

# Dimension Reduction in Polynomial Chaos Surrogates using Adaptive DGSM

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# POLYNOMIAL CHAOS EXPANSION

$$\mathcal{M}(x) \approx \mathcal{M}^{PC}(x) = \sum_{\alpha \in \mathcal{A}} c_{\alpha} \Psi_{\alpha}(x)$$

## Projection-based

$$c_{\alpha} = \mathbb{E}[\Psi_{\alpha}(x) \mathcal{M}(x)]$$

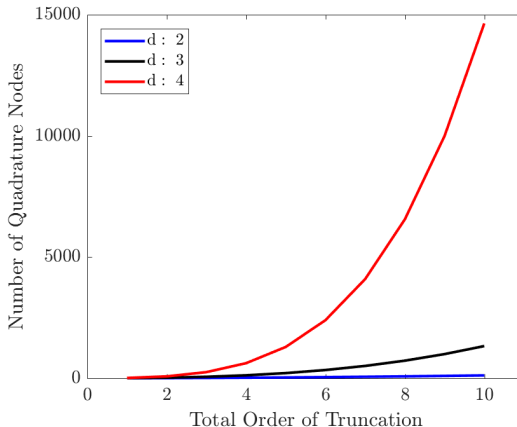
- ▶ Gaussian Quadrature
- ▶ Smolyak Sparse Quadrature
- ▶ Nested Quadrature

## Regression-based

$$\hat{c} = \operatorname{argmin} \mathbb{E} \left[ \left( c^T \Psi(x) - \mathcal{M}(x) \right)^2 \right]$$

- ▶ Ordinary Least-Squares
- ▶ Least Angle Regression
- ▶ Orthogonal Matching Pursuit

# MOTIVATION: DIMENSION REDUCTION



# MOTIVATION: DGSM

- Sensitivity analysis based on Sobol indices is commonly used to determine relative importance of the parameters.
- Sobol sensitivity indices are compute intensive:

$$\mathcal{T}(\theta_i) = \frac{\mathbb{E}_{\boldsymbol{\theta} \sim i}[\mathbb{V}_{\theta_i}(\mathcal{G}|\boldsymbol{\theta}_{\sim i})]}{\mathbb{V}(\mathcal{G})}$$

- Bounds on Sobol indices can be computed easily using DGSM and are shown to converge at a much faster rate.

# DGSM

- DGSM for Randomly distributed parameters [Sobol and Kucherenko, 2009]:

$$\mu_i = \mathbb{E} \left[ \left( \frac{\partial G(\mathbf{x})}{\partial x_i} \right)^2 \right]$$

where,

$$\frac{\partial G(\mathbf{x}^*)}{\partial x_i} = \lim_{\delta \rightarrow 0} \frac{[G(x_1^*, \dots, x_{i-1}^*, x_i^* + \delta, x_{i+1}^*, \dots, x_d^*) - G(\mathbf{x}^*)]}{\delta}$$

- Total number of model realizations required to compute  $\mu_i$  using  $N$  samples is  $N(d + 1)$ .

# BOUNDS ON SOBOL INDICES

- Upper bound ( $UB_i$ ) on Sobol Total Effect index ( $ST_i$ ) [Sobol and Kucherenko, 2009]:

$$ST_i \leq \frac{C_i \mu_i}{V} (\propto \hat{C}_i \mu_i)$$

$$\hat{C}_i \mu_i = \frac{C_i \mu_i}{\sum_i C_i \mu_i}$$

$C$ : Poincaré Constant     $V$ : Variance

- The Poincaré Constant is specific to a given probability distribution:

