EE910: Digital Communication Systems-I

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Lecture #3B: Pulse Amplitude Modulation, Phase Shift Keying and Quadrature Amplitude Modulation



• In digital PAM, the signal waveforms may be represented as

$$s_m(t) = A_m p(t), 1 \le m \le M \tag{1}$$

where p(t) is a pulse of duration T and $\{A_m, 1 \leq m \leq M\}$ denotes the set of M possible amplitudes corresponding to $M = 2^k$ possible k-bit blocks of symbols.

- The signal amplitudes A_m take the discrete values $A_m = 2m 1 M$, m = 1, 2, ..., M i.e., the amplitudes are $\pm 1, \pm 3, \pm 5, ..., \pm (M 1)$.
- The waveform p(t) is a real-valued signal pulse whose shape influences the spectrum of the transmitted signal.



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Pulse Amplitude Modulation (PAM)

• The energy in signal $s_m(t)$ is given by

$$\mathcal{E}_m = \int_{-\infty}^{\infty} A_m^2 \rho^2(t) dt = A_m^2 \mathcal{E}_p \tag{2}$$

where \mathcal{E}_p is the energy in p(t).

• From this,

$$\mathcal{E}_{avg} = \frac{\mathcal{E}_{p}}{M} \sum_{m=1}^{M} A_{m}^{2}$$

$$= \frac{2\mathcal{E}_{p}}{M} (1^{2} + 3^{2} + 5^{2} + \dots + (M-1)^{2})$$

$$= \frac{2\mathcal{E}_{p}}{M} \times \frac{M(M^{2} - 1)}{6}$$

$$= \frac{(M^{2} - 1)\mathcal{E}_{p}}{3}$$
(3)

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• Average energy per bit is given by

$$\mathcal{E}_{bavg} = \frac{(M^2 - 1)\mathcal{E}_p}{3\log_2 M} \tag{4}$$

• Usually the PAM signals are carrier-modulated bandpass signals with lowpass equivalents of the form $A_mg(t)$, where A_m and g(t) are real. In this case

$$s_m(t)$$
 = $Re \left[s_{ml}(t)e^{j2\pi f_c t} \right]$
 = $Re \left[A_m g(t)e^{2\pi f_c t} \right] = A_m g(t)\cos(2\pi f_c t)$

where f_c is the carrier frequency.

• In the generic form of PAM signaling if we substitute

$$p(t) = g(t)\cos(2\pi f_c t) \tag{5}$$

then we obtain the bandpass PAM.

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Pulse Amplitude Modulation (PAM)

• For bandpass PAM we have

$$\mathcal{E}_m = \frac{A_m^2 \mathcal{E}_g}{2} \tag{6}$$

where \mathcal{E}_g is the energy in g(t).

• From Equations (3) and (4) we conclude

$$\mathcal{E}_{avg} = \frac{(M^2 - 1)\mathcal{E}_g}{6}$$

$$\mathcal{E}_{bavg} = \frac{(M^2 - 1)\mathcal{E}_g}{6\log_2 M}$$
(7)

ullet Clearly, PAM signals are one-dimensional (N=1) since all are multiples of the same basic signals.



• We can use

$$\phi(t) = \frac{p(t)}{\sqrt{\mathcal{E}_p}} \tag{8}$$

as the basis for the general PAM signal of the form $s_m(t) = A_m p(t)$ and

$$\phi(t) = \sqrt{\frac{2}{\mathcal{E}_g}} g(t) \cos 2\pi f_c t \tag{9}$$

as the basis for the bandpass PAM signal given in Equation (5).

• Using these basis signals, we have

$$s_m(t) = A_m \sqrt{\mathcal{E}_p} \phi(t)$$
 for baseband PAM
$$s_m(t) = A_m \sqrt{\frac{\mathcal{E}_g}{2}} \phi(t)$$
 for bandpass PAM (10)

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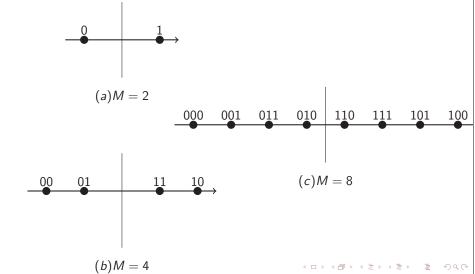
Pulse Amplitude Modulation (PAM)

• The one-dimensional vector representations for these signals are of the form

$$s_m = A_m \sqrt{\mathcal{E}_p}, \quad A_m = \pm 1, \pm 3, \cdots, \pm (M-1)$$
 (11)

$$s_m = A_m \sqrt{\frac{\mathcal{E}_g}{2}}, \qquad A_m = \pm 1, \pm 3, \cdots, \pm (M-1)$$
 (12)





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Pulse Amplitude Modulation (PAM)

• We note that the Euclidean distance between any pair of signal points is

$$d_{mn} = \sqrt{\|s_m - s_n\|^2}$$

$$= |A_m - A_n| \sqrt{\mathcal{E}_p}$$

$$= |A_m - A_n| \sqrt{\frac{\mathcal{E}_g}{2}}$$
(13)

where the last relation corresponds to a bandpass PAM.

