

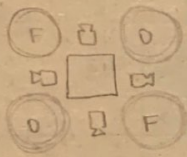
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Problem 8.4

Given: $\text{N}_2\text{O}_4/\text{MMH}$ propellant combo
 Equal volumes for both fuel & oxidizer tanks
 Payload mass = 10 kg
 $I_{sp} = 300 \text{ sec}$
 Required $\Delta v = 1000 \text{ m/s}$
 $\lambda = 0.5$

Find: a) propellant mixture ratio
 b) total propellant mass required
 c) radius of spherical tanks
 d) tank wall thickness if $P_{burst} = 5 \text{ MPa}$ and is titanium

Schematic:



Assumptions:

Each tank has same volume
 Keep grav in Δv eq so units work
 Thin wall tanks
 $\rho_{ox} = 1440 \text{ kg/m}^3$
 $\rho_f = 880 \text{ kg/m}^3$ } googled

Basic Equations:

$$r = \frac{m_{ox}}{m_f}, \quad \rho = \frac{m}{V}, \quad MR = \frac{m_o}{m_f}, \quad m_o = m_{pl} + m_p + m_i, \quad \lambda = \frac{m_p}{m_p + m_i}$$

$$V_{sph} = \frac{4}{3}\pi R^3, \quad \Delta v = I_{sp} \ln\left(\frac{m_o}{m_f}\right), \quad m_p = m_{pl} \left(\frac{MR-1}{MR-(MR-1)/\lambda} \right)$$

$$t_c = P_t R / \sigma_w, \quad \sigma_w = \min(F_t/1.1, F_{tu}/1.25)$$

6 or 1.4

Analysis:

a) Propellant mixture ratio

$$\Delta v = g I_{sp} \ln\left(\frac{m_o}{m_f}\right) \rightarrow \frac{m_o}{m_f} = e^{\Delta v / g I_{sp}}$$

$$\frac{m_o}{m_f} = e^{(1000 \text{ m/s}) / (9.81 \text{ m/s}^2)(300 \text{ s})}$$

$$\frac{m_o}{m_f} = 1.4 = MR$$

b) Total propellant mass required

$$m_p = m_{pl} \left(\frac{MR-1}{MR-(MR-1)/\lambda} \right) = 10 \left(\frac{0.4}{1.4 - \frac{0.4}{0.5}} \right) \text{ kg}$$

$$m_p = 6.67 \text{ kg}$$

c) Radius of spherical tanks

know $m_p = 6.67 \text{ kg}$

need $r = \frac{m_{ox}}{m_f}$

have $\rho_{ox} = \frac{m_{ox}}{V_{ox}}$ & $\rho_f = \frac{m_f}{V_f}$

told $V_f = V_{ox}$

\therefore we can say $\frac{\rho_{ox}}{\rho_f} = \frac{m_{ox}}{m_f}$

$\rho_{ox}/\rho_f = 1440/880 = 1.636 = r$

$m_f = \frac{m_p}{1+r} = 2.53 \text{ kg}$

$m_{ox} = r m_f = 4.14 \text{ kg}$

$V_f = \frac{m_f}{\rho_f} = 0.002875 \text{ m}^3$ } yes they are the same

$V_{ox} = \frac{m_{ox}}{\rho_{ox}} = 0.002875 \text{ m}^3$

$R = \sqrt[3]{\frac{3V}{4\pi}} = \sqrt[3]{\frac{3(0.002875 \text{ m}^3)}{4\pi}}$

$R = 0.0882 \text{ m}$

d) Tank wall thickness

$t_c = \frac{P_t(\max) R}{\sigma_w}$ $P_t = 5 \text{ MPa}$

$\sigma_w = \min\left(\frac{\text{yield}}{1.1}, \frac{\text{ult tens. strength}}{1.4}\right)$ look up for titanium

$\sigma_w = \min\left(\frac{241 \text{ MPa}}{1.1}, \frac{1400 \text{ MPa}}{1.4}\right) = 219.1 \text{ MPa}$

$t_c = \frac{5 (0.0882)}{219.1} \frac{\text{MPa} \cdot \text{m}}{\text{MPa}}$

$t_c = 0.00201 \text{ m} = 2.01 \text{ mm}$

Comments:

The wall thickness is allowed to be SUPER thin because of the material.

I also realized afterwards that (c) could just have been $V = \frac{m_p}{\rho_f + \rho_{ox}}$... but I guess it was good to make sure $V_f = V_{ox}$ like we assumed.

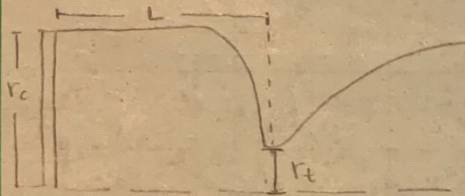
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Problem 8.6

Given: LOX & Ethanol
 $c^* = 5900 \text{ ft/s}$
 $\gamma = 1.2$
 $F_v = 30000 \text{ lbf}$
 $\epsilon = 50$
 $P_c = 1200 \text{ psi}$
 $M \leq 0.1$
 $L^* = 40 \text{ inches}$ - char. chamber dim.

Find: a) I_{sp}
 b) r_t
 c) r_c
 d) L (chamber)

Schematic:



Assumptions:

Purdue tables

~~Analysis~~ Basic Equations:

$$I_{sp} = \frac{c_{fv} \cdot c^*}{g}, \quad F_v = c_{fv} P_c A_t, \quad A_c = (N_{ox} + N_{fuel}) / N_D$$

$$\epsilon_c = A_c / A_t, \quad \frac{A_c}{A_t} = \frac{1}{M} \left[\frac{2 + (\gamma - 1) M^2}{\gamma + 1} \right]^{(\gamma + 1) / 2(\gamma - 1)}$$

$$L^* = \frac{\sqrt{V_c}}{A_t}$$

Analysis:

a) I_{sp}

$$I_{sp} = \frac{c_{fv} \cdot c^*}{g} \quad \text{Using } \gamma = 1.2, \epsilon = 50$$

$$c_{fv} = 1.90236$$

$$I_{sp} = \frac{(1.90236)(5900 \text{ ft/s})}{32.2 \text{ ft/s}^2}$$

$$I_{sp} = 348.57 \text{ sec}$$

b) r_t

$$F_v = C_{Fv} P_c A_t$$

$$A_t = \frac{F_v}{C_{Fv} P_c} = \frac{30000 \text{ lbf}}{(1.90236)(1200 \text{ lbf/in}^2)}$$

$$A_t = 13.14 \text{ in}^2$$

$$r_t = \sqrt{A_t / \pi}$$

$$r_t = 2.045 \text{ in}$$

c) r_c ($M=0.1$)

$$A_c = A_t \left(\frac{1}{0.1} \left[\frac{2 + (0.2)(0.1)^2}{2.2} \right]^{2.2/0.4} \right)$$

$$A_c = 78.22 \text{ in}^2$$

$$r_c = \sqrt{A_c / \pi}$$

$$r_c = 5.0 \text{ in}$$

d) L (chamber)

$$L^* = r_c^2 / A_t$$

$$L^* = \frac{\pi r_c^2 L_c}{A_t}$$

$$L_c = \frac{L^* A_t}{\pi r_c^2} = \frac{40 \text{ in} (13.14 \text{ in}^2)}{\pi (5.0 \text{ in})^2}$$

$$L_c = 6.69 \text{ in}$$

Comment

$r_c > r_t \rightarrow$ expected

L_c is close to r_c