# Lecture 5: Experiment 4 EE380 (Control Systems)

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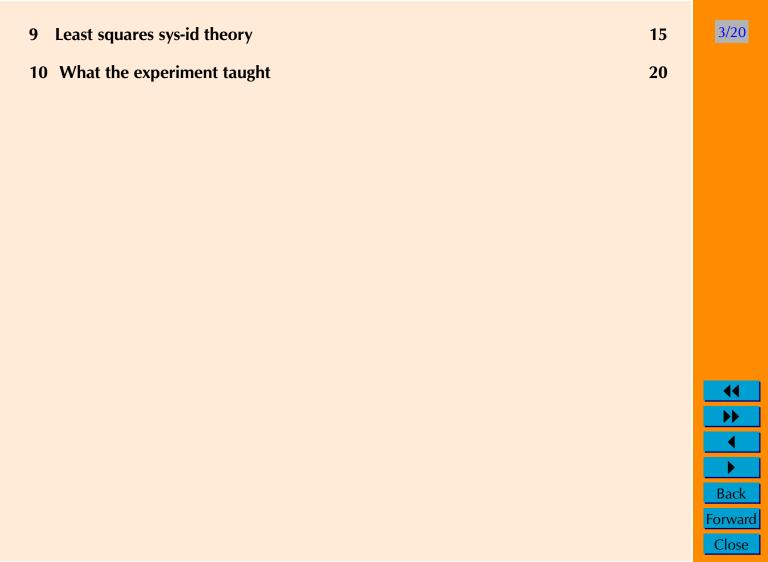
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### **Announcements**

- Before doing an experiment, download latest versions of supporting documents from Brihaspati.
- Latest version of program listings are on Brihaspati.
- Turn off power supply to board when not programming dsPIC or taking readings.
- After completion of experiment
  - Shut down PC, FG, PS.
  - Remove PICkit 2 from dsPIC board.







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Procedure of Exp.4

Part I

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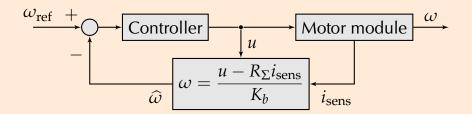
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# Outline of the experiment

Feedback of  $\omega$  assumed absent. Want  $\omega$  to track  $\omega_{\text{ref}}$ . Steps:

- Obtain estimate  $\widehat{\omega}$  of  $\omega$  using u and i.
- Use feedback of  $\widehat{\omega}$  to track  $\omega_{\text{ref}}$  with controller from Exp.1.



- Repeat control using feedback of  $\omega$  with controller from Exp.1.
- Is  $\widehat{\omega}$  an adequate replacement for  $\omega$ ?







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# Tasks common to all 6 experiments

#### **Simulation**

- Perform PC-based simulation of CL system using GNU Octave.
- Perform PC-based simulation of digital control of a continuous-time system using GNU Octave.

#### Realization on hardware

- Utilize the various components of an integrated development environment (IDE): editor, compiler, linker, debugger, and programmer to program a  $\mu$ C.
- Program controller using C language into  $\mu$ C.
- Monitoring: read data into PC from  $\mu$ C using UART modules.

#### **Analysis**

• Compare actual performance with predicted performance.







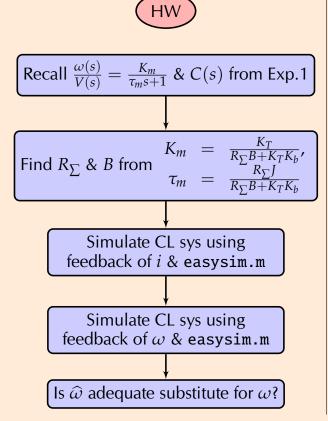
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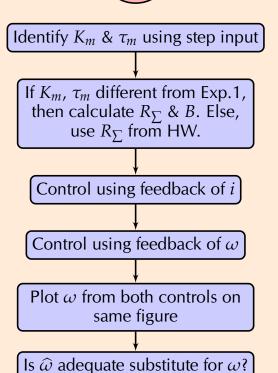
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### Homework (HW) vs. Lab work (LW)

