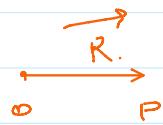


Scalar  $\rightarrow$  magnitude (eg - Temp, mass, ...)

Vector  $\rightarrow$  magnitude & direction. (eg, force, velocity, acceleration)



$$\vec{A} \neq \vec{B}$$

$$\vec{A} = \vec{B}$$

vector of unit mag  $\rightarrow$  unit vector

vector  $\vec{A}$  can be written as

$$\boxed{\vec{A} = A \cdot \vec{a}_A}$$

unit vector in the same direction  
magnitude of  $\vec{A}$

$$\vec{a}_A = \frac{\vec{A}}{A}$$

**Textbooks:**

1. Electromagnetic Waves and Radiating Systems- Jordan and Balmain, PHI, 2nd edition
2. Principles of Electromagnetics Engineering- Matthew N. O.Sadiku , S.V.Kulkarni, Oxford university press, 6<sup>th</sup> edition
3. Antenna Theory: Analysis and Design, Costantine A. Balanis, John Wiley Publication, 4<sup>th</sup> edition
4. Antenna and wave Propagation, John D Kraus, A S Khan, McGraw Hill, 4<sup>th</sup> edition
5. Antenna Theory and Design. Stutzman, Theile, John Wiley and Sons, 3<sup>rd</sup> edition

**Reference Books:**

1. Engineering Electromagnetics, William H Hayt and John A Buck, Tata McGraw-Hill Publishing Company Limited, 7<sup>th</sup> edition
2. Antennas and Radio Wave Propagation, R. E. Collin, McGraw Hill, International Student Edition

## Introduction to Electrostatic Field

- Source:

Stationary Charge

- What is Charge?

Excess or deficiency of Electron in an atomic structure

- Example

Rub the surface of the balloon with the cloth and hold the balloon a short distance above your head and watch your hair stick to it!



- The balloon gains electrons from the cloth and becomes negatively-charged, so it attracts your hair, which is positively-charged

- Coulomb's Law

- Electric Field Intensity,

- Electric Field due to

- {
  - o Point charge
  - o Line charge and
  - o Surface charge distributions

## \* Coulomb's Law.

- Experimental law deals with force between two point charges
- The law states that the force  $F$  between two point charges  $Q_1$  and  $Q_2$  is-
  - directly proportional to the products ( $Q_1 \times Q_2$ ) of the charges
  - Inversely proportional to square of distance ( $R$ ) between them
  - along the line joining them.
  - depends upon medium
  - depends upon the nature of charges (+ or -).



- The force is expressed as -
- $F = \frac{Q_1 Q_2}{4\pi\epsilon R^2}$
- where  $\epsilon$  is permittivity of the medium. For free space  $\epsilon = \epsilon_0 \epsilon_r = \epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$  i.e.  $\epsilon_r = 1$

$$F = \frac{Q_1 Q_2}{4\pi\epsilon R^2}$$

$$\epsilon = \epsilon_0 \cdot \epsilon_r$$

$$\epsilon_r = 1$$

$$\epsilon = \epsilon_0$$

## Vector Form:

- The force  $\bar{F}_2$  on  $Q_2$  due to  $Q_1$  is given by-

$$\therefore \bar{F}_2 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \bar{a}_{12}$$

Where  $\bar{a}_{12}$  is unit vector in the direction of  $\bar{R}_{12}$

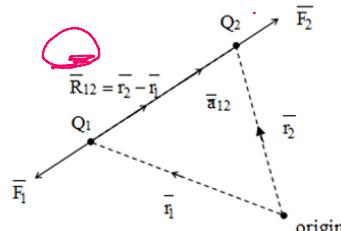
$$\bar{a}_{12} = \frac{\bar{R}_{12}}{|\bar{R}_{12}|} = \frac{\bar{r}_2 - \bar{r}_1}{|\bar{r}_2 - \bar{r}_1|}$$

Similarly, force  $\bar{F}_1$  on  $Q_1$  due  $Q_2$  is given by

$$\bar{F}_1 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{21}^2} \bar{a}_{21}$$

$$= \frac{-Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \bar{a}_{12}$$

$$\bar{F}_1 = -\bar{F}_2$$



$$\epsilon = \epsilon_0 \epsilon_r$$

$$\epsilon_r \approx 1$$

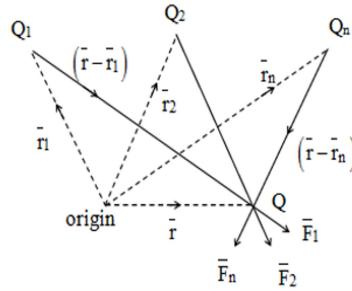
$$\epsilon = \epsilon_0$$

## Principle of Superposition:

- Consider system of  $n$  point charges. The total force is given as-

$$\bar{F} = \bar{F}_1 + \bar{F}_2 + \bar{F}_3 + \dots + \bar{F}_n$$

$$\begin{aligned} &= \frac{QQ_1(\bar{r} - \bar{r}_1)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_1\|)^3} + \frac{QQ_2(\bar{r} - \bar{r}_2)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_2\|)^3} + \dots + \frac{QQ_n(\bar{r} - \bar{r}_n)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_n\|)^3} \\ &= \frac{Q}{4\pi\epsilon_0} \sum_{k=1}^n \frac{Q_k(\bar{r} - \bar{r}_k)}{\|\bar{r} - \bar{r}_k\|^3} \end{aligned}$$



$\Rightarrow$

Consider charge  $Q_1 = 3 \times 10^{-4} C$  at  $M(1, 2, 3)$  &  
 $Q_2 = -10^{-4} C$  at  $N(2, 0, 5) \rightarrow$  in a vacuum  
we desire to find the force exerted on  $Q_2$  by  $Q_1$

The force exerted on  $Q_2$  by  $Q_1$  is given by

$$\rightarrow F_2 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \cdot \vec{a}_{12} = F_2$$

$$\begin{aligned} \vec{r}_{12} &= \vec{r}_2 - \vec{r}_1 = (2-1)\hat{a}_x + (0-2)\hat{a}_y + (5-3)\hat{a}_z \\ R_{12} &= \sqrt{a_x^2 + a_y^2 + a_z^2} \end{aligned}$$

Find  $|R_{12}|$  & the unit vector

$$|\vec{r}_{12}| = 3$$

$$\rightarrow \vec{a}_{12} = \frac{\vec{r}_2 - \vec{r}_1}{|\vec{r}_2 - \vec{r}_1|} = \frac{1}{3} (a_x - 2a_y + 2a_z)$$

$$\therefore F_2 = \frac{3 \times 10^{-4} \times (-10^{-4})}{4\pi (1/36\pi) \times 10^{-9} \times (3)^2} \times \frac{1}{3} (a_x - 2a_y + 2a_z)$$

$$\therefore F_2 = \frac{3 \times 10^{-4} \times (-10^4)}{4\pi(1/36\pi) \times 10^{-9} \times (3)^2} \times \frac{1}{3} (q_2 - 2q_1 + 2q_3)$$

$$F_2 = -30 \left( \frac{q_2 - 2q_1 + 2q_3}{3} \right) N$$

$$F_2 = -10 q_2 + 20 q_1 - 20 q_3 N$$

P1. Three point charges  $Q_1=1 \text{ mC}$ ,  $Q_2=2 \text{ mC}$  and  $Q_3=-3 \text{ mC}$  are respectively located at  $(0,0,4)$ ,  $(-2,6,1)$  and  $(3,-4,-8)$ . Calculate force on  $Q_1$ .

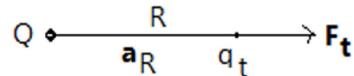
## Electric Field Intensity(E):

- Consider source charge  $Q$ .
- Place test charge( $q_t$ ) in the region surrounding it
- The force experienced by test charge is –

$$F_t = \frac{Qq_t \hat{a}_R}{4\pi\epsilon R^2}$$

- Express it as force per unit charge
- $\frac{F_t}{q_t} = \text{Electric Field Intensity}(E)$

$$E = \frac{Q \hat{a}_R}{4\pi\epsilon R^2}$$



- The electric field intensity( E ) is defined as the force per unit charge.
- Unit=Volts/meter

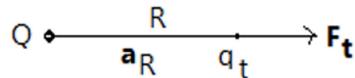
## Electric Field Intensity(E):

- Consider source charge Q.
- Place test charge( $q_t$ ) in the region surrounding it
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$$\mathbf{F}_t = \frac{Qq_t \hat{\mathbf{a}}_R}{4\pi\epsilon R^2}$$

- Express it as force per unit charge
- $\frac{\mathbf{F}_t}{q_t}$  = Electric Field Intensity(E)

$$\mathbf{E} = \frac{Q \hat{\mathbf{a}}_R}{4\pi\epsilon R^2}$$



- The electric field intensity( E) is defined as the force per unit charge.
- Unit=Volts/meter

### \* Principle of superposition

The electric field intensity ( $\bar{E}$ ) due to 'n' pt charges at a pt in free space = vector sum of the ( $E$ ) due to each charge acting alone.

The charges are located by  $\vec{r}_1, \vec{r}_2, \dots, \vec{r}_n$  & the field pt is located by radius vector  $\vec{r}$

$$\bar{E} = \frac{Q_1}{4\pi\epsilon_0} \frac{(\vec{r}-\vec{r}_1)}{|r-r_1|^3} + \frac{Q_2}{4\pi\epsilon_0} \frac{(\vec{r}-\vec{r}_2)}{|r-r_2|^3} + \dots + \frac{Q_n}{4\pi\epsilon_0} \frac{(\vec{r}-\vec{r}_n)}{|r-r_n|^3}$$

$$\boxed{\bar{E} = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^n Q_k \frac{(\vec{r}-\vec{r}_k)}{|\vec{r}-\vec{r}_k|^3}} \rightarrow R$$

- Q) Two pt charges of  $20\text{nC}$  &  $-20\text{nC}$  are situated at  $(1, 0, 0)$  &  $(0, 1, 0)$  in free space. Determine the  $\bar{E}$  at  $(0, 0, 1)$

$$\Rightarrow \begin{aligned} q_1 = 20 \text{ nC at } (1, 0, 0) \rightarrow r_1 = a_x \\ q_2 = -20 \text{ nC at } (0, 1, 0) \rightarrow r_2 = a_y \end{aligned} \quad \left. \begin{array}{l} \\ \end{array} \right\} \Rightarrow \begin{aligned} r - r_1 &= (a_z - a_{x_0}) \\ r - r_2 &= (a_z - a_{y_0}) \end{aligned}$$

$$G \bar{E} \text{ at } (0, 0, 1) \rightarrow r = a_z$$

$$\text{w.k.t. } E = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^n \frac{q_k (r - r_k)}{|r - r_k|^3} = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^2 \frac{q_k (r - r_{k'})}{|r - r_{k'}|^3}$$

$$= \frac{1}{4\pi\epsilon_0} \left[ \frac{20 \times 10^{-9} (a_z - a_x)}{(\sqrt{2})^3} + \frac{(-20 \times 10^{-9}) (a_z - a_y)}{(\sqrt{2})^3} \right]$$

$$E = -63.63 a_x + 63.63 a_y \quad \text{V/m (N/C)}$$

## \* Charge Configurations

- 1) Point charge .
- 2) line charge
- 3) Surface charge
- 4) Volume charge

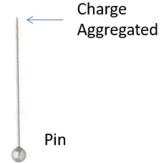
### (1) Point charge

- Point charge: A point charge mean a charge whose dimensions are much smaller than other relevant dimensions

### 2) Line charge

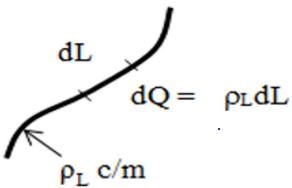
- It has filament like distribution of charge e.g. sharp beam in CRT, charged conductor of very small radius.

- Examples
- Charge aggregated on pin head



- Metallic spheres



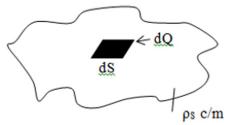


- Consider  $dQ = \rho_L dL$
- We define the line charge density  $\rho_L$  C/m as charge per unit length.
- Hence

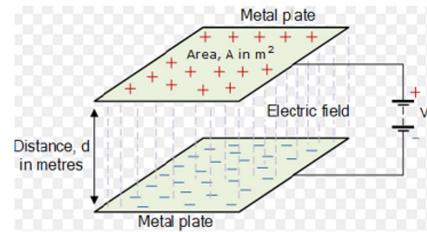
$$\therefore \rho_L = \lim_{dL \rightarrow 0} \frac{dQ}{dL} \text{ C/m}$$

### 3) Surface charge

- An electric charge accumulated on a surface is called surface charge.
- Example: Parallel plate capacitor



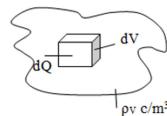
- Consider incremental charge  $dQ = \rho_s dS$
- We define the surface charge density ( $\rho_s$ ) as the charge per unit area.
- Hence  $\therefore \rho_s = \lim_{dS \rightarrow 0} \frac{dQ}{dS} \text{ C/m}^2$



### 4) Volume charge

Here charge is confined within a volume.

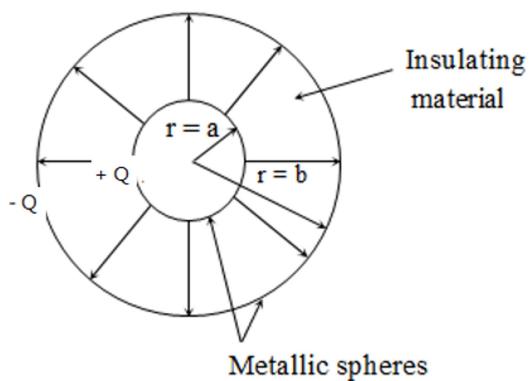
It is volume like distribution of charge  
e.g. Region surrounding cathode in CRT



- Consider  $dQ = \rho_v dV$
- We define the volume charge density  $\rho_v$  C/m as charge per unit volume.
- Hence

$$\rho_v = \lim_{dV \rightarrow 0} \frac{dQ}{dV} \text{ C/m}^3$$

## Faraday's Experiment



- With the equipment dismantled, the inner sphere was given a known positive charge ( $+Q$ )
- The hemispheres were then clamped together around the charged sphere with dielectric material between them.
- The outer sphere was discharged.
- The charge on inner surface of outer sphere is measured.
- Faraday found that the total charge on the outer sphere was equal in magnitude to the original charge placed on the inner sphere
- This was true regardless of the dielectric material separating the two spheres
- He concluded that, there was some sort of 'displacement' from the inner sphere to the outer sphere
- From Faraday's experiment,
- Electric Flux ( $\psi$ )  $\propto$  charge ( $Q$ )
- $\therefore \psi = KQ$
- In SI system,  $K = 1$
- $\therefore \psi = Q$  coulomb

- Faraday found that the total charge on the outer sphere was equal in magnitude to the original charge placed on the inner sphere
- This was true regardless of the dielectric material separating the two spheres
- He concluded that, there was some sort of 'displacement' from the inner sphere to the outer which was independent of the medium
- We will refer this as displacement flux or simply electric flux( $\psi$ )

#### From Faraday's experiment,

- Electric Flux ( $\psi$ )  $\propto$  charge (Q)
- $\therefore \psi = KQ$
- In SI system,  $K = 1$
- $\therefore \psi = Q$  coulomb



## Electric Flux Density( $D$ )

- The electric flux density(**D**) at any point is defined as electric flux or electric displacement per unit area.
- It is a vector quantity.
- Its direction being taken as that of the normal to the surface element which makes the displacement through the element of area a maximum

- The flux density is-**

$$\mathbf{D} = \frac{\text{Flux}}{\text{Area}} = \frac{Q}{4\pi R^2} \hat{\mathbf{a}}_r$$

## \* Relation between **E** and **D**

The electric flux density ( $\bar{D}$ ) at a point P which is at distance  $r$  meters from point charge Q is given as-

$$\bar{D} = \frac{Q}{4\pi r^2} \hat{\mathbf{a}}_r$$


Similarly  $\bar{E}$  at a point P in free space is-

$$\bar{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{\mathbf{a}}_r$$


From above equations

$$\therefore \bar{D} = \epsilon_0 \bar{E} \quad (\text{for free space})$$

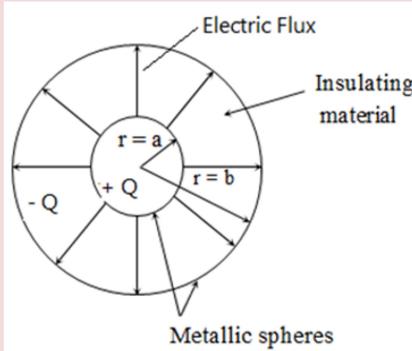
- The Electric field intensity(**E**) is dependent on the medium in which the charge is placed.
- Electric flux density(**D**) is independent of medium
- D** provides the same information as **E** does

## \* Maxwell's Equation for Static Field

### Gauss's Law

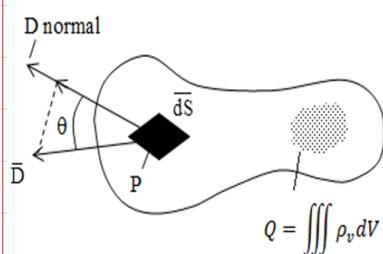
- From Faraday's experiment,
    - Electric Flux ( $\psi$ )  $\propto$  charge (Q)
    - $\therefore \psi = KQ$
    - In SI system,  $K = 1$
    - $\therefore \psi = Q$  coulomb
  - Statement: The electric flux passing through any closed surface is equal to the total charge enclosed by that surface
- 

### • Faraday's Experiment



## Mathematical Form

- Consider volume like distribution of charge, surrounded by a closed surface of any shape
- Let D be the flux density on surface which will vary in magnitude and direction from point to point on the surface.
- The incremental flux( $d\Psi$ ) through incremental surface ( $d\mathbf{S}$ ) are given as-
- $d\Psi = D_{\text{normal}} dS = D \cos \theta dS = \mathbf{D} \cdot d\mathbf{S}$



$\therefore$  total flux through the closed surface

$$\Psi = \int d\Psi = \oint \bar{D} \cdot \bar{dS} \quad \text{--- (3)}$$

*closed surface*

$= \Phi = \text{charge enclosed.}$

$$d\psi = D_{\text{normal}} dS$$

$$d\psi = D \cos\theta \cdot dS \quad \text{--- (1)}$$

$$d\psi = \bar{D} \cdot \bar{dS} \quad \text{--- (2)}$$

$$\Psi = \int d\psi = \oint \bar{D} \cdot \bar{dS} \quad \text{--- (3)}$$

closed surface

$\underline{Q}$  = charge enclosed

For volume charge density ( $\rho_v$ ), we can write

$$\oint_S \bar{D} \cdot \bar{dS} = \int_{\text{Vol}} \rho_v \cdot dv \quad \text{--- (4)}$$

$\hookrightarrow$  Eqn (4) represents

MAXWELL'S EQUATION → Integral form

\* Differential or Point form of Gauss's Law

To obtain point form → use divergence theorem

$\downarrow$   
relates surface integral with volume integral

$$\oint_S \bar{A} \cdot \bar{dS} = \int_{\text{Vol}} (\nabla \cdot \bar{A}) dv$$

Applying Divergence theorem to eqn (4)

$$\therefore \oint_S \bar{D} \cdot \bar{dS} = \int_{\text{Vol}} (\nabla \cdot \bar{D}) \cdot dv = \int_{\text{Vol}} \rho_v dv \quad \text{--- (5)}$$

Comparing two volume integrals

$$\nabla \cdot \bar{D} = \rho_v \quad \text{--- (6)} \quad \text{--- (Maxwell's eqn point-form)}$$

## Divergence defined in all coordinate system

$$\text{div } \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad (\text{cartesian})$$

$$\text{div } \mathbf{D} = \frac{1}{r} \frac{\partial}{\partial r} (r D_r) + \frac{1}{r} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z} \quad (\text{cylindrical})$$

$$\text{div } \mathbf{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_\theta) + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi} \quad (\text{spherical})$$

\* Applications of Gauss's Law

used to determine  $\vec{D}$  &  $\vec{E}$  → symmetrize charge distributions

$\vec{D}$  &  $\vec{E}$  derivations { → L Point-charge  
→ Uniform line charge  
→ → Infinite surface charge

(i) Point-charge

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{ar}$$

$$\vec{E} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{ar} \quad \left\{ \vec{D} = \epsilon_0 \vec{E} \right\}$$

(ii) Uniform line charge

$$\vec{D} = \frac{\epsilon_L}{2\pi r} \hat{a}_\rho$$

$$\vec{E} = \frac{\epsilon_L}{2\pi \epsilon_0 r} \hat{a}_\rho$$

(iii) Infinite surface charge

$$\vec{D} = \frac{\epsilon_S}{2} \hat{a}_z$$

$$\vec{E} = \frac{\epsilon_S}{2\epsilon_0 (z)} \hat{a}_z$$

$$\bar{E} = \frac{\epsilon_0}{\epsilon_0 (2)} \bar{q}_2$$

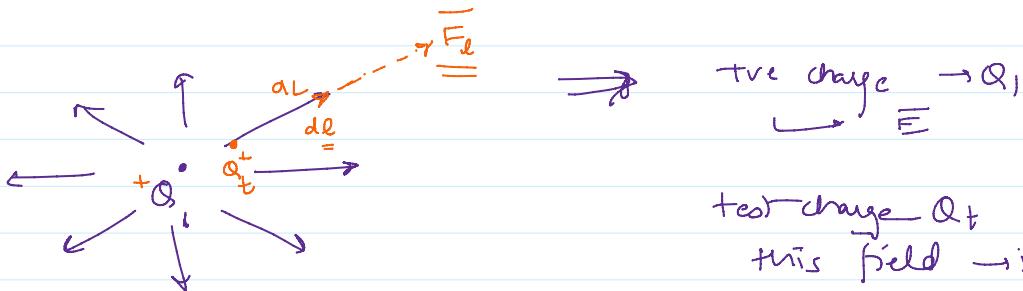
→ (i) Work done

(ii) Potential difference

## \* WORK DONE

Consider a charge  $+Q$  → electric field present -

- - - a unit test charge  $q_t$



test charge  $q_t$  placed in  
this field → it will  
move due to the repulsive  
force.

