

*Fakulta elektrotechniky a informatiky VŠB-TU Ostrava (bakalářský)*

Datum aktualizace originálu: **26. 12. 2023 v 9:16:20**

Datum vygenerování PDF: **2. 7. 2025 v 14:41:20**

# Obsah

---

- Real Voltage Sources
  - Linear Voltage Sources
    - Voltage Stabilizer with Zenor Diode
    - Voltage Stabilizer with Transistor
  - Sources using Rectifiers and Transformes
  - Switched Power Voltage Sources
  - Feedback
- Operational Amplifier
  - Non-inverting Amplifier
  - Real Operational Amplifier
    - Transfer Voltage Characteristic

# Real Voltage Sources

## Linear Voltage Sources

Their internal resistance is non-zero, so their voltage depends on the load connected to the terminals.

Figure 1

$$\begin{aligned} -U + R_i \bullet I_S + U_S &= 0 \\ U_S &= U - R_i I_S \\ U_S = 0 \Rightarrow I_S &= I_{KS} = \frac{U}{R_i} \\ I_S = 0 \Rightarrow U_S &= U \end{aligned}$$

Plot 1 Load Line

Figure 2

$$U_n = U \bullet \frac{R_2}{R_i + R_1 + R_2}; R_n = \frac{(R_i + R_1) R_2}{R_i + R_1 + R_2}$$

### Voltage Stabilizer with Zenor Diode

Figure 3

$$R = \frac{U - U_D}{I_D}; I_{Dmin} < I_D < I_{Dmax}$$

Voltage stabilizer operates from the certain value of voltage up to certain value of current.

### Voltage Stabilizer with Transistor

Figure 4

$$\begin{aligned} (U_L \&= U_D - U_{BE} @ 0.65 < U_{BE} < 0.7 @ \& I_E = (h_{21E} + 1) \bullet I_B @ I_{R1} \&= I_D + I_B \approx I_D @ R_1 \&= \frac{U - U_D}{I_D} @ I_D \& \gg I_B; U_L \approx U_D) \\ I_{Cmax} &< I_C \end{aligned}$$

$$P_C = U_{CE} \bullet I_C < P_{Cmax} - \text{power deception}$$

## Sources using Rectifiers and Transformes

- **Single Phase Transformer**

Figure 5 – Single Phase Transformer consists of a core (typically iron with magnetic features) forming a magnetic circuit; around it we can found a primary wiring connected to a input source of sine AC, and a secondary wiring where appears output voltage  $U_2$  of sine AC.

- It galvanically separates the wirings – the DC cannot pass through the SPT.
- It operates on the Faraday Electromagnetic Law –changes of magnetic flux in the core induce the output voltage on the secondary wiring.
- $\frac{U_1}{U_2} = n = \frac{N_1}{N_2} = \frac{I_2}{I_1}; P_1 = P_2; \eta = \frac{P_2}{P_1}; 75\% < \eta < 98\%$

- **Half-Wave Rectifier**

Figure 6

- **Bridged Full-Wave Rectifier**

Figure 7

- **Smoothing Capacitor**

Figure 8

The difference  $\Delta U = U_{1m} - U_{1\min}$  is called **ripple**.

## Switched Power Voltage Sources

They have much greater efficiency than linear sources, are lighter and smaller. They don't operate continuously, but on switching regimes which switch at high frequency, so they seem to be continuous.

Property	Linear Power Sources	Switched Power Sources
Efficiency	$\eta < 40\%$	$\eta > 75\%$
Size and Weight	heavy	small
Complexity	not complex	more complex
Noise and Ripple	$f = 50\text{ Hz}$ , noisy, $\Delta U$ can be small	$20\text{ kHz} < f < 1\text{ MHz}$ , quiet, $\Delta U$ is large
Reliability	high	worse

- **AC to DC Switched Convertor**
- **Buck-Boost Convertor**

## Feedback

Put part of output back to the input in such manner, that the input is increased, we speak about **positive feedback** (leads to instability in system, is used in oscillators), in otherwise it's **negative feedback** used to maintain stability in amplifiers.

## Operational Amplifier

### Non-inverting Amplifier

Figure 1

The polarity of input voltage is the same as the polarity of output voltage. It has high input resistance

Figure 2

$$\begin{aligned}
 I_1 - I_2 &= 0 \\
 I_1 &= \frac{U_{R1}}{R_1} ; -U_2 + U_{R2} + U_{R1} = 0 \\
 I_2 &= \frac{U_{R1}}{R_1} \quad U_{R2} = U_2 - U_1 \quad U_1 \bullet \frac{R_1 + R_2}{R_1} = U_2
 \end{aligned}$$

Amplification factor  $\frac{R_1 + R_2}{R_1}$  is greater than one. When we replace resistor  $R_2$  by the short, we get the **voltage follower** – output voltage is the same as input voltage.

### Real Operational Amplifier

Figure 3

$$\begin{aligned}
I_B &\sim I_A \sim 10 \dots 80 \text{ nA} & U_d &= U_A - U_B \sim 3 \dots 10 \text{ mV} \\
I_S &= I_A + I_B & R_d &\sim 1 \text{ M}\Omega \\
I_O &= I_A - I_B & R_{CM} &\sim 100 \text{ M}\Omega \\
U_{CM} &= \frac{U_A + U_B}{2} & R_O &\sim 50 \text{ }\Omega \\
U_2 &= A_{CM} \bullet U_{CM} & A_0 &\sim 10^4 \dots 10^5 \\
H_{CMR} &= 20 \bullet \log \left( \frac{A_0}{A_{CM}} \right) & A_{CM} &\sim 0.1 \\
[H_{CMR}] &= 1 \text{ dB} & H_{CMR} &\sim 100 \text{ dB}
\end{aligned}$$

## Transfer Voltage Characteristic

Figure 4 – non-inverting amplifier

We supply our amplifier by the symmetrical source  $U_{CC}$  and  $-U_{CC}$  with a common ground.

$$|U_{2SAT}| = |U_{CC}| - 1.5$$

For the **rail to rail** amplifiers, it holds true:  $|U_{2SAT}| \approx |U_{CC}|$ . In all real cases, the linear amplifier is only about **3 mV**.

---

Veškeré materiály na této stránce jsou osobními poznámkami autora, vytvořenými na základě univerzitních přednášek. Jsou poskytovány bez záruky a slouží výhradně ke studijním účelům.

Obsah je licencován pod [Creative Commons Uvedte původ-Neužívejte komerčně-Zachovejte licenci 4.0 Mezinárodní](#). To znamená, že materiály můžete volně sdílet a upravovat pro nekomerční účely, pokud uvedete původního autora a zachováte stejnou licenci.

## **Závěrečné informace**

Veškeré materiály v tomto dokumentu jsou osobními poznámkami autora, vytvořenými na základě univerzitních přednášek. Jsou poskytovány bez záruky a slouží výhradně ke studijním účelům.

Datum aktualizace originálu: **26. 12. 2023 v 9:16:20**

Datum vygenerování PDF: **2. 7. 2025 v 14:41:20**

*Licencováno pod Creative Commons BY-NC-SA 4.0.*