOU!