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## Problem 4.1

Oblique shock wave with wave angle of  $35^\circ$ Upstream of wave,  $p_1 = 2000 \text{ lb/ft}^2$ ,  $T_1 = 520^\circ\text{R}$ , and  $v_1 = 3355 \text{ ft/s}$ Calculate  $p_2$ ,  $T_2$ ,  $v_2$ , and flow deflection angle

$$M_1 = \frac{v_1}{a_1}$$

$$a_1 = \sqrt{\gamma R T_1} \quad \text{assuming ideal real gas} \rightarrow \text{air}$$

$$a_1 = \sqrt{(1.4)(1716 \text{ ft}^2/\text{s}^2\text{R})(520^\circ\text{R})}$$

$$a_1 = 1117.7 \text{ ft/s}$$

$$\therefore M_1 = 3355 \text{ ft/s} / 1117.7 \text{ ft/s}$$

$$M_1 = 3$$

We are told  $\beta = 35^\circ$ 

$$\text{so, } M_{n1} = M_1 \sin \beta = 3 \sin(35^\circ)$$

$$M_{n1} = 1.72$$

Use this  $M_{n1}$  in table A2 and get

$$p_2/p_1 = 3.285, \quad T_2/T_1 = 1.473, \quad M_{n2} = 0.6355$$

Therefore:

$$p_2 = (2000 \text{ lb/ft}^2)(3.285) = 6570 \text{ lb/ft}^2 = p_2$$

$$T_2 = (520^\circ\text{R})(1.473) = 765.96^\circ\text{R} = T_2$$

Using  $\theta$ - $\beta$ - $M$  figure with  $\beta = 35^\circ$  and  $M = 3$ 

$$\theta \approx 18^\circ$$

$$M_2 = \frac{M_{n1}}{\sin(\beta - \theta)} = \frac{0.6355}{\sin(17^\circ)} = 2.1736$$

$$v_2 = M_2 a_2 = 2.1736 \sqrt{1.4(1716)(765.96)}$$

$$v_2 = 2948.53 \text{ ft/s}$$

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Problem 4.2

Wedge with half angle of  $10^\circ$  flying at Mach 2

Calculate ratio of TOTAL pressures across shockwave emanating from wedge LE

Using  $\theta$ - $\beta$ -M chart with  $\theta = 10^\circ$ ,  $M = 2$ We get  $\beta \approx 38^\circ$ 

$$M_{n1} = M_1 \sin \beta$$

$$M_{n1} = 2 \sin(38^\circ) = 1.23$$

Using table A2 with  $M = 1.23$  & interpolating

$$\frac{P_{02}}{P_{01}} = 0.99455$$



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Problem 4.3

Calculate maximum surface pressure  $[N/m^2]$  that can be achieved on forward face of wedge flying at Mach 3 at std sea level conditions ( $P_1 = 1.01 \times 10^5 N/m^2$ ) with attached shock wave

Using  $\theta$ - $\beta$ - $M$  we want  $\theta_{max}$  for  $M=3$  ( $\theta_{max} \Rightarrow$  attached)

We get  $\theta \approx 34^\circ$  at  $\beta \approx 65^\circ$

$$M_{n1} = M_1 \sin(\beta) = 3 \sin(65^\circ) = 2.72$$

Table A2 with  $M = 2.72$  & interpolating

$$P_2/P_1 = 8.4652$$

$$P_2 = (8.4652)(1.01 \times 10^5 N/m^2)$$

$$P_2 = 854985.2 N/m^2 = 8.55 \times 10^5 N/m^2$$

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Problem 4.4

In flow past compression corner, upstream  $M_1 = 3.5$  and  $P_1 = 1 \text{ atm}$ .  
Downstream of corner,  $P_2 = 5.48 \text{ atm}$ .  
Calculate deflection angle of corner