$\mathcal{U}[a, b]$	$(b - a)^2 / \pi^2$
$\mathcal{N}(\mu, \sigma^2)$	$\sigma^2$

# ALGORITHM: PARAMETER SCREENING

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1 Generate  $n_1$  points in  $\mathbb{R}^d$ ;
2 Compute  $UB_i$  for parameters  $\theta_i$  using  $n_1$  points;
   %  $NF = n_1(d+1)$ ,  $NF$ : Number of model realizations;
3 Rank Parameters ( $\theta_i$ ) based on  $UB_i$  estimates ( $\mathcal{R}^{old}$ );
4 set  $k = 1$  %  $k$ : Iteration counter;
5 repeat
6     Generate  $\beta n_1$  new points in  $\mathbb{R}^d$  ( $\beta n_1 \in \mathbb{Z}$ );
7     Compute  $UB_i^{new}$  using  $(1+\beta k)n_1$  points;
       %  $NF = (1+\beta k)n_1(d+1)$ ;
8     Rank Parameters based on  $UB_i^{new}$  estimates ( $\mathcal{R}^{new}$ );
9     if ( $\mathcal{R}^{new} = \mathcal{R}^{old}$ ) then
10         Compute:  $r_i = \frac{UB_i^{new}}{\max(UB_i^{new})}$ ;
11         Construct a set  $s = \{\theta_i \ni r_i < \alpha\}$ ;
12         Exit the loop;
13     end
14     set  $k = k + 1$ ;
15 until  $\mathcal{R}^{new} \neq \mathcal{R}^{old}$ ;
16 Construct a validation set:  $(\theta_j, \mathcal{M}(\theta_j))$ ,  $j=1, 2, \dots, NF$ ;

```

# REDUCED MORRIS FUNCTION

$$f(x) = \sum_{i=1}^4 b_i x_i + \sum_{i \leq j}^4 b_{ij} x_i x_j + \sum_{i \leq j \leq k=4}^4 b_{ijk} x_i x_j x_k$$

$$x_i \sim \mathcal{U}[0, 1]$$

$$b_i = \begin{bmatrix} 0.05 \\ 0.59 \\ 10 \\ 0.21 \end{bmatrix}, \quad b_{ij} = \begin{bmatrix} 0 & 80 & 60 & 40 \\ 0 & 30 & 0.73 & 0.18 \\ 0 & 0 & 0.64 & 0.93 \\ 0 & 0 & 0 & 0.06 \end{bmatrix}, \quad b_{ijk} = \begin{bmatrix} 0 & 10 & 0.98 & 0.19 \\ 0 & 0 & 0.49 & 50 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$



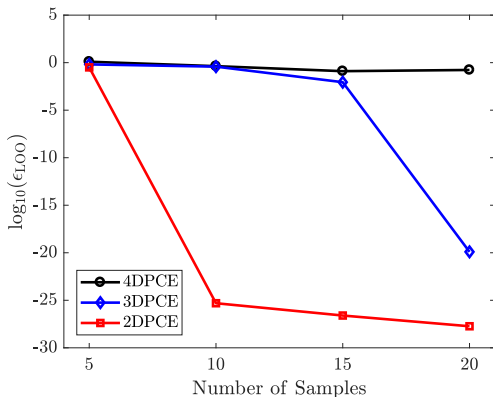