• For adjacent signal points $|A_m - A_n| = 2$, and hence the minimum distance of the constellation is given by

$$d_{min} = 2\sqrt{\mathcal{E}_p} = \sqrt{2\mathcal{E}_g} \tag{14}$$



• The resulting expression is

$$d_{min} = \sqrt{\frac{12\log_2 M}{M^2 - 1}} \mathcal{E}_{bavg} \tag{15}$$

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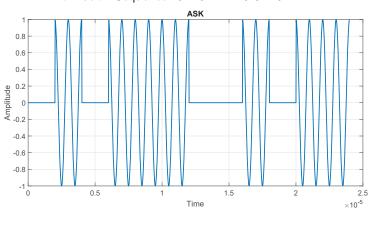
Amplitude Shift Keying (ASK)

- Can be viewed as a special case of PAM where g(t) is a sinusoid.
- Here amplitude of the carrier signal is varied according to the information sequence.
- Simplest form of ASK is on-off keying where either bursts of a carrier signal are transmitted or nothing is transmitted depending whether the input message signal is 1 or 0.

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Amplitude Shift Keying (ASK)

Information Sequence: 0 1 0 1 1 1 0 0 1 0 1 1



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Phase Modulation

• In digital phase modulation, the M signal waveforms are represented as

$$s_{m}(t) = Re \left[g(t)e^{j\frac{2\pi(m-1)}{M}}e^{j2\pi f_{c}t} \right], \quad m = 1, 2, \dots, M \quad (16)$$

$$= g(t)\cos \left[2\pi f_{c}t + \frac{2\pi}{M}(m-1) \right]$$

$$= g(t)\cos \left(\frac{2\pi}{M}(m-1) \right)\cos 2\pi f_{c}t$$

$$-g(t)\sin \left(\frac{2\pi}{M}(m-1) \right)\sin 2\pi f_{c}t$$

where g(t) is the signal pulse shape and $\theta_m = 2\pi \frac{(m-1)}{M}, \quad m=1,2,\cdots,M$ is the M possible phases of the carrier that convey the transmitted information.

Phase Modulation

- Digital phase modulation is usually called phase-shift keying (PSK).
- We note that these signal waveforms have equal energy.

$$\mathcal{E}_{avg} = \mathcal{E}_m = \frac{1}{2}\mathcal{E}_g \tag{17}$$

and therefore,

$$\mathcal{E}_{bavg} = \frac{\mathcal{E}_g}{2\log_2 M} \tag{18}$$

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Phase Modulation

• We note that $g(t)\cos 2\pi f_c T$ and $g(t)\sin 2\pi f_c t$ are orthogonal, and therefore $\phi_1(t)$ and $\phi_2(t)$ given as

$$\phi_1(t) = \sqrt{\frac{2}{\mathcal{E}_g}} g(t) \cos 2\pi f_c t \tag{19}$$

$$\phi_2(t) = -\sqrt{\frac{2}{\mathcal{E}_g}}g(t)\sin 2\pi f_c t \tag{20}$$

ullet We can write $s_m(t), 1 \leq m \leq M$, as

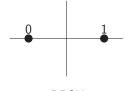
$$s_{m}(t) = \sqrt{\frac{\mathcal{E}_{g}}{2}} \cos\left(\frac{2\pi}{M}(m-1)\right) \phi_{1}(t) + \sqrt{\frac{\mathcal{E}_{g}}{2}} \sin\left(\frac{2\pi}{M}(m-1)\right) \phi_{2}(t)$$
(21)

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Phase Modulation

 \bullet The signal space dimensionality is ${\it N}=2$ and the resulting vector representations are

$$s_{m} = \left(\sqrt{\frac{\mathcal{E}_{g}}{2}}\cos\left(\frac{2\pi}{M}(m-1)\right), \sqrt{\frac{\mathcal{E}_{g}}{2}}\sin\left(\frac{2\pi}{M}(m-1)\right)\right), m = 1, 2, \cdots, M$$
(22)



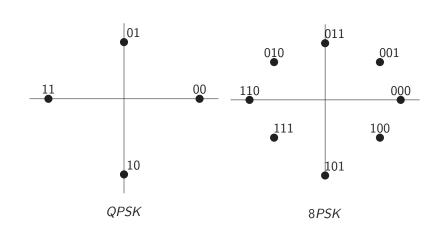
BPSK

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Phase Modulation



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Phase Modulation

• The Euclidean distance between signal points is

$$d_{mn} = \sqrt{\|s_m - s_n\|^2}$$

$$= \sqrt{\mathcal{E}_g \left[1 - \cos\left(\frac{2\pi}{M}(m - n)\right)\right]}$$
(23)

