## **Department of Electrical, Computer, and Software Engineering**

## **ELECTENG 734**

# Technical Design Report

Group Number: 24

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**Declaration of Originality** 

This report is our own unaided work and was not

copied from nor written in collaboration with any

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## **Buck Conveter Design - Part I**

### **Specifications**

Parameter	Value	Unit
Nominal Vin(avg)	15.00	V
Max lin(avg)	1.30	Α
Max Vout(avg)	9.70	V
Max RL(max)	10.00	Ω
Min RL(min)	2.00	Ω
Design η	90.00	%
Operating fs	100.00	kHz

### **Evaluating Steady-State Operating Conditions**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.00	Ω	4.00	Ω	10.00	Ω
Pout	17.55	W (1)	17.55	W (1)	9.41	W (2)
lo=IL(avg)	2.96	A (3)	2.10	A (3)	1.33	A (3)
lin(avg)=ls(avg)	1.30	A (4)	1.30	A (4)	0.70	A (4)
D	43.88	% (5)	62.07	% (5)	71.85	% (5)
Vout	5.92	V (6)	8.38	V (6)	9.70	V (6)

## **Evaluating Minimum Inductance**

Parameter	Value	Unit (eq)
Vin(critical)	15.00	V
RL(critical)	10.00	Ω
D @ RL(critical)	71.85	%
Lmin	10.27	μH (7)

#### **Selected Inductance**

Parameter	Value	Unit (eq)
L(selected)	25.00	μН

### **Evaluating Steady-State Ripple and RMS Curents**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.00	Ω	4.00	Ω	10.00	Ω
ΔIL	1.33	A (8)	1.27	A (8)	1.09	A (8)
IL,pk	3.63	A (9)	2.74	A (9)	1.88	A (9)
IL,rms	2.98	A (10)	2.13	A (10)	1.37	A (10)
lin,rms=ls,rms	1.98	A (11)	1.68	A (11)	1.16	A (11)
IC,rms	0.38	A (12)	0.37	A (12)	0.31	A (12)

### **Buck Conveter Design - Part II**

#### **Specifications**

Parameter	Value	Unit
Selected L	25.00	μН
Max IL,pk	3.63	Α
Max IL,rms	2.98	Α
Operating fs	100.00	kHz
Design Bmax	0.25	Т
Design Jmax	5.00	A/mm^2

#### **Core, Former & Magnet Wire Details**

Parameter	Value	Unit
Core type	EFD20	
Core material	N87	
Ae	31.00	mm^2
le	47.00	mm
Ve	1460.00	mm^3
AN	28.10	mm^2
In	40.20	mm
Wire ρ	1.8E-08	Ωm
Wire μ0	1.3E-06	H/m
Achievable Kf	0.65	

#### **Design Choices**

Parameter	Value	Unit (eq)
Selected Air-gap (lg)	0.15	mm
Wire dcu	0.43	mm (13)

#### **Evaluating Inductor Parameters**

Parameter	Value	Unit (eq)
N	14 (13.64)	Turns (14)
Bc(max)	0.22	T (15)
Acu per strand	1.45E-07	m^2 (16)
Np	9	Strands (17)
Acu per bundle	1.31E-06	m^2 (18)
Jmax	2.27	A/mm^2 (19)
Bundle Rw(dc)	7.7	mΩ (20)

### **Evaluating Steady-State Inductor Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.0	Ω	4.0	Ω	10.0	Ω
IL,rms	2.98	Α	2.13	Α	1.37	Α
ΔIL	1.33	Α	1.27	Α	1.09	Α
Bac	40.30	mT (21)	38.48	mT (21)	33.03	mT (21)
Pcu	68.67	mW (22)	35.08	mW (22)	14.51	mW (22)
Pv	8.99	mW (23)	8.01	mW (23)	5.47	mW (23)
Ptotal	77.66	mW (24)	43.09	mW (24)	19.98	mW (24)

## **Buck Conveter Design - Part III**

## **Specifications**

Parameter	Value	Unit
Max Vc	9.70	V
Max IC,rms	0.38	А
Max ΔIC=ΔIL	1.33	А
Ripple fs	100.00	kHz
Design ΔVo	1.00	%

## Minimum Capacitance to Meet ΔVo

Parameter	Value	Unit (eq)
Co(min)	17.14	μF (25)
ESR(max)	72.93	mΩ (26)

## **Selecting a Capacitor**

Parameter	Value	Unit
Manufacturer	Panasonic	
Series	TP	
Voltage rating	35	V
Capacitance Co	330	μF
ESR	52	mΩ
IC,rms rating	1.1	А

