



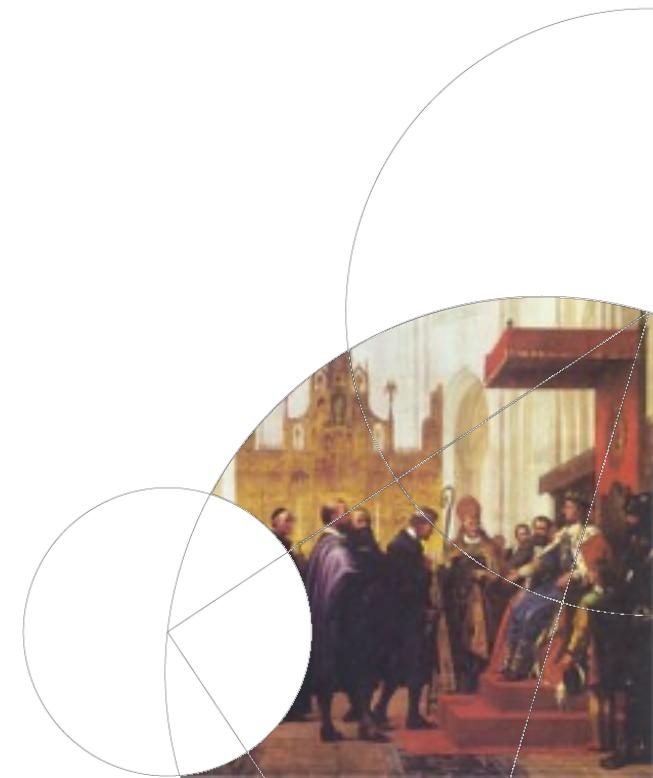
Faculty of Science

Computational Astrophysics

2b. Hydrodynamics Riemann Solvers, shocks, and AMR

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Topics today

- ❑ Overview of hydrodynamics
- ❑ Jump conditions and shock properties
- ❑ Shocks and Riemann solver
- ❑ Consistency and Approximate solvers
- ❑ **Assignment 2b:**
 - Blast wave
- ❑ Adaptive Mesh Refinement



Hydrodynamics

- Hydrodynamics describes the evolution of a fluid.
- Many formulations exist depending on the subject, but in astrophysics we normally consider the compressible Euler equations
- These are governed by three conservation principles for mass, momentum, and energy

$$\partial_t \rho + \nabla \cdot [\rho \mathbf{v}] = 0$$

$$\partial_t \rho \mathbf{v} + \nabla \cdot [\rho \mathbf{v} \otimes \mathbf{v} + P \mathbf{I}] = 0$$

$$\partial_t E + \nabla \cdot [(E + P) \mathbf{v}] = 0$$

- E is the total energy: $E = \rho e_{int} + \frac{1}{2} \rho v^2$, with equation of state $P(\rho, T)$
- The difficulty with solving these equations comes predominantly from the Navier-Stokes equation that is non-linear in the velocity. This is what generates the rich structure seen in e.g. turbulent flows and enables shocks.



Why do shocks occur in nature?

What is a shock?

Shocks are in some sense very non-linear waves. They occur due to two reasons:

- Wave steepening related to the density dependence of the speed of sound: higher density → higher temperature → higher sound speed. Upper crest gradually overtakes (weak shock)

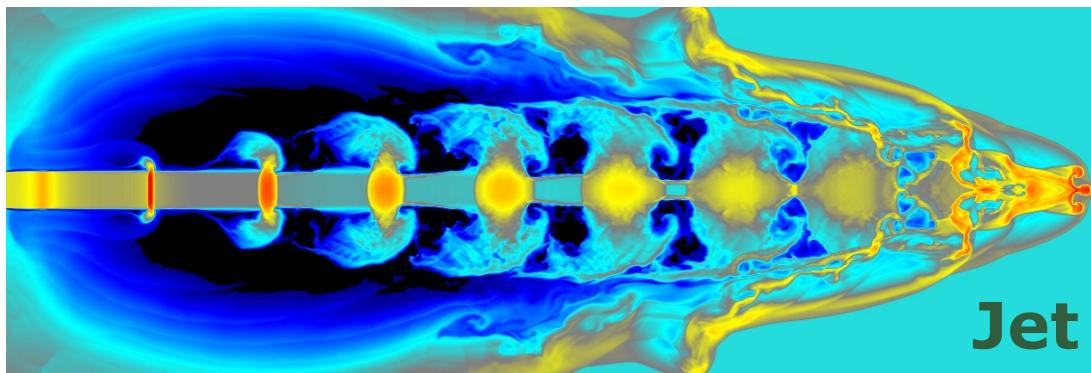
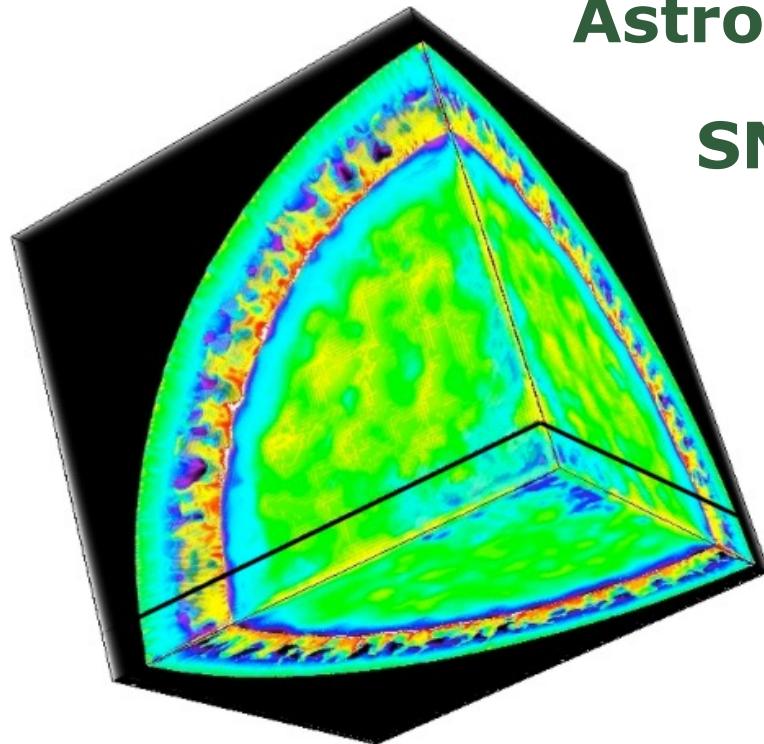
- Failure of the fluid to communicate about a discontinuity – supersonic shocks (strong shocks)

- End result: *kinetic energy is converted to heat*

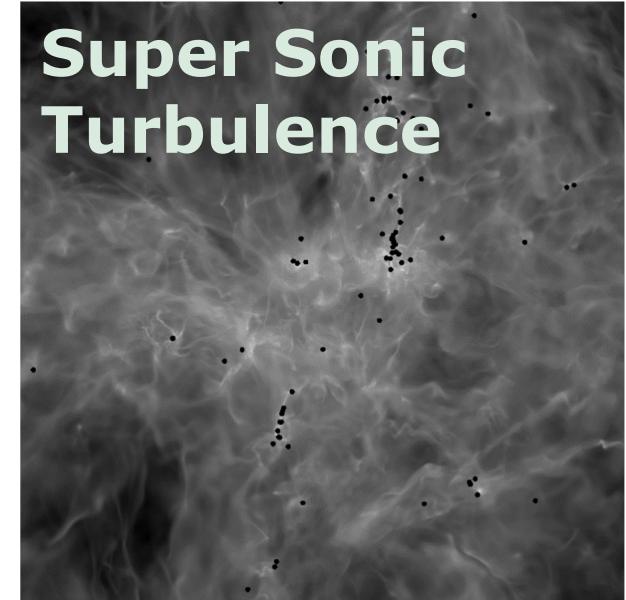


Astrophysics is full of shocks

SN remnant



Jet



Super Sonic
Turbulence

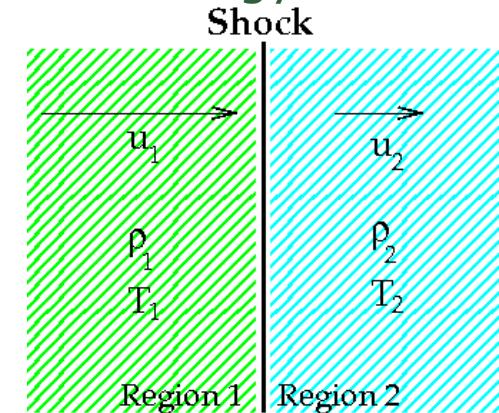
How to calculate shock properties

- Start with the conservation of mass, momentum, and energy:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0$$

$$\frac{\partial \rho \vec{u}}{\partial t} + \nabla \cdot (\rho \vec{u} \vec{u} + P \vec{I}) = 0$$

$$\frac{\partial E_{tot}}{\partial t} + \nabla \cdot ((E_{tot} + P) \vec{u}) = 0, \quad E_{tot} = \rho e + \frac{1}{2} \rho \vec{u}^2$$



- Assume we are in the rest-frame of the shock, then the flux is zero, and we get the **shock-jump or Rankine-Hugoniot conditions**

$$\rho_1 u_1 = \rho_2 u_2$$

$$\rho_1 u_1^2 + P_1 = \rho_2 u_2^2 + P_2$$

$$u_1 \left(\rho_1 e_1 + \frac{1}{2} \rho_1 u_1^2 + P_1 \right) = u_2 \left(\rho_2 e_2 + \frac{1}{2} \rho_2 u_2^2 + P_2 \right)$$

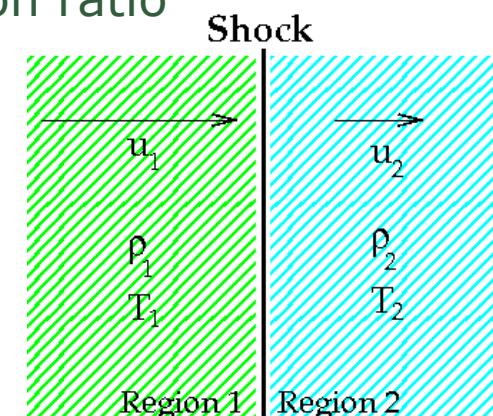
How to calculate (adiabatic) shock properties

- This can be used to calculate e.g. the compression ratio

$$\frac{\rho_2}{\rho_1} = \frac{P_2 + m^2 P_1}{P_1 + m^2 P_2}, \quad m = \frac{\gamma - 1}{\gamma + 1}$$

$\gamma = \frac{5}{3}$: max compression is 4

$\gamma = 1$: max compression is infinite



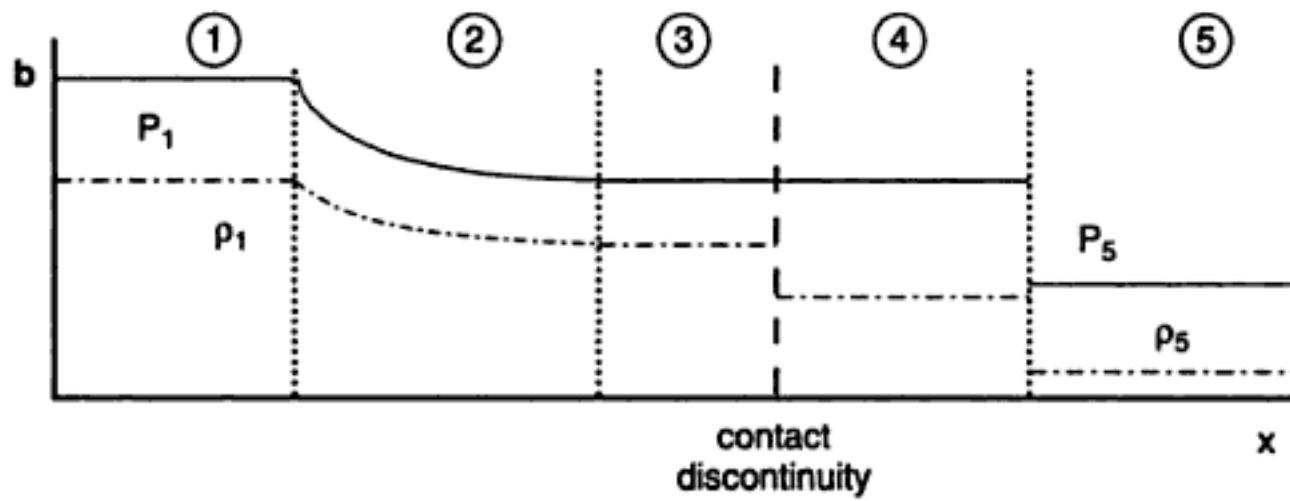
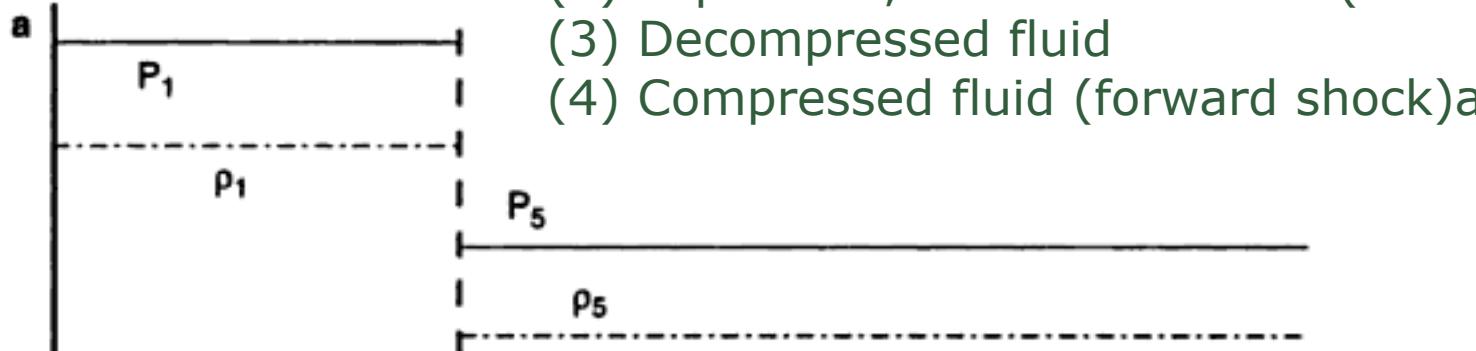
- In a moving shock, the shock speed can also be calculated
- Shocks are often characterized by the Mach number, the ratio between the shock speed and the upstream (or incoming) sound speed

$$M = \frac{u_1}{c_{s,1}}, \quad c_s^2 = \gamma \frac{P}{\rho}$$

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma + 1)M_1^2}{2 + (\gamma - 1)M_1^2}$$

HD shock structure in general (between two cells)

- (1)+(5) undisturbed fluid
- (2) expansion; rarefaction wave (reverse shock)
- (3) Decompressed fluid
- (4) Compressed fluid (forward shock)

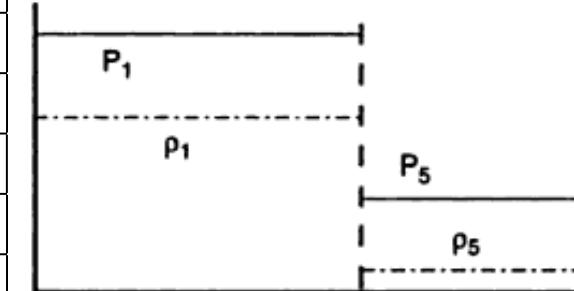


(see also fig. 6.5 in the book)

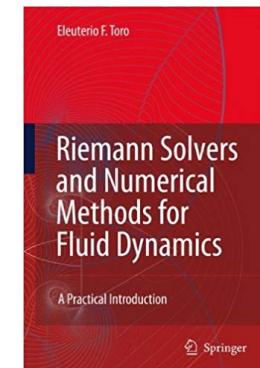


Shocks as a probe of numerical methods

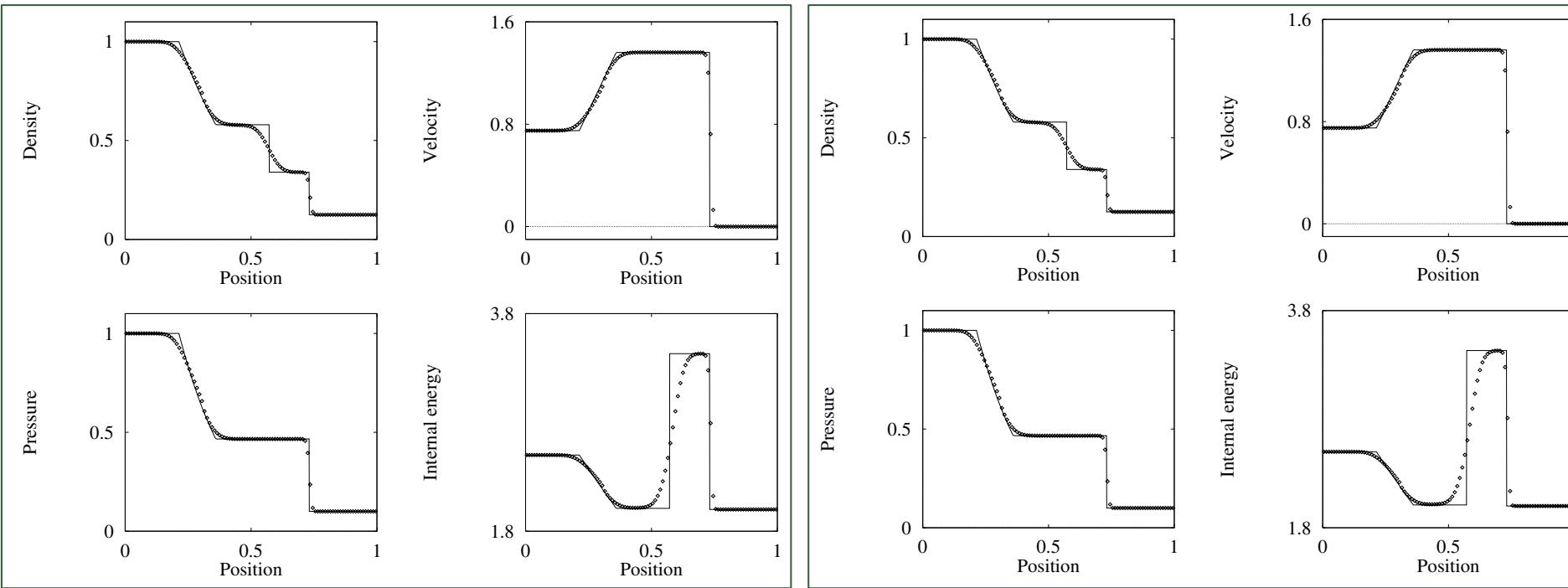
Test	ρ_L	u_L	p_L	ρ_R	u_R	p_R
1	1.0	0.75	1.0	0.125	0.0	0.1
2	1.0	-2.0	0.4	1.0	2.0	0.4
3	1.0	0.0	1000.0	1.0	0.0	0.01
4	5.99924	19.5975	460.894	5.99242	-6.19633	46.0950
5	1.0	-19.59745	1000.0	1.0	-19.59745	0.01
6	1.4	0.0	1.0	1.0	0.0	1.0
7	1.4	0.1	1.0	1.0	0.1	1.0



- Shock Tubes has long been a way to test numerical methods
- It is possible with iterative methods to find the exact solution to the shock problem
- Alternative is to run a code at high resolution
- Good selection of problem's given in Toro's book
<https://link.springer.com/book/10.1007/b79761>
 Free PDF(!) when downloaded on KU premise.