# PARAMETER SCREENING

$UB_i$ : 5 Samples	$UB_i$ : 10 Samples	$ST_i$ : $10^5$ Samples
$x_1$ : 1.4539	$x_1$ : 0.6926	$x_1$ : 0.4323
$x_2$ : 1.3303	$x_2$ : 0.6804	$x_2$ : 0.4051
$x_4$ : 0.3761	$x_4$ : 0.2531	$x_4$ : 0.1300
$x_3$ : 0.3374	$x_3$ : 0.1443	$x_3$ : 0.0928

# PCE CONVERGENCE

$$\epsilon_{LOO} = \frac{\sum_{i=1}^N (\mathcal{M}(\mathbf{x}^{(i)}) - \mathcal{M}^{PCE \setminus i}(\mathbf{x}^{(i)}))^2}{\sum_{i=1}^N (\mathcal{M}(\mathbf{x}^{(i)}) - \hat{\mu}_Y)^2}$$

$$\hat{\mu}_Y = \frac{1}{N} \sum_{i=1}^N \mathcal{M}(\mathbf{x}^{(i)})$$



- The PCE is constructed using Least Angle Regression with Latin Hypercube Sampling.

# PCE VERIFICATION

- Generate an independent set of validation points in the 4D input parameter space.
- Compute the following error:

$$\epsilon_{val} = \frac{\left[ \sum_{i=1}^N (\mathcal{M}(\mathbf{x}^{(i)}) - \mathcal{M}^{PCE}(\mathbf{x}^{(i)}))^2 \right]^{\frac{1}{2}}}{\left[ \sum_{i=1}^N (\mathcal{M}(\mathbf{x}^{(i)}))^2 \right]^{\frac{1}{2}}}$$

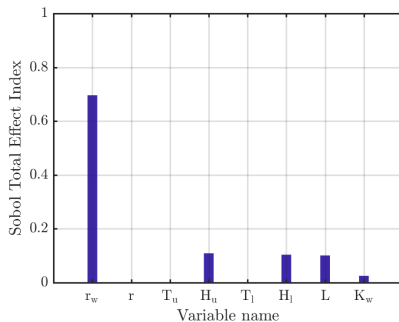
- $\epsilon_{val}$  was found to be  $\mathcal{O}(10^{-1})$  in the case of 4D PCE and 2D PCE constructed using 15 and 5 training points respectively.

# THE BOREHOLE FUNCTION

$$Q = \frac{2\pi T_u (H_u - H_l)}{\ln\left(\frac{r}{r_w}\right) \left(1 + \frac{2LT_u}{\ln\left(\frac{r}{r_w}\right) r_w^2 K_w} + \frac{T_u}{T_l}\right)}$$

$Q$ : Discharge of water through a borehole

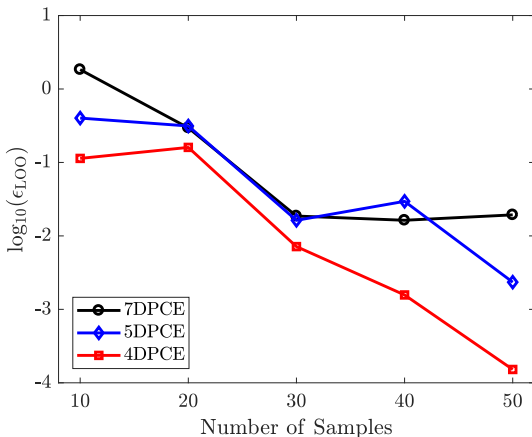
$r_w$	$\mathcal{N}(0.1, 0.016)$	Radius of the borehole (m)
$r$	$\log \mathcal{N}(7.71, 1.006)$	Radius of influence (m)
$T_u$	$\mathcal{U}[63070, 115600]$	Transmissivity of upper aquifer (m <sup>2</sup> /yr)