## **Evaluating Steady-State Capacitor Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.0	Ω	4.0	Ω	10.0	Ω
IC,rms	0.38	Α	0.37	Α	0.31	А
PC	7.5	mW (27)	7.1	mW (27)	5.0	mW (27)

### **Buck Conveter Design - Part IV**

#### **Specifications**

Parameter	Value	Unit
Max Vsw	15.00	V
Max Is,rms	1.98	Α
Max Isw,pk	3.63	A
Switching fs	100.00	kHz
Та	30.00	Degrees C

### **Selecting a N-Channel MOSFET**

Parameter	Value	Unit
Manufacturer	Infineon	
Model no	IPP052N06L3	
Vdss	60	V
ID(max)	80	А
tr	5	ns
tf	12	ns
Crss @ Max Vsw/2	175	pF
Vgs(Io)	3.6	V
Rds,on	3.9	mΩ
RthJA - no heatsink	62	C/W

#### **Gate Drive Details**

Parameter	Value	Unit (eq)
Design Vgg	15.00	V
Design Igg	1.00	А
Rg	15.00	Ω (28)

### **Evaluating Steady-State Switch Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.00	Ω	4.0	Ω	10.0	Ω
IL,avg	2.96	А	2.10	А	1.33	А
ls,rms	1.98	Α	1.68	A	1.16	А
ΔIL	1.33	Α	1.27	Α	1.09	Α
Is @ on	2.30	A (29)	1.47	A (29)	0.79	A (29)
Is @ off	3.63	A (30)	2.74	A (30)	1.88	A (30)
tvf	3.45	ns (31)	3.45	ns (31)	3.45	ns (31)
trv	10.93	ns (32)	10.93	ns (32)	10.93	ns (32)
ts,on	8.45	ns (33)	8.45	ns (33)	8.45	ns (33)
ts,off	22.93	ns (34)	22.93	ns (34)	22.93	ns (34)
Pswitching	77.00	mW (35)	56.44	mW (35)	37.34	mW (35)
Pconduction	15.30	mW (36)	11.01	mW (36)	5.25	mW (36)
Ptotal	92.30	mw (37)	67.45	mw (37)	42.59	mw (37)

#### **Evaluating Junction Temprature**

Parameter	Value	Unit (eq)
Tj,max	35.72	C (38)

## **Buck Conveter Design - Part V**

### **Specifications**

Parameter	Value	Unit (eq)
Max Vd	15.00	V
Max Id,avg	1.66	А
Switching fs	100.00	kHz
Та	30.00	Degrees C

### **Selecting a Diode**

Parameter	Value	Unit
Manufacturer	Vishay	
Model no	VS-MBR1045-M3	
Vr(max)	45	V
IF(max) - dual	10	A
VF	0.57	V
RthJA - D2Pak	70	C/W

Assuming same thermal resistance as the other diodes with same case

## **Evaluating Steady-State Switch Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load RL	2.00	Ω	4.0	Ω	10.0	Ω
IL,avg	2.96	А	2.10	А	1.33	А
D	43.88	%	62.07	%	71.85	%
ID,avg	1.66	A (39)	0.80	A (39)	0.37	A (39)
Pconduction	0.94	W (40)	0.46	W (40)	0.21	W (40)
Prr	0.00	W (41)	0.00	W (41)	0.00	W (41)
Ptotal	0.94	W (42)	0.94	W (42)	0.94	W (42)

### **Evaluating Junction Temprature**

Parameter	Value	Unit (eq)
Tj,max	95.80	C (43)

#### **Buck Converter Design - Part VI**

#### **Specifications**

Parameter	Value	Unit
Vout,nominal	9.70	V
Max Is,pk	3.63	А
Co	330.00	μF
ESR	52	mΩ
Switching fs	100.00	kHz
Max Td	5.00	%

#### **Oscilator Setup**

Parameter	Value	Unit (eq)
СТ	1	nF
RT	18k	kΩ
Td	320	ns

#### **Current Feedback Setup**

Parameter	Value	Unit (eq)
Rs	0.28	Ω (44)
RC filter - Rrc	100.00	Ω
RC filter - Crc	159.15	pF (45)

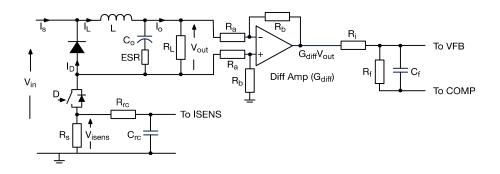
#### **Voltage Feedback Setup**

Parameter	Value	Unit (eq)
Tp(s) Pole fo @ 2Ω	241.14	Hz (46)
Tp(s) Zero fz @ 2Ω	9.27	kHz (47)
Tp(0) @ 2Ω	17.71	dB (48)
Design TOL(s) fcross	10.00	kHz
Tm(s)	1.00	
Required TOL(0) @ 2Ω	32.35	dB (49)
Required Tc(0)	14.63	dB (50)
Compensator Rf	22.00	kΩ
Compensator Cf	0.78	nF (51)
Compensator Ri	4.08	kΩ (52)
Diff Amp Gain Gdiff	0.26	Gain (53)