Let the movement of charge  $q_t \rightarrow dl$

& the direc. of movement  $\rightarrow \bar{a}_L$  (unit vector)

↳ in the direc. of  $dl$

∴ According to Coulomb's law the force exerted by  $\bar{E}$  is given by -

$$\bar{F} = q_t \cdot \bar{E} \quad \text{--- (1)}$$

Thus, the comp'g  $\bar{E}$  in the direction of unit vector  $\bar{a}_L$  is given by -

$$\bar{F}_t = F \cos \theta = \bar{E} \cdot \bar{a}_L = q_t \cdot \bar{E} \bar{a}_L \quad \text{--- (2)}$$

This is the force responsible to move the charge  $q_t$  through the distance  $dl$  in the direction of the field -

To keep the charge in equilibrium

↳ reqd to apply the force which  
is equal & opposite to the force exerted by the  
field in the direc. of  $dl$ .

field in the direction of  $\vec{dl}$ .

$$\vec{F}_{\text{Applied}} = -\vec{F}_E = -Q_t \vec{E} \cdot \hat{a}_L \text{ (N)} \quad \text{---(3)}$$

In this case, the work is said to be done.

$\hookrightarrow$  is expenditure of energy which is given by the prod. of force & the distance

Hence, mathematically the differential work done by an external source in moving the charge  $Q_t$  through a distance  $dl$ , against the direction of field  $\vec{E}$  is given by

$$dW = \vec{F}_{\text{Applied}} \times dl$$

$$= -Q_t \vec{E} \cdot \hat{a}_L \cdot dl \quad \text{---(4)}$$

But distance vector  $dl$

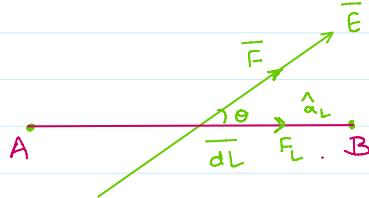
$$\rightarrow dl \cdot \hat{a}_L = dL \quad \text{---(5)}$$

$$dW = -Q_t \vec{E} \cdot \vec{dL} \quad \text{Joules} \quad \text{---(6)}$$

#### \* Electric Potential(V)

- Consider a region of Electrostatic field ( $\vec{E}$ )
- We have to move the charge from B to A
- The force we must apply is equal and opposite to force experienced by charge  $Q$ , i.e., we have to do work.
- Suppose we have to move charge  $Q$  a distance  $dL$  in an electric field  $\vec{E}$ . The force on  $Q$  is

$$\vec{F} = QE \quad \text{---(1)}$$



The component of force in the direction  $dL$ , which must be overcome is

$$F_L = \vec{F} \cdot \hat{a}_L = QE \cdot \hat{a}_L \quad \text{---eqn(2)}$$

We have to apply equal and opposite force to move the charge

$$\vec{F}_{\text{apply}} = -QE \cdot \hat{a}_L \quad \text{---(3)}$$

If it moves through distance  $dL$ , work done will be

$$dW = -QE \cdot dL \quad \text{---(4)}$$

Hence total work done or the potential energy required to move from B to A is -

$$W = -Q \int_{B(\text{initial})}^{A(\text{final})} \vec{E} \cdot dL \quad \text{---(5)}$$

\* Potential Difference (V)  $\Rightarrow$  [units Volts]

Potential difference is defined as work done in moving a unit charge from one point to another in an electric field

$$\therefore \text{Potential difference } (V_{AB}) = \frac{W}{Q} = - \int_B^A \vec{E} \cdot d\vec{L}$$

**P1:** Find potential difference between points A and B at radial distance  $r_A$  and  $r_B$  from a point charge Q.

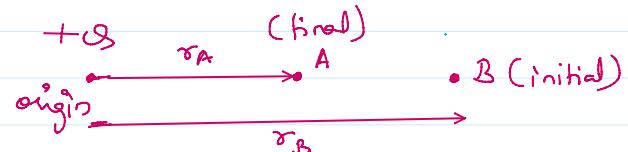
- Consider Charge Q at the origin of the spherical coordinate system

- The  $\mathbf{E}$  is given as

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

- The differential length is

$$d\vec{L} = dr \hat{a}_r$$



- By definition the potential difference is

$$\rightarrow V_{AB} = - \int_B^A \vec{E} \cdot d\vec{L} = - \int_{r_B}^{r_A} \frac{Q}{4\pi\epsilon_0 r^2} \cdot dr = \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r_A} - \frac{1}{r_B} \right]$$

$$\therefore V_{AB} = \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r_A} - \frac{1}{r_B} \right] = V_B - V_A \quad \text{where } V_B \text{ & } V_A \text{ are potentials at B & A}$$

### Absolute Potential (V) also called as Scalar potential

- If we select infinity as reference with zero potential i.e.

- $r_B$  tends to infinity and  $V_B = 0$

- Hence the absolute potential of point A is –

$$V = \frac{Q}{4\pi\epsilon_0 r}$$

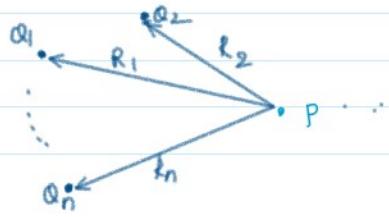
### \* Potential field of a system of charges

Consider a system with n number of pt charges  $q_1, q_2, \dots, q_n$

$$V_p = \frac{q_1}{r_1} + \frac{q_2}{r_2} + \dots + \frac{q_n}{r_n}$$



$$V_p = \frac{Q_1}{4\pi\epsilon_0 R_1} + \frac{Q_2}{4\pi\epsilon_0 R_2} + \dots + \frac{Q_n}{4\pi\epsilon_0 R_n}$$



$$V_p = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^n \frac{Q_k}{R_k}$$

(i) 'V' due to line charge

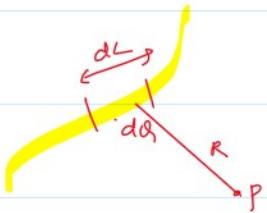
diff charge on the line is given by

$$dQ = \rho_L dL$$

$$\therefore dV = \frac{dQ}{4\pi\epsilon_0 R} = \frac{\rho_L \cdot dL}{4\pi\epsilon_0 R}$$

∴ The total potential at pt P due to line charge is

$$V = \int dV = \int \frac{\rho_L dL}{4\pi\epsilon_0 R}$$



(ii) V due to surface charge

$$V = \int \frac{\sigma ds}{4\pi\epsilon_0 R}$$

(iii) V due to volume charge

$$V = \int \frac{\rho_v dv}{4\pi\epsilon_0 R}$$

$$dW = -Q_t \vec{E} \cdot d\vec{l} \quad \text{Joules} \quad \rightarrow \textcircled{6}$$

The total work done  $\rightarrow$  by integrating the diff work done over the distance from initial position to the final position

$\therefore$  From eqn 6 we have

$$W = \int_{\text{Initial}}^{\text{Final}} dW = \int_{\text{Initial}}^{\text{Final}} -Q_t \vec{E} \cdot d\vec{l}$$

$$\therefore W = -Q \int_{\text{Initial}}^{\text{Final}} \vec{E} \cdot d\vec{l} \quad \rightarrow \textcircled{7}$$

### \* Potential diff (V)

w.k.t. work done in moving the p+ charge  $Q$  from pt-B to pt-A in the electric field  $\vec{E}$  is given by

$$W = -Q \int_B^A \vec{E} \cdot d\vec{l} \quad \rightarrow \textcircled{1}$$

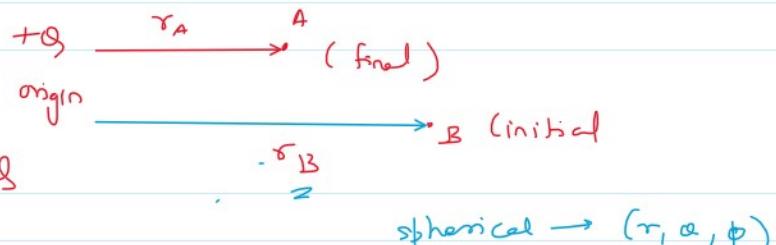
Potential diff (V) is defn as the work done per unit charge in moving the unit charge from B to A in the field  $\vec{E}$

$$V_{AB} = V = \frac{W}{Q} = - \int_B^A \vec{E} \cdot d\vec{l} \quad \rightarrow \textcircled{2}$$

Ex:- Find the potential diff. b/w pts A & B at radial distance  $r_A$  &  $r_B$  from the p+ charge  $Q$

Consider charge  $Q$  at origin

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r}$$



spherical  $\rightarrow (r, \theta, \phi)$

$$dl = dr \hat{r} + r d\theta \hat{\theta} + r \sin\theta d\phi \hat{\phi}$$

$$dL = d\sigma \hat{a}_r$$

$$V_{AB} = - \int_B^A \vec{E} \cdot d\vec{L} = - \int_{r_B}^{r_A} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \cdot [d\sigma \cdot \hat{a}_r] = \int_{r_B}^{r_A} \frac{Q}{4\pi\epsilon_0 r^2} d\sigma$$

$$V_{AB} = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_A} - \frac{1}{r_B} \right)$$

Absolute or scalar potential

It is often convenient to speak  $\rightarrow$  absolute (scalar) potential  
 $\Downarrow$  is possible

If we have selected specific ref pt with zero potential  
 (It is customary to choose infinity as ref-pt)

$\therefore$  The potential at any pt ( $r_B \rightarrow \infty$ ) due to a pt charge  $Q$  located at origin is given by

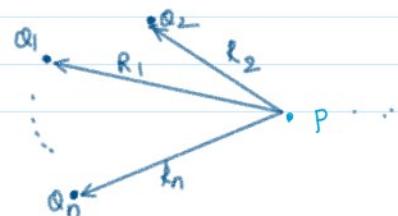
$$V = \frac{Q}{4\pi\epsilon_0 r}$$

\* Potential field of a system of charges

Consider a system with  $n$  number of pt charges  $Q_1, Q_2, \dots, Q_n$

$$V_p = \frac{Q_1}{4\pi\epsilon_0 R_1} + \frac{Q_2}{4\pi\epsilon_0 R_2} + \dots + \frac{Q_n}{4\pi\epsilon_0 R_n}$$

$$V_p = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^n \frac{Q_k}{R_k}$$



(i) 'V' due to line charge

diff charge on the line is given by

$$dL = p \cdot dl$$



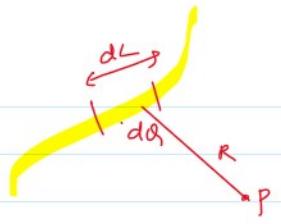
∴  $V = \frac{q}{4\pi\epsilon_0 R}$

$$dQ = \rho_L \cdot dL$$

$$\therefore dV = \frac{dQ}{4\pi\epsilon_0 R} = \frac{\rho_L \cdot dL}{4\pi\epsilon_0 R}$$

∴ The total potential at pt P due to line charge is

$$V = \int dV = \int \frac{\rho_L \cdot dL}{4\pi\epsilon_0 R}$$



(ii)  $V$  due to surface charge

$$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 R}$$

(iii)  $V$  due to volume charge

$$V = \int_V \frac{\rho_v dv}{4\pi\epsilon_0 R}$$

## Relationship between $\bar{E}$ & $\bar{V}$ — Maxwell's equation

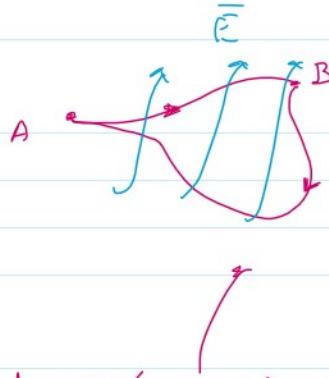
The pot. diff. between pt A & B is independent of the path. Hence,

$$V_{AB} = -V_{BA} \quad \text{--- (1)}$$

$$\therefore V_{AB} + V_{BA} = \oint_L \bar{E} \cdot d\bar{l} \quad \text{--- (2)}$$

(OR)

$$\oint_L \bar{E} \cdot d\bar{l} = 0 \quad \text{--- (3)}$$



This shows that the line integral of  $\bar{E}$  along a closed path (ref. fig.) must be zero.

$\Rightarrow$  Physically this implies that no net work is done in moving a charge along the closed path in an electrostatic field

Apply Stokes theorem to eq (3)

Stokes theorem relates line integral with surface integral

$$\oint_L \bar{A} \cdot d\bar{l} = \int_S (\nabla \times \bar{A}) \cdot d\bar{s}$$

$$\therefore \oint_L \bar{E} \cdot d\bar{l} = \int_S (\nabla \times \bar{E}) \cdot d\bar{s} = 0$$

$$\therefore \nabla \times \bar{E} = 0 \quad \text{--- (4)}$$

Any vector field that satisfies eq (3) & eq (4) is said to be conservative or irrotational field

\* Potential gradient

$$\text{w.k.t. } V = - \int \bar{E} \cdot d\bar{l}$$

$$dV = -\bar{E} \cdot d\bar{l} = -E_x dx - E_y dy - E_z dz$$

(a)

$dV \rightarrow$  change in 'v'  $\rightarrow$  from vector calculus we have

$$dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz \quad \text{---(b)}$$

Comparing (a) & (b)

$$E_x = -\frac{\partial V}{\partial x}; \quad E_y = -\frac{\partial V}{\partial y}; \quad E_z = -\frac{\partial V}{\partial z}$$

$\therefore$  Thus,  $E = -\nabla V$

→ (2)

Hence  $\bar{E}$  is the gradient of  $V$ . The -ve sign shows that the direction of  $\bar{E}$  is opposite to the direction in which  $V$  increases.

NOTE

1) Cartesian coordinate system

$$\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$$

2) Cylindrical coordinate system

$$\nabla V = \frac{\partial V}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial V}{\partial \phi} \hat{a}_\phi + \frac{\partial V}{\partial z} \hat{a}_z$$

3) Spherical coordinate system

$$\nabla V = \frac{\partial V}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \hat{a}_\phi$$

\* Energy Density in Electrostatic field ( $W_E$ )

It is def as energy / cubic meter

$$\therefore W_E = \frac{1}{2} \bar{D} \cdot \bar{E}$$

$$= \frac{1}{2} \epsilon E^2$$

$$= \frac{1}{2} \frac{\bar{D}^2}{\epsilon} \quad \text{Joules.}$$

The energy stored in terms of energy density is

$$W = \int_{\text{vol}} \rho E dV = \frac{1}{2} \int \bar{D} \cdot \bar{E} dV$$

\* Current, Current-density and continuity equation

(i) Current  $\rightarrow$  electric charge in motion constitutes ch

$$I = \frac{dQ}{dt} \quad \text{--- (1)}$$

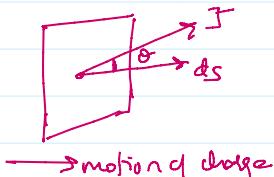
(ii) Current-density ( $\bar{J}$ )

$\bar{J}$  at a given pt is defined as the ch through a unit normal area at that pt. The incremental amount of ch  $dI$  crossing an incremental surface  $dS$  is

$$dI = \bar{J} dS \cos \theta$$
$$= \bar{J} \cdot d\vec{s}$$

$\therefore$  The total ch is given by

$$\boxed{I = \int_S \bar{J} \cdot d\vec{s}} \quad \text{--- (2)}$$



→ motion of charge

## \* Current, Current density and continuity equation

(i) Current  $\rightarrow$  electric charge in motion constitutes CIn

$$I = \frac{dQ}{dt} \quad \text{--- (1)}$$

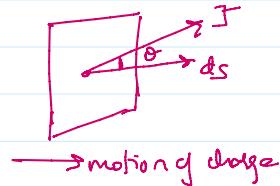
(ii) Current density ( $\bar{J}$ )

$\bar{J}$  at a given pt. is defined as the CIn through a unit normal area at that pt. The incremental amount of CIn  $dI$  crossing an incremental surface  $ds$  is

$$dI = J ds \cos\theta \\ = \bar{J} \cdot \bar{ds}$$

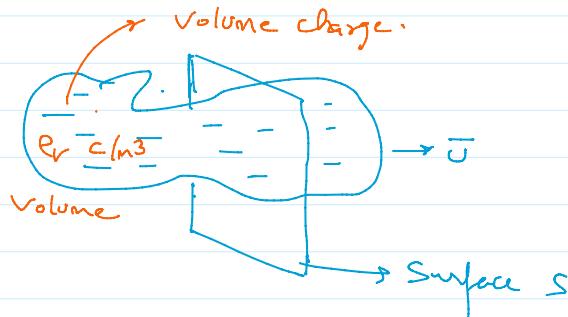
$\therefore$  The total CIn is given by

$$I = \int_s \bar{J} \cdot \bar{ds} \quad \text{--- (2)}$$



## \* Convection CIn density

when charge passes through surface 's' it constitutes a convection CIn with density ( $\bar{J}$ )



$$\bar{J} = \rho_v \bar{v} \quad \text{--- (3)}$$

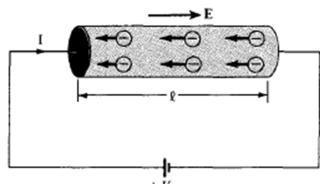
where  $\rho_v \rightarrow$  vol. charge density

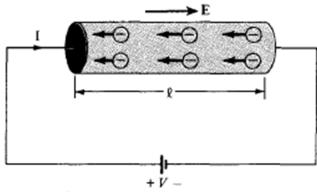
\* Do not satisfy Ohm's law

$\bar{v} \rightarrow$  velocity to the right

- It occurs when current flows through insulating medium such as liquid, vacuum etc. Example: Electron beam in CRT

## \* Conduction CIn density





When an electric field is applied to a conductor, conduction current occurs due to the drift motion of electrons.