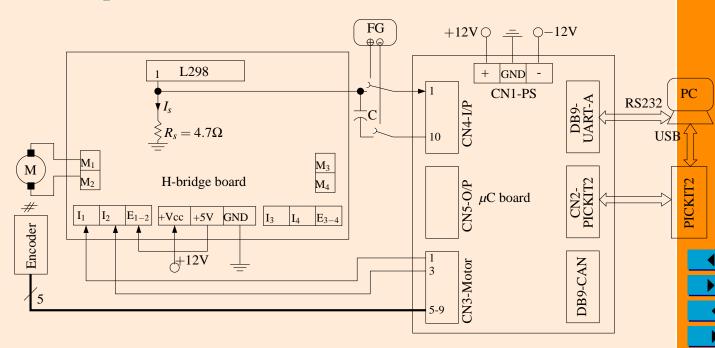




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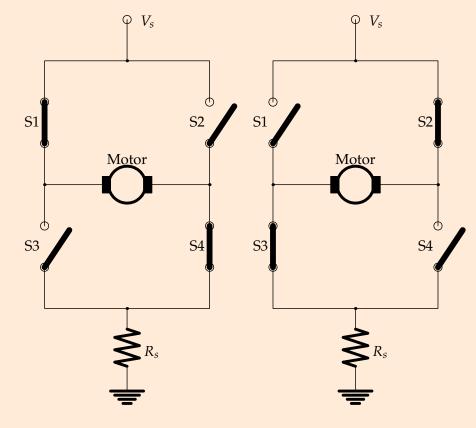
### Hardware connections

#### The setup



Pin 1 of L298 is connected to Pin 1 of CN4-I/P of  $\mu$ C board.

#### Where $R_s$ is in the H-bridge



Armature resistance includes all the resistance in the path of the armature:  $R_H$  (sum of resistance of S1 & S2 or S3 & S4, whichever pair is conducting),  $R_m$  (resistance of motor's armature), and  $R_s$ .

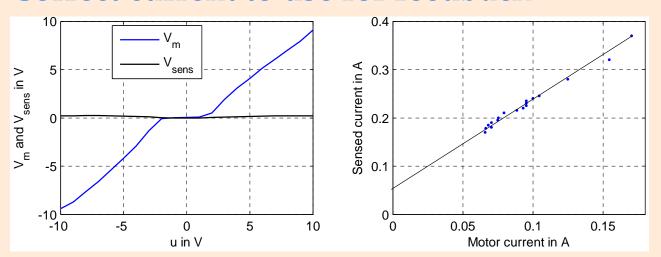






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### Correct current to use for feedback



- Instead of  $i_{\text{sens}}$ , more accurate to use  $i_m \approx \frac{1}{1.8}i_{\text{sens}} \frac{1}{30}$ , which fits the straight line in the right hand figure.
- If time permits, replace  $i_{sens}$  with  $i_m$  and redo experiment.



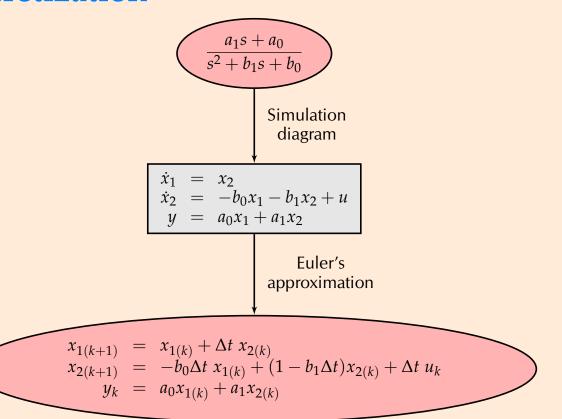






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### Discretization



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# Simulate; LW: C code, Implement, Analyze

- Simulation: easysim.m
- Discretized controller
  - $\longrightarrow$  C code:

- Implement: As in demo slides
- Analyze: Compare results

```
  \begin{aligned}
    x_1(k+1) &= a_{11}x_1(k) + a_{12}x_2(k) + b_1u(k) \\
    x_2(k+1) &= a_{21}x_1(k) + a_{22}x_2(k) + b_2u(k) \\
    y(k) &= c_1x_1(k) + c_2x_2(k) + du(k)
  \end{aligned}
```

In main-prog.c before main() insert float x1[2],x2[2];
In main() insert x1[0] = x2[0] = 0;

```
x1[1] = a11 * x1[0] + a12 * x2[0] + b1 * u;

x2[1] = a21 * x1[0] + a22 * x2[0] + b2 * u;

y = c1 * x1[0] + c2 * x2[0] + d * u;

x1[0] = x1[1];

x2[0] = x2[1];
```









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Part II

Review of Exp.2



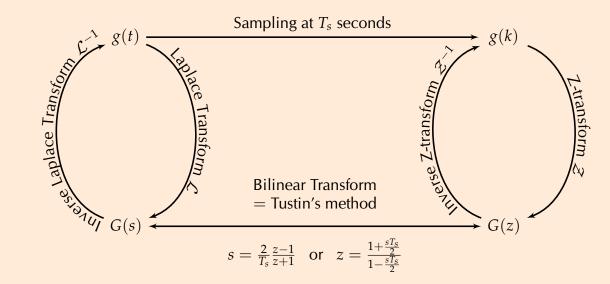




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# Least squares sys-id theory

#### Bilinear transform and Z-transform



- Both *s*-domain & *z*-domain are fictitious domains.
- They simplify working with differential equations & difference equations respectively.
- Bilinear transform is not the only way to go  $G(s) \leftrightarrow G(z)$ .
- $T_s$  constrained by Nqyquist sampling rate.