#### Hint:

It is strongly reccomended you plot the bode magnitude and phase response of the plant transfer function Tp(s) of the current controlled buck converter under the 2  $\Omega$  load condition using MATLAB prior to attempting the compensator design.

#### **Schematic of Controller**



### **Buck Converter Design Equations**

Eq. #	Equation
	$I_{OUT(MAX)} = \sqrt{\frac{V_{IN}I_{IN}\eta}{R_{LOAD}}}$
(1)	$V_{OUT} = I \times R_{LOAD}$
	$P_{OUT} = \frac{{V_{OUT}}^2}{R_{LOAD}}$
(2)	$P_{OUT} = \frac{V_{OUT(MAX)}^2}{R_{LOAD}}$
(3)	$I_{OUT} = \frac{V_{OUT}}{R_{LOAD}}$
	$D = \frac{V_{OUT}}{V_{IN} \times \eta}$
(4)	$R_{IN} = \frac{1}{D^2} \times R_{OUT}$
	$I_{IN} = \frac{V_{IN}}{R_{IN}}$
(5)	$D = \frac{V_{OUT}}{V_{IN} \times \eta}$
(6)	$V_{OUT} = I_{OUT} \times R_{OUT}$ ( $I_{OUT}$ is limited by $I_{OUT(MAX)}$ OR $V_{OUT(MAX)}$ )
(7)	$L_{min} = \frac{V_{OUT(MAX)}(1-D)T_S}{\Delta I_L}$
	Where: $\Delta I_L = 2I_{L(AVG)}$
(8)	$\Delta I_L = \frac{V_{OUT}(1-D)T_S}{L}$
(9)	$I_{L(peak)} = \frac{1}{2} \Delta I_L \times I_{L(AVG)}$
(10)	$I_{L(RMS)} = \sqrt{I_{L(AVG)} + \frac{\Delta I_L^2}{12}}$
(11)	$I_{S(RMS)} = \sqrt{\left(D\left[I_{L(AVG)}^2 + \frac{\Delta I_L^2}{12}\right]\right)}$

(12)	$I_{C(RMS)} = \frac{\Delta I_L}{\sqrt{(12)}}$
(13)	$d_{cu} \le 2\delta$ $\delta = \sqrt{\frac{\rho}{\pi \mu_0 \mu_r f}}$
(14)	$N = \sqrt{\frac{2l_g L}{A_e \mu_0}}$
(15)	$B_{C(MAX)} = \frac{N\mu_0 I_{MAX}}{2l_g}$
(16)	$A_{CU(STRAND)} = \pi \frac{d_{cu}^2}{4}$
(17)	$N_{CU} = \frac{K_f \cdot A_N}{N \cdot A_{CU}}$
(18)	$A_{CU(BUNDLE)} = N_P \times A_{CU(STRAND)}$
(19)	$J_{MAX} = rac{I_{RMS(MAX)}}{A_{CU(STRAND)}  imes 10^6} (\ln Amm^{-2})$
(20)	$R_{W(BUNDLE, DC)} = \frac{\rho \cdot N \cdot I_n}{A_{CU(BUNDLE)}}$
(21)	$B_{ac} = \frac{B_{MAX}}{I_{L(MAX)}} \times \frac{\Delta I_L}{2}$
(22)	$R_{w(DC)} = \frac{\rho N I_n}{A_{CU(BUNDLE)}}$ $P_{CU} = R_{w(DC)} \times I_{L(RMS)}^2$
	$P_V = k \cdot f^a \cdot B_{ac}{}^b$
	Where:
	$k = 1.5 \cdot 10^{-6}$
(23)	a = 1.3
	b = 2.5
	$P_{LOSS(AC)} = P_V \times V_e$
	Results given in $mW$
(24)	$P_{TOTAL} = P_{cu} + P_{LOSS(AC)}$
(25)	$C_{O(MIN)} \ge \frac{\Delta I_L T_s}{8\Delta V_o}$