Shocks as a probe of numerical methods



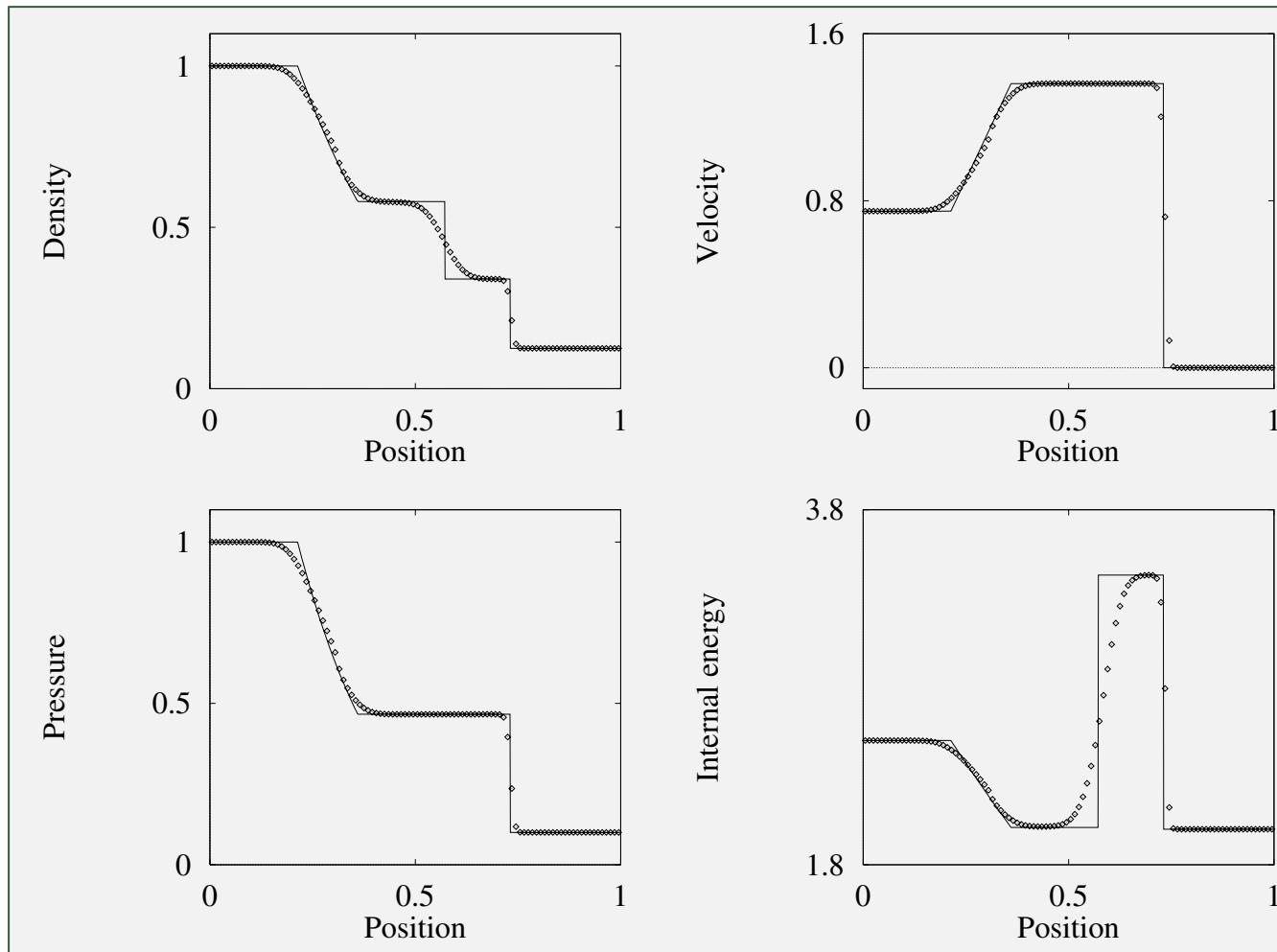
HLLC solver

HLL solver

Test	ρ_L	u_L	p_L	ρ_R	u_R	p_R
1	1.0	0.75	1.0	0.125	0.0	0.1



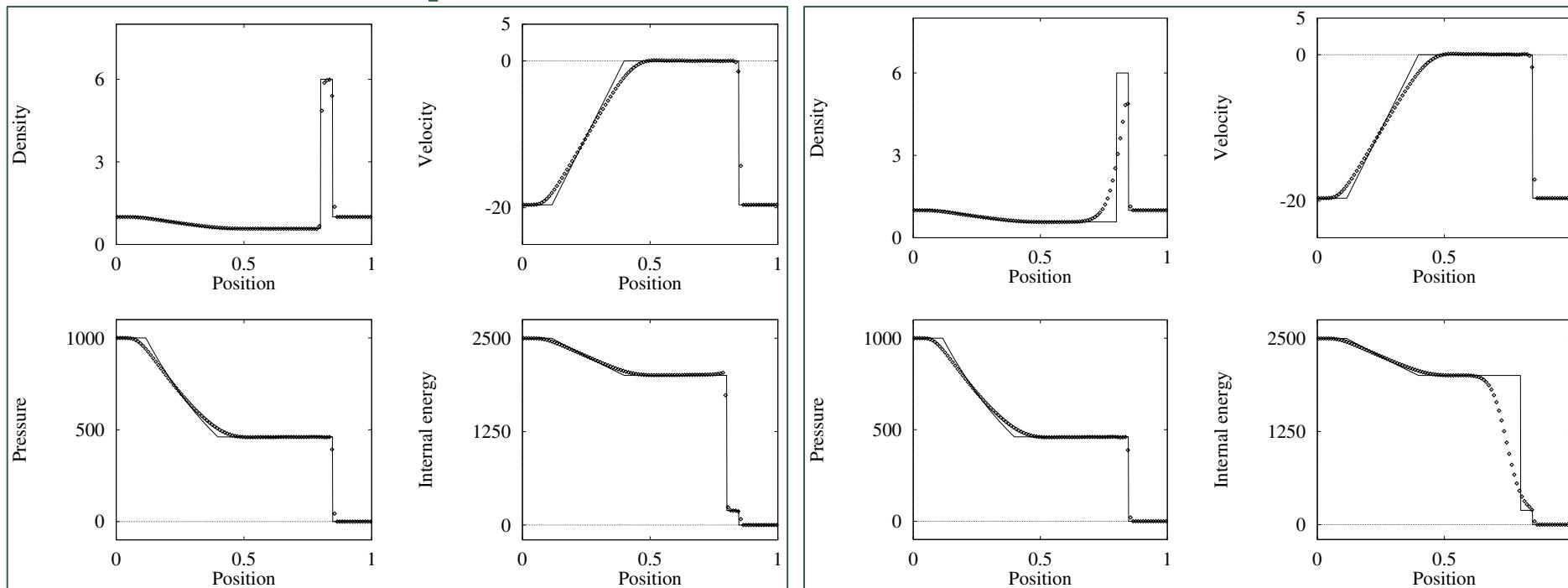
Shocks as a probe of numerical methods



Test	ρ_L	u_L	p_L	ρ_R	u_R	p_R
1	1.0	0.75	1.0	0.125	0.0	0.1



Shocks as a probe of numerical methods



HLLC solver

HLL solver

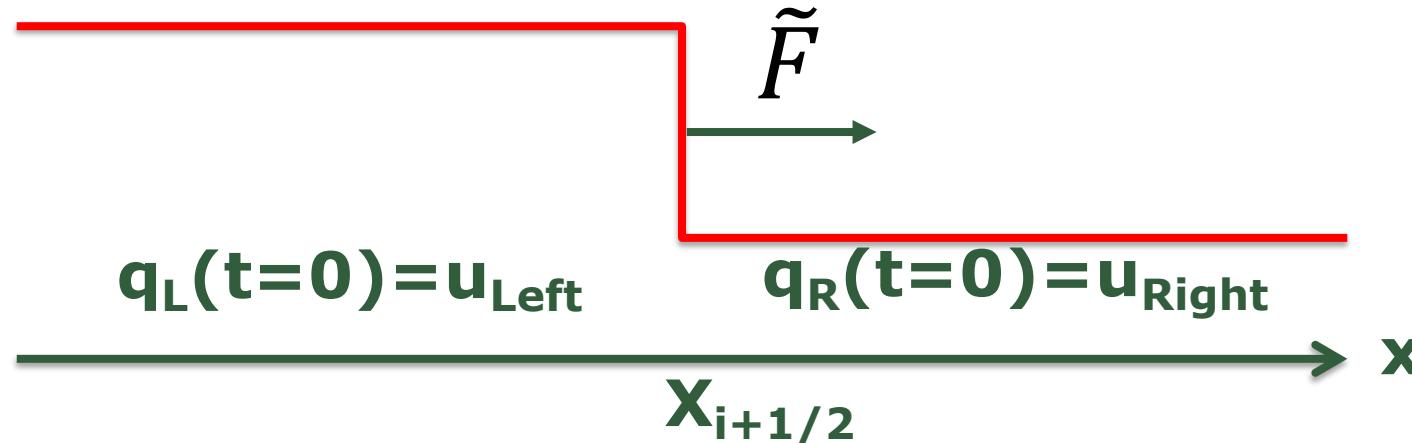
Test	ρ_L	u_L	p_L	ρ_R	u_R	p_R
5	1.0	-19.59745	1000.0	1.0	-19.59745	0.01



Godunov method

- ❑ Exploit the wave nature and full conservation properties of the equations and find the flux through a cell interface
- ❑ Use the flux to update the values in the cells

$$\tilde{F}_{i+1/2}^{n+1/2} = \frac{1}{\Delta t} \int_t^{t+\Delta t} dt F_{i+1/2}[q(x_{i+1/2})]$$

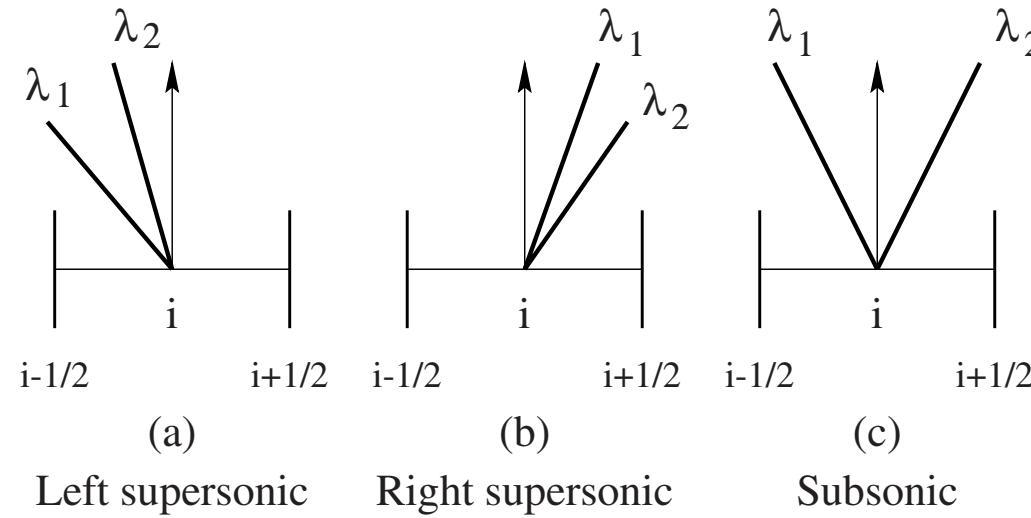


Godunov method

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$$\tilde{F}_{i+1/2}^{n+1/2} = \frac{1}{\Delta t} \int_t^{t+\Delta t} dt F_{i+1/2}[q(x_{i+1/2})]$$

- Flux depends on wave speeds



Comp. Astro.
Slide 14

Fig. 8.2. Possible flow patterns in cell I_i at time n : (a) supersonic flow to the left
 (b) supersonic flow to the right (c) subsonic flow



Approximate Riemann Solvers – HLL

```
# HLL (Harten, Lax, van Leer) is a bit less diffuse.
# We compute individual wave speeds for each state
# ql, qr are state vectors for the _primitive_ variables
def HLL(ql,qr):
    # sound speed for each side of interface (l==left, r==right)
    c_left = (ql.gamma*ql.P / ql.D)**0.5
    c_right = (qr.gamma*qr.P / qr.D)**0.5
    c_max = np.maximum(c_left,c_right)

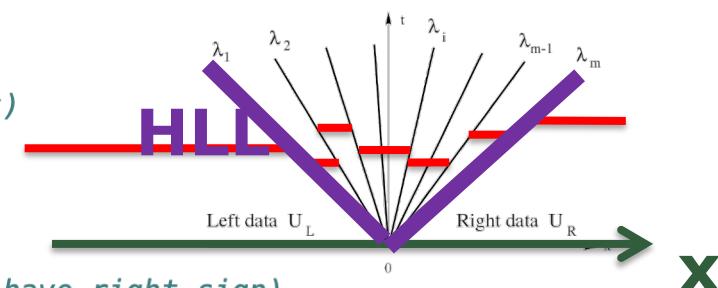
    # maximum wave speeds to the left and right (guaranteed to have right sign)
    SL = np.minimum(np.minimum(ql.U,qr.U)-c_max,0) # <= 0.
    SR = np.maximum(np.maximum(ql.U,qr.U)+c_max,0) # >= 0.

    # Hydro conservative variable
    Ul = primitive_to_conservative(ql)
    Ur = primitive_to_conservative(qr)

    # Hydro fluxes
    Fl = Hydro_Flux(ql,Ul)
    Fr = Hydro_Flux(qr,Ur)

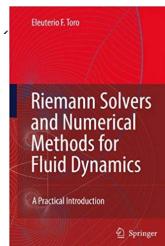
    # HLL flux based on wavespeeds. If SL < 0 and SR > 0 then mix state appropriately
    # The general form is
    #    $(SR * F_{left} - SL * F_{right} + SL * SR * (U_{right} - U_{left})) / (SR - SL)$ 
    # where U is the state vector of the conserved variables
    Flux = void()
    Flux.D = (SR*Fl.D - SL*Fr.D + SL*SR*(Ur.D - Ul.D)) / (SR - SL)
    Flux.mU = (SR*Fl.mU - SL*Fr.mU + SL*SR*(Ur.mU - Ul.mU)) / (SR - SL)
    # Flux.Etot = ...

    return Flux
```



Approximate Riemann Solvers – HLL

$$\int_{x_L}^{x_R} \mathbf{U}(x, T) dx = \int_{x_L}^{x_R} \mathbf{U}(x, 0) dx + \int_0^T \mathbf{F}(\mathbf{U}(x_L, t)) dt - \int_0^T \mathbf{F}(\mathbf{U}(x_R, t)) dt$$