$\therefore$  Current density is given by

$$\bar{J} = \sigma \bar{E} \quad \text{--- (4)}$$

where

$\sigma \rightarrow$  conductivity of the material

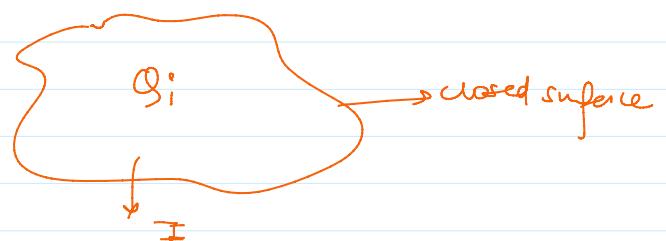
## \* Continuity Equation

### Conservation of Charge:-

"The Principle of conservation of charge states that Charge can be neither created nor destroyed. Although equal amounts of positive and negative charge may be simultaneously created, obtained by separation, destroyed or lost by recombination".

The current through the closed surface is given by

$$I = \oint_S \bar{J} \cdot d\bar{s} \quad \text{--- (1)}$$



This outward flow must be balanced by a decrease in net charge within the closed surface

$Q$  &  $eV$

$$I = \oint_S \bar{J} \cdot d\bar{s} = - \frac{dQ_i}{dt} \quad \text{--- (2)}$$

$$\therefore I = \oint_S \bar{J} \cdot d\bar{s} = - \frac{d}{dt} \int_{\text{vol.}} e_V dv \quad \text{--- (3)}$$

$\Rightarrow$  Integral form of  
CONTINUITY EQUATION

Apply divergence theorem

$$\therefore \oint_{\text{S}} \bar{J} \cdot d\bar{s} = \int_{\text{Vol}} (\nabla \cdot \bar{J}) dv = -\frac{\partial}{\partial t} \int_{\text{Vol}} \rho v dv$$

If the surface is kept constant, the derivative becomes partial derivative & may appear within the integral sign

$$\therefore \int_{\text{Vol}} (\nabla \cdot \bar{J}) dv = - \int_{\text{Vol}} \frac{\partial \rho v}{\partial t} dv$$

Since this expression is true for any volume, it is true for incremental volume

$$\therefore \nabla \cdot \bar{J} = -\frac{\partial \rho v}{\partial t} \quad \text{--- (4)}$$

⇒ Point form of  
CONTINUITY  
EQN

### Poisson's & Laplace's Equation

Poisson's & Laplace's eq<sup>n</sup> are easily derived from  
Gauss's Law.

$$\nabla \cdot \bar{J} = \rho v \quad \text{--- (1)}$$

$$\text{w.k.t} \quad \bar{D} = \epsilon \bar{E} \quad \text{--- (2)}$$

& also the gradient relationship for  $\bar{E}$

$$\bar{E} = -\nabla V \quad \text{--- (3)}$$

Substituting (2) & (3) in (1)

$$\nabla \cdot \bar{J} = \nabla \cdot (\epsilon \bar{E}) = \nabla \cdot (-\epsilon \nabla V) = \rho v$$

For a homogeneous medium in which ' $\epsilon$ ' is constant

$$\nabla \cdot \nabla V = -\frac{\rho v}{\epsilon}$$

↓

$$\nabla^2 V = -\frac{\rho_v}{\epsilon} \quad \text{Eq ④}$$

This is known as POISSON'S EQ<sup>N</sup>

A special case of the above eq<sup>n</sup> occurs when  $\rho_v=0$  (ie. for a charge free region).  
 $\therefore$  Eq<sup>n</sup> ④ is written as,

$$\nabla^2 V = 0 \quad \text{LAPLACE'S EQ<sup>N</sup>}$$

i) FCS  $\Rightarrow \nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$

ii) CCS  $\Rightarrow \nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \theta^2} + \frac{\partial^2 V}{\partial \phi^2}$

iii) SCS  $\Rightarrow \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{r^2 \sin \theta \sin \phi} \frac{\partial^2 V}{\partial \phi^2}$

If a potential  $V = r^2yz + A y^3 z$

(i) Find 'A' so that Laplace's eq<sup>n</sup> is satisfied.

(ii) With the value of 'A' determine elec. field at (2, 1, -1)

## Application of Laplace's and Poisson's Equation

- Using Laplace or Poisson's equation we can obtain:
  1. Potential at any point in between two surface when potential at two surface are given.
  2. We can also obtain capacitance between these two surface.

## POYNTING THEOREM

27 February 2023 20:03

### Poynting Theorem :

When electromagnetic waves propagate through space from their source to distant receiving points, there is a transfer of energy from the source to the receivers. In order to find the power in an electromagnetic waves, it is necessary to develop a power theorem, which is known as Poynting theorem. It can be obtained from Maxwell's equation as follows

Consider Maxwell's equation from modifies Ampere's circuit law,

$$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t} \quad \dots (1)$$

Dot each side of equation (1) with  $\bar{E}$

$$\bar{E} \cdot (\nabla \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t} \quad \dots (2)$$

Now make use of vector identity,

$$\nabla \cdot (\bar{E} \times \bar{H}) = \bar{H} \cdot \nabla \times \bar{E} - \bar{E} \cdot \nabla \times \bar{H} \quad \dots (3)$$

from (2) and (3)

$$\therefore \bar{H} \cdot \nabla \times \bar{E} - \nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t} \quad \dots (4)$$

but  $\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$

and therefore,

$$-\bar{H} \cdot \frac{\partial \bar{B}}{\partial t} - \nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t} \quad \dots (5)$$

or

$$-\nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \epsilon \bar{E} \cdot \frac{\partial \bar{E}}{\partial t} + \mu \bar{H} \cdot \frac{\partial \bar{H}}{\partial t} \quad \dots (6)$$

However

$$\epsilon \cdot \bar{E} \cdot \frac{\partial \bar{E}}{\partial t} = \frac{\epsilon}{2} \frac{\partial E^2}{\partial t} = \frac{\partial}{\partial t} \left( \frac{\epsilon E^2}{2} \right)$$

$$\mu \bar{H} \cdot \frac{\partial \bar{H}}{\partial t} = \frac{\mu}{2} \frac{\partial H^2}{\partial t} = \frac{\partial}{\partial t} \left( \frac{\mu H^2}{2} \right)$$

Thus equation (6) becomes,

$$-\nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \frac{\partial}{\partial t} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) \quad \dots (7)$$

Integrate equation (7) throughout a volume

$$-\int_{\text{vol}} \nabla \cdot (\bar{E} \times \bar{H}) dv = \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv + \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \quad \dots (8)$$

Apply divergence theorem to left hand side of equation (8)

$$-\oint_s (\bar{E} \times \bar{H}) \cdot d\bar{s} = \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv + \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \quad \dots (9)$$

The equation (9) can be written as

$$\begin{aligned} \oint_s (\bar{E} \times \bar{H}) \cdot d\bar{s} &= - \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv - \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \\ &\text{I term} \qquad \text{II term} \qquad \text{III term} \end{aligned} \quad \dots (10)$$

Equation (10) is referred to as Poynting theorem

**Physical Interpretation :**

$$\text{II term : } \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv$$

This term represents power dissipated in the volume V. Consider a conductor of cross sectional area A, carrying current I and voltage drop E per unit length. Therefore power loss per unit length is EI.

∴ Power dissipated per unit volume would be

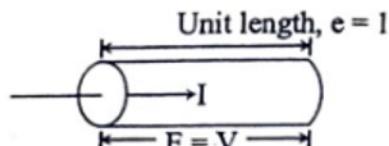
$$\frac{EI}{A} = E J \text{ watts per unit volume.}$$

∴ In general, when  $\bar{E}$  and  $\bar{J}$  are not in same direction,

$$\text{Power dissipated per unit volume} = \bar{E} \cdot \bar{J}$$

∴ The total power dissipated in a volume V would be

$$\int_v (\bar{E} \cdot \bar{J}) dv$$



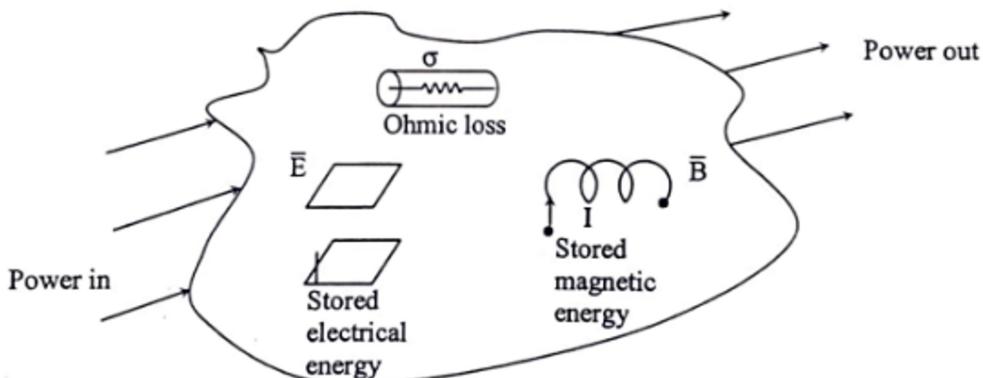
$$\text{III term : } -\frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv$$

In electrostatic, the quantity  $\frac{1}{2} \epsilon E^2$  is energy density or stored energy per unit volume of the electric field. Also for the steady magnetic field the quantity  $\frac{1}{2} \mu H^2$  represents the stored energy density of the magnetic field. The negative time derivative of this quantity represents the rate at which the stored energy in the volume is decreasing.

$$\text{I}^{\text{st}} \text{ term : } \oint_s (\bar{E} \times \bar{H}) \cdot ds$$

The interpretation of I term follows from the application of the law of conservation of energy. The rate of energy dissipation in the volume v must equal the rate at which the stored energy in v is decreasing, plus the rate at which energy is entering the volume v from outside.

$\therefore \oint_s (\bar{E} \times \bar{H}) \cdot ds$  represents outward flow of energy through the surface enclosing the volume and  $-\oint_s (\bar{E} \times \bar{H}) \cdot ds$  represents inward flow of energy through the surface enclosing the volume.



**Statement :** The net power flowing out of a given volume v is equal to the time rate of decrease in the energy stored within v minus the conduction loss :

#### The Poynting Vector :

The interpretation of poynting theorem, leads to the conclusion that the integral of  $\bar{E} \times \bar{H}$  over any, closed surface gives the rate of energy flow through that surface. This cross product  $\bar{E} \times \bar{H}$  is known as poynting vector  $\bar{P}$ ,

$$\bar{P} = \bar{E} \times \bar{H} \quad \dots (11)$$

The poynting vector has dimensions of watts per square meter. It is a measure of rate of energy flow per unit area at that point. The direction of flow is perpendicular to  $\bar{E}$  and  $\bar{H}$  in the direction of the vector  $\bar{E} \times \bar{H}$ .

In perfect dielectrics,  $\bar{E}$  and  $\bar{H}$  fields are given as

$$E_x = E_0 \cos(\omega t - \beta z)$$

$$H_y = \frac{E_0}{\eta} \cos(\omega t - \beta z)$$

The Poynting vector is

$$\bar{P} = \bar{E} \times \bar{H}$$

$$\therefore P_z \hat{a}_z = E_x \hat{a}_x \times H_y \hat{a}_y$$

$$\therefore P_z = \frac{E_0^2}{\eta} \cos^2(\omega t - \beta z)$$

To find the time average power density, integrate over one cycle and divide by the period  $T = \frac{1}{f}$ .

$$\begin{aligned} \therefore P_{z, \text{av}} &= f \int_0^{1/f} \frac{E_0^2}{\eta} \cos^2(\omega t - \beta z) dt \\ &= \frac{f}{2} \frac{E_0^2}{\eta} \int_0^{1/f} [1 + \cos(2\omega t - 2\beta z)] dt \\ &= \frac{f}{2} \frac{E_0^2}{\eta} \left[ t + \frac{1}{2\omega} \sin(2\omega t - 2\beta z) \right]_0^{1/f} \\ &= P_{z, \text{av}} = \frac{1}{2} \frac{E_0^2}{\eta} \frac{\omega}{m^2} \end{aligned} \quad \dots (12)$$

If medium is lossy dielectric,

$$E_x = E_0 e^{-\alpha z} \cos(\omega t - \beta z)$$

$$H_y = \frac{E_0}{|\eta|} e^{-\alpha z} \cos(\omega t - \beta z - \theta_n)$$

$$\therefore P_z = \frac{E_0^2}{|\eta|} e^{-2\alpha z} \cos(\omega t - \beta z) \cos(\omega t - \beta z - \theta_n)$$

$$\therefore P_{z, \text{av}} = \frac{1}{T} \int_0^T P_z dt$$

$$\therefore \cos A \cos B = \frac{1}{2} [\cos(A-B) + \cos(A+B)]$$

$$P_{z, \text{av}} = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} \cos \theta_n$$

If we use, rms values instead of peak amplitudes, the factor of  $\frac{1}{2}$  would not be present. It can be shown that, the time average poynting vector can be also written as

$$P_z, \text{av} = \frac{1}{2} \operatorname{Re} (\bar{E} \times \bar{H})$$

Finally, the average power flowing through any area 'S' normal to the z-axis is

$$P_{\text{ave}} = \frac{1}{2} \frac{E_0^2}{\eta} S \text{ watt.} \quad \dots (13)$$

For any given surface 'S', it is given by

$$P_{\text{ave}} = \int_S \bar{P}_{\text{av}} \cdot d\bar{S} \quad \dots (14)$$

Q) If a potential  $V = x^2yz + Ay^3z$

(i) Find  $A$  so that Laplace's eq<sup>n</sup> is satisfied.

(ii) With the value of 'A' determine elec. field at  $(2, 1, -1)$

$$V = x^2yz + Ay^3z \leftarrow$$

(i) Find  $A$

Laplace's eq<sup>n</sup> in CCS (RCS)

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = 0 \quad \text{--- (1)}$$

$$\frac{\partial V}{\partial x} = 2xyz; \quad \frac{\partial^2 V}{\partial x^2} = 2yz$$

$$\frac{\partial V}{\partial y} = x^2z + 3Ay^2z; \quad \frac{\partial^2 V}{\partial y^2} = 0 + 6Ayz$$

$$\frac{\partial V}{\partial z} = x^2y + Ay^3; \quad \frac{\partial^2 V}{\partial z^2} = 0$$

Substituting above values in eq<sup>n</sup> (1)

$$\nabla^2 V = 2yz + 6Ayz = 0$$

$$\therefore A = -1/3$$

(ii)  $\vec{E}$  at  $(2, 1, -1)$

$$\vec{E} = -\nabla V = - \left[ \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right]$$

w.k.t.

$$V = x^2yz - \frac{1}{3}y^3z$$

$$\vec{E} = -(2xyz) \hat{a}_x + (x^2z - \frac{3y^2z}{3}) \hat{a}_y + (x^2y - \frac{y^3}{3}) \hat{a}_z$$

$$\therefore \vec{E} \text{ at } (2, 1, -1) = 4 \hat{a}_x + 3 \hat{a}_y - \frac{11}{3} \hat{a}_z$$

\* Steady Magnetic field

$\rightarrow$  Biot Savart's Law (Coulomb's Law)

## → Ampere's Circuital Law (Gauss's law)

→ static. Elec. field  $\rightarrow$  charac. by  $\vec{E}$  or  $D$

Likewise

Static mag. field  $\rightarrow$  charac. by  $\vec{H}$  or  $B$

Electrostatics  $\rightarrow$  produced by static or stationary charges

If charges are moving with const. velocity  $\Rightarrow$   $\underbrace{\text{magnetostatic field}}$   
 $\underbrace{\text{is produced}}$

Magnetic field in free space due to direct curr. is considered.

Two major Law's governing magnetostatic fields

1) Biot-Savart Law (Ampere Law)

2) Ampere Circuital Law

\* Biot-Savart's Law.

It gives differential magnetic field intensity ( $d\vec{H}$ ) due to differential curr. element ( $I dL$ )

Mag. of  $d\vec{H}$  at pt P is proportional to  
the product of curr., diff. length  $dL$  & the sine  $I$   
of  $\angle \theta$  b/w the filament & the line connecting  
differential length to the pt. of interest - P.

It is inversely prop. to the square of the distance from  
filament to point P. The constant of proportionality is given  
by  $(1/4\pi)$

$$\therefore d\vec{H} = \frac{I dL \sin \theta}{4\pi R^2}$$



Direction of  $d\vec{H}$  is normal to the plane containing the diff. element & the  
line drawn from the filament to the pt. P.