• The minimum distance corresponding to |m-n|=1 is

$$d_{min} = \sqrt{\mathcal{E}_g \left[1 - \cos\left(\frac{2\pi}{M}\right) \right]} = \sqrt{2\mathcal{E}_g \sin^2\frac{\pi}{M}}$$
 (24)

ullet Solving Equation (18) for \mathcal{E}_g and substituting the result in Equation (24) result in

$$d_{min} = 2\sqrt{\left(\log_2 M \times \sin^2 \frac{\pi}{M}\right)\mathcal{E}_b} \tag{25}$$

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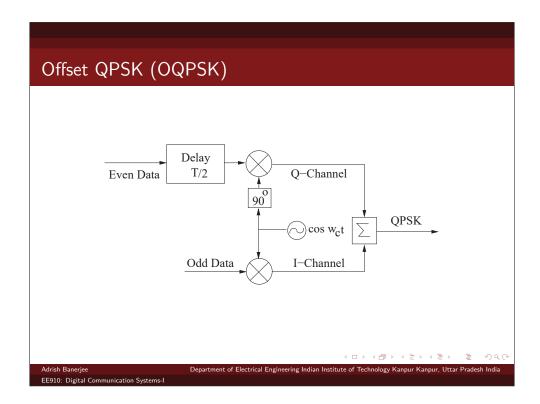
Phase Modulation

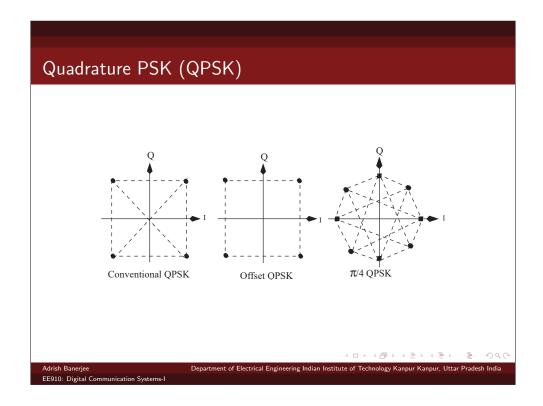
• For large values of M, we have $\sin \frac{\pi}{M} \approx \frac{\pi}{M}$, and d_{min} can be approximated by

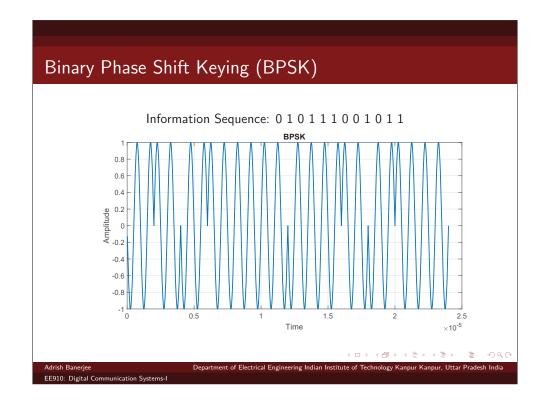
$$d_{min} \approx 2\sqrt{\frac{\pi^2 \log_2 M}{M^2} \mathcal{E}_b} \tag{26}$$

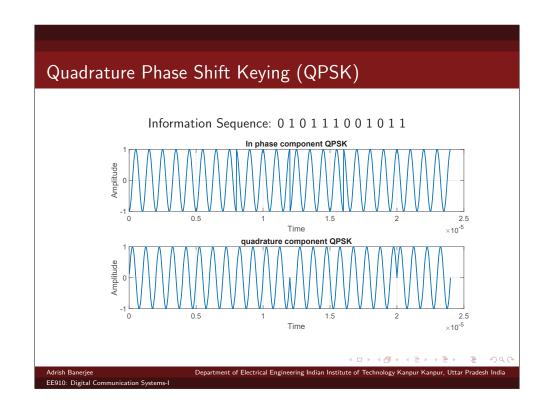
- \bullet Variants of four-phase PSK (QPSK) include offset QPSK and $\pi/4$ QPSK.
- In Offset QPSK, the phase transitions are limited to 90 degrees, the transitions on the I and Q channels are staggered.
- In $\pi/4$ QPSK the set of constellation points are toggled each symbol, so transitions through zero cannot occur.