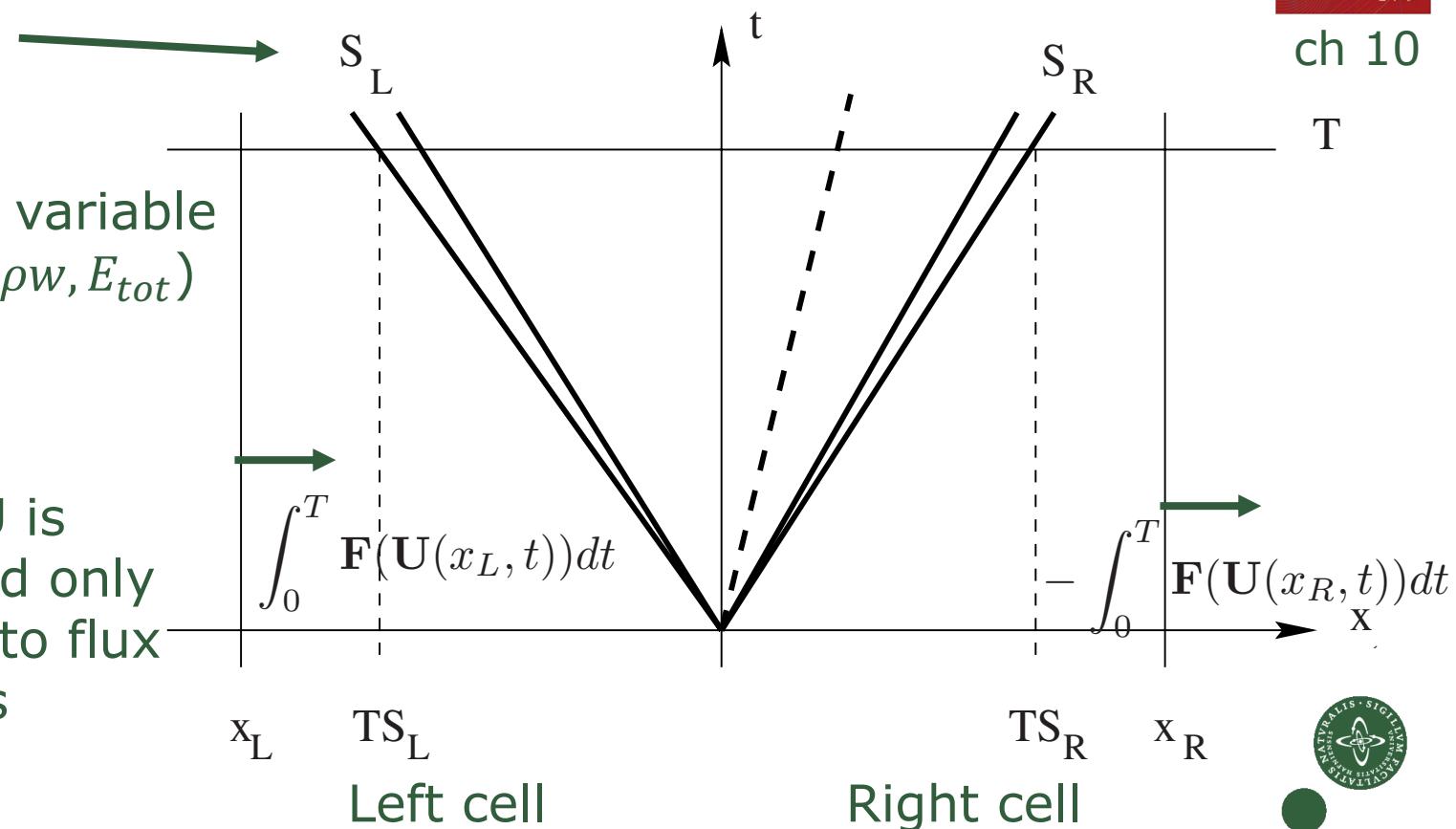
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Fastest speed

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Strategy:

Exploit that U is conserved and only changes due to flux at boundaries



Approximate Riemann Solvers – HLL

$$\int_{x_L}^{x_R} \mathbf{U}(x, T) dx = \int_{x_L}^{x_R} \mathbf{U}(x, 0) dx + \int_0^T \mathbf{F}(\mathbf{U}(x_L, t)) dt - \int_0^T \mathbf{F}(\mathbf{U}(x_R, t)) dt$$

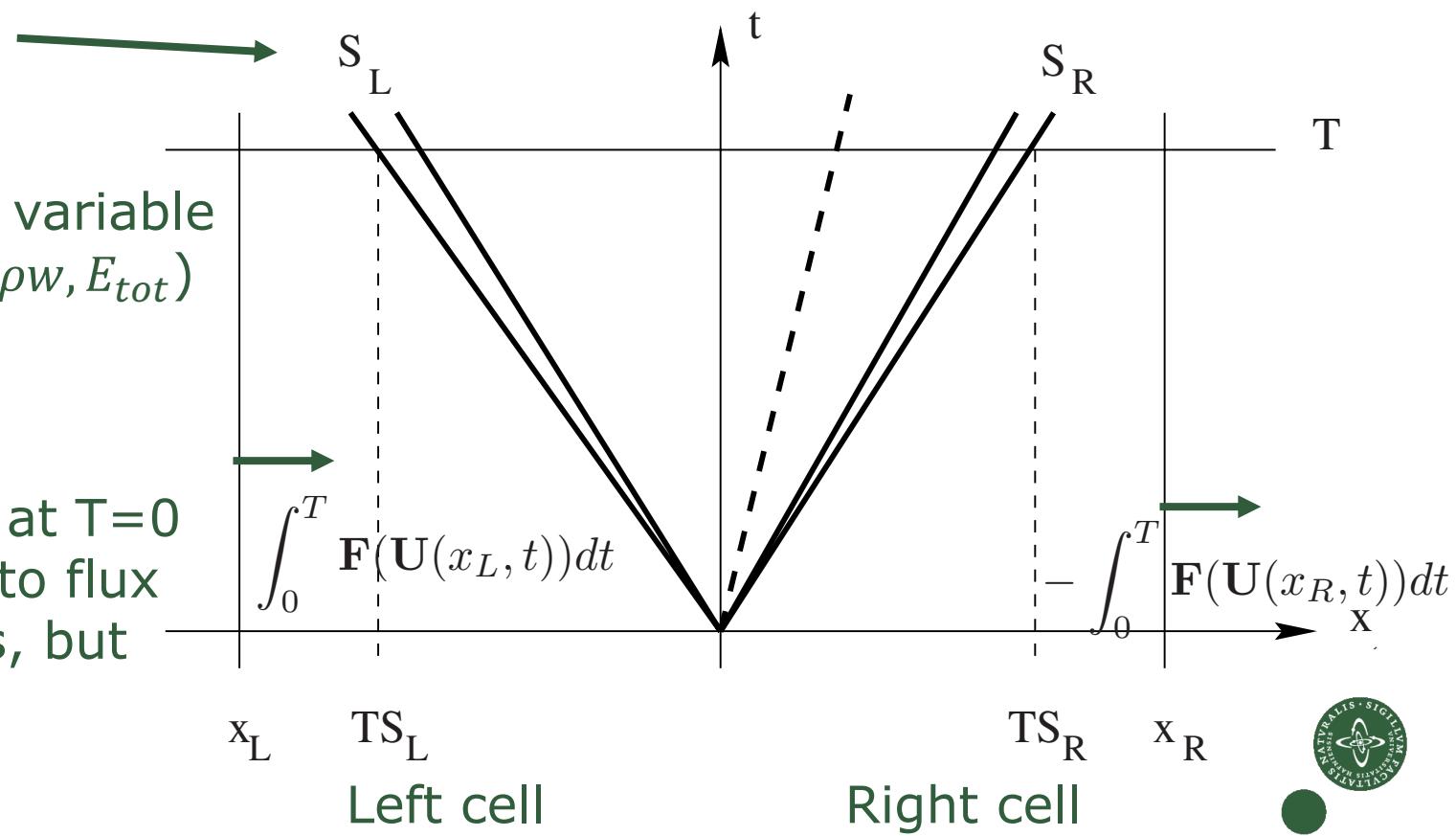
$$= x_R \mathbf{U}_R - x_L \mathbf{U}_L + T(\mathbf{F}_L - \mathbf{F}_R)$$

Fastest speed

\mathbf{U} : conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 \mathbf{F} : flux for \mathbf{U}

Integrals:

\mathbf{U} is constant at $T=0$
 changes due to flux at boundaries, but
 \mathbf{U} constant at boundaries



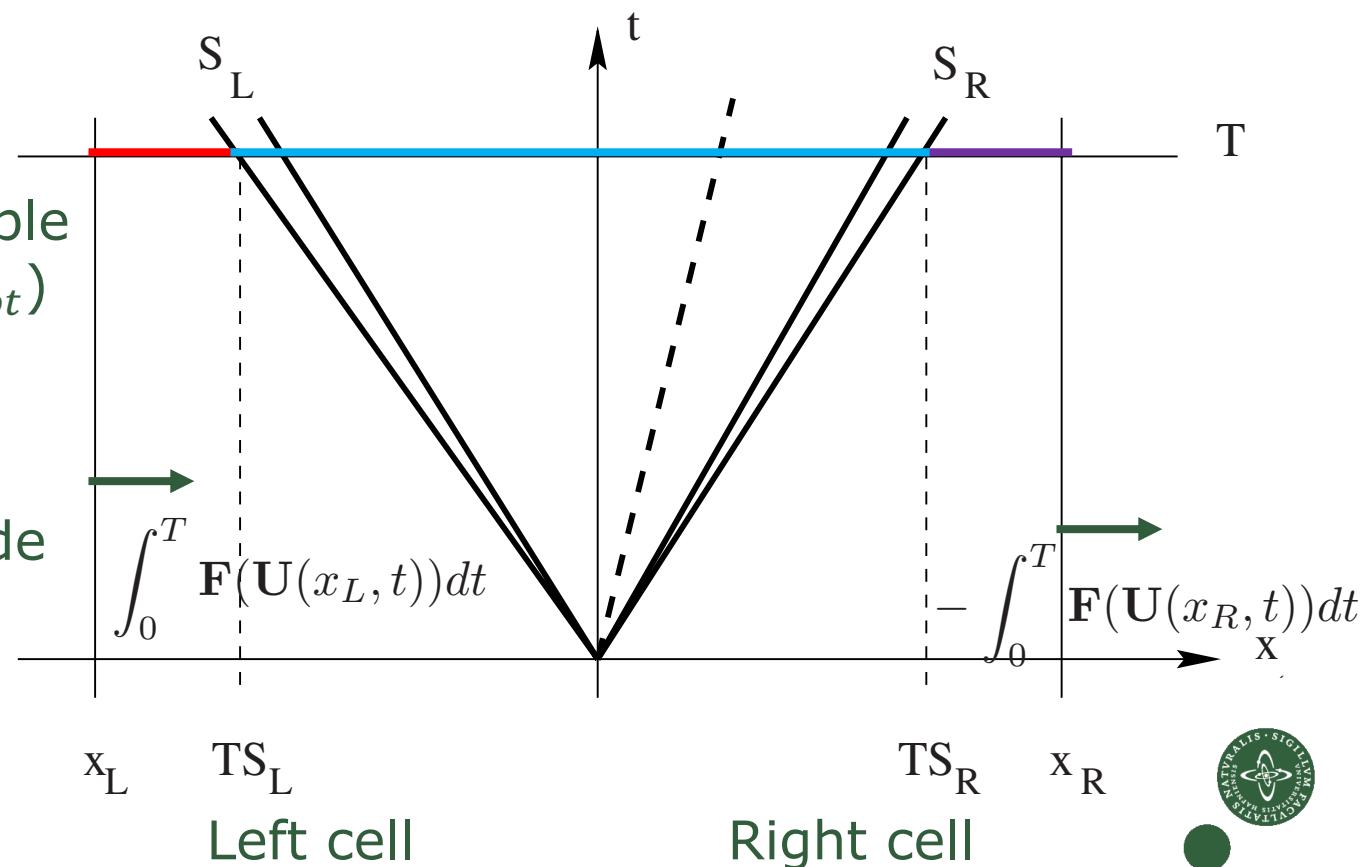
Approximate Riemann Solvers – HLL

$$\int_{x_L}^{x_R} \mathbf{U}(x, T) dx = \underbrace{\int_{x_L}^{TS_L} \mathbf{U}(x, T) dx}_{\text{Red}} + \underbrace{\int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx}_{\text{Blue}} + \underbrace{\int_{TS_R}^{x_R} \mathbf{U}(x, T) dx}_{\text{Purple}}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Spatial integrals:

U is constant outside
 $[S_L: S_R]$ -cone



Approximate Riemann Solvers – HLL

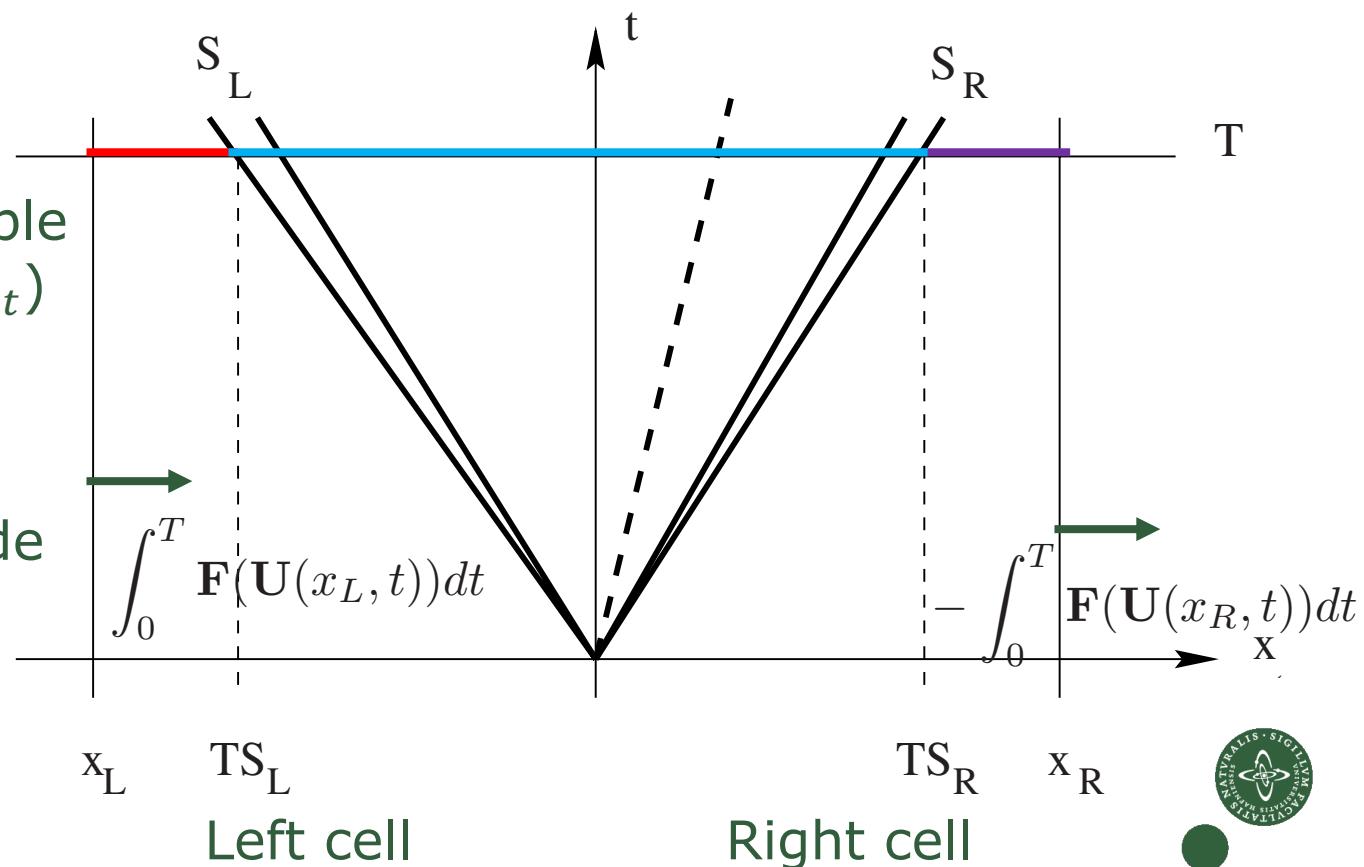
$$\int_{x_L}^{x_R} \mathbf{U}(x, T) dx = \underbrace{\int_{x_L}^{TS_L} \mathbf{U}(x, T) dx}_{\text{Red}} + \underbrace{\int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx}_{\text{Blue}} + \underbrace{\int_{TS_R}^{x_R} \mathbf{U}(x, T) dx}_{\text{Purple}}$$

$$= \underbrace{\int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx}_{\text{Blue}} + \underbrace{(TS_L - x_L)\mathbf{U}_L}_{\text{Red}} + \underbrace{(x_R - TS_R)\mathbf{U}_R}_{\text{Purple}}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Spatial integrals:

U is constant outside
 $[S_L: S_R]$ -cone



Approximate Riemann Solvers – HLL

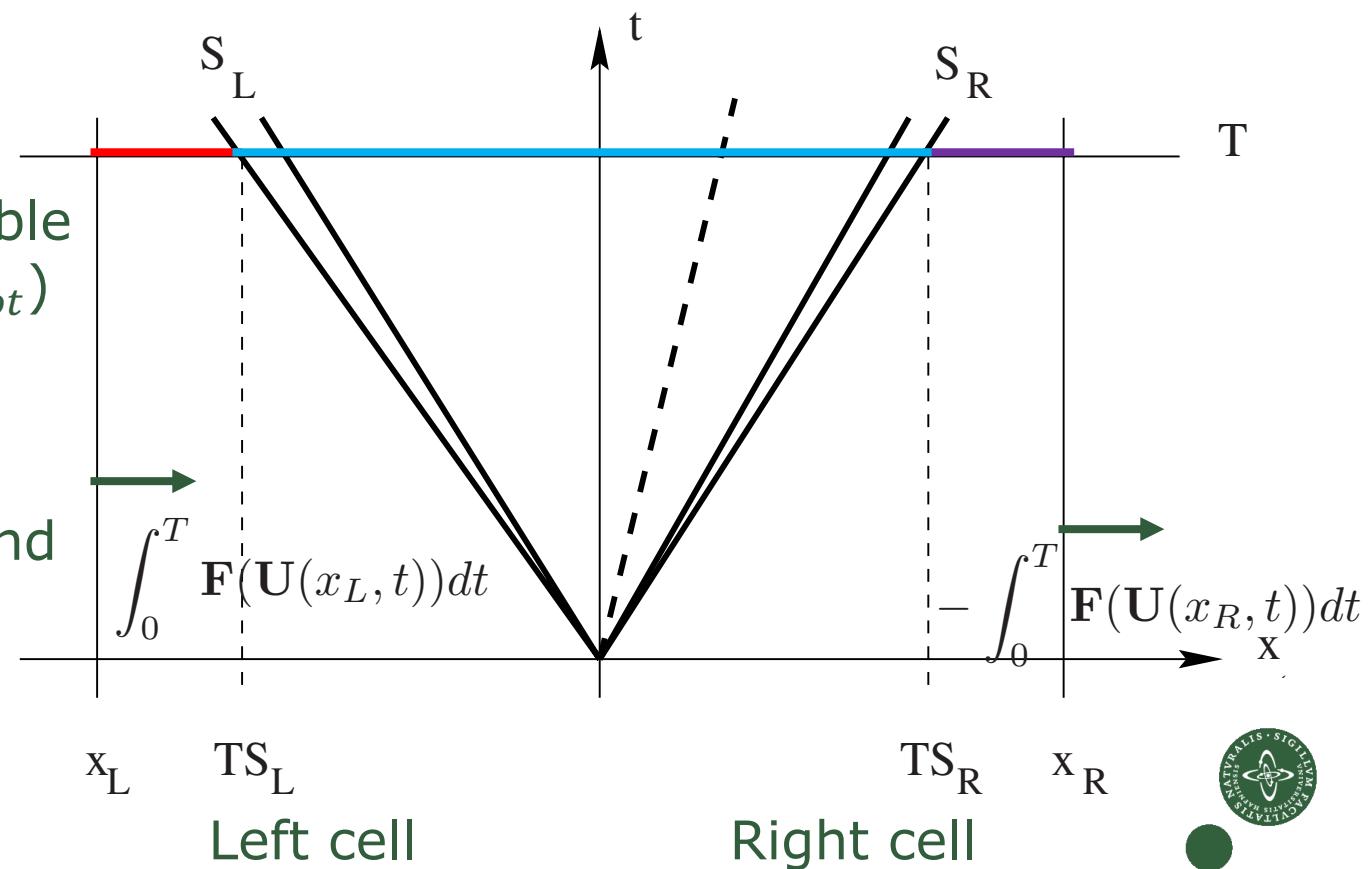
$$\int_{x_L}^{x_R} \mathbf{U}(x, T) dx = \underbrace{\int_{x_L}^{TS_L} \mathbf{U}(x, T) dx}_{\text{Red}} + \underbrace{\int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx}_{\text{Blue}} + \underbrace{\int_{TS_R}^{x_R} \mathbf{U}(x, T) dx}_{\text{Purple}}$$

$$x_R \mathbf{U}_R - x_L \mathbf{U}_L + T(\mathbf{F}_L - \mathbf{F}_R) = \underbrace{\int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx}_{\text{Red}} + \underbrace{(TS_L - x_L) \mathbf{U}_L}_{\text{Blue}} + \underbrace{(x_R - TS_R) \mathbf{U}_R}_{\text{Purple}}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Combine:

Combine results, and
 then arbitrary
 boundaries (x_L, x_R)
 drop out



Approximate Riemann Solvers – HLL

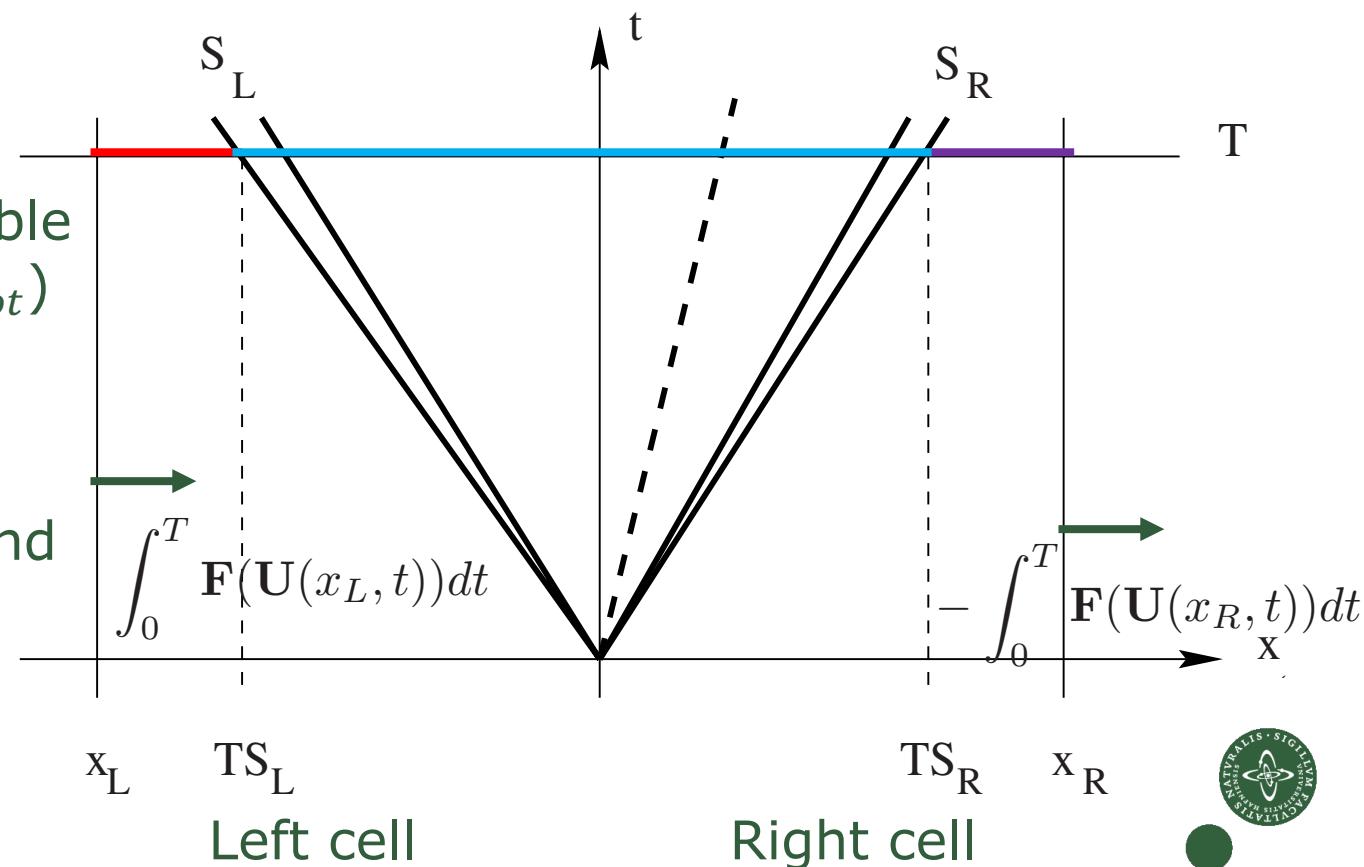
$$\frac{1}{T(S_R - S_L)} \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx = \frac{S_R \mathbf{U}_R - S_L \mathbf{U}_L + F_L - F_R}{S_R - S_L}$$

$$x_R \cancel{\mathbf{U}_R} - x_L \cancel{\mathbf{U}_L} + T(\mathbf{F}_L - \mathbf{F}_R) = \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx + \cancel{(TS_L - x_L)\mathbf{U}_L} + \cancel{(x_R - TS_R)\mathbf{U}_R}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
F: flux for U

Combine:

Combine results, and
then arbitrary
boundaries (x_L , x_R) —
drop out



Approximate Riemann Solvers – HLL

$$\mathbf{U}^{hll} = \frac{1}{T(S_R - S_L)} \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx = \frac{S_R \mathbf{U}_R - S_L \mathbf{U}_L + F_L - F_R}{S_R - S_L}$$

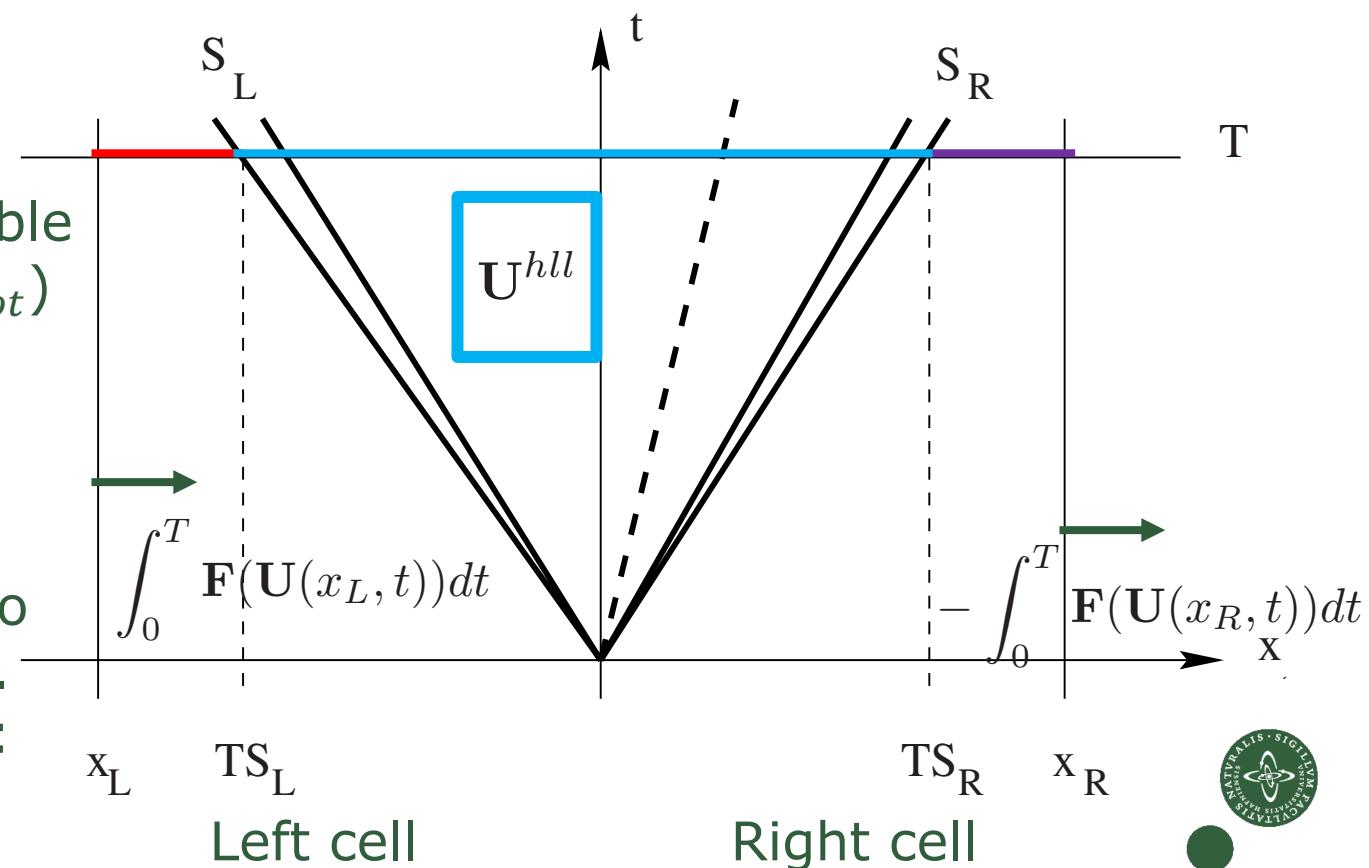
$$\cancel{x_R \mathbf{U}_R - x_L \mathbf{U}_L} + \cancel{T(\mathbf{F}_L - \mathbf{F}_R)} = \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx + \cancel{(TS_L - x_L) \mathbf{U}_L} + \cancel{(x_R - TS_R) \mathbf{U}_R}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Average state:

U is conserved and only changes due to flux at boundaries.

New average state:
 \mathbf{U}^{hll}



Approximate Riemann Solvers – HLL

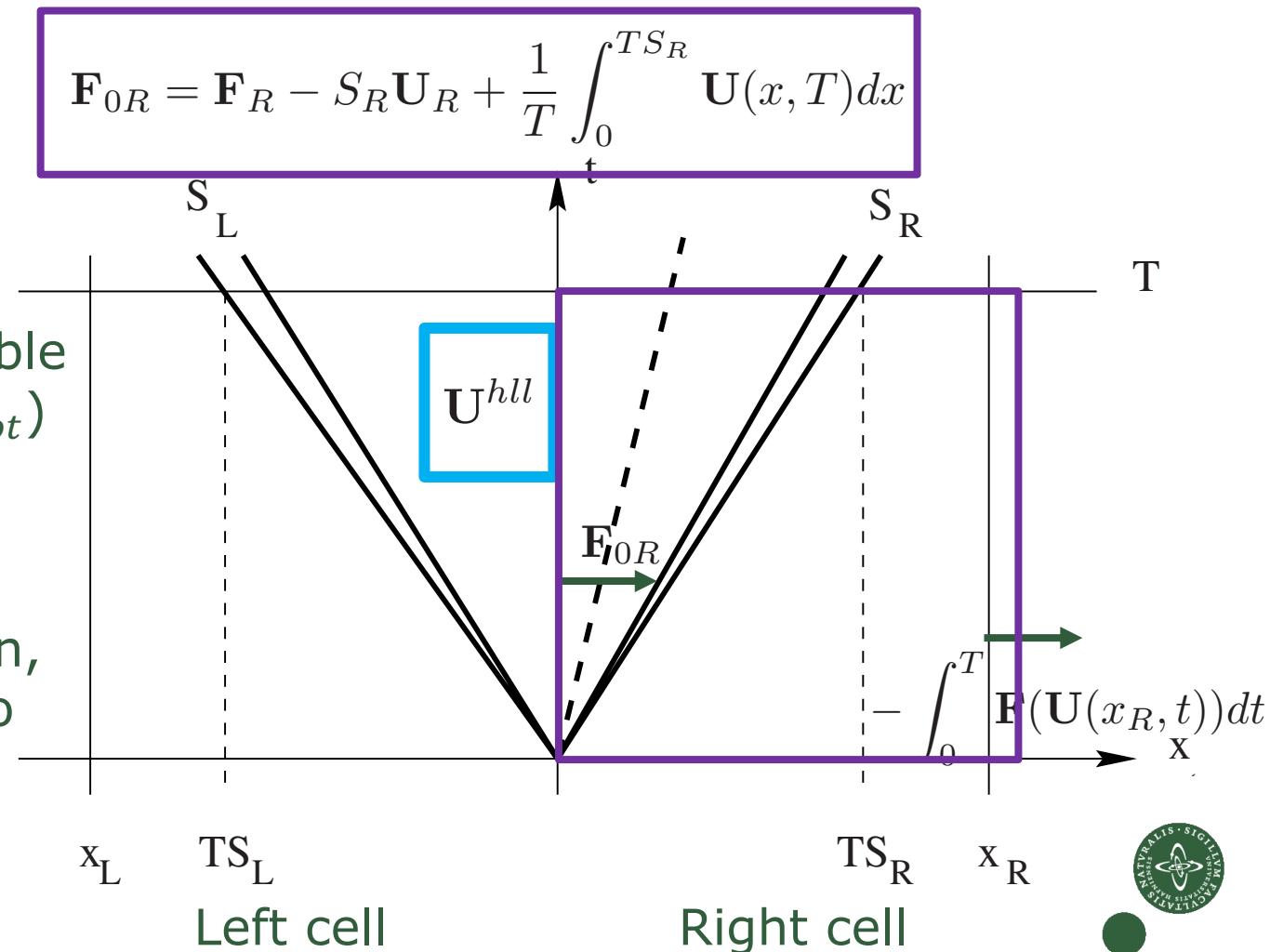
$$\mathbf{U}^{hll} = \frac{1}{T(S_R - S_L)} \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx = \frac{S_R \mathbf{U}_R - S_L \mathbf{U}_L + F_L - F_R}{S_R - S_L}$$

$$\mathbf{F}_{0R} = \mathbf{F}_R - S_R \mathbf{U}_R + \frac{1}{T} \int_0^{TS_R} \mathbf{U}(x, T) dx$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

Interface flux:

Repeat computation,
 but only at $x > 0$ to
 find interface flux



Approximate Riemann Solvers – HLL

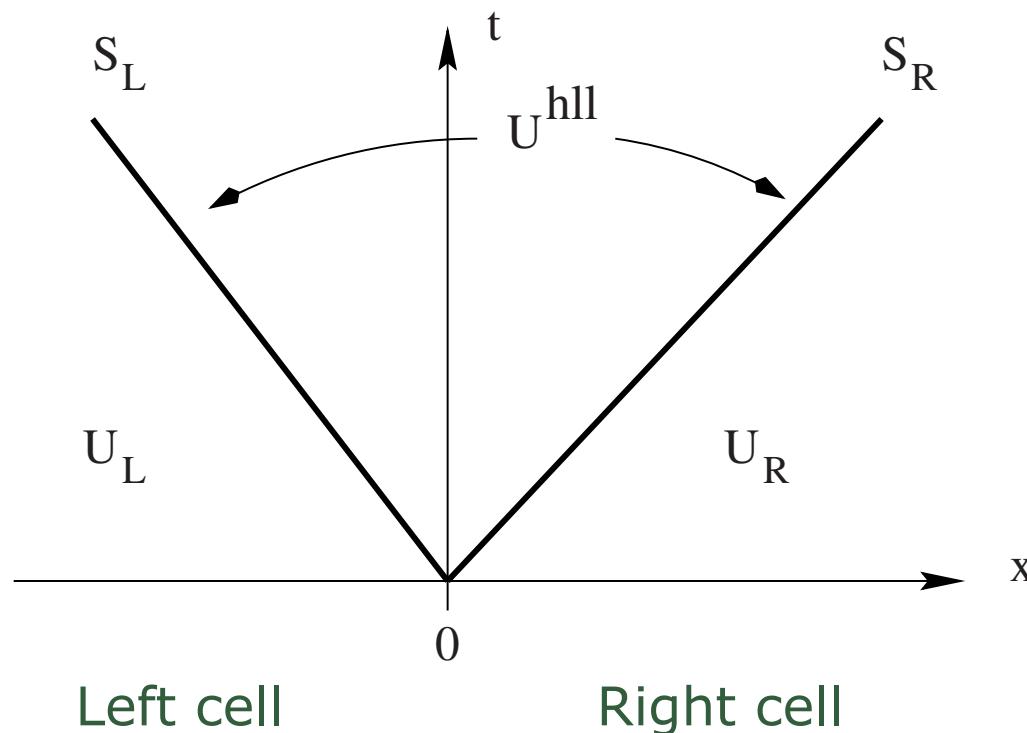
$$\mathbf{U}^{hll} = \frac{1}{T(S_R - S_L)} \int_{TS_L}^{TS_R} \mathbf{U}(x, T) dx = \frac{S_R \mathbf{U}_R - S_L \mathbf{U}_L + F_L - F_R}{S_R - S_L}$$

$$\mathbf{F}_{0R} = \mathbf{F}^{hll} = \frac{S_R \mathbf{F}_L - S_L \mathbf{F}_R + S_L S_R (\mathbf{U}_R - \mathbf{U}_L)}{S_R - S_L}$$

U: conserved variable
 $\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$
 F: flux for U

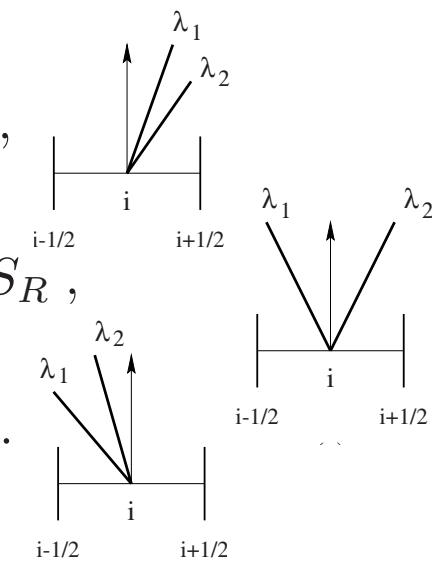
Interface flux:

Evaluate integral with
HLL state and
 rearrange to find
HLL flux



Approximate Riemann Solvers – HLL

$$\mathbf{F}_i^{hll} = \begin{cases} \mathbf{F}_L & \text{if } 0 \leq S_L, \\ \frac{S_R \mathbf{F}_L - S_L \mathbf{F}_R + S_L S_R (\mathbf{U}_R - \mathbf{U}_L)}{S_R - S_L}, & \text{if } S_L \leq 0 \leq S_R, \\ \mathbf{F}_R & \text{if } 0 \geq S_R. \end{cases}$$



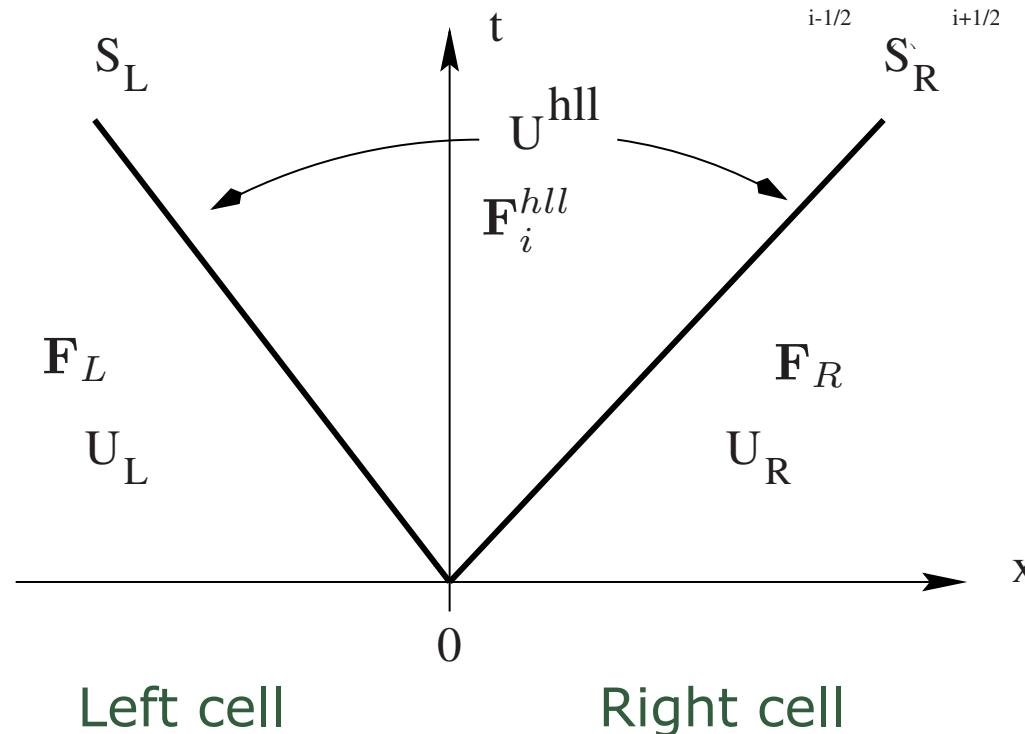
U: conserved variable

$$\mathbf{U} = (\rho, \rho u, \rho v, \rho w, E_{tot})$$

F: flux for U

$$S_L: \min(u_L, u_R) - c_{\text{sound}}$$

$$S_R: \max(u_L, u_R) + c_{\text{sound}}$$



Approximate Riemann Solvers – HLLC

- HLLC solver adds a new characteristic speed
- Less diffusive than HLL, more physical
- Very stable solver for hydrodynamics
- Widely used method of choice in codes!
- States found by assuming pressure and velocity continuous at S_*
- Review by Toro 2019 - doi: 10.1007/s00193-019-00912-4

U : conserved variable

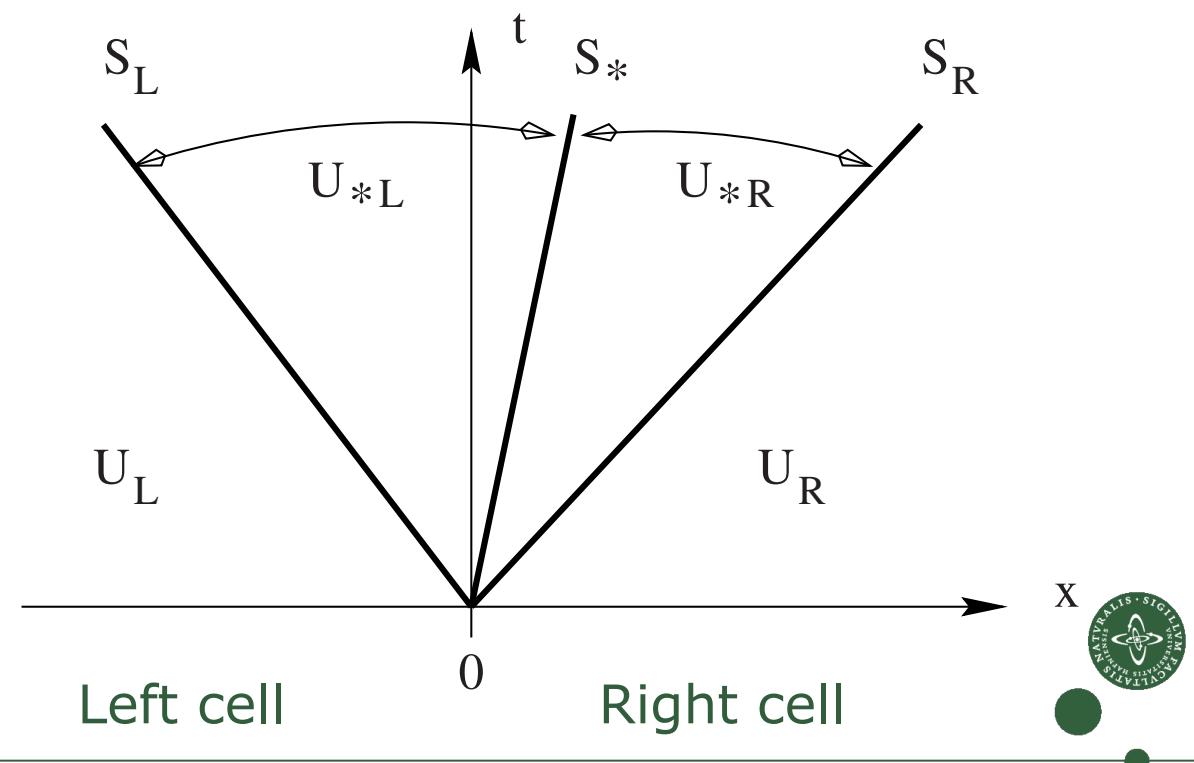
$$U = (\rho, \rho u, \rho v, \rho w, E_{tot})$$

F : flux for U

$$S_L: \min(u_L, u_R) - c_{\text{sound}}$$

$$S_R: \max(u_L, u_R) + c_{\text{sound}}$$

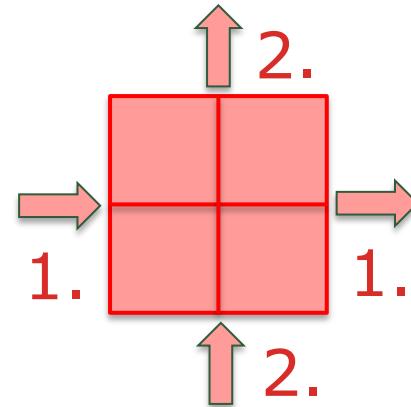
S_* : determined from jump conditions!!



Higher dimensionalities

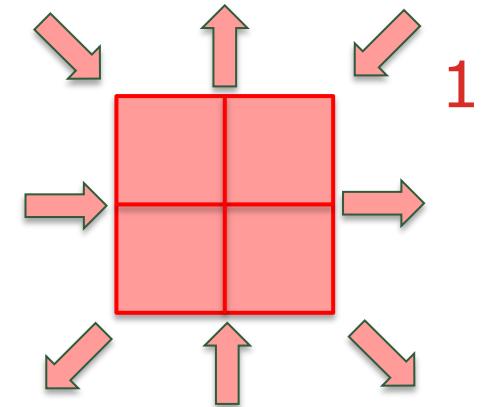
(non)-split fluxes:

- Compute fluxes sequentially through each edge (face) in 2D (3D).
- Problem is overadvection where density or pressure becomes negative
- Solution also not manifestly isotropic
- Can induce *carbuncle* instability



Higher dimensionality fluxes:

- Compute fluxes thorough each edge and corner (face, edge) in 2D (3D).
- This is much more isotropic
- Super complicated to solve Riemann problem.
- Done only by few groups. Implementation papers are small books.





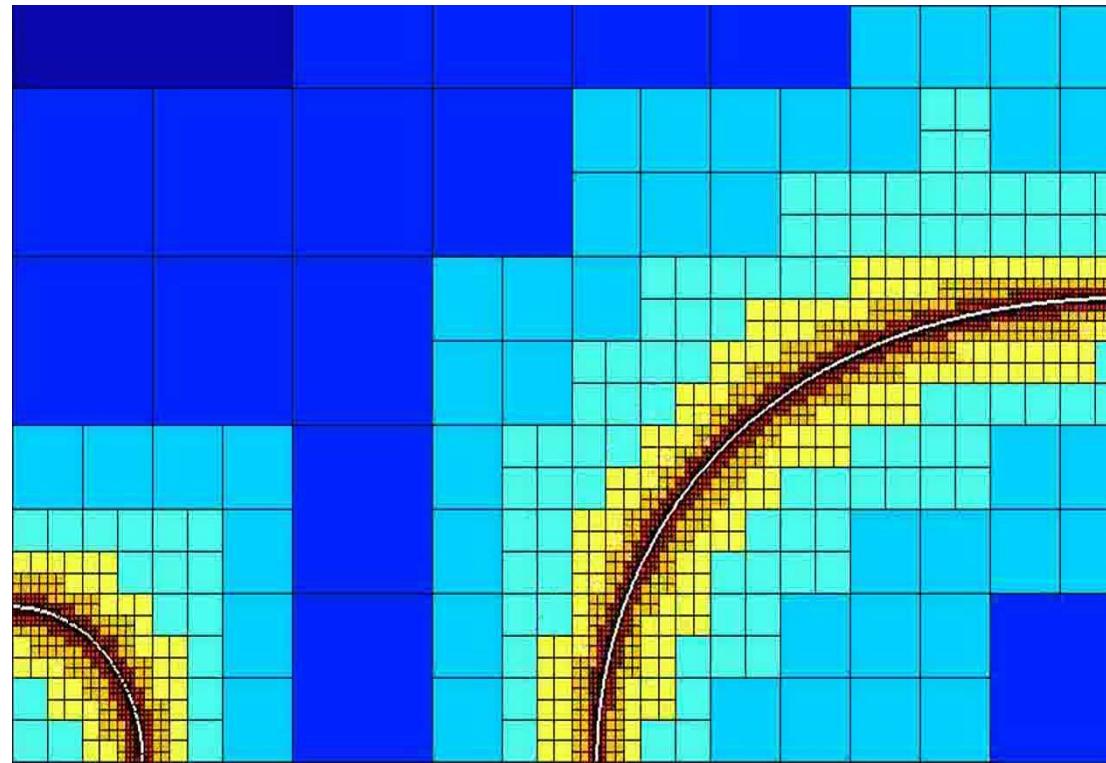
Faculty of Science

Adaptive Mesh Refinement (AMR)

What is Adaptive Mesh Refinement (AMR) ?