In vector notation

$- \quad - \quad - \quad -$

$$d\vec{H} = \frac{I dL \sin \theta}{4\pi R^2} \hat{n}$$

In vector notation

$$d\bar{H} = \frac{I d\bar{L} \times \hat{a}_R}{4\pi R^2}$$

where

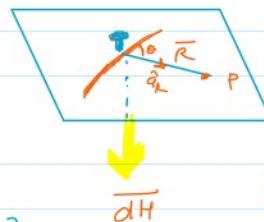
$\hat{a}_R \rightarrow$  unit vector from diff ch element to pt P

$d\bar{L} \Rightarrow$  differential ch element

$R \Rightarrow$  distance of diff ch element from pt P

$\therefore$  Biot-Savart Law is integral form

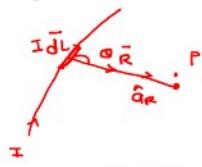
$$\bar{H} = \int \frac{I d\bar{L} \times \hat{a}_R}{4\pi R^2}$$



Right-hand screw

## Biot-Savart for different current distributions

A) Line current



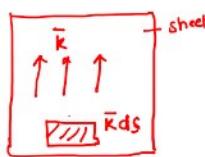
$$d\bar{H} = \frac{I d\bar{L} \times \hat{a}_R}{4\pi R^2}$$

Total magnetic field intensity ( $\bar{H}$ )

$$\bar{H} = \int_L \frac{I d\bar{L} \times \hat{a}_R}{4\pi R^2}$$

⑤

B) Surface current

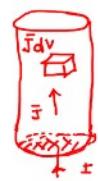


$\bar{k}$  = surface current density ( $A/m$ )  
(current per unit width)

$$\bar{H} = \int_S \frac{\bar{k} dS \times \hat{a}_R}{4\pi R^2}$$

⑥

C) Volume current



$\bar{j}$  = volume current density ( $A/m^2$ )

$$\bar{H} = \int_V \frac{\bar{j} dv \times \hat{a}_R}{4\pi R^2}$$

$$\begin{aligned} I dL &= \bar{k} dS \\ &= \bar{j} dv \end{aligned}$$

④

Biot-Savart's is also called as Ampere's law for the (Co) elements -

### Applications

(i)  $\vec{H}$  due to infinitely long straight conductor

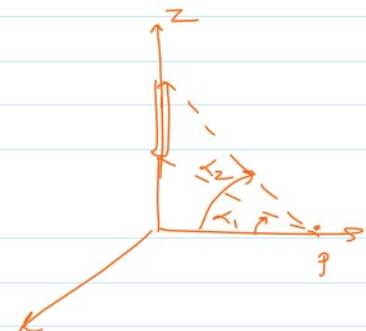
$$\rightarrow \vec{H} = \frac{I}{2\pi r} \hat{a}_\phi \text{ Am}$$

$$\rightarrow \vec{B} = \mu \vec{H} = \frac{\mu I}{2\pi r} \hat{a}_\phi \text{ wb/m}^2$$

(ii)  $\vec{H}$  due to straight conductor of finite length

$$\vec{H} = \frac{I}{4\pi r} [\sin \alpha_2 - \sin \alpha_1] \hat{a}_\phi \text{ Am}$$

$$\vec{B} = \mu \vec{H} = \frac{\mu I}{4\pi r} [\sin \alpha_2 - \sin \alpha_1] \hat{a}_\phi \text{ wb/m}^2$$



(iii)  $\vec{H}$  at the centre of a circular conductor

$$\vec{H} = \frac{I}{2R} \hat{a}_\theta \text{ Am}$$

$$\vec{B} = \mu \vec{H} = \frac{\mu I}{2R} \hat{a}_\theta \text{ wb/m}^2$$

### \* Ampere's Circuital Law

#### Statement :-

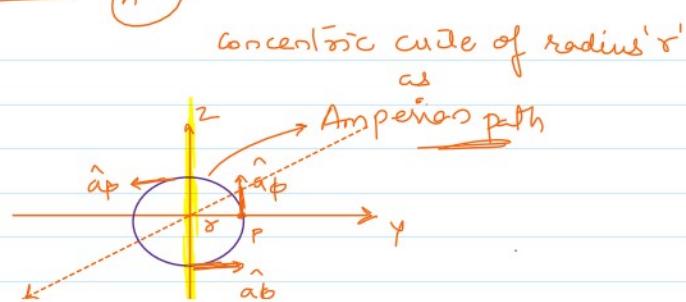
Ampere's circuital law states that the line integral of the tangential component of the magnetic field around a closed path is equal to the (Co) enclosed by the path.

$$\oint \vec{H} \cdot d\vec{l} = I_{\text{enc}} \quad \text{--- (A)}$$

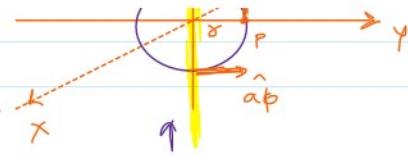
Proof :- Here  $\vec{H} = H_\phi \hat{a}_\phi$

$$\therefore d\vec{l} = r d\phi \hat{a}_\phi \quad \text{--- (1)}$$

while  $\vec{H}$  obtained at pt P, from Biot-Savart's



while  $\bar{H}$  obtained at pt P from Biot-Savart's law due to infinitely long conductor is given by



$$\bar{H} = \frac{I}{2\pi r} \hat{a}_\phi \quad \text{---(2)}$$

$$I \underset{\text{end}}{=} I$$

$$\therefore \bar{H} \cdot d\bar{l} = \frac{I}{2\pi r} \cdot \hat{a}_\phi \cdot (r d\phi \hat{a}_\phi)$$

$$= \frac{I}{2\pi r} r d\phi = \frac{I}{2\pi} d\phi$$

Integrating  $\bar{H} \cdot d\bar{l}$  over the entire closed path

$$\oint \bar{H} \cdot d\bar{l} = \int_{\phi=0}^{2\pi} \frac{I}{2\pi} d\phi = \frac{I}{2\pi} [2\pi] = I = \text{current enclosed by the conductor}$$

This proves that the integral  $\bar{H} \cdot d\bar{l}$  along the closed path gives the area enclosed by that closed path.

Appn

(i)  $\bar{H}$  due to infinitely long straight conductor

(ii)  $\bar{H}$  due to infinite sheet of current

Curl

$$\text{Curl } \bar{H} = \nabla \times \bar{H} = \bar{J} \Rightarrow \text{gt-form of amperes circuital law.}$$

w.k.t.

$$\oint \bar{H} \cdot d\bar{l} = I_{\text{end.}} \quad \text{---(1)}$$

The above eqn can also be expressed as

$$\oint \bar{H} \cdot d\bar{l} = \mathcal{F}_{\text{end.}} = \int_S \bar{J} \cdot d\bar{s} \quad \text{---(2)}$$

Applying Stokes theorem to eqn (2)

$$\oint_L \bar{H} \cdot d\bar{l} = \int_S (\nabla \times \bar{H}) \cdot d\bar{s} = \int_S \bar{J} \cdot d\bar{s}$$

Comparing the surface integrals

-  $\int_S$  -

Comparing the surface integrals

$$\nabla \times \vec{H} = \vec{J} \quad \text{--- (3)}$$

$\hookrightarrow$  Maxwell's eq in pt form

\* Magnetic flux density ( $\vec{B}$ )

$\omega \cdot k \cdot t$

$$\vec{B} = \mu_0 \vec{H} \quad \text{--- (1)}$$

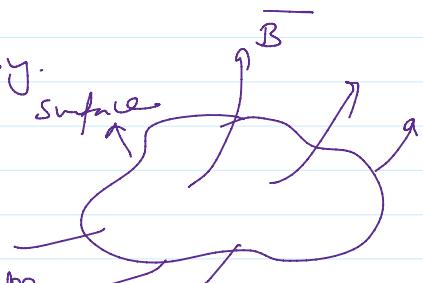
$$\vec{D} = \epsilon_0 \vec{E}$$

$$\vec{B} = \mu_0 H$$

where  $\mu_0 = \text{permeability of free space}$   
 $= 4\pi \times 10^{-7} \text{ Vs/A m}$

Mag. flux through an open surface ' $S$ ' is given by.

$$\phi = \int_S \vec{B} \cdot d\vec{s} \quad \text{--- (3)}$$



The flux penetrating a closed surface is equal to the flux leaving the closed surface. Therefore, for a closed surface,

$$\oint_S \vec{B} \cdot d\vec{s} = 0 \quad \text{--- (4)}$$

Applying divergence theorem

$$\oint_S \vec{B} \cdot d\vec{s} = \int_V (\nabla \cdot \vec{B}) \cdot dV = 0$$

or

$$\int_V (\nabla \cdot \vec{B}) \cdot dV = 0 \quad \text{--- (5)}$$

$\rightarrow$  This is called as  $\beta$ -form or diff form  
of Gauss's Law for MAGNETIC FIELD

4<sup>th</sup> Maxwell eq

Maxwell's eq for static field

Maxwells eq<sup>n</sup> for static field

magnetic & electric

Differential (pt form)

$$1) \nabla \cdot \vec{D} = \rho_v \quad \left. \begin{array}{l} \\ \text{div} \end{array} \right\}$$

$$2) \nabla \cdot \vec{B} = 0$$

$$3) \nabla \times \vec{E} = 0 \quad \left. \begin{array}{l} \\ \text{curl} \end{array} \right\}$$

$$4) \nabla \times \vec{H} = \vec{J} \quad \left. \begin{array}{l} \\ \text{curl} \end{array} \right\}$$

Integral form

$$\oint \vec{D} \cdot d\vec{s} = \int \rho_v dV$$

$$\oint \vec{B} \cdot d\vec{s} = 0$$

$$\int_s \vec{B} \cdot d\vec{s} = 0$$

$$\oint \vec{E} \cdot d\vec{l} = 0$$

$$\oint_L \vec{H} \cdot d\vec{l} = \int_S \vec{J} \cdot d\vec{s}$$

Remark

→ Gauss's Law

→ Non-existence of mag. monopole

→ Conservation nature of  
elec.-static field

## \* Scalar Magnetic Potential ( $V_m$ ), Vector potential ( $\bar{A}$ )

Mag. potential  $\begin{cases} \text{Scalar } (V_m) \\ \text{Vector } (\bar{A}) \end{cases}$

### ① Scalar Mag. Potential ( $V_m$ )

The mag. field intensity ( $\bar{H}$ )

$$\bar{H} = -\nabla V_m \quad \text{--- (1)}$$

Minus signs  $\rightarrow$  analogy to the electric potential

This definition must satisfy results of magnetic fields.  
i.e., example.

$$\nabla \times \bar{H} = \bar{J} \quad \text{--- (2)}$$

from (1) & (2)

$$\nabla \times (-\nabla V_m) = \bar{J} \Rightarrow$$

w.r.t. curl of gradient of any scalar  $\Rightarrow$

Thus to define  $\bar{H}$  as gradient of a scalar mag. potential, the curl density must be zero throughout the region in which scalar mag. potential is defined.

$$\therefore \bar{H} = (-\nabla V_m) \text{ if } \bar{J} = 0 \quad \text{--- (3)}$$

## \* Vector mag potential ( $\bar{A}$ )

From magnetostatic field w.r.t.,

$$\nabla \cdot \bar{B} = 0 \quad \text{--- (1)}$$

Also from vector calculus, divergence of curl of any vector field is zero

$\hookrightarrow$  i.e.  $\nabla \cdot (\nabla \times \bar{A}) = 0 \quad \text{--- (2)}$

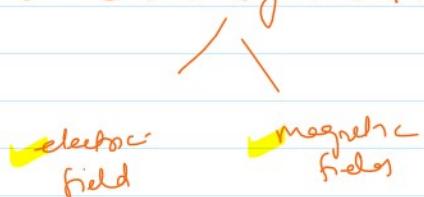
In order to satisfy eq<sup>n</sup>s (1) & (2) simultaneously

$$\vec{B} = \nabla \times \vec{A} \quad \text{--- (3)}$$

where  $\vec{A}$  signifies a vector magnetic potential.

1.0		Introduction to Static fields
	1.1	Charge, Coulomb's law, Charge configurations, Electric field intensity, Electric flux density, Gauss's law and applications, Current density, and Continuity equation
	1.2	Scalar Electric Potential, Potential gradient, Laplace's and Poisson's equations
	1.3	Biot Savart Law, Ampere Circuit law, Gauss's law for magnetic field, Vector magnetic potential
2.0		Electromagnetic Field and Maxwell's Equations
	2.1	Faraday's Law, Displacement current density, Maxwell's equation for time varying field, Boundary conditions.
	2.2	EM wave propagation through lossy, perfect dielectric and conducting medium.
	2.3	Power in EM Wave: Poynting theorem and Poynting vector

## Chapter 2:- Electromagnetic Field & Maxwell's Equations



- ① static elec. field → produced by stationary electric charges
- ② static mag. field → motion of the electric charges with uniform velocity
- ③ Time varying field → produced due to time varying chgs

\* Faradays Law  $\Rightarrow$  Maxwell eq<sup>n</sup>

He observed that

- { (i) when a closed path moves in a mag-field → emf gets induced & this may establish chgs in a suitable closed cur-
- (ii) when closed path is kept fixed & the mag. field is varied ↑  
effect → commonly called → electromagnetic induction.

Faradays law can be stated as

$$e.m.f = e = -N \frac{d\phi}{dt} \quad \text{volts} \quad \text{--- (4)}$$

N → no. of turns (Assume N=1 → single turn)

$N \rightarrow$  no. of turns (Assume  $N=1 \rightarrow$  single turn)  
 $e \rightarrow$  induced e.m.f.

$$\therefore e = - \frac{d\phi}{dt} \quad \text{--- (2)}$$

Lenz's Law  $\rightarrow$  The direction of induced emf is such that it opposes the cause producing it i.e. changes in mag. flux.

We already know that there must exist an electric field inside a conductor to sustain a C/I within the conductor. So we define the induced e.m.f. in a conductor in terms of induced elec. field intensity ( $E$ ) inside the conductor as

$$\text{emf} = e = \oint \vec{E} \cdot d\vec{l} \quad \text{--- (3)}$$

where path of integration is in the direction of the induced C/I

Also, The total flux enclosed by a closed path is expressed as

$$\Phi = \int_S \vec{B} \cdot d\vec{s} \quad \text{--- (4)}$$

From eq<sup>n</sup>s  $\textcircled{2}$ ,  $\textcircled{3}$  &  $\textcircled{4}$

$$e = - \frac{d\Phi}{dt} = \oint \vec{E} \cdot d\vec{l} = - \frac{d}{dt} \int_S \vec{B} \cdot d\vec{s} \quad \text{--- (5)}$$

$$\oint \vec{E} \cdot d\vec{l} = - \frac{d}{dt} \int_S \vec{B} \cdot d\vec{s} \quad \text{--- (5)}$$

There are 2 conditions for the induced emf as explained below

case(i) :- A closed circuit stationary, while a mag. flux density varying with time. (Time changing flux linking a stationary closed path)

∴ from eqn (5) we have

$$\oint \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \quad \text{--- (6)}$$

This is similar to transformer action & emf  $\Rightarrow$  transformer e.m.f.

Using Stokes theorem, a line integral can be converted to surface integral

$$\oint_S (\nabla \times \vec{E}) \cdot d\vec{s} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \quad \text{--- (7)}$$

Assuming that both the surfaces  $\int_S$  taken over identical surfaces.

$$(\nabla \times \vec{E}) \cdot d\vec{s} = - \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

Finally we have,

$$\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} \quad \text{--- (8)}$$

Eqn (8)  $\rightarrow$  represents one of the Maxwell's eqn.

If  $\vec{B}$  is not varying with time, then eqn (6) & (8)  $\rightarrow$  give the results obtained previously (electrostatic)

$$\therefore \oint \vec{E} \cdot d\vec{l} = 0 \quad \&$$

$$\nabla \times \vec{E} = 0$$

case(ii) :-

A magnetic flux density stationary, while a closed path moving.

Here the emf induced is called as generator emf (motional emf)

Consider that a charge  $q$  is moved in a mag. field  $\vec{B}$  with a velocity  $\vec{v}$ . Then the force on a charge is given by

Consider that a charge  $Q$  is moved in a mag. field  $\vec{B}$  with a velocity  $\vec{V}$ . Then the force on a charge is given by

$$\vec{F} = Q\vec{V} \times \vec{B} \quad \text{--- (9)}$$

But the motional electric field intensity is defined as the force per unit charge.

$$\therefore \vec{E}_m = \frac{\vec{F}}{Q} = \vec{V} \times \vec{B} \quad \text{--- (10)}$$

Thus the induced emf is given by

$$\text{em.f} = \oint \vec{E}_m \cdot d\vec{L} = \oint (\vec{V} \times \vec{B}) \cdot d\vec{L} \quad \text{--- (11)}$$

Eq (11) represents total emf induced when a conductor is moved in a uniform constant mag. field.

\* Maxwell's eq from Ampere's Law

w.k.t. Ampere's Law is point form as

$$\nabla \times \vec{H} = \vec{J} \quad \text{--- (1)}$$

We will show, its inadequacy for time varying cond' by taking divergence of each side

$$\nabla \cdot (\nabla \times \vec{H}) = \vec{\nabla} \cdot \vec{J} \quad \text{--- (2)}$$

But the divergence of the curl of any vector field is zero.

Hence  $\vec{\nabla} \cdot \vec{J} = 0$

However from continuity eq

$$\nabla \cdot \vec{J} = - \frac{\partial \rho_v}{\partial t} \quad \text{--- (3)}$$

This is an unrealistic limitation for time varying field.

So eq (1) must be modified before we accept it for time varying field

To do this, we add a term to eq (1)  
so that it becomes

$$\nabla \times \vec{H} = \vec{J} + \vec{G} \quad \text{--- (4)}$$

Again taking the divergence

$$\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} + \nabla \cdot \vec{G} = 0$$

$$\nabla \cdot \vec{G} = -\nabla \cdot \vec{J} = \frac{\partial \epsilon_v}{\partial t}$$

$$\text{But } \epsilon_v = \nabla \cdot \vec{D}$$

$$\therefore \nabla \cdot \vec{G} = \frac{\partial}{\partial t} (\nabla \cdot \vec{D}) = \nabla \cdot \underbrace{\frac{\partial \vec{D}}{\partial t}}$$

from which,

$$\vec{G} = \frac{\partial \vec{D}}{\partial t} \quad \text{--- (5)}$$

Hence eq<sup>n</sup> (4) becomes

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

--- (6)

This is Maxwell's eq<sup>n</sup> (based on Ampere's Law) for time varying field

The term  $\frac{\partial \vec{D}}{\partial t} = \vec{J}_d \rightarrow$  known as displacement current density  $\vec{Q}$

$\vec{J} \rightarrow$  conduction current density ( $\vec{J} = \sigma \vec{E}$ )

For any arbitrary open surface  $S$  bounded by closed loop.

we can write eq<sup>n</sup> (6) as

$$\oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{s} + \int \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$$

--- (7)

Generalized form of Maxwell's Eq<sup>n</sup>s (Time varying fields)

Differential form

Integral form

Remark

(1)  $\nabla \cdot \vec{D} = \epsilon_v$

$$\oint \vec{D} \cdot d\vec{s} = \int_V \epsilon_v dV$$

Gauss's Law

(2)  $\nabla \cdot \vec{B} = 0$

$$\oint \vec{B} \cdot d\vec{s} = 0$$

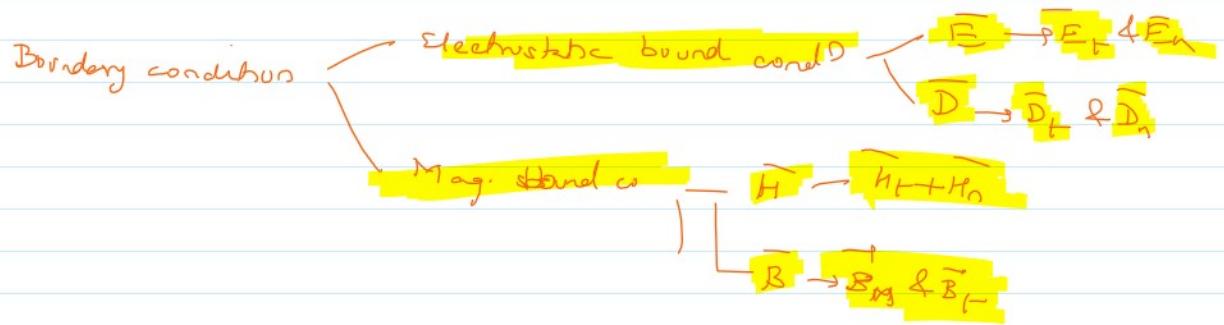
Gauss's Law for mag. field

(3)  $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$

$$\oint \vec{E} \cdot d\vec{l} = \frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{s}$$

Faraday's Law

$$④ \nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial r} \quad \oint \bar{H} \cdot d\bar{l} = \int_s \left( \bar{J} + \frac{\partial \bar{D}}{\partial r} \right) \cdot d\bar{s} \quad \text{Modified form A.C. Law}$$



$$\text{eqn } \bar{E} = |E| \cos(\omega t + \phi) \quad \begin{matrix} \text{mag} \\ \uparrow \\ \omega t + \phi \end{matrix} \quad \begin{matrix} \downarrow \\ \text{phase} \end{matrix}$$

\* Maxwell's eq<sup>n</sup> - Phasor representation (Time Varying field)

The partial derivative of a phasor w.r.t. time is equivalent to multiplying the corresponding phasor by  $j\omega$

Similarly → the second derivative is equivalent to  $(j\omega)^2$

\* Maxwell's eq<sup>n</sup> in Phasor form (Time Varying field)