(26)	$R_{ESR(MAX)} = \frac{\Delta V_o}{\Delta I_L}$
(27)	$P_C = I_{C(RMS)}^2 \times R_{ESR}$
(28)	$R_g = \frac{V_{gg}}{I_{gg}}$
(29)	$I_{S(ON)} = I_{L(AVG)} - \frac{\Delta I_L}{2}$
(30)	$I_{S(OFF)} = I_{L(AVG)} + \frac{\Delta I_L}{2}$
(31)	$t_{fv} = \left(V_{ds(OFF)} - R_{DS(ON)}I_{S(ON)}\right) \times \frac{R_g C_{rss(Vsoff/2)}}{V_{gg} - V_{gs(I_o)}}$
(32)	$t_{rv} = \left(V_{ds(OFF)} - R_{DS(ON)}I_{S(OFF)}\right) \times \frac{R_g C_{rss(Vsoff/2)}}{V_{gs(I_o)}}$
(33)	$T_{S(ON)} = t_r + t_{fv}$
(34)	$T_{S(OFF)} = t_f + t_{rv}$
(35)	$P_{SWITCHING} = \frac{V_{S(OFF)}f_s}{2} \times \left[I_{S(ON)}t_{S(ON)} + I_{S(OFF)}t_{S(OFF)}\right]$
(36)	$P_{CONDUCTION} = I_{S(RMS)}^2 \times R_{DS(ON)}$
(37)	$P_{TOTAL} = P_{CONDUCTION} + P_{SWITCHING}$
(38)	$T_{j(MAX)} = T_a + P_T \times R_{\theta j a}$
(39)	$I_{D(AVG)} = I_{L(AVG)}(1-D)$
(40)	$P_{CONDUCTION} = I_{D(AVG)} \cdot V_F$
(41)	$P_{rr} = V_R Q_{rr} f_s$
(42)	$P_{TOTAL} = P_{CONDUCTION} + P_{SWITCHING}$
(43)	$T_{j(MAX)} = T_a + P_T \times R_{\theta j a}$
(44)	$R_S = \frac{1}{I_{S(MAX)}}$
(45)	$C_{rc} = \frac{1}{2\pi R_c f_{cutoff}}$
(46)	$T_p(s) = \frac{R_L}{R_S} \times \frac{sC_{out}r_{esr} + 1}{sC_{out}R_L + 1}$
(47)	$f_p = \frac{1}{2\pi C_o R_L}$

(48)	$f_z = \frac{1}{2\pi C_o R_c}$
	$T_c(0) = log\left[\frac{f_{cross}}{f_p}\right] \times 20 - T_p(0)$
(49)	$T_p(0) = \frac{R_L}{R_s}$
	$T_{OL}(0) = T_p(0) \cdot T_c(0) \cdot T_m(0)$
(50)	$T_c(0) = log \left[ \frac{f_{cross}}{f_p} \right] \times 20 - T_p(0)$
(51)	$C_f = \frac{1}{2\pi f_p R_f}$
	Where: $f_p$ is set to cancel plant zero
(52)	$R_i = \frac{R_f}{10^{\frac{T_c(0)}{20}}}$
	Where: $T_c(0)$ is gain in dB
(53)	$G_{DIFF} = \frac{2.5}{V_{OUT(NOMINAL)}}$

## Pick-up Converter Design - Part I

## **Specifications**

Parameter	Value	Unit
Nominal Vout(avg)	15.00	V
Isc(rms)	1.17	Α
Voc(rms)	7.12	V
Winding L2	25.00	μН
Track f0	38.40	kHz

## **Evaluating Steady-State Operating Conditions**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load	10.00	Ω	15.00	Ω	25.00	Ω
lo	1.29	A (1)	1.00	A (2)	0.60	A (2)
Vout	12.87	V (3)	15.00	V (3)	15.00	V (3)
Ро	16.56	W (4)	15.00	W (4)	9.00	W (4)
D	0.00	% (5)	22.30	% (5)	53.38	% (5)
Qmax	1.99	(6)	2.32	(6)	2.32	(6)
Qavg	1.99	(7)	1.80	(7)	1.08	(7)

## **Evaluating Compensation Capacitor**

Parameter	Value	Unit (eq)
C2	0.67	μF (8)
Max V2	16.50	V (9)
Max IC2	2.67	A (10)

## Pick-up Converter Design - Part II

## **Specifications**

Parameter	Value	Unit
Max fs	1000.00	Hz
Nominal Vout	15.00	V
Max lout	1.29	Α
Design ΔVo	1.00	V,peak to peak

## Minimum Capacitance to Meet ΔVo

Parameter	Value	Unit (eq)
C(min)	324.89	μF (11)

### **Selecting a Capacitor**

Parameter	Value	Unit
Manufacturer	Panasonic	
Series	TP	
Voltage rating	25	V
Capacitance	470	μF
ESR	130	mΩ
IC,rms rating	1.1	A