Some of you may know about Adaptive Mesh Refinement or have heard about the concept. But here is a quick summary:

- AMR-codes can (recursively) resolve small details, by using patches (small or large) with increasingly large resolutions
- It is *adaptive*, because the cell placement can change with time



Motivations for Adaptive Mesh Refinement

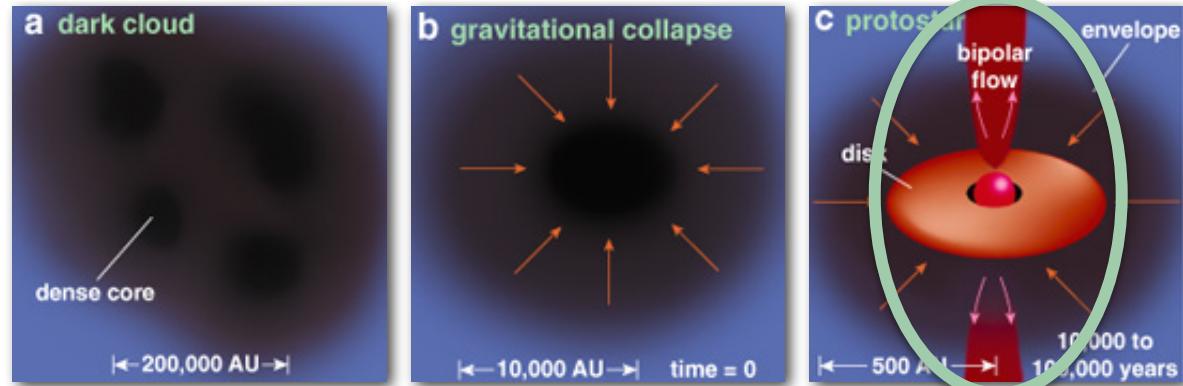
- Fluid dynamics in three dimensions is costly:
 - Cost of a uniform grid scales as the resolution to the fourth power
 - Even today only $\sim 1024^3$ is routine, and the largest unigrid run to date is $\sim 16384^3$
 - Many problems in astrophysics contain relevant, coupled processes at very different scales
 - Use a sub-grid model description
 - Use different resolution at different places → AMR in space
 - If velocities are approximately (order of magnitude!) constant the dynamical time-scale scales with the physical scale
 - Large scales evolve slower than small scales → AMR in time
 - Using adaptive meshes we can “easily” supply realistic boundaries to a local problem; the ladder of astrophysical AMR is:
 - Cosmology → Galaxy formation → Star formation → Planet Formation



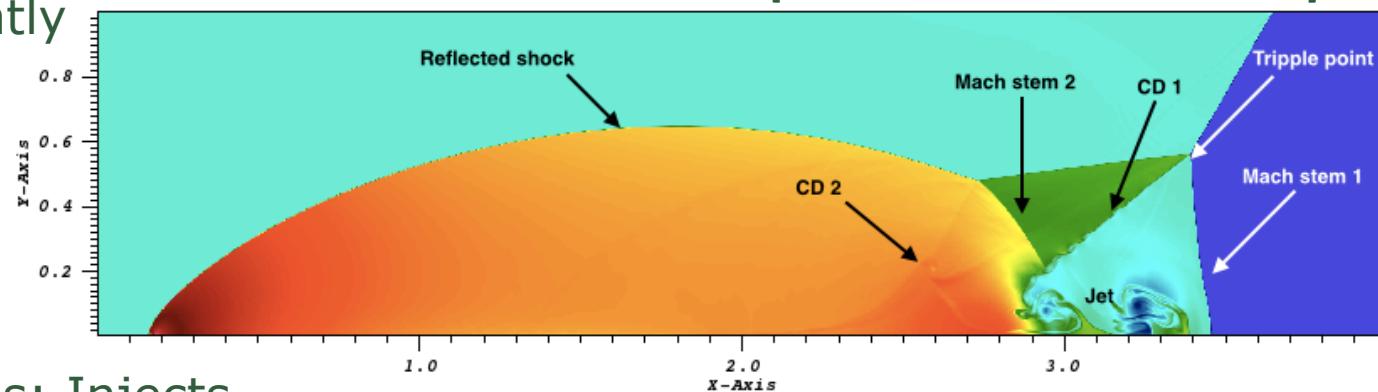
Multiscale Astrophysics

[Spitzer Science Center]

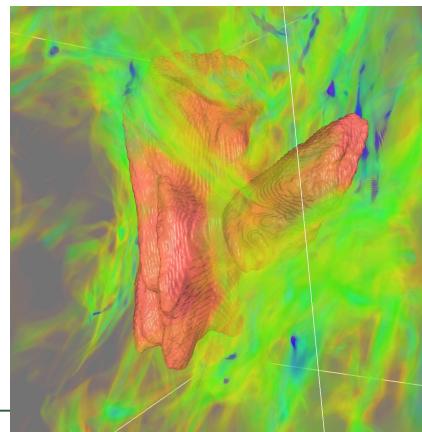
- Selfgravity: induces collapse, with a rapid decrease in scales



- Shocks: inherently localized; often part of complex flows



- Compact sources: Injects energy from the smallest scales to the largest



[Ionization front in a molecular cloud launched by central source]

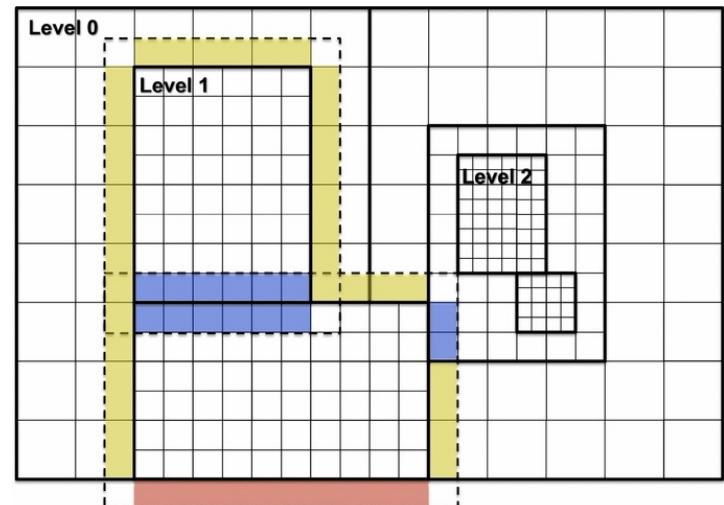


Flavors of Adaptive Mesh Refinement

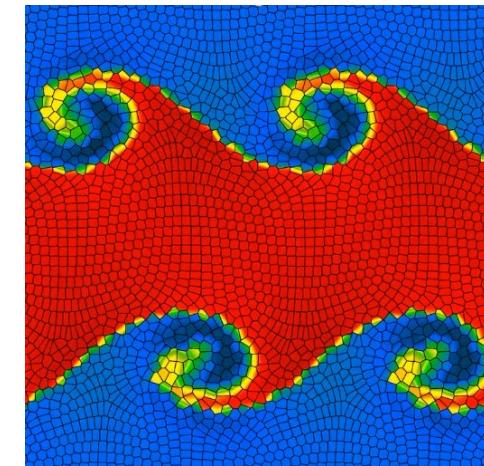
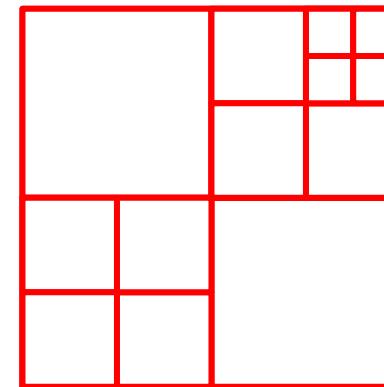
- Block based AMR (original Collela, Berger, Oliger '84 & '89) [FLASH, **Enzo, Nirvana, Pluto, AZeus**]
 - Use patches of higher resolution completely contained inside lower resolution patches

- Oct based Fully-Threaded-Tree (Khokhlov '98) [**RAMSES, AMRVAC, ART**]
 - Refine on a cell-by-cell basis, with one cell being split in to 8 (in 3D)

- Unstructured Meshes [AREPO, GIZMO, finite elements]
 - Partition space using one volume per tracer particle; f.ex. using a Voronoi tessellation.

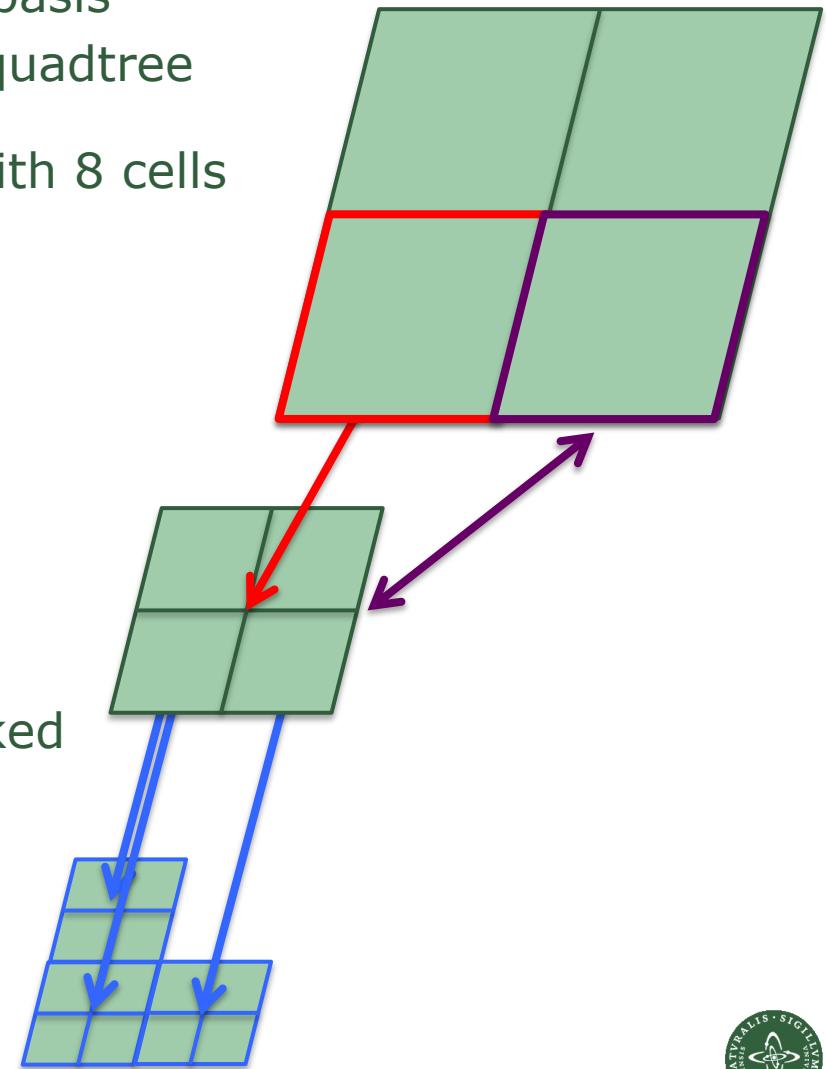


[PLUTO AMR paper]



Fully-Threaded-Tree Adaptive Mesh Refinement

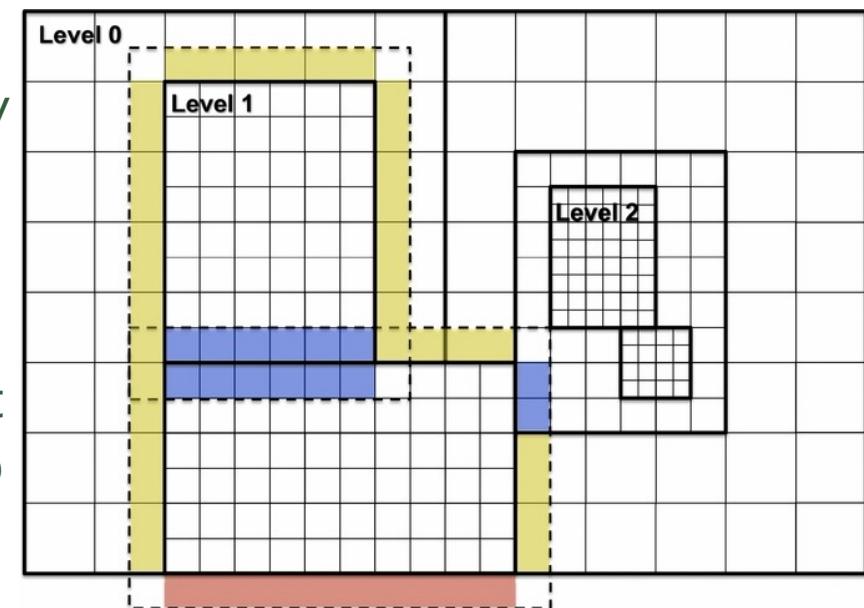
- Refinement is done on a cell-by-cell basis
 - 3D: octree (8 cells per oct), 2D: quadtree
- Each cell can be refined to one oct with 8 cells
 - Very adaptive grid
- Very simple relationship structure
 - 1 parent cell
 - 6 neighbor parent cells
 - Potentially 8 children octs
- Everything is constructed recursively
 - Position and relationships are picked up from parent cell at creation
- All cells in the tree are kept
 - Leaf cells have no children octs
 - Refined cells are inactive



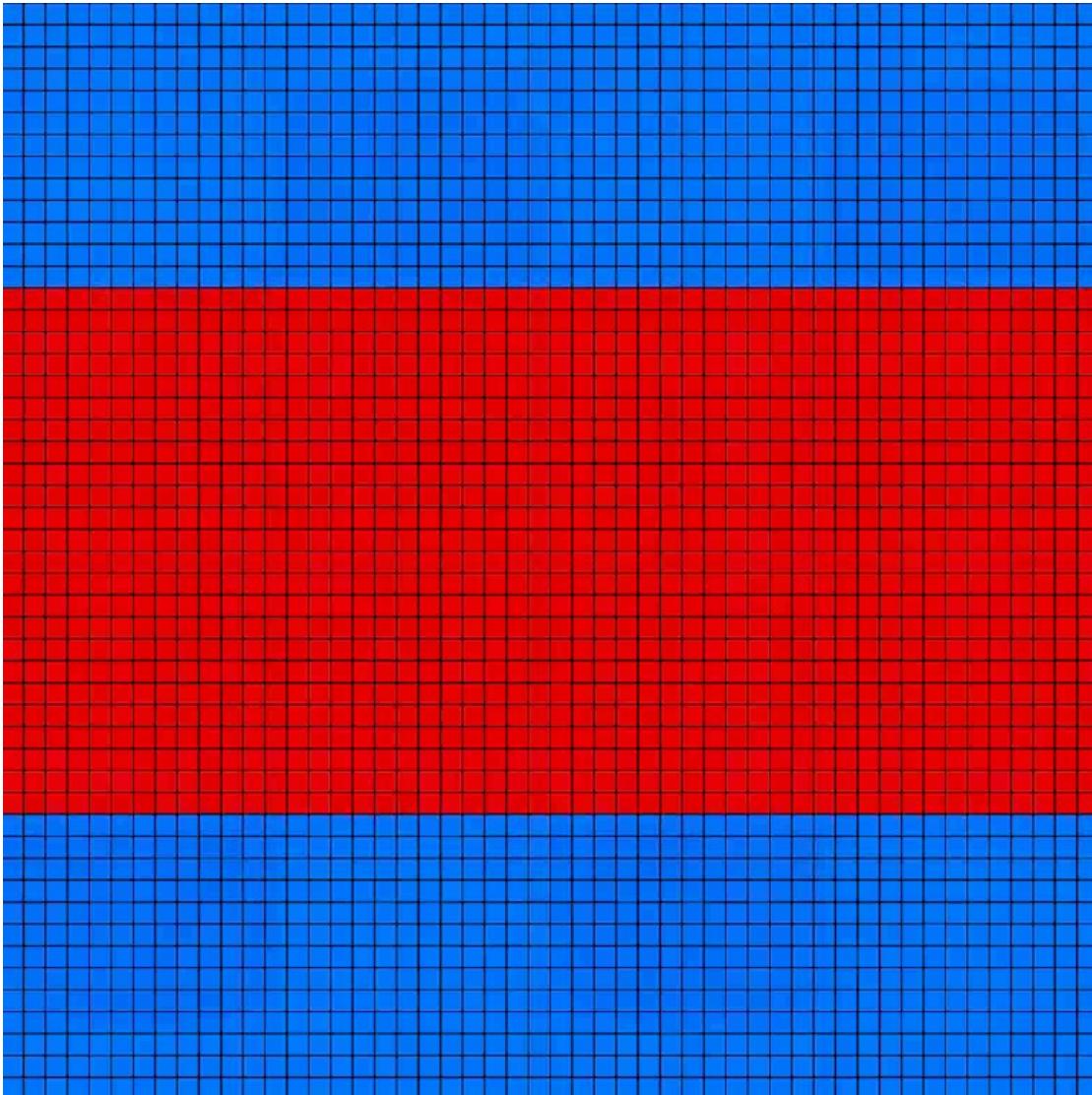
Block based Adaptive Mesh Refinement

- ❑ Refinement is done in a number of cells inside a patch to create a new patch
- ❑ Typical size of a patch is $(12\text{-}16)^{N_{\text{dim}}}$
 - ❑ Reasonable grid size. Efficient to manage
- ❑ Complex but flexible relationship structure
 - ❑ 1 parent patch (in simplest version)
 - ❑ N_{bor} neighbor patches (at different levels)
 - ❑ N_{child} children patches
- ❑ Everything is constructed recursively
 - ❑ Position and relationships are picked up from parent patches at creation
- ❑ Normally all cells in a patch are kept
 - ❑ Leaf cells have no patches on top
 - ❑ Refined cells are inactive

[PLUTO AMR paper]