Differential form

$$\textcircled{1} \quad \nabla \cdot \bar{D} = \rho_V$$

Integral form

$$\oint \bar{D} \cdot d\bar{s} = \int \rho_V dV$$

$$\textcircled{2} \quad \nabla \cdot \bar{B} = 0$$

$$\oint \bar{B} \cdot d\bar{s} = 0$$

**PHASOR  
REPRESENT.**

$$\textcircled{3} \quad \nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$$

$$\oint \bar{E} \cdot d\bar{l} = -\frac{\partial}{\partial t} \int \bar{B} \cdot d\bar{s}$$

$$\textcircled{4} \quad \nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t}$$

$$\oint \bar{H} \cdot d\bar{l} = \int \left( \bar{J} + \frac{\partial \bar{D}}{\partial t} \right) \cdot d\bar{s}$$

**PHASOR REPRESENTATION**

Point form

$$\nabla \cdot \bar{D} = \rho_V$$

Integral form

$$\oint \bar{D} \cdot d\bar{s} = \int \rho_V dV$$

$$\nabla \cdot \bar{B} = 0$$

$$\oint \bar{B} \cdot d\bar{s} = 0$$

$$\nabla \times \bar{E} = -j\omega \bar{B}$$

$$\oint \bar{E} \cdot d\bar{l} = -j\omega \int \bar{B} \cdot d\bar{s}$$

$$\nabla \times \bar{H} = \bar{J} + j\omega \bar{D}$$

$$\oint \bar{H} \cdot d\bar{l} = \int \bar{J} \cdot d\bar{l} + j\omega \int \bar{D} \cdot d\bar{s}$$

## \* Boundary conditions

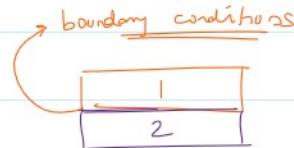
→ Integral form of Maxwell's eq<sup>n</sup>

ii) Electrostatic boundary conditions

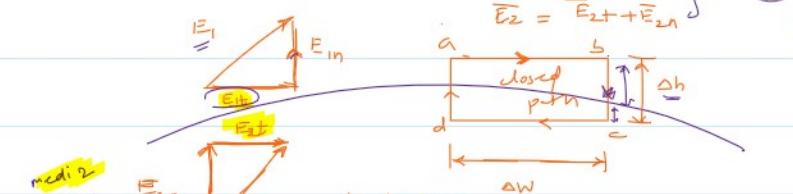
$$\oint \bar{D} \cdot d\bar{l} = 0 \quad \textcircled{1} \quad \&$$

$$\oint \bar{D} \cdot d\bar{s} = Q_{\text{end.}} \quad \textcircled{2}$$

$$\bar{E} = \bar{E}_t + \bar{E}_{n\perp} \quad \& \quad \bar{D} = \bar{D}_t + \bar{D}_{n\perp} \quad \textcircled{3}$$



\* Dielectric-Dielectric boundary cond'n



Medium 1

$$\epsilon_1 = \epsilon_0 \epsilon_r$$

\* Tangential component

$$\textcircled{3} \quad \bar{E}_{1t} = \bar{E}_{2t}$$

$$\int \bar{E}_{1t} = \bar{E}_{2t}$$

Tangential comp. of  $\bar{E}$  are same on the 2 sides of boundary

If it is continuous across boundary [  $E_t$  undergoes no change on the boundary ]

Since  $\bar{D} = \frac{\Sigma E}{\Sigma} = D_1 + D_2$

$$\frac{D_{1t}}{\epsilon_1} = \bar{E}_{1t} = \bar{E}_{2t} = \frac{D_{2t}}{\epsilon_2}$$

$$\therefore \frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}$$

6

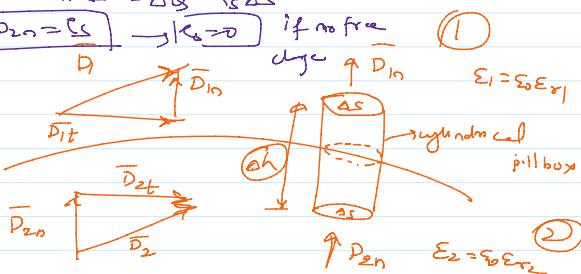
↗

$D_t$  undergoes some change across the interface - Hence  $D_t$  is said to be discontinuous across the interface

\* Normal component  $\rightarrow D_{in} \Delta S - D_{2n} \Delta S = \Delta Q = P_s \Delta S$

$$(1) \quad | D_{in} = D_{2n} | \quad \boxed{D_{in} - D_{2n} = P_s} \rightarrow [K_s = 0] \text{ if no free dye} \quad (1)$$

$D_n$  undergoes no change at the boundary.



Since  $\bar{D} = \Sigma \bar{E}$

$$\epsilon_1 E_{1n} = \epsilon_2 E_{2n}$$

Normal component of  $\bar{E}$  is discontinuous at the boundary.

→ we make use of Gauss's Law for magnetic fields

$$\oint \bar{B} \cdot d\bar{s} = 0 \quad \rightarrow (1)$$

& Ampere circ law

$$\oint \bar{H} \cdot d\bar{l} = I \quad \rightarrow (2)$$

$$B_{1n} = B_{2n} \quad \text{or} \quad \mu_1 H_{1n} = \mu_2 H_{2n}$$

$$\begin{aligned} \bar{B} &\rightarrow \bar{B}_t + \bar{B}_n \\ \bar{H} &\rightarrow \bar{H}_t + \bar{H}_n \end{aligned}$$

normal component of  $\bar{B}$  is continuous at the boundary whereas normal component of  $\bar{H}$  is discontinuous at the boundary

$$H_{1t} = H_{2t} \quad \text{or} \quad \frac{B_{1t}}{\mu_1} = \frac{B_{2t}}{\mu_2}$$

The tangential component of  $\bar{H}$  is continuous while that of  $\bar{B}$  is discontinuous at the boundary.

(i) Derive wave equation (Helmholtz wave eq?)

(ii) Determine solution of vector wave equations.

## \* WAVE PROPAGATION

In the solution of any EM problem the fundamental relations that must be satisfied are the four

relations that must be satisfied are the four field equations:

$$\nabla \times \bar{H} = \bar{J} + \frac{\delta \bar{D}}{\delta t}$$

$$\nabla \times \bar{E} = -\frac{\delta \bar{B}}{\delta t} = -\mu \frac{\delta \bar{H}}{\delta t}$$

$$\nabla \cdot \bar{D} = \rho v$$

$$\nabla \cdot \bar{B} = 0$$

and the characteristics of the medium in which the field exists.

$$\rightarrow \bar{D} = \epsilon \bar{E}, \bar{B} = \mu \bar{H} \text{ and } \bar{J} = \sigma \bar{E}$$

The medium is homogeneous, isotropic and source free. A homogenous medium is one for which the quantities  $\epsilon$ ,  $\mu$  and  $\sigma$  are constant throughout the medium. The medium is isotropic, if  $\epsilon$  is scalar constant.

### Wave propagation in a conducting medium (lossy dielectrics)

A lossy dielectric is a medium in which an EM wave loses power as it propagates due to poor conduction, i.e.  $\sigma \neq 0$ . It is imperfect dielectric.

Consider charge free ( $\rho v = 0$ ), a linear, isotropic homogenous and lossy dielectric medium.

Maxwell's equation in phasor notation are

$$\nabla \times \bar{H} = \bar{J} + j\omega \epsilon \bar{E} = \sigma \bar{E} + j\omega \epsilon \bar{E} = (\sigma + j\omega \epsilon) \bar{E} \quad \dots (1)$$

$$\nabla \times \bar{E} = -j\omega \mu \bar{H} \quad \dots (2)$$

$$\nabla \cdot \bar{E} = 0 \quad \dots (3)$$

$$\nabla \cdot \bar{H} = 0 \quad \dots (4)$$

$$\begin{aligned} \rightarrow \nabla \times \bar{H} &= \bar{J} + \frac{\delta \bar{D}}{\delta t} \\ &= \bar{J} + (j\omega \epsilon) \bar{E} \\ &= \bar{J} + j\omega \epsilon \bar{E} \\ &= \sigma \bar{E} + j\omega \epsilon \bar{E} \\ &\Rightarrow \boxed{\bar{E} = \bar{E}(G + j\omega \epsilon)} \end{aligned}$$

Taking curl of eq (2)

$$\nabla \times \nabla \times \bar{E} = -j\omega \mu \nabla \times \bar{H} \quad \dots (5)$$

Apply vector identity,

$$\nabla \times \nabla \times \bar{A} = \nabla(\nabla \cdot \bar{A}) - \nabla^2 \bar{A} \quad \dots (6)$$

$$\text{i.e. } \nabla \times \nabla \times \bar{E} = \nabla(\nabla \cdot \bar{E}) - \nabla^2 \bar{E}$$

$$\text{since } \nabla \cdot \bar{E} = 0$$

$$\therefore \nabla \times \nabla \times \bar{E} = -\nabla^2 \bar{E} = -j\omega \mu \nabla \times \bar{H}$$

$$\nabla^2 \bar{E} = j\omega \mu (\sigma + j\omega \epsilon) \bar{E} \quad \dots (7)$$

$$\text{Put } \gamma^2 = j\omega \mu (\sigma + j\omega \epsilon) \quad \dots (8)$$

$$\therefore \nabla^2 \bar{E} - \gamma^2 \bar{E} = 0 \quad \dots (9)$$

where  $\gamma$  is propagation constant. By similar procedure it can be shown that

$$\nabla^2 \bar{H} - \gamma^2 \bar{H} = 0 \quad \dots (10)$$

Equation (9) and (10) are known as homogeneous vector Helmholtz equation or simply vector wave equation.

The propagation constant ( $\gamma$ ) : Attenuation constant ( $\alpha$ ) and phase constant or wave number ( $\beta$ ).

The propagation constant  $\gamma$  is a complex quantity.

$$\gamma = \alpha + j\beta \quad \dots (11)$$

Consider equation (8)

$$\gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$$

=

From equation (8) and equation (11)  $\alpha$  and  $\beta$  can be obtained.

Squaring equation (11)

$$\gamma^2 = \alpha^2 + 2j\alpha\beta - \beta^2 = (\alpha^2 - \beta^2) + 2j\alpha\beta \quad \dots (12)$$

Equating real part of equation (8) and (12)

$$\alpha^2 - \beta^2 = -\omega^2\mu\epsilon$$

$$\therefore \beta^2 - \alpha^2 = \omega^2\mu\epsilon \quad \dots (13)$$

$$\text{Also } |\gamma^2| = \beta^2 + \alpha^2 \quad \dots (14)$$

$$|\gamma^2| = \omega\mu\sqrt{\sigma^2 + \omega^2\epsilon^2} \quad \dots (15)$$

$$\therefore \beta^2 + \alpha^2 = \omega\mu\sqrt{\sigma^2 + \omega^2\epsilon^2} \quad \dots (16)$$

Solving (13) and (16)

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} + 1 \right)} \quad \dots (17)$$

$$\text{and } \alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} - 1 \right)} \quad \dots (18)$$

$\gamma = \alpha + j\beta$

Also

$$\gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$$

Solving (13) and (16)

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2}} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} + 1 \right) \quad \dots (17)$$

$$\text{and } \alpha = \omega \sqrt{\frac{\mu\epsilon}{2}} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} - 1 \right) \quad \dots (18)$$

Propagation constant -

$r = \alpha + j\beta$

←  
attenuation constant -

→  
phase constant -  
(wave number)

## \* Solution of wave eq

From eqn (9) we have.

$$\nabla^2 E - \gamma^2 E = 0$$

$$\nabla^2 \bar{E} = \gamma^2 \bar{E}$$

from eqn (5)

 $(\lambda, \nu, z)$ 

$$\gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$$

Expanding  $\nabla^2$  and  $\bar{E}$  in Cartesian co-ordinate system.

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}, \text{ and } \bar{E} = E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z$$

$$\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) (E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z) = \gamma^2 (E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z)$$

Thus equation (9) is equivalent to three scalar equations

One for each component of  $\bar{E}$  along  $\hat{a}_x$ ,  $\hat{a}_y$  and  $\hat{a}_z$ .

The wave equation reduces to a very simple form if uniform plane wave is considered.

Consider uniform plane wave traveling in  $+\hat{a}_z$  direction,  $\bar{E}$  is independent of  $x$  and  $y$  and there is no component in the direction of propagation.

Therefore equation (9) reduces to,

$$\nabla^2 \bar{E} = \frac{\partial^2 \bar{E}}{\partial z^2} = \gamma^2 \bar{E} \quad \dots (19)$$

which is equivalent to

$$\frac{\partial^2 E_x}{\partial z^2} = \gamma^2 E_x \quad \dots 20(a)$$

$$\frac{\partial^2 E_y}{\partial z^2} = \gamma^2 E_y \quad \dots 20(b)$$

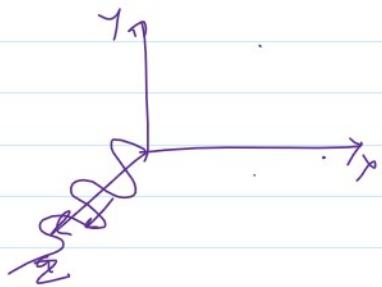
$$\frac{\partial^2 E_z}{\partial z^2} = \gamma^2 E_z = 0 \quad \dots 20(c)$$

In general for uniform plane wave traveling in  $z$  direction,  $\bar{E}$  may have  $x$  and  $y$  component but not  $E_z$ .

Proof: In a region in which there is no charge density,

$$\nabla \cdot \bar{E} = \frac{1}{\epsilon} \nabla \cdot \bar{D} = 0$$

$$\text{i.e. } \frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z} = 0$$

For uniform plane in which  $\bar{E}$  is independent of  $x$  and  $y$ , the first two terms of this relation are equal to zero so that it reduces to  $\frac{\partial E_z}{\partial z} = 0$ 

$$\nabla^2 E = \gamma^2 E$$

$(E_x, E_y, E_z)$

 $D & E$ 

$$\nabla \cdot E = 0$$

$$D = \epsilon E$$

$$E = \frac{D}{\epsilon}$$

There is no variation of  $E_z$  in  $z$  direction. So second derivative then must be zero. It requires that  $E_z$  must be zero or constant. If it is constant, it would not be a part of wave motion. So  $E_z$  must be zero.

Without loss of generality, we assume that  $E$  has only one component say  $E_x$  knowing that result will be same for  $E_y$ .

$$\therefore \frac{\partial^2 E_x}{\partial z^2} = -\gamma^2 E_x \quad \dots (21)$$

This is linear homogenous differential equation, by inspection its solution may be written as

$$E_x = E_0 e^{-\gamma z} + E_0' e^{+\gamma z} \quad \dots (22)$$

where  $E_0$  and  $E_0'$  are constants. The fact that the field must be finite at infinity requires that  $E_0' = 0$ . The factor  $e^{\gamma z}$  denotes wave traveling in  $-\hat{a}_z$  direction as  $e^{-\gamma z}$  represents wave traveling in  $+\hat{a}_z$  direction.

$$\therefore E_x = E_0 e^{-\gamma z} \quad \dots (23)$$

reinsert  $e^{j\omega t}$  factor and reduce to trigonometric form by taking real part of it.

$$\therefore E_x = \operatorname{Re} E_0 e^{-\alpha z} e^{-j\beta z} e^{j\omega t} \quad \dots (24)$$

$$E_x = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (25)$$

$$\therefore \bar{E}(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \hat{a}_x$$

**Calculation of  $\bar{H}$ :**

Given  $\bar{E}$ ,  $\bar{H}$  can be calculated using Maxwell's equation,

$$\nabla \times \bar{E} = -j\omega\mu \bar{H}$$

Since  $\bar{E}$  has only  $x$  component and is independent of  $x$  and  $y$  since wave is traveling in  $z$ -direction.

$$\therefore \nabla \times \bar{E} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0 & 0 & \frac{\partial}{\partial z} \\ E_x & 0 & 0 \end{vmatrix} = -j\omega\mu \bar{H}$$

Here  $E_x = E_0 e^{-\gamma z}$

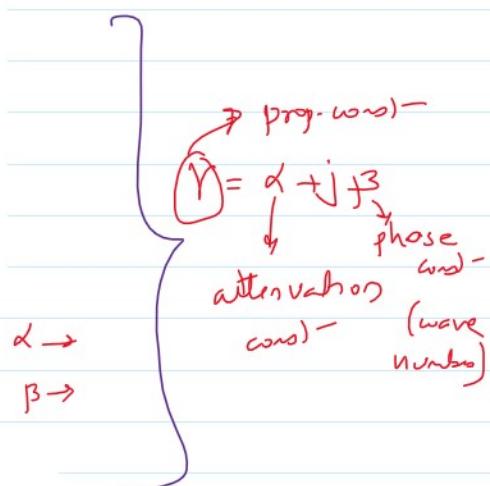
$$\begin{aligned} \nabla \times \bar{E} &= +\hat{a}_y \frac{\partial}{\partial z} E_x = -j\omega\mu H_y \hat{a}_y \\ &= -\gamma e^{-\gamma z} E_0 \hat{a}_y = -j\omega\mu H_y \hat{a}_y \end{aligned}$$

$$\therefore H_y = \frac{\gamma}{j\omega\mu} E_0 e^{-\gamma z} \quad \dots (26)$$

Reinsert  $e^{j\omega t}$  and taking real part of it.

$$H_y = \frac{\operatorname{Re} \gamma}{j\omega\mu} E_0 e^{j\omega t} e^{-\gamma z}$$

$$\therefore H_y = \frac{\gamma E_0}{j\omega\mu} e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (27)$$



Intrinsic Impedance ( $\eta$ )

Now taking ratio

$$\begin{aligned}\frac{E_x}{H_y} &= \frac{E_0 e^{-\gamma z}}{\gamma E_0 e^{-\gamma z}} = \frac{j\omega\mu}{\gamma} \\ &= \frac{j\omega\mu}{\sqrt{j\omega\mu(\sigma + j\omega\epsilon)}} = \sqrt{\frac{j\omega\mu}{(\sigma + j\omega\epsilon)}} = \text{complex quantity} \\ &= \eta \text{ (intrinsic impedance)}\end{aligned}$$

$\eta = \frac{\text{Elec field}}{\text{Mag field}}$

where  $\eta$  is complex quantity, which may be expressed as

$$\eta = \sqrt{\frac{j\omega\mu}{(\sigma + j\omega\epsilon)}} = |\eta| e^{j\theta_n} = |\eta| e^{j\theta_n}$$

$$\therefore \quad \begin{aligned} &\omega^2 \epsilon^2 \\ &\omega \mu \\ &\omega^2 \epsilon^2 \end{aligned}$$

$$\therefore \theta_n = \frac{1}{2} \tan^{-1} \frac{\sigma \omega \mu}{\omega^2 \mu \epsilon} = \frac{1}{2} \tan^{-1} \frac{\sigma}{\omega \epsilon}$$

$$|\eta| = \sqrt{\frac{\mu/\epsilon}{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2}}$$

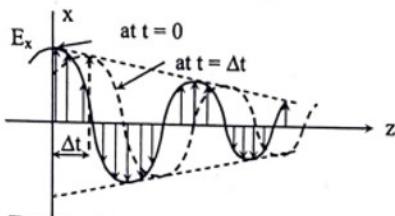
Hence the equation (27) may be written as -

$$H_y = \frac{E_0}{|\eta| e^{j\theta_n}} e^{j\alpha z} \cos(\omega t - \beta z)$$

$$\bar{H}(z, t) = \frac{E_0}{|\eta|} e^{-\alpha z} \cos(\omega t - \beta z - \theta_n) \hat{a}_y \quad \dots (28)$$

$$\therefore \bar{E}(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \hat{a}_x \quad \dots (25)$$

From equation (25) and (28), as the wave propagates along  $+\hat{a}_z$ , it decreases or attenuates in amplitude by a factor  $e^{-\alpha z}$ , hence  $\alpha$  is known as the attenuation constant or factor of the medium. It is a measure of the spatial rate of decay of the wave in the medium, measured in nepers per meter (Np/m) or in decibels per meter (dB/m). An attenuation of 1 neper denotes a reduction to  $e^{-1}$  of the original value whereas an increase of 1 neper indicates an increase by a factor of  $e$ .