- The bandwidth efficiency of PAM can also be obtained by simultaneously impressing two separate k-bit symbols from the information sequence on two quadrature carriers $\cos 2\pi f_c t$ and $\sin 2\pi f_c t$.
- The resulting modulation technique is called quadrature PAM or QAM, and the corresponding signal waveforms may be expressed as

$$s_{m}(t) = Re \left[(A_{mi} + jA_{mq})g(t)e^{j2\pi f_{c}t} \right]$$

$$= A_{mi}g(t)\cos 2\pi f_{c}t - A_{mq}g(t)\sin 2\pi f_{c}t, \quad m = 1, 2, \dots, M$$
(27)

where A_{mi} and A_{mq} are the information-bearing signal amplitudes of the quadrature carriers and g(t) is the signal pulse.

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Quadrature Amplitude Modulation

• Alternatively, the QAM signal waveforms may be expressed as

$$s_m(t) = Re \left[r_m e^{j\theta_m} e^{j2\pi f_c t} \right]$$

= $r_m \cos(2\pi f_c t + \theta_m)$ (28)

where
$$r_m = \sqrt{A_{mi}^2 + A_{mq}^2}$$
 and $heta_m = tan^{-1}(A_{mi}/A_{mq})$

- Similar to the PSK case, $\phi_1(t)$ and $\phi_2(t)$ given in Equations (19) and (20) can be used as an orthonormal basis for expansion of QAM signals.
- The dimensionality of the signal space for QAM is N = 2.



• Using this basis, we have

$$s_m(t) = A_{mi} \sqrt{\frac{\mathcal{E}_g}{2}} \phi_1(t) + A_{mq} \sqrt{\frac{\mathcal{E}_g}{2}} \phi_2(t)$$
 (29)

which results in vector representations of the form

$$s_{m} = (s_{m1}, s_{m2})$$

$$= \left(A_{mi}\sqrt{\frac{\mathcal{E}_{g}}{2}}, A_{mq}\sqrt{\frac{\mathcal{E}_{g}}{2}}\right)$$
(30)

and

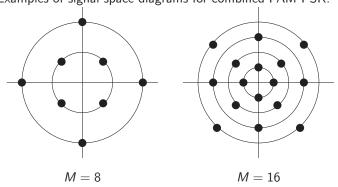
$$\mathcal{E}_{m} = \|s_{m}\|^{2} = \frac{\mathcal{E}_{g}}{2} (A_{mi}^{2} + A_{mq}^{2})$$
 (31)

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Quadrature Amplitude Modulation

• Examples of signal space diagrams for combined PAM-PSK.



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• The Euclidean distance between any pair of signal vectors in QAM is

$$d_{mn} = \sqrt{\|s_m - s_n\|^2}$$

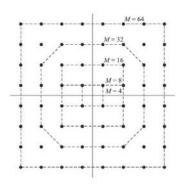
$$= \sqrt{\frac{\mathcal{E}_g}{2} \left[(A_{mi}^2 - A_{ni}^2) + (A_{mq}^2 - A_{nq}^2) \right]}$$
(32)

• In the special case where the signal amplitudes take the set of discrete values $\{(2m-1-M), m=1,2,\cdots,M\}$, the signal space diagram is rectangular.



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Quadrature Amplitude Modulation



• In this case, the Euclidean distance between adjacent points, i.e., the minimum distance, is

$$d_{min} = \sqrt{2\mathcal{E}_g} \tag{33}$$

which is the same result as for PAM.

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• In the special case of a rectangular constellation with $M=2^{2k_1}$, i.e., $M=4,16,64,256,\cdots$, and with amplitudes of $\pm 1,\pm 3,\cdots,\pm (\sqrt{M}-1)$ on both directions, from equation (31) we have

$$\mathcal{E}_{avg} = \frac{1}{M} \frac{\mathcal{E}_g}{2} \sum_{m=1}^{\sqrt{M}} \sum_{n=1}^{\sqrt{M}} (A_m^2 + A_n^2)$$

$$= \frac{\mathcal{E}_g}{2M} \times \frac{2M(M-1)}{3} = \frac{(M-1)}{3} \mathcal{E}_g$$
(34)

Thus

$$\mathcal{E}_{bavg} = \frac{M-1}{3\log_2 M} \mathcal{E}_g \tag{35}$$

• Using equation (33), we have

$$d_{min} = \sqrt{\frac{6\log_2 M}{M - 1}\mathcal{E}_{bavg}} \tag{36}$$

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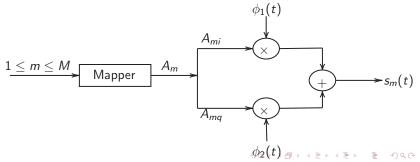
Quadrature Amplitude Modulation

 From the discussion of bandpass PAM, PSK, and QAM, it is clear that all these signaling schemes are of the general form

$$s_m(t) = Re \left[A_m g(t) e^{j2\pi f_c t} \right], \quad m = 1, 2, \cdots, M$$
 (37)

where A_m is determined by the signaling scheme.

• The structure of the modulator for this general class of signaling schemes is shown below



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