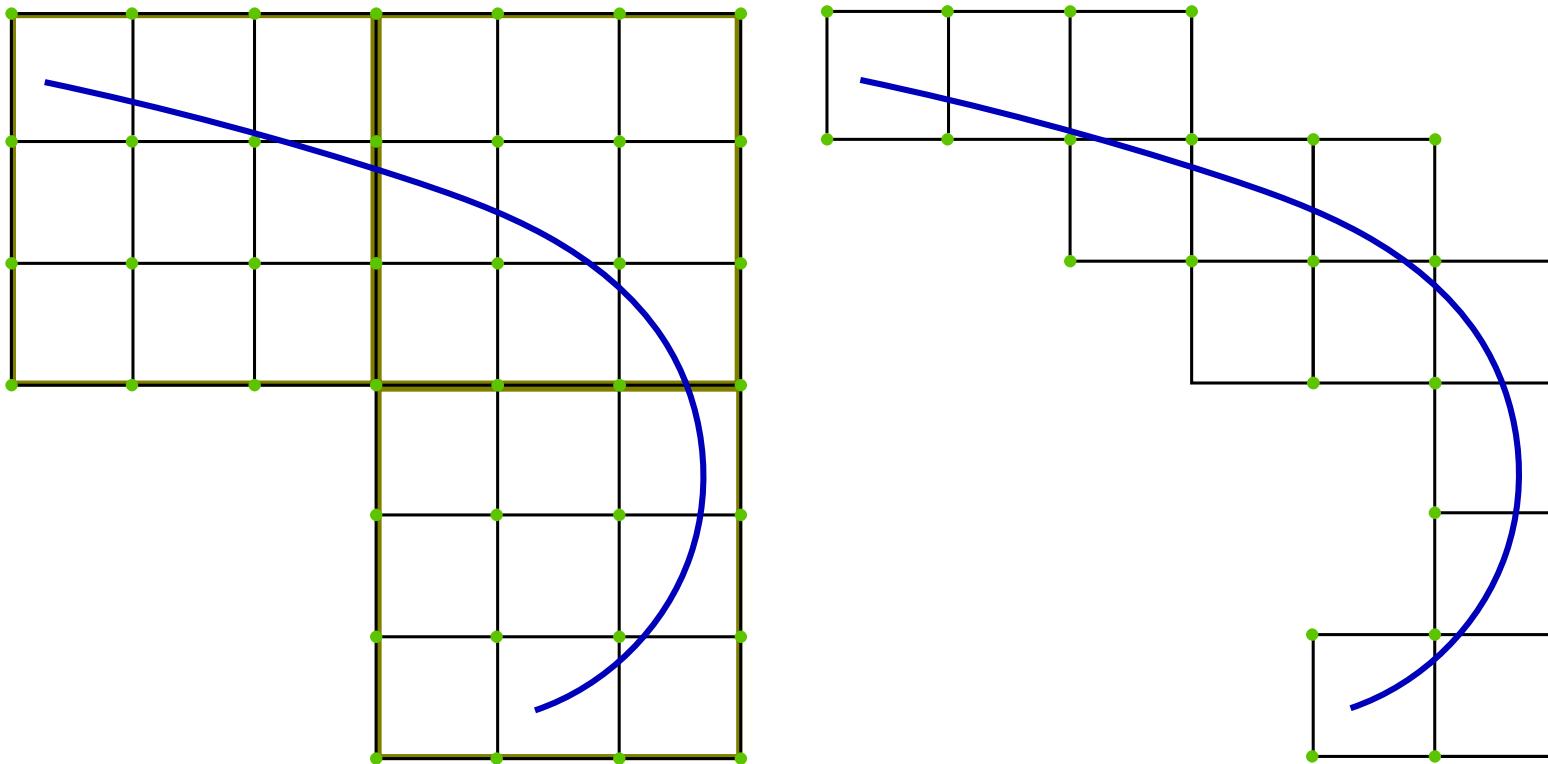


Unstructured (moving) meshes



- ❑ Unstructured codes are using tracer points for their geometry.
- ❑ F.x. the AREPO and GIZMO codes use unstructured and meshless representations, respectively.
- ❑ Their representation has the important advantage (over fixed-grid codes), to respect Galilean invariance; i.e., their results are the same, independent of any bulk motion of the system under study.
- ❑ The Courant condition is only due to *relative motion*.
- ❑ But cost is high!

Patch versus Tree based AMR



- ❑ A patch based AMR structure is much better at adapting to complex flows, like turbulence
- ❑ CPU overhead is larger; hard to vectorize efficiently due to oct-by-oct structure. Difficult to move to GPUs

Ingredients of an AMR method



Fluid Dynamics on an AMR patch / in an oct

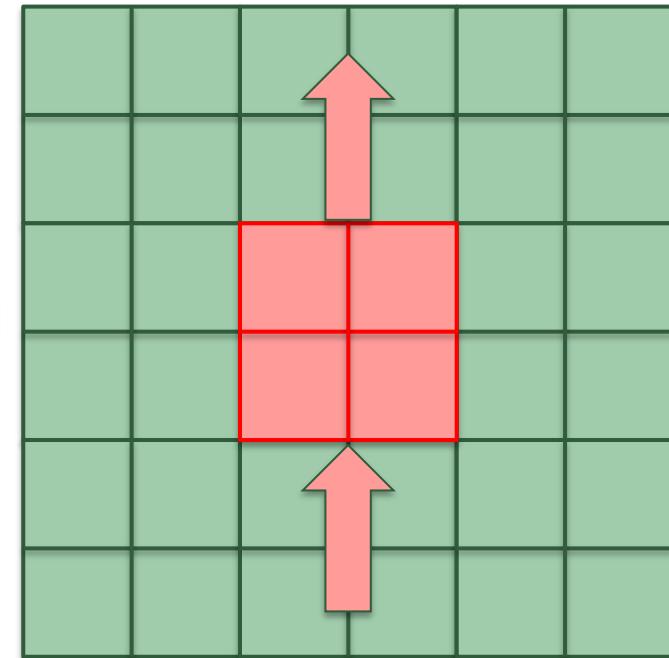
- The fluid dynamics in an adaptive mesh is solved exactly as on a normal mesh

1. Extract patch
2. Pick up “guard cells”:
 1. Check if neighbors exist
 2. Else create new cells on-the-fly

- Calculate fluxes with a finite volume method

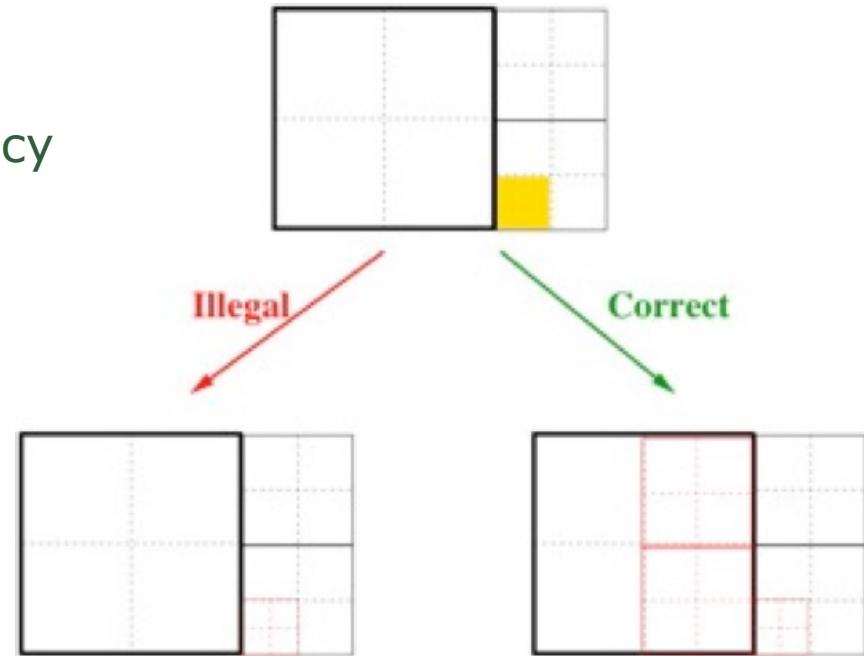
- Hard to use higher order methods; we typically only use 2 guard cells to maintain a reasonable surface-to-volume ratio
 - Motivates the use of Godunov methods or very compact finite differences

- *Parent neighbors always need to exist*, or we cannot get boundaries on-the-fly



AMR Refinement Rules

- Most codes enforce mesh consistency and grading of patches
 - All neighbors have to be at the same level or one level below or above
- Specific Criteria
 - Jeans Criteria
 - Gradients
 - Quasi-Lagrangian
 - Geometrical (zoom)



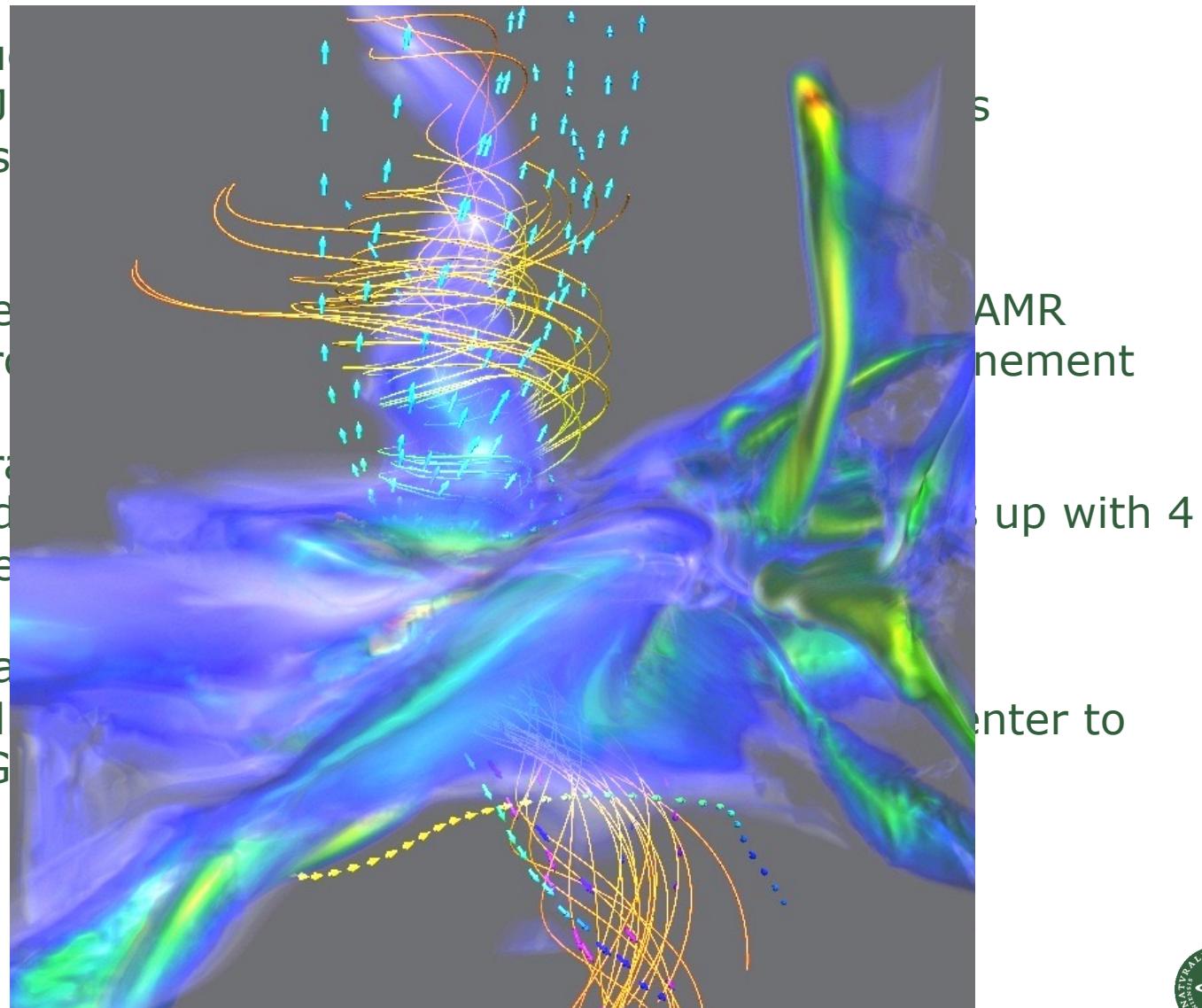
Refinement Criteria

- Jeans / Truelove Criteria
 - If the Jeans length is not resolved, collapse becomes unphysical
- Gradients
 - Beware of shocks; if encounter a real jump you get AMR catastrophe -> individual max level for gradient-refinement
- Quasi-Lagrangian
 - Related to Jeans. F.x. refine every time density goes up with 4 to have same Jeans resolution on all levels
- Geometrical (zoom)
 - Only allow code to refine in specific region. Adapt center to flow; Gallilean transform; follow star



Refinement Criteria

- Jeans / Truncation
 - If the Jeans length is unphysical
- Gradients
 - Beware of numerical catastrophe
- Quasi-Lagrangian
 - Related to the fact that it's hard to have a good coordinate system
- Geometrical
 - Only allows refinement along flow; Good for jets



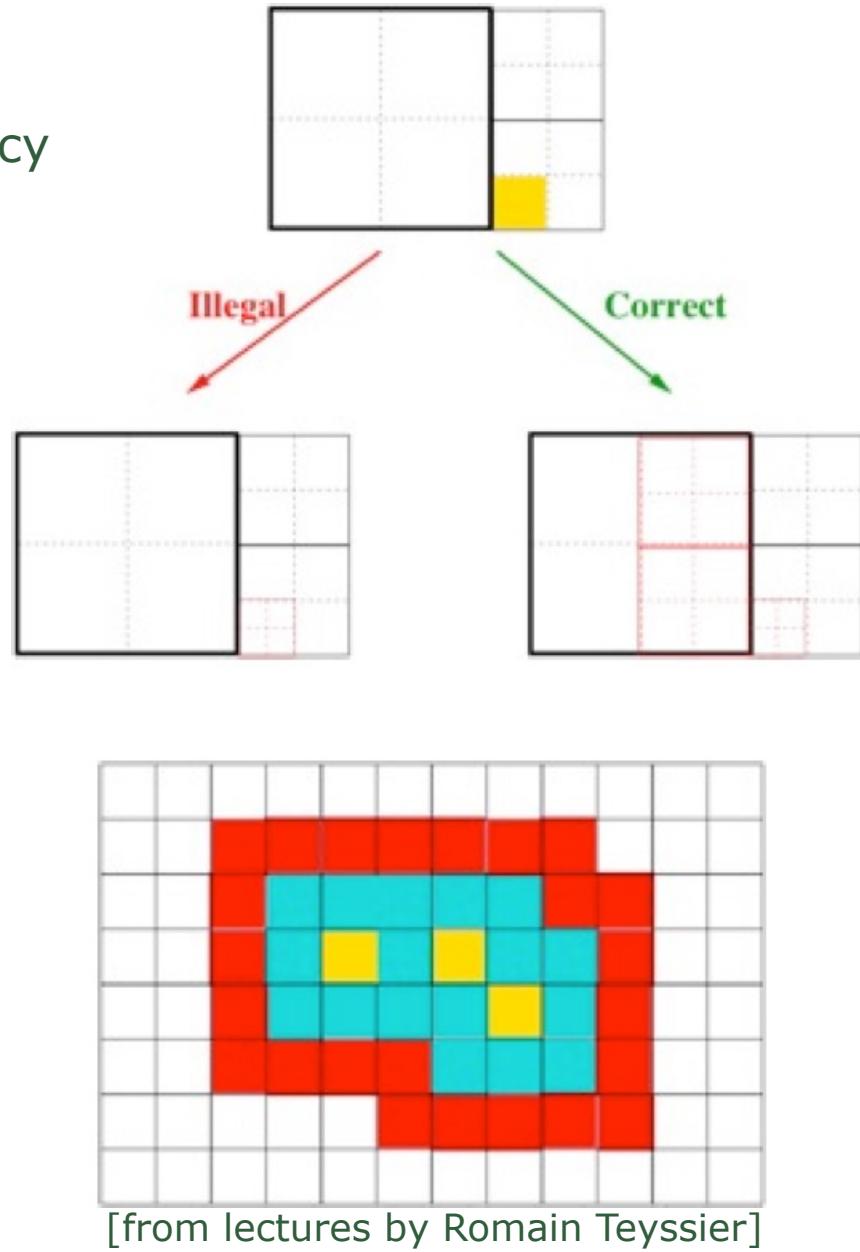
[Refinement to pick up Jet; VAPOR viz by M. Küffmeier]

AMR Refinement Rules

- Most codes enforce mesh consistency and grading of patches
 - All neighbors have to be at the same level or one level below or above

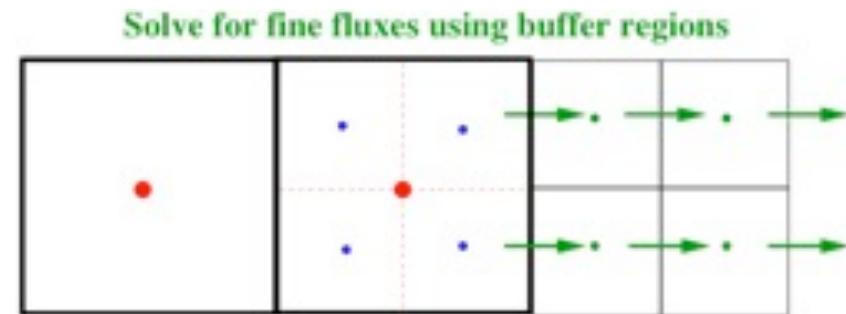
- Specific Criteria
 - Jeans Criteria
 - Gradients
 - Quasi-Lagrangian
 - Geometrical (zoom)