Fig :  $\bar{E}$  field with y-comp. traveling in  $+\hat{a}_x$  direction

The quantity  $\beta$  is a measure of the phase shift per length and is called the phase constant or wave number.

In terms of  $\beta$ , the velocity of propagation and wavelength are given by,

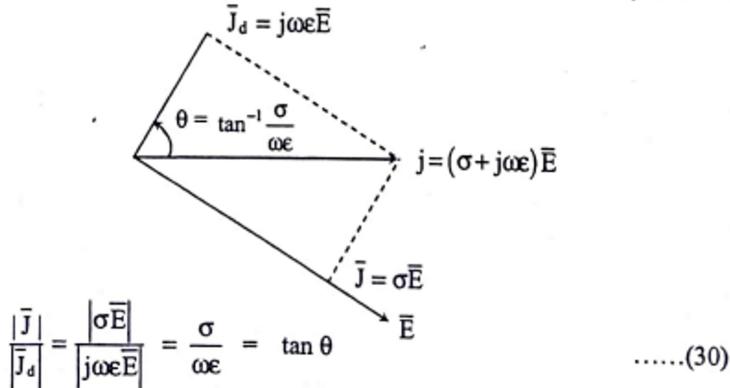
$$v = \frac{\omega}{\beta}, \quad \lambda = \frac{2\pi}{\beta} \quad \dots (29)$$

$$E_x = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (24)$$

$$\therefore H_y = \frac{\gamma E_0}{j\omega\mu} e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (27)$$

$$H_y = \frac{E_0}{|\eta| < \theta_n} e^{\alpha z} \cos(\omega t - \beta z)$$

From equation (24) and (27) it is clear that  $\bar{E}$  and  $\bar{H}$  are out of phase by  $\theta_n$  at any instant of time due to the complex intrinsic impedance of the medium. The ratio of the magnitude of the conduction current density  $\bar{J}$  to the displacement current density  $\bar{J}_d$  in lossy medium is



where  $\tan \theta$  is known as the loss tangent and  $\theta$  is the loss angle of the medium.

If  $\tan \theta$  is very small ( $\sigma \ll \omega \epsilon$ ) the medium is said to be good dielectric.

If  $\tan \theta$  is very large ( $\sigma > \omega \epsilon$ ), the medium is good conductor

Also from the view point of wave propagation the characteristic behavior of medium depends not only on  $\sigma$ ,  $\epsilon$ , and  $\mu$  but also on the frequency of operation.

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} + 1 \right)} \quad \dots \dots (17)$$

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon^2}} - 1 \right)} \quad \dots \dots (18)$$

$$\eta = \sqrt{\frac{j\omega\mu}{(\sigma + j\omega\epsilon)}} = |\eta| < \theta_n = |\eta| e^{j\theta_n}$$

#### Wave Motion in Perfect (Lossless) Dielectrics :

It is a special case of lossy dielectrics.

Here  $\sigma \ll \omega \epsilon$ ,

$$\therefore \sigma \approx 0, \quad \epsilon = \epsilon_0 \epsilon_r, \quad \mu = \mu_0 \mu_r \quad \dots \dots (31)$$

$$\theta_n = \frac{1}{2} \tan^{-1} \frac{\sigma \omega \mu}{\omega^2 \mu \epsilon} = \frac{1}{2} \tan^{-1} \frac{\sigma}{\omega \epsilon}$$

Substituting above relations into equation (17), (18)

$$\alpha = 0 \quad \dots \dots (32)$$

$$\beta = \omega \sqrt{\mu \epsilon} \quad \dots \dots (33)$$

$$|\eta| = \frac{\sqrt{\mu/\epsilon}}{\left[ 1 + \left( \frac{\sigma}{\omega \epsilon} \right)^2 \right]^{1/4}}$$

$$p = \omega \sqrt{\mu \epsilon}$$

.....(33)

$$\left[ 1 + \left( \frac{1}{\omega \epsilon} \right) \right]$$

## WAVE PROPAGATION IN A GOOD CONDUCTOR

In perfect conductor,

$$\sigma > \omega \epsilon \text{ so that } \sigma / \omega \epsilon \rightarrow \infty, \text{ that is}$$

[  $\sigma = \infty, \epsilon = \epsilon_0, \mu = \mu_0 \mu_r$  ]

.....(37)

Also,

Thus

Consider expression for  $\alpha$  and  $\beta$

$$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} - 1 \right)} \quad \text{and} \quad \beta = \omega \sqrt{\frac{\mu \epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} + 1 \right)}$$

Substitute  $\frac{\sigma}{\omega \epsilon} \gg 1$ ,

$$\therefore \alpha = \beta = \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma} \quad \dots \dots \dots (38)$$

$$\therefore v = \frac{\omega}{\beta} = \sqrt{\frac{2\omega}{\mu \sigma}} \quad \dots \dots \dots (39)$$

$$\lambda = \frac{2\pi}{\beta} \quad \dots \dots \dots (40)$$

The expression for  $\gamma$  may be written as

$$\because \gamma^2 = j\omega \mu (\sigma + j\omega \epsilon) = j\omega \mu \sigma \left[ 1 + \frac{j\omega \epsilon}{\sigma} \right]$$

$$\therefore \frac{\sigma}{\omega \epsilon} \gg 1$$

$$\therefore \gamma^2 = j\omega \mu \sigma = \sqrt{\omega \mu \sigma} \angle 90^\circ \quad \dots \dots \dots (41)$$

$$\therefore \gamma = \sqrt{\omega \mu \sigma} \angle 45^\circ \quad \dots \dots \dots (42)$$

The intrinsic impedance of the conductor is

$$\therefore \frac{\sigma}{\omega \epsilon} \gg 1$$

$$\eta = \sqrt{\frac{j\omega \mu}{\sigma + j\omega \epsilon}}$$

Dividing the numerator and denominator by  $j\omega \epsilon$  we get,

$$\eta = \sqrt{\frac{j\omega \mu / j\omega \epsilon}{(\sigma + j\omega \epsilon) / j\omega \epsilon}}$$

$$\begin{aligned}
 &= \sqrt{\frac{\mu/\epsilon}{1 + \frac{\sigma}{j\omega\epsilon}}} = \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{1}{1 + \frac{\sigma}{j\omega\epsilon}}} \\
 \therefore \frac{\sigma}{j\omega\epsilon} &> 1 \\
 \therefore 1 + \frac{\sigma}{j\omega\epsilon} &= \frac{\sigma}{j\omega\sigma} \\
 \eta &= \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{1}{\frac{\sigma}{j\omega\epsilon}}} = \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{j\omega\epsilon}{\sigma}} \\
 &= \sqrt{\frac{j\omega\mu}{\sigma}} \\
 \eta &= \sqrt{\frac{\mu\omega}{\sigma}} \angle 45^\circ \quad \dots\dots(43)
 \end{aligned}$$

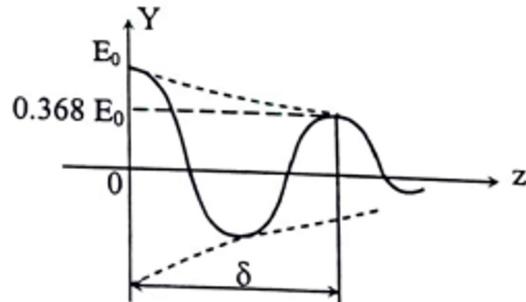
Thus in good conductor  $\bar{E}$  leads  $\bar{H}$  by  $45^\circ$ . If

$$\bar{E} = E_0 e^{-\alpha x} \cos(\omega t - \beta x) \hat{a}_y \quad \dots\dots(44)$$

$$\text{Then } \bar{H} = \frac{E_0}{\sqrt{\frac{\omega\mu}{\sigma}}} e^{-\alpha x} \cos(\omega t - \beta z - 45^\circ) \hat{a}_z \quad \dots\dots(45)$$

**Depth of Penetration:** In a medium which has a conductivity the wave is attenuated as it propagates owing to the losses which occur. In a good conductor at radio frequencies the rate of attenuation is very great and the wave may penetrate only a very short distance before being reduced to a negligibly small percentage of its original strength.

As  $\bar{E}$  and  $\bar{H}$  wave travels in a conducting medium, its amplitude is attenuated by the factor  $e^{-\alpha z}$ . The distance ' $\delta$ ' shown in figure, through which the wave amplitude decreases by a factor  $e^{-1}$  (about 37%) is called skin depth or penetration depth of the medium.



$$\therefore E_0 e^{-\alpha \delta} = E_0 e^{-1}$$

$$\text{or } \delta = \frac{1}{\alpha}$$

For good conductors

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

To get some idea of the magnitude of the skin depth, consider copper ( $\sigma = 5.8 \times 10^7 \text{ S/m}$ ,  $\mu = \mu_0$ ). The skin depth in copper at various frequencies is shown in table.

Frequency (Hz)	10	60	100	500	$10^4$	$10^8$	$10^{10}$
Skin depth (mm)	20.8	8.6	6.6	2.99	0.66	$6.6 \times 10^{-3}$	$6.6 \times 10^{-4}$

The phenomenon whereby field intensity in a conductor rapidly decreases is known as skin effect. The field and associated currents are confined to a very thin layer of the conductor surface.

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} + 1 \right)}$$

(1)

... (17) ←

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} - 1 \right)}$$

(2)

... (18) ←

$$\theta_n = \frac{1}{2} \tan^{-1} \frac{\sigma \omega \mu}{\omega^2 \mu \epsilon} = \frac{1}{2} \tan^{-1} \frac{\sigma}{\omega \epsilon}$$

(3)

$$\eta = n \angle \theta_n$$

$$|\eta| = \frac{\sqrt{\mu/\epsilon}}{\left[1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2\right]^{1/4}}$$

(4)

### Wave Motion in Perfect (Lossless) Dielectrics :

It is a special case of lossy dielectrics.

Here  $\sigma \ll \omega \epsilon$ ,

$$\therefore \sigma \approx 0, \epsilon = \epsilon_0 \epsilon_r, \mu = \mu_0 \mu_r \quad \dots \dots \dots (31)$$

Substituting above relations into equation (17), (18)

$$\alpha = 0 \quad \dots \dots \dots (32)$$

$$\beta = \omega \sqrt{\mu \epsilon} \quad \dots \dots \dots (33)$$

$$v = \frac{\omega}{\beta} = \frac{1}{\sqrt{\mu \epsilon}} \quad \dots \dots \dots (34)$$

$$\lambda = \frac{2\pi}{\beta} = \quad \dots \dots \dots (35)$$

$$\text{Also, } \eta = \sqrt{\frac{\mu}{\epsilon}} \angle 0^\circ \quad \dots \dots \dots (36)$$

Thus  $\bar{E}$  and  $\bar{H}$  are in time phase with each other.

## WAVE PROPAGATION IN A GOOD CONDUCTOR

In perfect conductor,

$\sigma \gg \omega \varepsilon$  so that  $\sigma / \omega \varepsilon \rightarrow \infty$ , that is

$$[\sigma = \infty, \varepsilon = \varepsilon_0, \mu = \mu_0 \mu_r] \quad \dots \dots \dots (37)$$

Consider expression for  $\alpha$  and  $\beta$

$$\alpha = \omega \sqrt{\frac{\mu \varepsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \varepsilon^2}} - 1 \right)} \quad \text{and} \quad \beta = \omega \sqrt{\frac{\mu \varepsilon}{2} \left( \sqrt{1 + \frac{\sigma^2}{\omega^2 \varepsilon^2}} + 1 \right)}$$

Substitute  $\frac{\sigma}{\omega \epsilon} >> 1$ ,

$$\therefore \alpha = \beta = \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma} \quad \dots \dots \dots (38)$$

$$\therefore v = \frac{\omega}{\beta} = \sqrt{\frac{2\omega}{\mu\sigma}} \quad \dots\dots(39)$$

$$\lambda = \frac{2\pi}{\beta} \quad \dots\dots\dots(40)$$

The expression for  $\gamma$  may be written as

$$\therefore \gamma^2 = j\omega\mu(\sigma + j\omega\epsilon) = j\omega\mu\sigma \left[ 1 + \frac{j\omega\epsilon}{\sigma} \right]$$

$$\therefore \frac{\sigma}{\omega\varepsilon} >> 1$$

$$\therefore \gamma^2 = j\omega\mu\sigma = \sqrt{\omega\mu\sigma} \angle 90^\circ \quad \dots\dots(41)$$

$$\therefore \gamma = \sqrt{\omega\mu\sigma} < 45^\circ \quad \dots\dots(42)$$

The intrinsic impedance of the conductor is

$$\therefore \frac{\sigma}{\omega e} >> 1$$

$$\rightarrow \eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\varepsilon}}$$

Dividing the numerator and denominator by  $j\omega$  we get,

$$\eta = \sqrt{\frac{j\omega\mu/j\omega}{(\sigma + j\omega\varepsilon)/j\omega\varepsilon}}$$

$$\omega = \sqrt{\frac{\mu\varepsilon}{2} \left( \sqrt{1 + \frac{\varepsilon^2}{\omega_0^2}} - 1 \right)}$$

$$\frac{6}{3} >> 1$$

$$\alpha = \omega \sqrt{\frac{\mu_\varepsilon}{2}} \left( \left( \frac{6}{\omega_\varepsilon} \right)^{-1} \right)$$

4

$$\frac{\omega}{\omega_0}$$

6  
8

$$= \sqrt{\frac{2\pi f M_0}{\mu}}$$

$$\gamma = \sqrt{\frac{\mu/\epsilon}{1 + \frac{\sigma}{j\omega}}} = \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{1}{1 + \frac{\sigma}{j\omega}}}$$

$$\therefore \frac{\sigma}{j\omega} > 1$$

$$\therefore 1 + \frac{\sigma}{j\omega} = \frac{\sigma}{j\omega} \cancel{+ 1}$$

$$\eta = \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{1}{\frac{\sigma}{j\omega}}} = \sqrt{\frac{\mu}{\epsilon}} \sqrt{\frac{j\omega}{\sigma}}$$

$$= \sqrt{\frac{j\omega}{\sigma}}$$

$$\eta = \sqrt{\frac{\mu\omega}{\sigma}} < 45^\circ$$

.....(43)

Thus in good conductor  $\bar{E}$  leads  $\bar{H}$  by  $45^\circ$ . If

$$\bar{E} = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \hat{a}_y$$

.....(44)

$$\text{Then } \bar{H} = \frac{E_0}{\sqrt{\mu\epsilon}} e^{-\alpha z} \cos(\omega t - \beta z - 45^\circ) \hat{a}_z$$

.....(45)

**Depth of Penetration:** In a medium which has a conductivity the wave is attenuated as it propagates owing to the losses which occur. In a good conductor at radio frequencies the rate of attenuation is very **great** and the wave may penetrate only a very short distance before being reduced to a negligibly small percentage of its original strength.

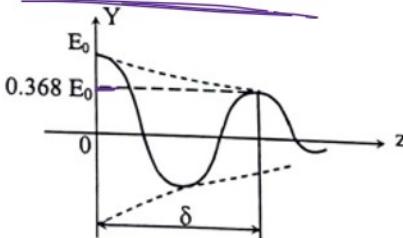
As  $\bar{E}$  and  $\bar{H}$  wave travels in a conducting medium, its amplitude is attenuated by the factor  $e^{-\alpha z}$ . The distance ' $\delta$ ' shown in figure, through which the wave amplitude decreases by a factor  $e^{-1}$  (about 37%) is called skin depth or penetration depth of the medium.

$$\therefore E_0 e^{-\alpha \delta} = E_0 e^{-1}$$

$$\text{or } \delta = \frac{1}{\alpha}$$

For good conductors

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$



To get some idea of the magnitude of the skin depth, consider copper ( $\sigma = 5.8 \times 10^7 \text{ S/m}$ ,  $\mu = \mu_0$ ). The skin depth in copper at various frequencies is shown in table.

Frequency (Hz)	10	60	100	500	$10^4$	$10^8$	$10^{10}$
Skin depth (mm)	20.8	8.6	6.6	2.99	0.66	$6.6 \times 10^{-3}$	$6.6 \times 10^{-4}$

The phenomenon whereby field intensity in a conductor rapidly decreases is known as skin effect. The field and associated currents are confined to a very thin layer of the conductor surface.

### Poynting Theorem :

When electromagnetic waves propagate through space from their source to distant receiving points, there is a transfer of energy from the source to the receivers. In order to find the power in an electromagnetic waves, it is necessary to develop a power theorem, which is known as Poynting theorem. It can be obtained from Maxwell's equation as follows

Consider Maxwell's equation from modified Ampere's circuit law,

$$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t} \quad \dots (1)$$

Dot each side of equation (1) with  $\bar{E}$

$$\bar{E} \cdot (\nabla \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t} \quad \dots (2)$$

Now make use of vector identity,

$$\nabla \cdot (\bar{E} \times \bar{H}) = \bar{H} \cdot \nabla \times \bar{E} - \bar{E} \cdot \nabla \times \bar{H} \quad \dots (3)$$

from (2) and (3)

$$\therefore \bar{H} \cdot \nabla \times \bar{E} - \nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t} \quad \dots (4)$$

but  $\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$

and therefore,

$$-\bar{H} \cdot \frac{\partial \bar{B}}{\partial t} - \nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \bar{E} \cdot \frac{\partial \bar{D}}{\partial t}$$

or

$$-\nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \epsilon \bar{E} \cdot \frac{\partial \bar{E}}{\partial t} + \mu \bar{H} \cdot \frac{\partial \bar{H}}{\partial t}$$

However  $\epsilon \bar{E} \cdot \frac{\partial \bar{E}}{\partial t} = \frac{\epsilon}{2} \frac{\partial E^2}{\partial t} = \frac{\partial}{\partial t} \left( \frac{\epsilon E^2}{2} \right)$

$$\mu \bar{H} \cdot \frac{\partial \bar{H}}{\partial t} = \frac{\mu}{2} \frac{\partial H^2}{\partial t} = \frac{\partial}{\partial t} \left( \frac{\mu H^2}{2} \right)$$

$$\boxed{\bar{A} \cdot \frac{\partial \bar{A}}{\partial t} = \frac{1}{2} \frac{\partial A^2}{\partial t}} \quad \dots (5)$$

$$\dots (6)$$

Thus equation (6) becomes,

$$-\nabla \cdot (\bar{E} \times \bar{H}) = \bar{E} \cdot \bar{J} + \frac{\partial}{\partial t} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) \quad \dots (7)$$

Integrate equation (7) throughout a volume

$$-\int_{\text{vol}} \nabla \cdot (\bar{E} \times \bar{H}) dv = \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv + \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \quad \dots (8)$$

Apply divergence theorem to left hand side of equation (8)

$$-\oint_S (\bar{E} \times \bar{H}) \cdot d\bar{s} = \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv + \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \quad \dots (9)$$

The equation (9) can be written as

$$\oint_S (\bar{E} \times \bar{H}) \cdot d\bar{s} = - \int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv - \frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv \quad \dots (10)$$

**I term**      **II term**      **III term**

Equation (10) is referred to as Poynting theorem

### Physical Interpretation :

II term :  $\int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv$

This term represents power dissipated in the volume  $V$ . Consider a conductor of cross sectional area  $A$ , carrying current  $I$  and voltage drop  $E$  per unit length. Therefore power loss per unit length is  $EI$ .