$H_u$	$\mathcal{U}[990, 1110]$	Potentiometric head of upper aquifer (m)
$T_l$	$\mathcal{U}[63.1, 116]$	Transmissivity of lower aquifer (m <sup>2</sup> /yr)
$H_l$	$\mathcal{U}[700, 820]$	Potentiometric head of lower aquifer (m)
$L$	$\mathcal{U}[1120, 1680]$	Length of borehole (m)
$K_w$	$\mathcal{U}[9855, 12045]$	Hydraulic conductivity of borehole (m/yr)



# PARAMETER SCREENING

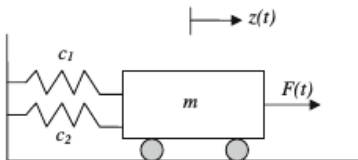
$UB_i$ : 5 Samples	$UB_i$ : 10 Samples	$UB_i$ : 15 Samples	$ST_i$ : $10^5$ Samples
$x_1$ : 0.2124	$x_1$ : 0.8671	$x_1$ : 0.8384	$x_1$ : 0.6942
$x_6$ : 0.0406	$x_3$ : 0.1505	$x_3$ : 0.1472	$x_3$ : 0.1062
$x_3$ : 0.0393	$x_5$ : 0.1505	$x_5$ : 0.1472	$x_5$ : 0.1059
$x_5$ : 0.0393	$x_6$ : 0.1466	$x_6$ : 0.1437	$x_6$ : 0.1026
$x_7$ : 0.0089	$x_7$ : 0.0337	$x_7$ : 0.0360	$x_7$ : 0.0250
$x_2$ : 0.0000	$x_2$ : 0.0000	$x_2$ : 0.0000	$x_2$ : 0.0000
$x_4$ : 0.0000	$x_4$ : 0.0000	$x_4$ : 0.0000	$x_4$ : 0.0000

# PCE CONVERGENCE AND VERIFICATION



- $\epsilon_{val}$  was found to be  $\mathcal{O}(10^{-2})$  in the case of 7D PCE and 4D PCE constructed using 60 and 30 training points respectively.

# NON-LINEAR OSCILLATOR

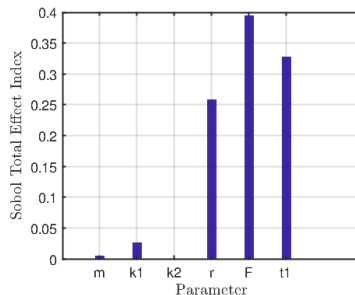


$m$	$\mathcal{N}(1,0.05)$	Mass
$k_1$	$\mathcal{N}(1,0.1)$	Spring Constant
$k_2$	$\mathcal{N}(0.1,0.01)$	Spring Constant
$r$	$\mathcal{N}(0.5,0.05)$	Displacement
$F$	$\mathcal{N}(1,0.2)$	Force
$t_1$	$\mathcal{N}(1,0.2)$	Time

**Limit State Function:**

$$g(\mathbf{X}) = 3r - \left| \frac{2F}{m\omega_0^2} \sin\left(\frac{\omega_0 t_1}{2}\right) \right|$$

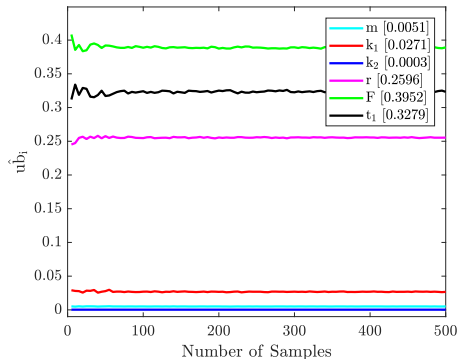
$$\mathbf{X} = \{m, k_1, k_2, r, F, t_1\} \quad \omega_0 = \sqrt{\frac{c_1 + c_2}{m}}$$



# PARAMETER RANK METRIC

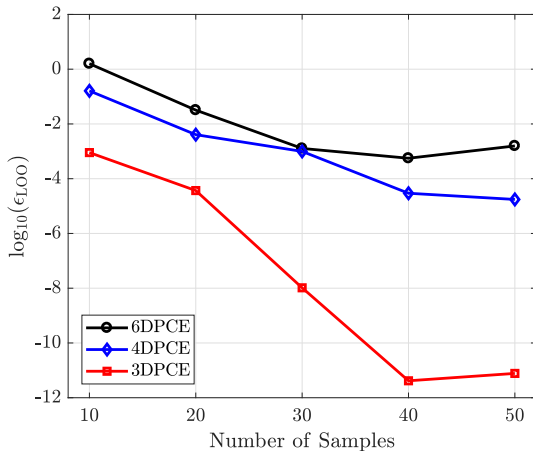