### **Evaluating Steady-State Capacitor Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load	10.0	Ω	15.0	Ω	25.0	Ω
fs	0.0	Hz (12)	479.1	Hz (12)	688.1	Hz (12)
IC,rms	0.0	A (13)	0.5	A (13)	0.6	A (13)
PC	0.0	mW (14)	37.3	mW (14)	53.8	mW (14)

### **Evaluating Feedback Resistor Network**

Parameter	Value	Unit
Vref	4.00	V
Vo,opamp	15.00	V
Selected Rb	10.00	kΩ
Ra	14.33	kΩ (15)
Rf	214.95	kΩ (16)

E12 Series Values used in slides

## Pick-up Converter Design - Part III

### **Specifications**

Parameter	Value	Unit
Max IL(Avg)	1.29	А
Ripple fs	38.40	kHz
Design Bmax	0.25	Т
Design Jmax	5.00	A/mm^2

### **Core & Magnet Wire Details**

Parameter	Value	Unit
Core type	Drum15	
Al	0.052	μН
Ae	28.30	mm^2
AN	36.00	mm^2
In	31.50	mm
Wire ρ	1.8E-08	Ωm
Wire μ0	1.3E-06	H/m
Achievable Kf	0.70	

## **Design Choices**

Parameter	Value	Unit (eq)
Selected L	200.00	μН
Selected dcu	0.56	mm

## **Evaluating Inductor Parameters**

Parameter	Value	Unit (eq)
N	63	Turns (17)
Bc(max)	0.14	T (18)
Acu (1 strand)	2.46E-01	mm^2 (19)
Used Winding Area	22.17	mm^2 (20)
Jmax	5.24	A/mm^2 (21)
Bundle Rw(dc)	145.0	mΩ (22)

## **Evaluating Steady-State Inductor Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load	10.0	Ω	15.0	Ω	25.0	Ω
IL,rms	1.3	А	1.3	А	1.3	А
Pcu	241.34	mW (23)	241.34	mW (23)	241.34	mW (23)

## Pick-up Conveter Design - Part IV

### **Specifications**

Parameter	Value	Unit
Max Vsw	15.00	V
Max Is,rms	1.29	А
Та	30.00	Degrees C

### **Selecting a N-Channel MOSFET**

Parameter	Value	Unit
Manufacturer	infineon	
Model no	IPP052N06L3	
Vdss	60	V
ID(max)	80	Α
tr	5	ns
tf	12	ns
Crss @ Max Vsw/2	47	pF
Vgs(Io)	4.5	V
Rds,on	5	mΩ
RthJA - no heatsink	62	C/W

### **Gate Drive Details**

Parameter	Value	Unit (eq)
Design Vgg	15.00	V
Design Igg	0.10	А
Rg	150.00	Ω (24)

#### **Evaluating Steady-State Switch Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load	10.00	Ω	15.0	Ω	25.0	Ω
fs	0.00	Hz	479.09	Hz	688.09	Hz
ls,rms	0.00	Α	0.61	A	0.94	Α
ls @ on	0.00	A (25)	0.66	A (25)	0.39	A (25)
Is @ off	0.00	A (25)	1.91	A (25)	2.18	A (25)
tfv	10.07	ns (26)	10.07	ns (26)	10.07	ns (26)
trv	23.49	ns (27)	23.49	ns (27)	23.49	ns (27)
ts,on	15.07	ns (28)	15.07	ns (28)	15.07	ns (28)
ts,off	35.49	ns (29)	35.49	ns (29)	35.49	ns (29)
Pswitching	0.00	mW (30)	0.28	mW (30)	0.43	mW (30)
Pconduction	0.00	mw (31)	1.85	mw (31)	4.42	mw (31)
Ptotal	0.00	mw (32)	2.13	mw (32)	4.85	mw (32)

### **Evaluating Junction Temperature**

Parameter	Value	Unit (eq)
Tj,max	30.30	C (33)

## Pick-up Converter Design - Part V

## **Specifications**

Parameter	Value	Unit (eq)
Max Vd	15.00	V
Max Id,avg	1.29	А
Та	30.00	Degrees C

## **Selecting a Diode**

Parameter	Value	Unit
Manufacturer	Vishay	
Model no	VS-MBR:	1045-M3
Vr(max)	45	V
IF(max) - dual	10	А
VF	0.57	V
RthJA - D2Pak	n/a	C/W