- Smoothing is often done
 - Patch has to be convex
 - Expand patch sizes with *nexpand* layers (ex. 2 layers)



Interpolation and Flux consistency

- *Prolongation:* Interpolation to finer meshes
 - Creation of new cells
 - On-the-fly boundary cells
- *Restriction:* Averaging to coarser levels
 - Destruction / derefinement
 - Filling of the threaded tree
- Flux correction at boundaries
- Different interpolators
 - Conservative / internal energy
 - Apply different slope limiters
 - ***When changing the resolution the method looses one order***



[from lectures by Romain Teyssier]



Time-adaptivity: Fine \rightarrow coarse level time Evolution

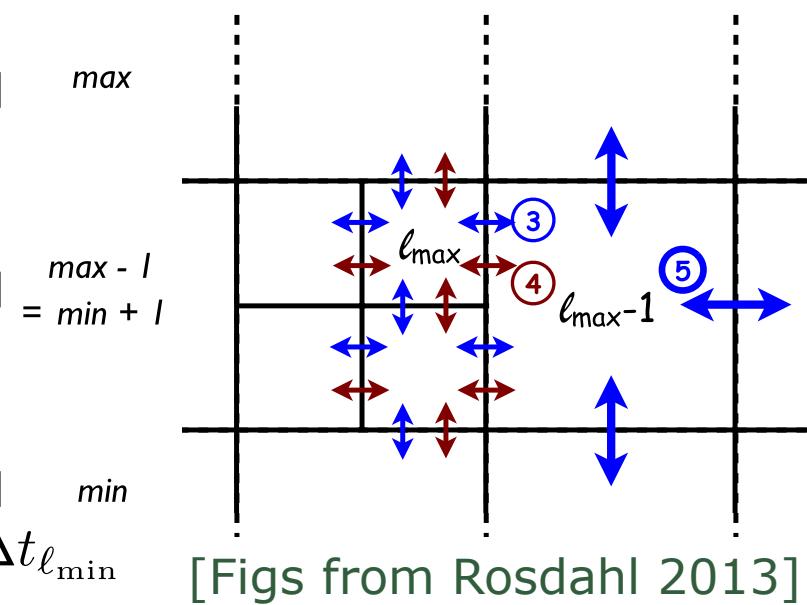
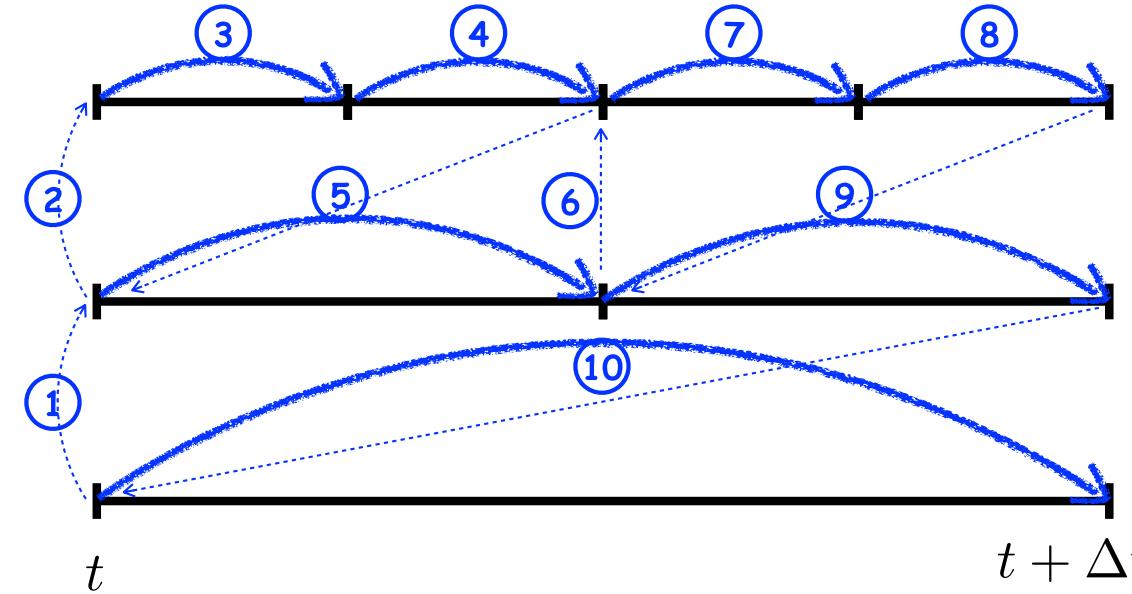
❑ Evolves in a W-cycle recursively from coarser to finer mesh and back

1. Prepare: Check on coarse level if we need to create new cells, prepare boundary conditions for finer levels. Then go to finer level.

- 2+6: Repeat step 1 and recursively progress to finer levels.

- 3-5,7-10. Evolve: Solve dynamics on finest level; update Courant, update flux for coarser cells via neighbor pointer; flag any cells on this level that have to be refined or destroyed.

Then recursively go to coarser level (diagonal lines) or repeat timestep



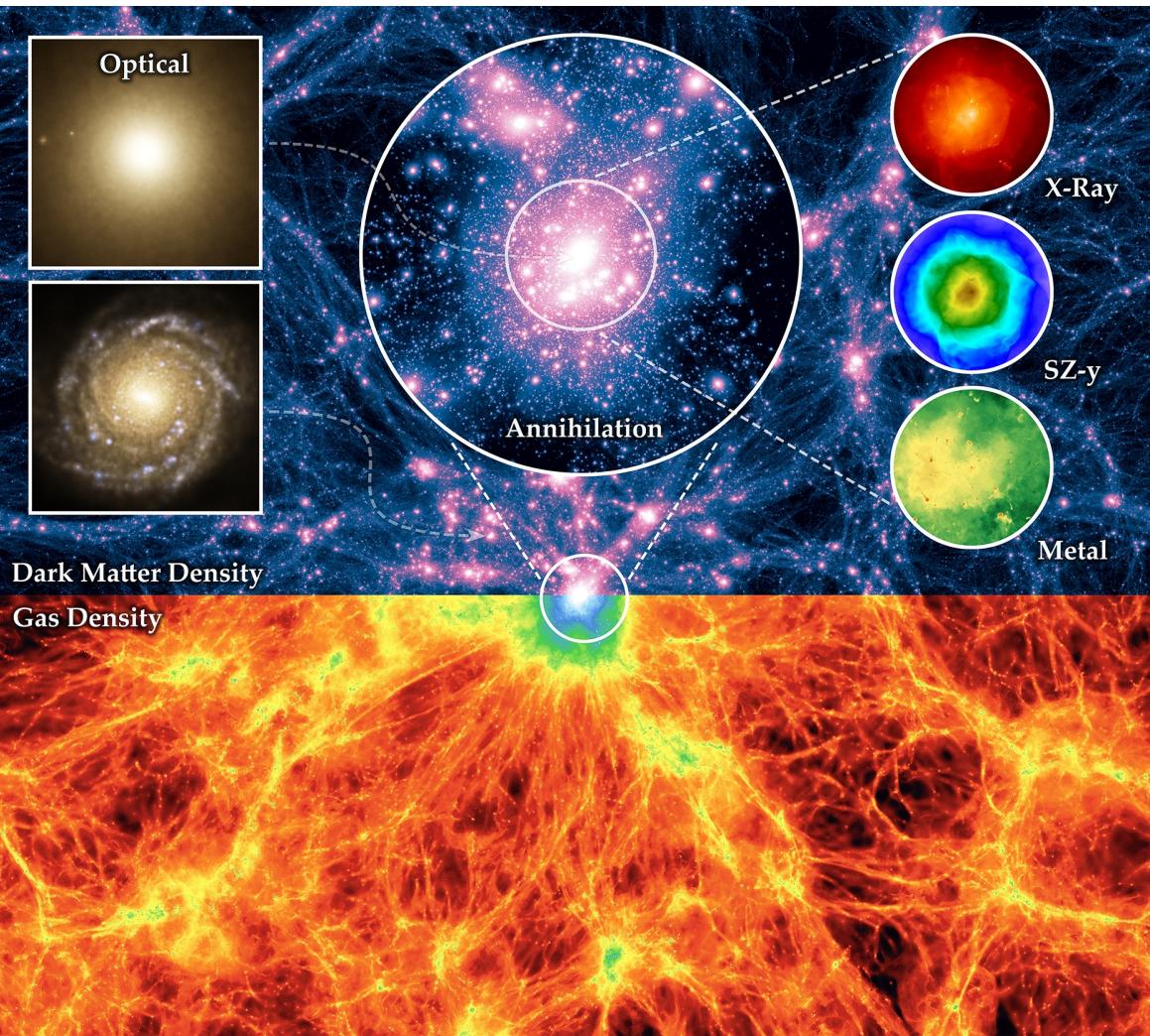
Astrophysical Applications

Cosmology and Star Formation



Astrophysical Applications - Cosmology

- ☐ ART, Enzo, FLASH, and RAMSES are in widespread use
- ☐ “Cosmology” is inherently a Multi-Scale problem



- ☐ Exemplified here by the *illustris* simulation, objects at the largest scales are coupled over at least four orders of magnitude
- ☐ Universe is statistically homogenous at $>100 \text{ Mpc } h^{-1}$
- ☐ Galaxies have sizes of $<100 \text{ kpc}$
- ☐ The large-scale filamentary web is needed to supply the boundary conditions for the formation and evolution of clusters and galaxies
- ☐ This was realized early, and “zoom-AMR” was used since the late ‘90

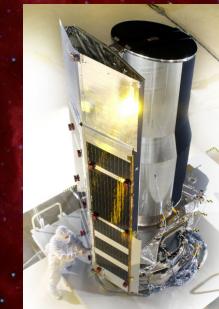


Astrophysical Applications – Star Formation

Star Cluster →

Supernova
Bubble ?

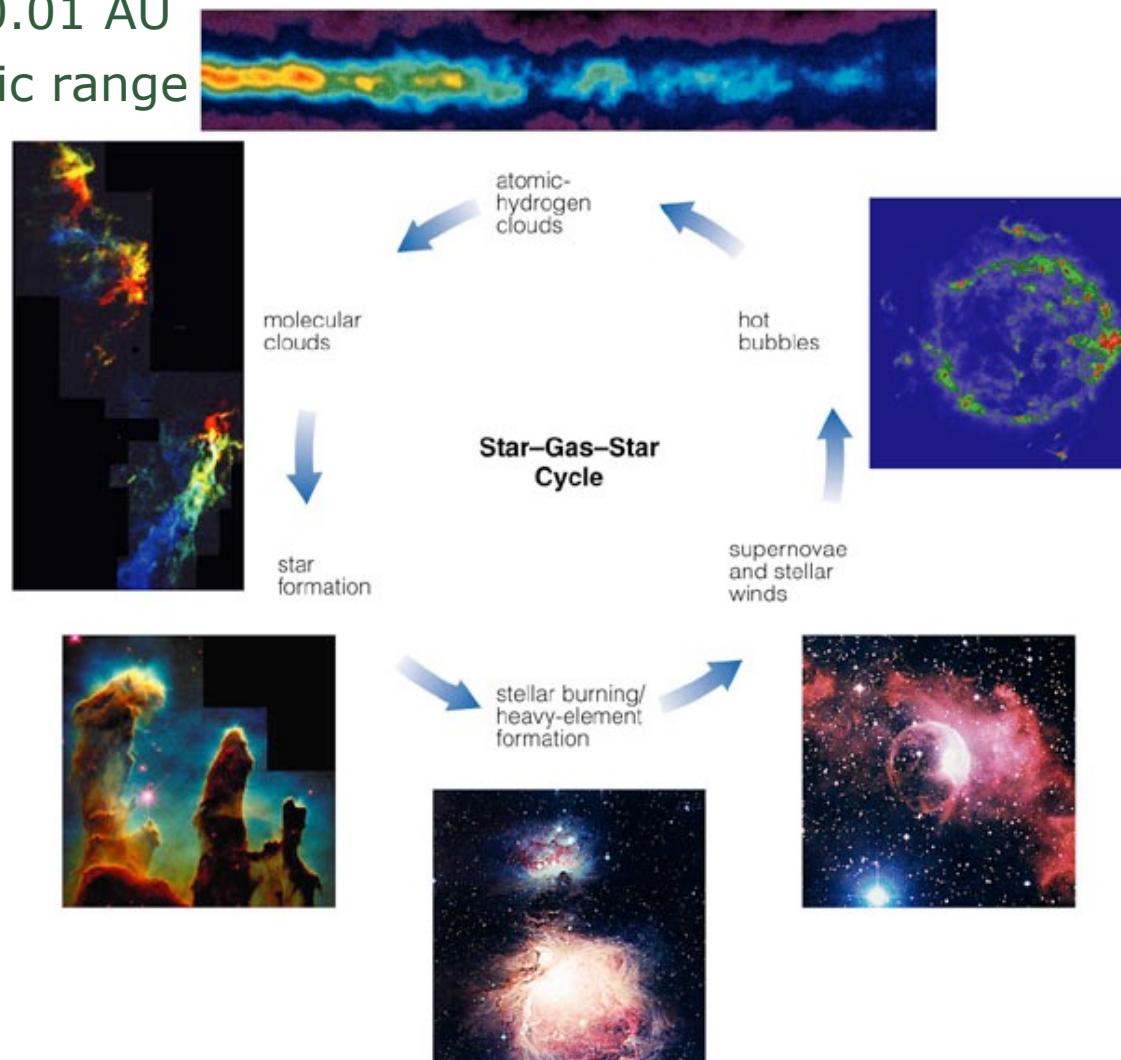
Intricate Gas
Filaments in
the Turbulent
Molecular Cloud



Spitzer

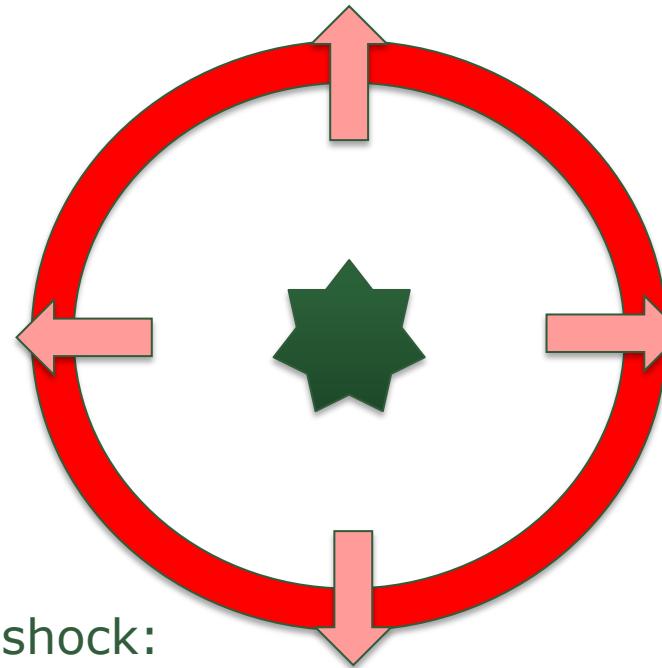
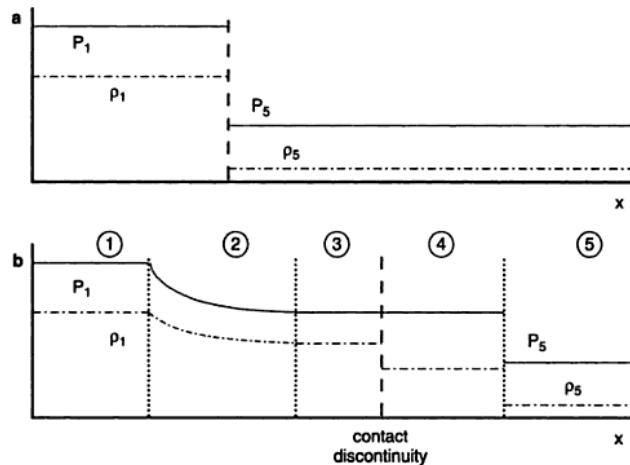
Astrophysical Applications – Star Formation

- Enzo, FLASH, Nirvana, Pluto, and RAMSES are in widespread use
- “Star Formation” is an even more extreme Multi-Scale problem
- 100 pc → 0.01 AU
- 10^9 dynamic range



Exercise: Sedov Blast Wave in 2D

- A simplified Supernova explosion: Concentrate thermal energy and add mass loading in a small volume. An expansion wave is launched:



See also
ch 3.8
in notes
from
Theoretical
Astrophysics

- Example of a pressure driven shock:
 - If there is mass it starts by coasting (free-stream phase)
 - The pressure is large and a strong shock is launched (Sedov phase)
 - Afterwards we reach a snow-plow phase where the shock is pushing ISM
 - When shock has displaced as much inertia as inside, it starts to decay
 - In the Sedov phase it evolves according to a simple scaling relation