$$\hat{C}_i \mu_i = \frac{C_i \mu_i}{\sum_i C_i \mu_i}$$

$C$ : Poincaré Constant     $\mu_i$ : DGSM





# PCE CONVERGENCE

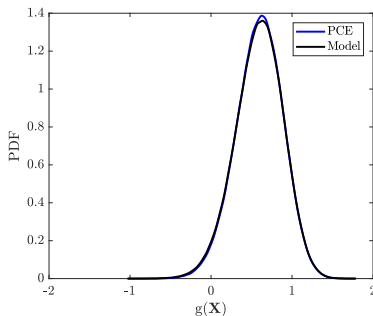


# PCE VERIFICATION

- Relative L-2 norm of the error is computed:

$$\epsilon_{val} = \frac{\left[ \sum_{i=1}^N \left( \mathcal{M}(x^{(i)}) - \mathcal{M}^{PCE}(x^{(i)}) \right)^2 \right]^{\frac{1}{2}}}{\left[ \sum_{i=1}^N \left( \mathcal{M}(x^{(i)}) \right)^2 \right]^{\frac{1}{2}}} \approx 8.35 \times 10^{-2}$$

- Comparison of PDFs:

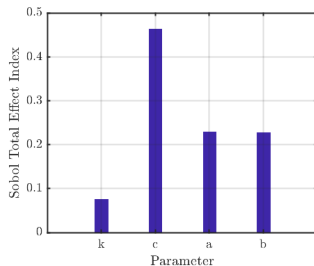
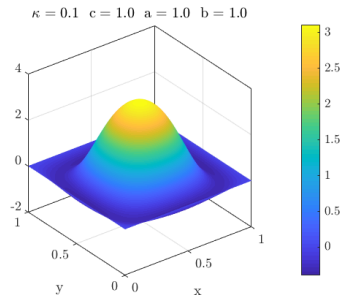


# ELLIPTIC PDE

$$-\kappa \Delta u + cu^3 = q$$

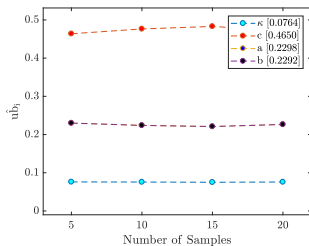
$$q = (-2\pi^2)(a \cos(2\pi x) \sin^2(\pi y) + b \cos(2\pi y) \sin^2(\pi x))$$

$\kappa$	$\mathcal{U}[0.09, 0.11]$
$c$	$\mathcal{U}[0.9, 1.1]$
$a$	$\mathcal{U}[0.9, 1.1]$
$b$	$\mathmathcal{U}[0.9, 1.1]$

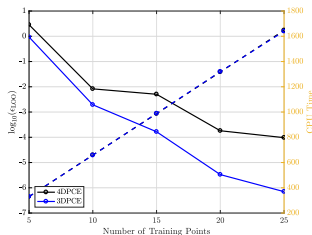


# ANALYSIS

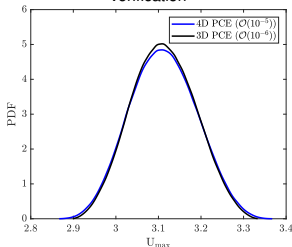
Parameter Screening



Convergence



Verification



# H<sub>2</sub>/O<sub>2</sub> REACTION MECHANISM

## ■ Reactions rates:

$$k = AT^n \exp(-E_a/RT)$$

$k$ : Reaction rate,  $A$ : Pre-Exponent

$E_a$ : Activation Energy

## ■ Uniform prior marginals:

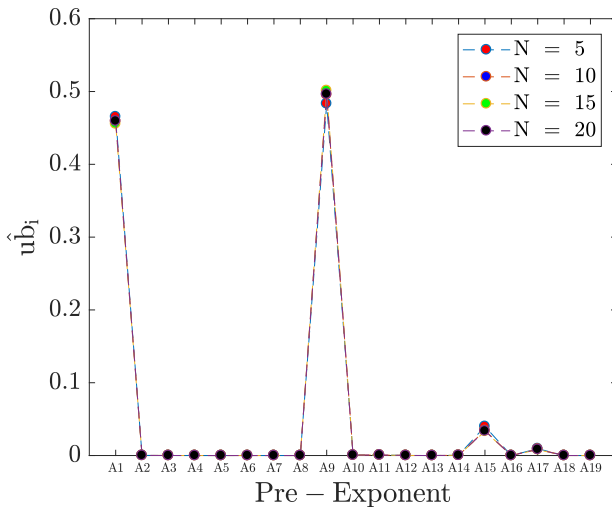
$$A_i \sim \mathcal{U}[0.9A_{i,\text{nom}}, 1.1A_{i,\text{nom}}]$$

$A_{i,\text{nom}}$ : Nominal value of the  $i^{\text{th}}$  Pre-Exponent

## ■ QoI: Ignition Delay

1.  $\text{H} + \text{O}_2 \rightleftharpoons \text{O} + \text{OH}$
2.  $\text{O} + \text{H}_2 \rightleftharpoons \text{H} + \text{OH}$
3.  $\text{H}_2 + \text{OH} \rightleftharpoons \text{H}_2\text{O} + \text{H}$