## **Evaluating Steady-State Switch Losses**

Parameter	Value	Unit (eq)	Value	Unit (eq)	Value	Unit (eq)
Load	10.00	Ω	15.0	Ω	25.0	Ω
D	0.00	%	22.30	%	53.38	%
ID,avg	1.29	A (34)	1.00	A (34)	0.60	A (34)
Pconduction	0.73	W (35)	0.57	W (35)	0.34	W (35)
Prr	0.00	W (36)	0.00	W (36)	0.00	W (36)
Ptotal	0.73	W (37)	0.57	W (37)	0.34	W (37)

## **Evaluating Junction Temperature**

Parameter	Value	Unit (eq)	
Tj,max	75.00	C (38)	Approximation assuming similar RthJA to MOSFET

## **IPT Pick-up Design Equations**

	<u> </u>
Eq. #	Equation
(1)	Io (for $R_L < 11.66\Omega$ ) is the largest current possible:
	$I_{out} = 1.1I_{sc} \approx 1.29$
(2)	L (C. D. > 11.000)
(2)	lo (for $R_L \ge 11.66\Omega$ ):
	$I_{out} = rac{V_{out(nominal)}}{R_{Load}}$
	$R_{Load}$
(3)	Vout:
(3)	$V_{out} = I_{out}R_{Load}$
	out - Tout Load
(4)	Pout:
( )	2
	$P_{out} = \frac{V_{out}^2}{R_{Load}} = I_{out}^2 R_{Load} = V_{out} I_{out}$
	··Louu
(5)	Duty Cycle (D):
	$P_{out} = P_{max}(1 - D)$ $D = 1 - \frac{P_{out}}{P_{max}}$
	$D=1-\frac{1}{P_{max}}$
	Where Pmax is given by:
	$P_{max} = (1.1I_{sc} \times V_{out(nominal)})$
(6)	Qmax:
	$Q_{max} = \frac{1.1  V_{out}}{V_{oc}}$
	$V_{oc}$
(7)	Onum
(7)	Qavg:
	$Q_{avg} = \frac{P_{out}}{S_u} = \frac{V_{out}I_{out}}{V_{oc}I_{sc}}$
	$u v_{oc}$
(8)	C2 Compensation Capacitor:
(-)	Impedance matching to increase overall power:
	$j\omega L_2 = -\frac{1}{j\omega C_2}$
	Rearranging and solving, we are able to find C2:
	$C_2 = \left  \frac{1}{(i\omega)^2 L_2} \right $
	$G_2 =  (j\omega)^2 L_2 $
(9)	Max V2:
	We know that VC2 is the voltage before the rectifier stage and due to parallel
	compensation:
	$V_{out,nominal} = \frac{V_2}{1.1}$
	1.1
	Rearranging and solving we are able to find V2:
L	<u> </u>

	17 44 17
	$V_2 = 1.1 \cdot V_{out,nominal}$
(10)	Max IC2: $I_{c_2,max} = \frac{V_2}{Z_{C_2}} =  j2\pi f_0 \cdot C_2 \cdot V_2 $
(11)	Cmin can be found with the following formula: $C_{min}=C_{dc}>\frac{\pi I_{sc}}{8\sqrt{2}f_{s,max}\Delta V_{out}}$
(12)	fs (for $R \geq 11.66\Omega$ ): $f_s \approx \frac{\pi I_{sc}}{8\sqrt{2} \ C_{dc} \Delta V_{out}}$
	fs (for $R < 11.66\Omega$ , i. e. not sufficient to begin switching): $f_S = 0$
(13)	IC,rms: Given the two states of IC,rms when the switch is on and off: $I_{C,RMS} = \sqrt{\frac{1}{T_s}} \int_0^{DT_s} -I_{out}^2  dt + \int_{DT_s}^{T_s} (I_{dc} - I_{out})^2$
(14)	Capacitor power loss ( $P_{loss,C_{dc}}$ ): $P_{loss,C_{dc}} = I_{rms,C_{dc}}^2 \cdot R_{esr,C_{dc}}$
(15)	Evaluating feedback resistor network: $1.  \Delta V_{out} = V_{op} \frac{R_a}{R_f}$ $2.  V_{out,avg} = V_{ref} \frac{R_a R_b + R_f (R_a + R_b)}{R_f R_b} - V_{op} \frac{R_a}{2R_f}$ Rearranging both equations for Rf and equating we get the following equation: $V_{op} \frac{R_a}{\Delta V_{out}} = \frac{-V_{op} R_a R_b + 2V_{ref} R_a R_b}{2V_{out,avg} R_b + 2V_{ref} R_a + + 2V_{ref} R_b}$ Subbing in chosen $R_b = 10 k\Omega$ and solving for Ra.
(16)	Rf can be found by using '1.' from above solution: $R_f = V_{op} \frac{R_a}{\Delta V_{out}}$
(17)	N: $L = A_L \cdot N_i^2$ $N = \sqrt{\frac{L}{A_L}}$