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$$G(s) \longleftrightarrow G(z)$$

ullet Consider definitions of  ${\mathcal L}$  and  ${\mathcal Z}$ 

$$Y(s) = \mathcal{L} \{y(t)\} \triangleq \int_{t=0}^{\infty} y(t)e^{-st}dt$$
 $Y(z) = \mathcal{Z} \{y(k)\} \triangleq \sum_{k=0}^{\infty} y(k)z^{-k}$ 

- Comparison suggests  $z = e^{sT_s}$ .
- To convert G(s) to G(z), can substitute  $s = \frac{\ln z}{T_s}$ .
- Easier to work with an approximation

$$z = e^{sT_s} = e^{\frac{sT_s}{2}} e^{\frac{sT_s}{2}} = \frac{e^{\frac{sT_s}{2}}}{e^{-\frac{sT_s}{2}}} = \frac{1 + \frac{\left(\frac{sT_s}{2}\right)}{1!} + \frac{\left(\frac{sT_s}{2}\right)^2}{2!} + \cdots}{1 + \frac{\left(-\frac{sT_s}{2}\right)}{1!} + \frac{\left(-\frac{sT_s}{2}\right)^2}{2!} + \cdots} \approx \frac{1 + \frac{sT_s}{2}}{1 - \frac{sT_s}{2}}$$

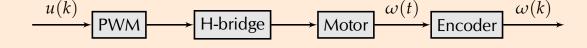
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### How Z-transform used in our sys-id



- u(k) denotes sample of u(t) at sampling instant  $t = kT_s$ .
- Let  $u(k) \to \omega(k)$  TF be G(z).
- Use u(k),  $\omega(k)$  pairs to build G(z).
- Use bilinear transform to go from G(z) to G(s).

Important property of Z-transform used:

$$z^{-l}X(z) \leftrightarrow x(k-l)$$
 given  $X(z) \leftrightarrow x(k)$ .









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### What is least squares sys-id? (1/2)

• Let 
$$G(z) = \frac{b_1 z^2 + b_2 z + b_3}{z^3 + a_1 z^2 + a_2 z + a_3} = \frac{Y(z)}{U(z)}$$
.

Cross multiply:

 $b_1 z^2 U(z) + b_2 z U(z) + b_3 U(z) = z^3 Y(z) + a_1 z^2 Y(z) + a_2 z Y(z) + a_3 Y(z)$ .

• Multiply throughout by  $z^{-3}$ :

$$Y(z) + a_1 z^{-1} Y(z) + a_2 z^{-2} Y(z) + a_3 z^{-3} Y(z).$$

• Take  $\mathcal{Z}^{-1}$  to obtain difference equation

$$b_1u(k-1) + b_2u(k-2) + b_3u(k-3) =$$

 $y(k) + a_1y(k-1) + a_2y(k-2) + a_3y(k-3)$ .

 $b_1 z^{-1} U(z) + b_2 z^{-2} U(z) + b_3 z^{-3} U(z) =$ 







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### What is least squares sys-id? (2/2)

Consider 
$$b_1 u(k-1) + b_2 u(k-2) + b_3 u(k-3) =$$
  
 $y(k) + a_1 y(k-1) + a_2 y(k-2) + a_3 y(k-3).$  (1)

- Let  $\sigma = |b_1 \quad b_2 \quad b_3 \quad -a_1 \quad -a_2 \quad -a_3|^{\mathsf{T}}$ .
- Suppose we have data of u(k) and y(k) for k = 0, 1, ..., N.
- Problem: Find  $\sigma$  such that (1) holds for this data. I.E., find parameters of a TF that <u>fits</u> to input-output data.
- Let error in the fit be  $\varepsilon(k,\sigma) = b_1 u(k-1) + b_2 u(k-2) + b_3 u(k-3) - y(k)$  $-a_1y(k-1)-a_2y(k-2)-a_3y(k-3).$
- Modified problem: Find  $\sigma$  to minimize  $\mathcal{J}(\sigma) \triangleq \sum_{k=0}^{N} \varepsilon^{2}(k, \sigma)$ .
- If  $\mathcal{J}(\sigma = \sigma_0) = 0$ , then find best estimate  $\hat{\sigma}$  of  $\sigma_0$ .











# What the experiment taught

- Sys-id techinques from Exp.1 & Exp.2 give different results.
- Likely cause is not only the dead zone nonlinearity in the plant, but also the input signals the sys-id technique uses.
  - E.g., the step input (u=7) in Exp.1 does not keep plant in dead zone, while the low-frequency (5 10 Hz) triangular input makes the plant go into dead zone twich every cycle.
- Will using rectangular waveform instead of triangular waveform (TW) give a different model with least squares sys-id (LSS)?
- If plant behaves as 1st order even with TW, LSS will say that plant has one LHP pole that is 10 20 times deeper than the other.







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