4.  $\text{OH} + \text{OH} \rightleftharpoons \text{O} + \text{H}_2\text{O}$
5.  $\text{H}_2 + \text{M} \rightleftharpoons \text{H} + \text{H} + \text{M}$
6.  $\text{O} + \text{O} + \text{M} \rightleftharpoons \text{O}_2 + \text{M}$
7.  $\text{O} + \text{H} + \text{M} \rightleftharpoons \text{OH} + \text{M}$
8.  $\text{H} + \text{OH} + \text{M} \rightleftharpoons \text{H}_2\text{O} + \text{M}$
9.  $\text{H} + \text{O}_2 + \text{M} \rightleftharpoons \text{HO}_2 + \text{M}$
10.  $\text{HO}_2 + \text{H} \rightleftharpoons \text{H}_2 + \text{O}_2$
11.  $\text{HO}_2 + \text{H} \rightleftharpoons \text{OH} + \text{OH}$
12.  $\text{HO}_2 + \text{O} \rightleftharpoons \text{O}_2 + \text{OH}$
13.  $\text{HO}_2 + \text{OH} \rightleftharpoons \text{H}_2\text{O} + \text{O}_2$
14.  $\text{HO}_2 + \text{HO}_2 \rightleftharpoons \text{H}_2\text{O}_2 + \text{O}_2$
15.  $\text{H}_2\text{O}_2 + \text{M} \rightleftharpoons \text{OH} + \text{OH} + \text{M}$
16.  $\text{H}_2\text{O}_2 + \text{H} \rightleftharpoons \text{H}_2\text{O} + \text{OH}$
17.  $\text{H}_2\text{O}_2 + \text{H} \rightleftharpoons \text{HO}_2 + \text{H}_2$
18.  $\text{H}_2\text{O}_2 + \text{O} \rightleftharpoons \text{OH} + \text{HO}_2$
19.  $\text{H}_2\text{O}_2 + \text{OH} \rightleftharpoons \text{HO}_2 + \text{H}_2\text{O}$

# DERIVATIVE-BASED SENSITIVITY MEASURES



# PCE VERIFICATION

- Relative L-2 norm of the error is computed:

$$\epsilon_{val} = \frac{\left[ \sum_{i=1}^N \left( \mathcal{M}(\mathbf{x}_{19D}^{(i)}) - \mathcal{M}^{PCE}(\mathbf{x}_{2D}^{(i)}) \right)^2 \right]^{\frac{1}{2}}}{\left[ \sum_{i=1}^N \left( \mathcal{M}(\mathbf{x}_{19D}^{(i)}) \right)^2 \right]^{\frac{1}{2}}} \approx 3.35 \times 10^{-2}$$