$B_{c max } = \frac{LI_{Lavg}}{NA_e}$ $(19)  Single strand copper cross sectional area (Acu): \\ A_{cu} = \frac{\pi \frac{d^2_{cu}}{4}}{4}$ $(20)  Used winding area: \\ K_f = \frac{NA_{cu}}{A_N} \leq 1 \\ A_N = \frac{NA_{cu}}{K_f}$ $(21)  J_{max}: \qquad J_{max} = \frac{I_{RMS(max)}}{A_{cu}}$ $(22)  Bundle Rw (dc): \qquad R_{\omega(dc)} = \frac{\rho NI_n}{A_{cu}}$ $(23)  Steady-state wire losses (Pcu): \qquad P_{cu} = R_{\omega(dc)} \cdot I_{LRMS}^2$ $(24)  Gate driver resistance (Rg): \qquad I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2} \\ Is @ on: \qquad I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ $Vhere \Delta I_L \text{ is given by:} \qquad \Delta I_L = \frac{8 \Delta V_{out} Cdc}{T_s}$ $L_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$ $(26)  \text{tvf:} \qquad L_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		
$A_{cu} = \frac{\pi}{4} \frac{d^2_{cu}}{4}$ (20) Used winding area: $K_f = \frac{NA_{cu}}{A_N} \leq 1$ $A_N = \frac{NA_{cu}}{K_f}$ (21) Jmax: $J_{max} = \frac{I_{RMS(max)}}{A_{cu}}$ (22) Bundle Rw (dc): $R_{\omega(dc)} = \frac{\rho N l_n}{A_{cu}}$ (23) Steady-state wire losses (Pcu): $P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^2$ (24) Gate driver resistance (Rg): $R_g = \frac{V_{gg}}{I_{gg}}$ (25) Is @ on: $I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8 \Delta V_{out} C dc}{T_s}$ (26) tvf: $t_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(to)}}$	(18)	Bc(max):
$A_{cu} = \frac{\pi}{4} \frac{d^2_{cu}}{4}$ (20) Used winding area: $K_f = \frac{NA_{cu}}{A_N} \leq 1$ $A_N = \frac{NA_{cu}}{K_f}$ (21) Jmax: $J_{max} = \frac{I_{RMS(max)}}{A_{cu}}$ (22) Bundle Rw (dc): $R_{\omega(dc)} = \frac{\rho N l_n}{A_{cu}}$ (23) Steady-state wire losses (Pcu): $P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^2$ (24) Gate driver resistance (Rg): $R_g = \frac{V_{gg}}{I_{gg}}$ (25) Is @ on: $I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8 \Delta V_{out} C dc}{T_s}$ (26) tvf: $t_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(to)}}$		$B_{c[max]} = \frac{LI_{L,avg}}{I_{c[max]}}$
$A_{cu} = \frac{\pi  d_{cu}^2}{4}$ (20) Used winding area: $K_f = \frac{NA_{cu}}{A_N} \leq 1$ $A_N = \frac{NA_{cu}}{K_f}$ (21) Jmax: $J_{max} = \frac{I_{RMS(max)}}{A_{cu}}$ (22) Bundle Rw (dc): $R_{\omega(dc)} = \frac{\rho N l_n}{A_{cu}}$ (23) Steady-state wire losses (Pcu): $P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^2$ (24) Gate driver resistance (Rg): $R_g = \frac{V_{gg}}{I_{gg}}$ (25) Is @ on: $I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8  \Delta V_{out} C dc}{T_s}$ (26) tvf: $t_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(to)}}$		$NA_e$
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$J_{max} = \frac{I_{RMS(max)}}{A_{cu}}$ $(22)  \text{Bundle Rw (dc):} \qquad \qquad R_{\omega(dc)} = \frac{\rho N l_n}{A_{cu}}$ $(23)  \text{Steady-state wire losses (Pcu):} \qquad \qquad P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^2$ $(24)  \text{Gate driver resistance (Rg):} \qquad \qquad R_g = \frac{V_{gg}}{I_{gg}}$ $(25)  \text{Is @ on:} \qquad \qquad I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ $\text{Is @ off:} \qquad \qquad I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ $\text{Where } \Delta I_L \text{ is given by:} \qquad \qquad \Delta I_L = \frac{8  \Delta V_{out}  C  dc}{T_s}$ $(26)  \text{tvf:} \qquad \qquad t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g  C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$	(20)	Used winding area:
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$R_{\omega(dc)} = \frac{\rho N l_n}{A_{cu}}$ $P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^2$ $R_g = \frac{V_{gg}}{I_{gg}}$ $I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ $\text{Where } \Delta I_L \text{ is given by:}$ $\Delta I_L = \frac{8 \Delta V_{out} C dc}{T_s}$ $t_{vf} = (V_{sw} - R_{ds,ON} \cdot I_{s,ON}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$A_{cu}$
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(23) Steady-state wire losses (Pcu): $P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^{2}$ (24) Gate driver resistance (Rg): $R_{g} = \frac{V_{gg}}{I_{gg}}$ (25) Is @ on: $I_{s,on} = I_{L,avg} - \frac{\Delta I_{L}}{2}$ Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_{L}}{2}$ Where $\Delta I_{L}$ is given by: $\Delta I_{L} = \frac{8 \Delta V_{out} C dc}{T_{s}}$ (26) tvf: $t_{vf} = (V_{sw} - R_{ds,ON} \cdot I_{s,ON}) \frac{R_{g} C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$R_{\omega(dc)} = \frac{\rho N l_n}{\Lambda}$
$P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}^{2}$ $(24)  \text{Gate driver resistance (Rg):} \qquad \qquad$		$A_{cu}$
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$R_g = \frac{V_{gg}}{I_{gg}}$ $I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ $Where \Delta I_L \text{ is given by:}$ $\Delta I_L = \frac{8 \Delta V_{out} C dc}{T_S}$ $t_{vf} = (V_{sw} - R_{ds,oN} \cdot I_{s,oN}) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$P_{cu} = R_{\omega(dc)} \cdot I_{L,RMS}$
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$I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$ Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8 \ \Delta V_{out} C dc}{T_S}$ (26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,oN} \cdot I_{s,oN}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		*gg
Is @ off: $I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8  \Delta V_{out} C dc}{T_S}$ (26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,oN} \cdot I_{s,oN}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$	(25)	
$I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$ Where $\Delta I_L$ is given by: $\Delta I_L = \frac{8  \Delta V_{out} C dc}{T_S}$ (26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$I_{s,on} = I_{L,avg} - \frac{\Delta I_L}{2}$
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(26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$I_{s,on} = I_{L,avg} + \frac{\Delta I_L}{2}$
(26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		Whore AI is given by:
(26) tvf: $t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		
$t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$		$\Delta I_L = {T_S}$
$t_{vf} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,ON}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{gg} - V_{gs(io)}}$	(26)	tvf:
(27) tvr:		$V_{gg} = V_{gs(io)}$
	(27)	tvr:

	$t_{vr} = \left(V_{sw} - R_{ds,ON} \cdot I_{s,OFF}\right) \frac{R_g C_{rss,V_{sw}/2}}{V_{as(io)}}$
	$v_{vr} - (v_{sw} - R_{ds,oN} \cdot I_{s,off}) - V_{gs(io)}$
(28)	ts,on:
	$t_{s,on}=t_{ir}+t_{vf}$ Where ${ m t_{ir}}$ = current rise time and $t_{vf}$ = voltage fall time.
	where $t_{\rm ir}$ – current rise time and $t_{vf}$ – voltage ran time.
(29)	ts,off:
	$t_{s,off}=t_{if}+t_{vr}$ Where ${ m t_{if}}$ = current fall time and $t_{vr}$ = voltage rise time.
(30)	Pswitching:
	$P_{switching} = \frac{V_{s,off}f_s}{2} \left[ I_{s,on}t_{s,on} + I_{s,off}t_{s,off} \right]$
(31)	Pconduction:
	$P_{conduction} = \frac{1}{T_s} \int_0^{T_{s,on}} V_s I_s dt = I_{s,RMS}^2 \cdot R_{ds,on}$
(32)	Ptotal:
	$P_{total} = P_{switching} + P_{conduction}$
(33)	Tj,max:
	$T_j = T_a + P_T R_{\theta j a}$
(34)	ID,avg:
	$I_{D,avg} = (1 - D)I_{D,avg[MAX]}$
(35)	Pconduction loss:
	$P_{conduction} = (1 - D)V_F I_{L,avg}$
(36)	Reverse recovery loss (Prr):
	$P_{rr} pprox V_R Q_{rr} f_S$
	Where $Q_{rr}=I_{rr}\frac{t_{rr}}{2}$ However, due to the Schottky diode's physical make-up:
	$P_{rr(schottky)} = 0W$
(37)	Ptotal:
	$P_{total} = P_{conduction} + P_{rr}$
(38)	Tj,max:
	Similar to (33): $T_j = T_a + P_T R_{\theta j a}$