$$P_2 / P_1 = 5.48$$

Using table A2 this gives

$$M = 2.2 = M_{n1}$$

$$M_{n1} = M_1 \sin(\beta)$$

$$\sin(\beta) = \frac{2.2}{3.5}$$

$$\beta = 38.9^\circ$$

Using  $\theta$ - $\beta$ - $M$  figure

$$\theta \approx 21^\circ$$



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Problem 4.5

Consider  $20^\circ$  half angle wedge at  $M=3$  at std. sea level conditions

$$P_1 = 2116 \text{ lb/ft}^2, \quad T_1 = 519^\circ\text{R}$$

Calculate wave angle, surface pressure, temperature, and mach number

Use  $\theta$ - $\beta$ - $M$ . with  $\theta = 20^\circ$ ,  $M=3$  and get

$$\beta \approx 47^\circ$$

$$M_{n1} = M_1 \sin(47^\circ) = 2.194$$

Use table A2 with  $M=2.19$  & interpolating

$$P_2/P_1 = 5.4292$$

$$T_2/T_1 = 1.8482$$

$$M_{z1} = 0.54848$$

$$P_2 = (5.4292)(2116 \text{ lb/ft}^2) = 11488.187 \text{ lb/ft}^2$$

$$T_2 = (1.8482)(519^\circ\text{R}) = 959.2^\circ\text{R}$$

$$M_2 = M_{n2} / \sin(\beta - \theta)$$

$$M_2 = 0.54848 / \sin(27^\circ)$$

$$M_2 = 1.208$$

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Problem 6

Consider viscous dissipation effects for supersonic flow approaching nosetip of RV  
at  $M = 3.3$

Local static temp of flow = 350 K

Specific heat at const P = 1008 J/kg K

Recovery factor = 0.83

a) Determine magnitude of KE in flow [ $\text{m}^2/\text{s}^2$ ]

$$KE = \frac{1}{2} v^2$$

$$v = Ma = M \sqrt{\gamma R T} \quad (\text{assuming ideal air})$$

$$v = 3.3 \cdot \sqrt{1.4 (287 \text{ J/kg K}) (350 \text{ K})} = 1237.5 \text{ m/s}$$

$$\therefore KE = 765730.35 \text{ m}^2/\text{s}^2 = 7.66 \times 10^5 \text{ m}^2/\text{s}^2$$

b) Mag of KE divided by  $C_p$  in K

$$\frac{KE}{C_p} = \frac{765730.35 \text{ m}^2/\text{s}^2}{1008 \text{ m}^2/\text{s}^2 \text{ K}} = 759.65 \text{ K} = \frac{KE}{C_p}$$

c) Determine stagnation temp of flow in K

$$\text{Using } C_p T + \frac{v^2}{2} = C_p T_0 \rightarrow T + \frac{v^2}{2 C_p} = T_0$$

$$\therefore \underset{(b)}{759.65 \text{ K}} + \underset{(\text{given})}{350 \text{ K}} = 1109.65 \text{ K} = T_0$$

d) Mag of KE in flow that is recovered isentropically

$$\text{recovery factor } \alpha = \frac{T_{AD} - T}{T_0 - T} \quad \text{solve for } T_{AD}$$

$$T_{AD} = \alpha (T_0 - T) + T = 0.83 (1109.65 - 350) + 350$$

$$T_{AD} = 980.5 \text{ K}$$

$$T_{\text{recovered isen}} = T_{AD} - T = 630.5 \text{ K}$$

$$KE_{\text{rec}} = (T_{AD} - T) \times C_p = 6.356 \times 10^5 \text{ m}^2/\text{s}^2 = KE_{\text{rec}}$$

e) Mag of KE lost due to viscous dissipation

$$T_{\text{lost}} = T_0 - T_{AD} = 129.15 \text{ K}$$

$$KE_{\text{lost}} = (T_0 - T_{AD}) C_p = 1.3 \times 10^5 \text{ m}^2/\text{s}^2 = KE_{\text{lost}}$$



f) Mag KE divided by  $c_p$  recovered isentropically in K

$$(d) KE_{rec} = 6.356 \times 10^5 \text{ m}^2/\text{s}^2$$

$$\frac{KE_{rec}}{c_p} = 630.5 \text{ K}$$

g) Mag KE divided by  $c_p$  lost to viscous dissipation in K

$$(e) KE_{lost} = 1.3 \times 10^5 \text{ m}^2/\text{s}^2$$

$$\frac{KE_{lost}}{c_p} = 129.15 \text{ K}$$