$\therefore$  Power dissipated per unit volume would be

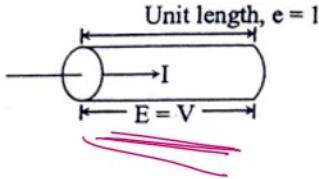
$$\frac{EI}{A} = E J \text{ watts per unit volume.}$$

$\therefore$  In general, when  $\bar{E}$  and  $\bar{J}$  are not in same direction,

$$\text{Power dissipated per unit volume} = \bar{E} \cdot \bar{J}$$

$\therefore$  The total power dissipated in a volume  $V$  would be

$$\int_{\text{vol}} (\bar{E} \cdot \bar{J}) dv$$



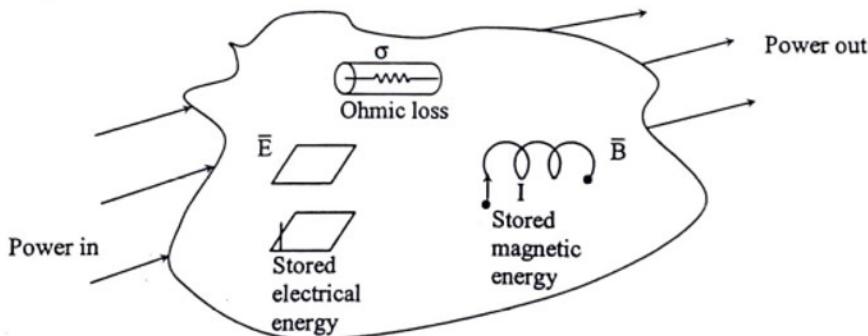
III term :  $-\frac{\partial}{\partial t} \int_{\text{vol}} \left( \frac{\epsilon E^2}{2} + \frac{\mu H^2}{2} \right) dv$

In electrostatic, the quantity  $\frac{1}{2} \epsilon E^2$  is energy density or stored energy per unit volume of the electric field. Also for the steady magnetic field the quantity  $\frac{1}{2} \mu H^2$  represents the stored energy density of the magnetic field. The negative time derivative of this quantity represents the rate at which the stored energy in the volume is decreasing.

I<sup>st</sup> term :  $\oint_s (\bar{E} \times \bar{H}) \cdot d\bar{s}$

The interpretation of I term follows from the application of the law of conservation of energy. The rate of energy dissipation in the volume  $v$  must equal the rate at which the stored energy in  $v$  is decreasing, plus the rate at which energy is entering the volume  $v$  from outside.

$\therefore \oint_s (\bar{E} \times \bar{H}) \cdot d\bar{s}$  represents outward flow of energy through the surface enclosing the volume and  $-\oint_s (\bar{E} \times \bar{H}) \cdot d\bar{s}$  represents inward flow of energy through the surface enclosing the volume.



**Statement :** The net power flowing out of a given volume  $v$  is equal to the time rate of decrease in the energy stored within  $v$  minus the conduction loss :



### The Poynting Vector :

The interpretation of poynting theorem, leads to the conclusion that the integral of  $\bar{E} \times \bar{H}$  over any, closed surface gives the rate of energy flow through that surface. This cross product  $\bar{E} \times \bar{H}$  is known as poynting vector  $\bar{P}$ ,

$$\bar{P} = \bar{E} \times \bar{H} \quad \dots (11)$$

The poynting vector has dimensions of watts per square meter. It is a measure of rate of energy flow per unit area at that point. The direction of flow is perpendicular to  $\bar{E}$  and  $\bar{H}$  in the direction of the vector  $\bar{E} \times \bar{H}$ .

$$a_x \times a_y = a_2$$

$$a_y \times a_x = a_1$$

$$a_z \times a_z = 0$$

In perfect dielectrics,  $\bar{E}$  and  $\bar{H}$  fields are given as

$$\begin{aligned} E_x &= E_0 \cos(\omega t - \beta z) \\ H_y &= \frac{E_0}{\eta} \cos(\omega t - \beta z) \end{aligned}$$

The Poynting vector is

$$\begin{aligned} \bar{P} &= \bar{E} \times \bar{H} \\ \therefore P_z \hat{a}_z &= E_x \hat{a}_x \times H_y \hat{a}_y \end{aligned}$$

$$\therefore P_z = \frac{E_0^2}{\eta} \cos^2(\omega t - \beta z)$$

To find the time average power density, integrate over one cycle and divide by the period  $T = \frac{1}{f}$ .

$$\begin{aligned} \therefore P_{z, \text{av}} &= f \int_0^{1/f} \frac{E_0^2}{\eta} \cos^2(\omega t - \beta z) dt \\ &= \frac{f}{2} \frac{E_0^2}{\eta} \int_0^{1/f} [1 + \cos(2\omega t - 2\beta z)] dt \\ &= \frac{f}{2} \frac{E_0^2}{\eta} \left[ t + \frac{1}{2\omega} \sin(2\omega t - 2\beta z) \right]_0^{1/f} \\ &= P_{z, \text{av}} = \frac{1}{2} \frac{E_0^2}{\eta} \omega / m^2 \end{aligned} \quad \dots (12)$$

If medium is lossy dielectric,

$$E_x = E_0 e^{-\alpha z} \cos(\omega t - \beta z)$$

$$H_y = \frac{E_0}{|\eta|} e^{-\alpha z} \cos(\omega t - \beta z - \theta_n)$$

$$\therefore P_z = \frac{E_0^2}{|\eta|} e^{-2\alpha z} \cos(\omega t - \beta z) \cos(\omega t - \beta z - \theta_n)$$

$$\therefore P_{z, \text{av}} = \frac{1}{T} \int_0^T P_z dt$$

$$\because \cos A \cos B = \frac{1}{2} [\cos(A-B) + \cos(A+B)]$$

$$P_{z, \text{av}} = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} \cos \theta_n$$

If we use, rms values instead of peak amplitudes, the factor of  $\frac{1}{2}$  would not be present. It can be shown that, the time average poynting vector can be also written as

$$P_{z, \text{av}} = \frac{1}{2} \operatorname{Re}(\bar{E} \times \bar{H})$$

Finally, the average power flowing through any area 'S' normal to the z-axis is

$$P_{\text{ave}} = \frac{1}{2} \frac{E_0^2}{\eta} S \text{ watt.} \quad \dots (13)$$

For any given surface 'S', it is given by

$$P_{\text{ave}} = \iint_S \bar{P}_{\text{av}} \cdot d\bar{S} \quad \dots (14)$$

#### Instantaneous, Average and Complex Poynting vector :

In a.c. circuit, the instantaneous power  $\tilde{W}$  is always given by the product of the instantaneous voltage  $\tilde{V}$  and the instantaneous current  $\tilde{I}$

$$\therefore \tilde{W} = \tilde{V} \tilde{I} \quad \text{complex power} \quad \dots (15)$$

$$\text{Let } \tilde{V} = |V| \cos(\omega t + \theta_v) \quad \dots (16)$$

$$\tilde{I} = |I| \cos(\omega t + \theta_i) \quad \dots (17)$$

$\therefore$  The instantaneous power,

$$\tilde{W} = |V| |I| \cos(\omega t + \theta_v) \cos(\omega t + \theta_i)$$

$$\begin{aligned} \eta &= \frac{\bar{E}}{\bar{H}} \\ \bar{H} &= \frac{\bar{E}}{\eta} \end{aligned}$$

ay  
a2

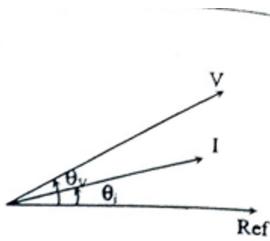
$$= \frac{|V||I|}{2} [\cos(\theta_v - \theta_i) + \cos(2\omega t + \theta_v + \theta_i)] \dots (18)$$

Taking average of equation (18) over one cycle,

$$W_{av} = \frac{|V||I|}{2} \cos(\theta_v - \theta_i) = \frac{|V||I|}{2} \cos\theta \dots (19)$$

where  $\theta = \theta_v - \theta_i$

$$\text{and } W_{react} = \frac{|V||I|}{2} \sin\theta \dots (20)$$



If  $V$  is voltage and  $I$  is current expressed in phasor,  $W = \frac{1}{2} VI^*$

where  $I^*$  is the complex conjugate of  $I$ .

$$W = W_{av} + jW_{react} \dots (21)$$

$$\text{Thus } W_{av} = \frac{1}{2} \operatorname{Re}[VI^*]$$

$$W_{react} = \frac{1}{2} I_m [VI^*]$$

In electromagnetic field theory, the instantaneous power flow per square meter is  
 $\tilde{P} = \tilde{E} \times \tilde{H}$

$\therefore$  the complex poynting vector  $\bar{P}$  may be defined as -

$$\bar{P} = \frac{1}{2} \bar{E} \times \bar{H}^* \dots (22)$$

$\therefore$  the average and reactive parts of the power flow per square meter.

$$\bar{P}_{av} = \frac{1}{2} \operatorname{Re}[\bar{E} \times \bar{H}^*] \quad \text{*real part*}$$

$$\bar{P}_{react} = \frac{1}{2} \operatorname{Im}[\bar{E} \times \bar{H}^*]$$

The product of  $\bar{E}$  and  $\bar{H}$  is a vector product only mutually perpendicular components of  $\bar{E}$  and  $\bar{H}$  contribute to the power flow, and the direction of the flow is normal to the plane containing  $\bar{E}$  and  $\bar{H}$ .

### The Poynting Theorem in complex form :

Maxwell's curl equations may be expressed in phasor form as

$$\nabla \times \bar{H} = (\sigma + j\omega\epsilon) \bar{E} + \bar{J} \quad \text{and} \dots (24)$$

$$\nabla \times \bar{E} = -j\omega\mu \bar{H} \dots (25)$$

in which  $\bar{J}$  represents non ohmic currents such as convection current or specified current source.

$$\therefore \nabla \cdot (\bar{E} \times \bar{H}^*) = \bar{H}^* \cdot \nabla \times \bar{E} - \bar{E} \cdot (\nabla \times \bar{H}^*) \\ = -j\omega\mu \bar{H} \cdot \bar{H}^* - (\sigma - j\omega\epsilon) \bar{E} \cdot \bar{E}^* - \bar{E} \cdot \bar{J}^* \dots (26)$$

Integrating over the volume  $V$  surrounding by surface 's', we have

$$\oint_s (\bar{E} \times \bar{H}^*) \cdot d\bar{s} = -j\omega \int_V \mu \bar{H} \cdot \bar{H}^* - \epsilon \bar{E} \cdot \bar{E}^* dv - \int_V \sigma \bar{E} \cdot \bar{E}^* dv - \int_V \bar{E} \cdot \bar{J}^* dv$$

The time average stored energy densities (electric and magnetic) are given by

$$U_e = \frac{1}{4} \epsilon \bar{E} \cdot \bar{E}^*$$

$$U_m = \frac{1}{4} \mu \bar{H} \cdot \bar{H}^* \dots (27)$$

The Poynting theorem now may be separated into real and imaginary part and written as -

$$\operatorname{Re} \oint_s \bar{P} \cdot d\bar{s} + \frac{1}{2} \int_V \sigma \bar{E} \cdot \bar{E}^* dv = -\frac{1}{2} \operatorname{Re} \int_V \bar{E} \cdot \bar{J}^* dv \dots (28)$$

$$I_m \oint_s \bar{P} \cdot d\bar{s} + 2\omega \int_V (U_m - U_e) dv = -\frac{1}{2} I_m \int_V \bar{E} \cdot \bar{J}^* dv \dots (29)$$

## Intrinsic Impedance

Now taking ratio

$$\frac{E_x}{H_y} = \frac{E_0 e^{-\gamma z}}{\frac{\gamma E_0}{j\omega\mu} e^{-\gamma z}} = \frac{j\omega\mu}{\gamma}$$

$$= \frac{j\omega\mu}{\sqrt{j\omega\mu(\sigma + j\omega\epsilon)}} = \sqrt{\frac{j\omega\mu}{(\sigma + j\omega\epsilon)}} = \text{complex quantity}$$

$$= \eta \text{ (intrinsic impedance)}$$

where  $\gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$

$$\gamma = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$$

$$e^{j\theta_n}$$

$$\eta = |\eta| \angle \theta_n$$

where  $\eta$  is complex quantity, which may be expressed as

$$\rightarrow \eta = \sqrt{\frac{j\omega\mu}{(\sigma + j\omega\epsilon)}} = |\eta| \angle \theta_n = |\eta| e^{j\theta_n}$$

$$\eta = \frac{E}{H}$$

$$H = \frac{E}{\eta}$$

$$|\eta| \angle \theta_n$$

$$E =$$

$$\therefore \eta^2 = \frac{j\omega\mu(\sigma - j\omega\epsilon)}{\sqrt{(\sigma + j\omega\epsilon)(\sigma - j\omega\epsilon)}} = \sqrt{\frac{\omega^2\mu\epsilon + j\sigma\omega\mu}{\sigma^2 + \omega^2\epsilon^2}}$$

$$\therefore \theta_n = \frac{1}{2} \tan^{-1} \frac{\sigma\omega\mu}{\omega^2\mu\epsilon} = \frac{1}{2} \tan^{-1} \frac{\sigma}{\omega\epsilon}$$

$$\rightarrow |\eta| = \sqrt{\frac{\mu/\epsilon}{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2}}$$

Hence the equation (27) may be written as -

$$\rightarrow H_y = \frac{E_0}{|\eta| \angle \theta_n} e^{j\alpha z} \cos(\omega t - \beta z)$$

$$\rightarrow \bar{H}(z, t) = \frac{E_0}{|\eta|} e^{-j\alpha z} \cos(\omega t - \beta z - \theta_n) \hat{a}_y$$

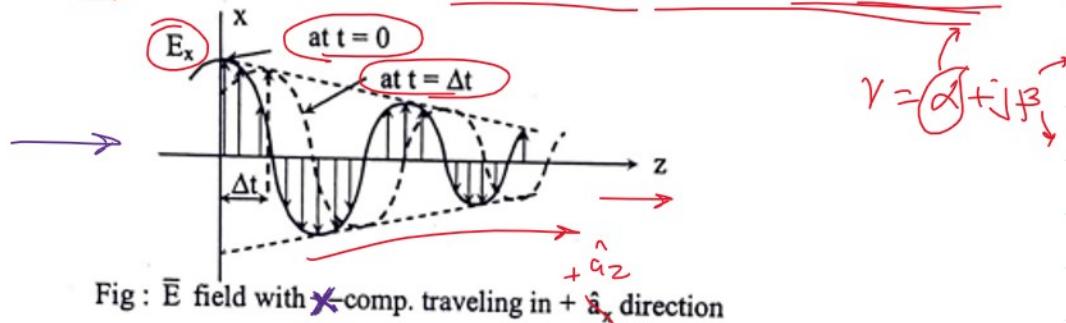
$$\left. \begin{array}{l} \\ \end{array} \right\}$$

$$(28)$$

$$\rightarrow \bar{E}(z, t) = E_0 e^{-j\alpha z} \cos(\omega t - \beta z) \hat{a}_x$$

$$\dots (25)$$

From equation (25) and (28), as the wave propagates along  $\hat{a}_z$ , it decreases or attenuates in amplitude by a factor  $e^{-\alpha z}$ , hence  $\alpha$  is known as the attenuation constant or factor of the medium. It is a measure of the spatial rate of decay of the wave in the medium, measured in nepers per meter (Np/m) or in decibels per meter (dB/m). An attenuation of 1 neper denotes a reduction to  $e^{-1}$  of the original value whereas an increase of 1 neper indicates an increase by a factor of  $e$ .



The quantity  $\beta$  is a measure of the phase shift per length and is called the phase constant or wave number.

In terms of  $\beta$ , the velocity of propagation and wavelength are given by,

$$\rightarrow v = \frac{\omega}{\beta}, \quad \lambda = \frac{2\pi}{\beta} \quad \dots (29)$$

$$\rightarrow E_x = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (24)$$

$$\therefore H_y = \frac{\gamma E_0}{j\omega\mu} e^{-\alpha z} \cos(\omega t - \beta z) \quad \dots (27)$$

$$\rightarrow H_y = \frac{E_0}{|\eta| \sin \theta_n} e^{\alpha z} \cos(\omega t - \beta z)$$

From equation (24) and (27) it is clear that  $\bar{E}$  and  $\bar{H}$  are out of phase by  $\theta_n$  at any instant of time due to the complex intrinsic impedance of the medium. The ratio of the magnitude of the conduction current density  $\bar{J}$  to the displacement current density  $\bar{J}_d$  in lossy medium is

$$\begin{aligned} |\bar{J}| &= \frac{|\sigma \bar{E}|}{|j\omega\epsilon \bar{E}|} = \sqrt{\frac{\sigma}{\omega\epsilon}} = \tan \theta \\ \dots &\dots (30) \end{aligned}$$

$$\frac{|\bar{J}|}{|\bar{J}_d|} = \frac{|\sigma \bar{E}|}{|j\omega \epsilon \bar{E}|} = \boxed{\frac{\sigma}{\omega \epsilon} = \tan \theta} \rightarrow \bar{E} \quad \dots\dots(30)$$

where  $\tan \theta$  is known as the loss tangent and  $\theta$  is the loss angle of the medium.

If  $\tan \theta$  is very small ( $\sigma < < \omega \epsilon$ ) the medium is said to be good dielectric.  
 If  $\tan \theta$  is very large ( $\sigma > > \omega \epsilon$ ), the medium is good conductor

Also from the view point of wave propagation the characteristic behavior of medium depends not only on  $\sigma$ ,  $\epsilon$ , and  $\mu$  but also on the frequency of operation.

(NOTE)

## Condition at a Boundary Surface

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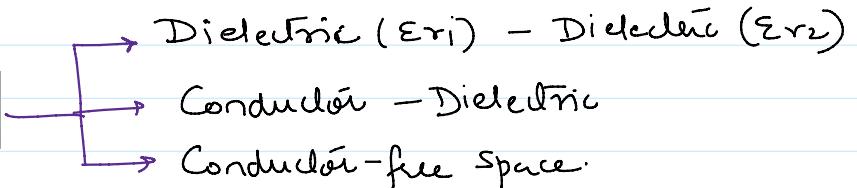
### Generalized Form of Maxwell's Equation:

Differential form	Integral form	Remarks
$\nabla \cdot \bar{D} = \rho_v$	$\oint_S \bar{D} \cdot d\bar{S} = \int_{\text{vol}} \rho_v dv$	Gauss's Law
$\nabla \cdot \bar{B} = 0$	$\oint_S \bar{B} \cdot d\bar{S} = 0$	Gauss's Law for magnetic field
$\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$	$\oint_S \bar{E} \cdot d\bar{L} = \frac{\partial}{\partial t} \int_S \bar{B} \cdot d\bar{S}$	Faraday's law
$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t}$	$\oint_S \bar{H} \cdot d\bar{L} = \int_S \left( \bar{J} + \frac{\partial \bar{D}}{\partial t} \right) \cdot d\bar{S}$	Modified form of Ampere's circuital law

### Maxwell's Equation in Phasor Form:

Point Form	Integral Form
$\nabla \times \bar{H} = \bar{J} + j\omega \bar{D}$	$\oint_L \bar{H} \cdot d\bar{L} = \int_S \bar{J} \cdot d\bar{S} + j\omega \int_S \bar{D} \cdot d\bar{S}$
$\nabla \times \bar{E} = -j\omega \bar{B}$	$\oint_L \bar{E} \cdot d\bar{L} = -j\omega \int_S \bar{B} \cdot d\bar{S}$
$\nabla \cdot \bar{D} = \rho_v$	$\oint_S \bar{D} \cdot d\bar{S} = \int_{\text{vol}} \rho_v dv$
$\nabla \cdot \bar{B} = 0$	$\oint_S \bar{B} \cdot d\bar{S} = 0$
$\nabla \cdot \bar{J} = -j\omega \rho_v$	$\oint_S \bar{J} \cdot d\bar{S} = -j\omega \int_{\text{vol}} \rho_v dv$

### Condition at a Boundary Surface:



If the field exist in a region consisting of two different media, the conditions that must satisfy at the interface separating the media are called boundary conditions.

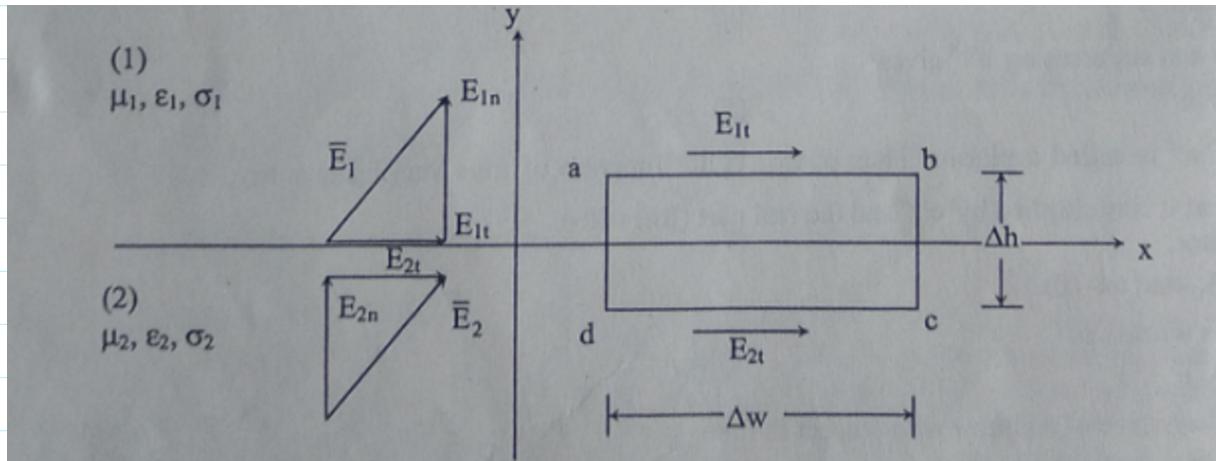
The integral form of Maxwell's equation can be used to determine boundary conditions.

### Tangential component of $\bar{E}$ and $\bar{H}$ :

Let two dielectric media of permittivities of  $\epsilon_1$  and  $\epsilon_2$  and permeability  $\mu_1$  and  $\mu_2$  be separated by plane boundary as shown in figure. Let  $\sigma_1$  and  $\sigma_2$  be the conductivities of two media.

Consider Maxwell's equation from Faraday's law,

$$\oint \bar{E} \cdot d\bar{L} = - \int_S \frac{\partial \bar{B}}{\partial t} \cdot d\bar{S} \quad \dots(1)$$



Apply equation (1) to the closed path abcd $a$  assuming that the path is very small with respect to variation of  $\bar{E}$ .

$$E_{1t}\Delta w - \frac{1}{2}E_{1n}\Delta h - \frac{1}{2}E_{2n}\Delta h - E_{2t}\Delta w + \frac{1}{2}E_{2n}\Delta h + \frac{1}{2}E_{1n}\Delta h = -\frac{\partial B_z}{\partial t} \Delta w \Delta h \quad \dots(2)$$

Where  $B_z$  is average magnetic flux density through rectangle  $\Delta w \Delta h$ . Now consider condition as the area of the rectangle is made to approach zero by reducing the height  $\Delta h$ .

$$\begin{aligned} \therefore \text{As } \Delta h \rightarrow 0 \\ \therefore E_{1t} \Delta w - E_{2t} \Delta w = 0 \end{aligned}$$

$$\therefore E_{1t} = E_{2t}$$

the tangential component of  $E$  is continuous.

### Tangential component of $\bar{D}$

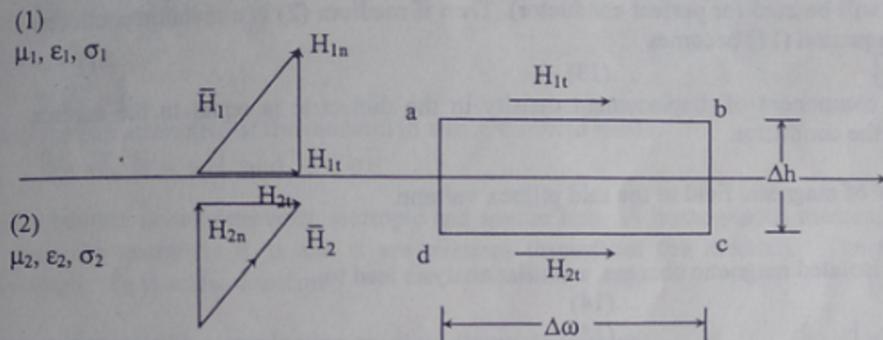
$$\frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2} \leftarrow (\text{discontinuous})$$

\* Tangential Component of  $\bar{H}$

Similarly, for the tangential component of  $\mathbf{H}$  consider Maxwell's equation from Ampere's circuital law,

$$\oint_L \bar{\mathbf{H}} \cdot d\bar{\mathbf{L}} = \int_S \left( \bar{\mathbf{J}} + \frac{\partial \bar{\mathbf{D}}}{\partial t} \right) \cdot d\bar{\mathbf{S}} \quad \dots(4)$$

Apply to closed path abcda,



$$H_{1t}\Delta w - \frac{1}{2}H_{1n}\Delta h - \frac{1}{2}H_{2n}\Delta h - H_{2t}\Delta w + \frac{1}{2}H_{2n}\Delta h + \frac{1}{2}E_{1n}\Delta h = \left( \frac{\partial D_Z}{\partial t} + J_Z \right) \Delta h \Delta w \quad \dots(5)$$

As  $\Delta h \rightarrow 0$

$$\begin{aligned} H_{1t} - H_{2t} &= 0 \\ \boxed{H_{1t} = H_{2t}} \end{aligned}$$

## Electric and Magnetic field boundary conditions

02 February 2023 08:48

### Generalized Form of Maxwell's Equation:

Differential form	Integral form	Remarks
$\nabla \cdot \bar{D} = \rho_v$	$\oint_S \bar{D} \cdot d\bar{S} = \int_{\text{vol}} \rho_v dv$	Gauss's Law
$\nabla \cdot \bar{B} = 0$	$\oint_S \bar{B} \cdot d\bar{S} = 0$	Gauss's Law for magnetic field
$\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$	$\oint_L \bar{E} \cdot d\bar{L} = \frac{\partial}{\partial t} \int_S \bar{B} \cdot d\bar{S}$	Faraday's law
$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t}$	$\oint_S \bar{H} \cdot d\bar{L} = \int_S \left( \bar{J} + \frac{\partial \bar{D}}{\partial t} \right) \cdot d\bar{S}$	Modified form of Ampere's circuital law

### Maxwell's Equation in Phasor Form:

Point Form	Integral Form
$\nabla \times \bar{H} = \bar{J} + j\omega \bar{D}$	$\oint_L \bar{H} \cdot d\bar{L} = \int_S \bar{J} \cdot d\bar{S} + j\omega \int_S \bar{D} \cdot d\bar{S}$
$\nabla \times \bar{E} = -j\omega \bar{B}$	$\oint_L \bar{E} \cdot d\bar{L} = -j\omega \int_S \bar{B} \cdot d\bar{S}$
$\nabla \cdot \bar{D} = \rho_v$	$\oint_S \bar{D} \cdot d\bar{S} = \int_{\text{vol}} \rho_v dv$
$\nabla \cdot \bar{B} = 0$	$\oint_S \bar{B} \cdot d\bar{S} = 0$
$\nabla \cdot \bar{J} = -j\omega \rho_v$	$\oint_S \bar{J} \cdot d\bar{S} = -j\omega \int_{\text{vol}} \rho_v dv$

### Boundary conditions

If the field exist in a region consisting of two different media, the conditions that must satisfy at the interface separating the media are called boundary conditions.

### Electrostatic Boundary conditions

### \* Electrostatic Boundary conditions

If the field exists in a region consisting of two different media, the conditions that must satisfy at the interface separating the media are called boundary conditions. These conditions are helpful in determining the field on one side of the boundary if field on the other side is known.

To determine the boundary conditions, we need to use Maxwell's eq' for electrostatic fields.

$$\oint \vec{E} \cdot d\vec{l} = 0 \quad \text{--- } 1$$

$$\oint \vec{D} \cdot d\vec{s} = Q_{\text{enc}} \quad \text{--- } 2$$

The electric field intensity & flux density is decomposed into two orthogonal components such as:

$$\vec{E} = \vec{E}_t + \vec{E}_n \quad \& \quad \vec{D} = \vec{D}_t + \vec{D}_n \quad \text{--- } 3$$

### (a) [A] Dielectric-dielectric boundary conditions:-

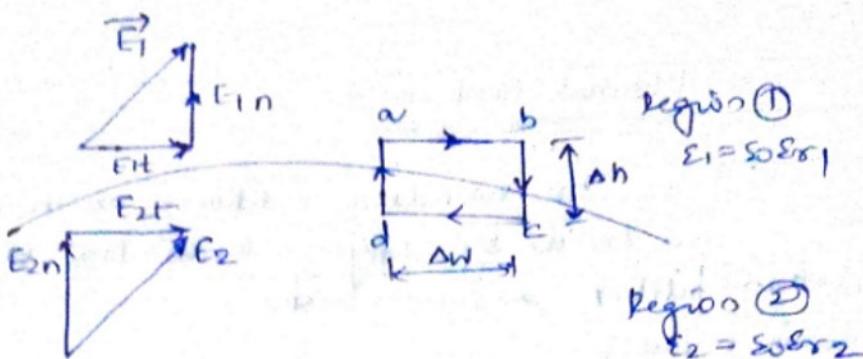
Consider the  $\vec{E}$  field existing in a region consisting of two different dielectrics characterized by

$$\epsilon_1 = \epsilon_0 \epsilon_r 1 \quad \& \quad \epsilon_2 = \epsilon_0 \epsilon_r 2 \quad \text{as shown in fig.}$$

$\vec{E}_1$  &  $\vec{E}_2$  in media 1 & 2 respectively can be decomposed as

$$\vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1n}$$

$$\vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2n} \quad \text{--- } 4$$



Tangential components

## Tangential components

Apply eq ① to the closed path abcdab assuming that the path is very small w.r.t. the variation of  $\vec{E}$ . we have

$$0 = E_1 t \Delta W - \frac{1}{2} E_1 n \frac{\Delta h}{2} - E_2 t \Delta W + \frac{1}{2} E_2 n \Delta h \\ + \frac{1}{2} E_1 n \Delta h$$

As  $\Delta h \rightarrow 0$

$$\boxed{E_1 t = E_2 t} \quad \text{--- (5)}$$

Thus the tangential components of  $\vec{E}$  are same on the two sides of boundary. In other words, it is continuous across boundary [  $E_t$  undergoes no change on the boundary ]  
since  $\vec{D} = \epsilon \vec{E} = D_t + D_n$

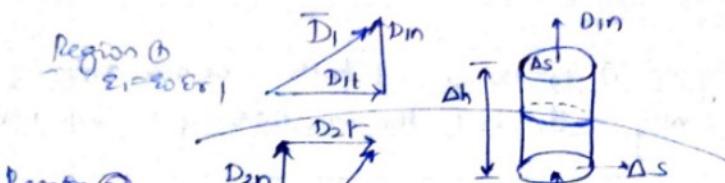
$$\therefore \frac{D_{1t}}{\epsilon_1} = \frac{E_{1t}}{\epsilon_1} = E_{2t} = \frac{D_{2t}}{\epsilon_2}$$

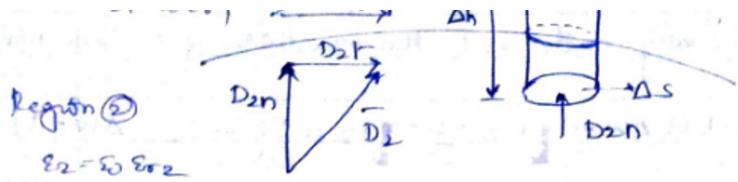
$$\therefore \boxed{\frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}} \quad \text{--- (6)}$$

$D_t$  undergoes some changes across the interface. Hence  $D_t$  is said to be discontinuous across the interface.

## Normal components

The boundary conditions on the normal components are found by applying Gauss's law to the small cylindrical pillbox as shown below.  
(Gaussian surface)





The sides are again very short, & the flux leaving the top & bottom surfaces is the difference

$$D_{1n} \Delta S - D_{2n} \Delta S = \Delta Q = \rho_s \Delta S$$

from which

$$\boxed{D_{1n} - D_{2n} = \rho_s} \quad \rightarrow \textcircled{P}$$

where  $\rho_s$  is the free charge density forced discontinuously at the boundary. If no free charge exists at the interface  $\rho_s = 0$ , & eq<sup>n</sup> ② becomes

$$\boxed{D_{1n} = D_{2n}} \quad \rightarrow \textcircled{Q}$$

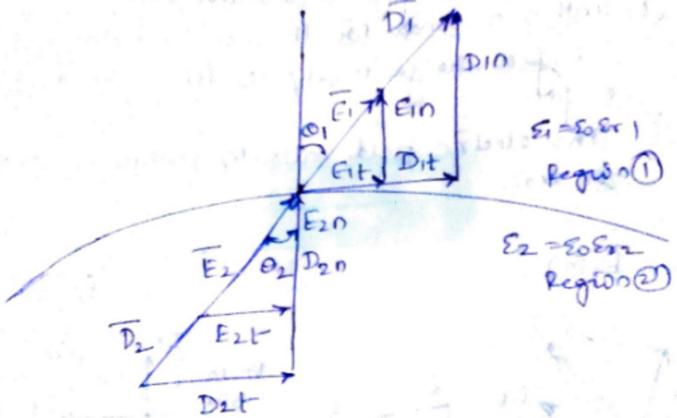
Thus the normal component of  $\vec{D}$  is continuous across the interface, that is  $D_n$  undergoes no change at the boundary. Since  $\vec{D} = \epsilon \vec{E}$

$$\boxed{\epsilon_1 E_{1n} = \epsilon_2 E_{2n}} \quad \rightarrow \textcircled{R}$$

This shows that normal component of  $\vec{E}$  is discontinuous at the boundary.

The boundary conditions are usually applied to  
→ find the electric field on one side of the boundary given  
the field on the other side  
→ to determine the 'discontinuity' of  $\vec{E}$  across the interface

Consider  $\vec{D}_1$  &  $\vec{E}_1$  &  $\vec{D}_2$  &  $\vec{E}_2$  making  $\angle \theta_1$  &  $\theta_2$  with the normal to the interface as illustrated in fig.



From fig  
 $E_1 \sin \theta_1 = E_{1t} = E_{2t} = E_2 \sin \theta_2$

or  
 $E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \text{--- (1)}$

Similarly  
 $E_1 E_1 \cos \theta_1 = D_{1n} = D_{2n} = \epsilon_2 E_2 \cos \theta_2$

$\therefore E_1 E_1 \cos \theta_1 = E_2 E_2 \cos \theta_2 \quad \text{--- (11)}$

Dividing eq (1) by eq (11)

$$\frac{\tan \theta_1}{\epsilon_1} = \frac{\tan \theta_2}{\epsilon_2} \quad \text{--- (12)}$$

$\therefore \frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2} = \frac{\epsilon_0 \epsilon_{r1}}{\epsilon_0 \epsilon_{r2}} = \frac{\epsilon_{r1}}{\epsilon_{r2}}$  --- (13)

This is the law of refraction of the electric field at a boundary of free space (since  $\epsilon_0 = 1$  is assumed at the interface).

## Magnetostatic Boundary conditions

## \* Magnetic boundary conditions

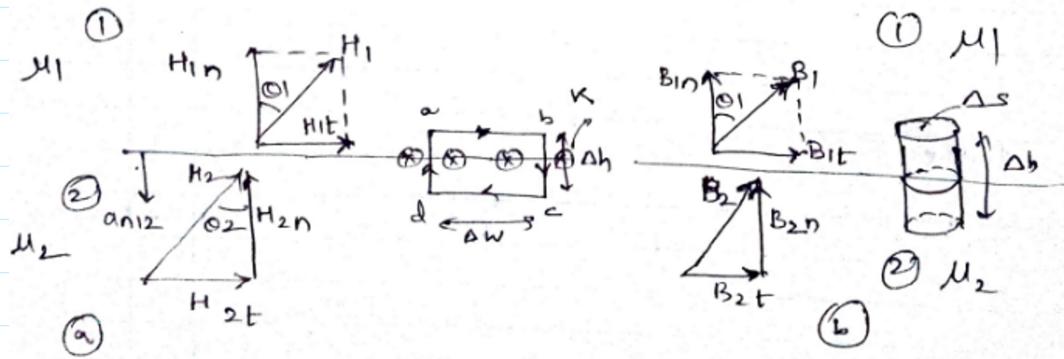
We define magnetic boundary conditions as the conditions that  $\mathbf{H}$  (or  $\mathbf{B}$ ) field must satisfy at the boundary between two different media. Our derivations (derivations here are similar to those for electrostatic fields) we make use of Gauss's law for magnetic fields.

$$\oint \mathbf{B} \cdot d\mathbf{s} = 0 \quad \text{--- (1)}$$

& Ampere's circ law

$$\oint \mathbf{H} \cdot d\mathbf{l} = I \quad \text{--- (2)}$$

Consider the boundary between two magnetic media (1) & (2), characterized, respectively, by  $\mu_1$  &  $\mu_2$  as shown in fig below.



Apply eqn (1) to the pillbox (Gaussian surface) of fig (b) & allowing  $\Delta h \rightarrow 0$ , we obtain

$$B_{1n} \Delta s - B_{2n} \Delta s = 0 \quad \text{--- (3)}$$

Thus

$$\boxed{B_{1n} = B_{2n}} \quad \text{--- (4)} \quad \text{or} \quad \mu_1 H_{1n} = \mu_2 H_{2n}$$

Since  $\mathbf{B} = \mu \mathbf{H}$ , eq (4) shows that the normal comp. of  $\mathbf{B}$  is continuous at the boundary. It also shows that the normal comp. of  $\mathbf{H}$  is discontinuous at the boundary;  $\mathbf{H}$  undergoes some change at the interface.

Similarly, we apply eq (2) to the closed path abca of fig (a), where surface  $\text{cn } k$  on the boundary is assumed normal to the path. We obtain

$$k \cdot \Delta W = H_1 t \cdot \Delta x_0 + H_2 n \cdot \frac{\Delta h}{2} + H_2 n \cdot \frac{\Delta h}{2} - H_2 t \cdot \Delta x - H_2 n \cdot \frac{\Delta h}{2} - H_1 n \cdot \frac{\Delta h}{2} \quad \rightarrow (5)$$

As  $\Delta h \rightarrow 0$ , eq (5) leads to,

$$H_1 t - H_2 t = k \quad \rightarrow (6)$$

This shows that the tangential component of  $H$  is also discontinuous. Eq (6) may be written in terms of  $B$  as

$$\frac{B_1 t}{\mu_1} - \frac{B_2 t}{\mu_2} = k \quad \rightarrow (7)$$

In the general case eq (6) becomes

$$(H_1 t - H_2 t) \times a_{n12} = k \quad \rightarrow (8)$$

where  $a_{n12}$  is a unit-vector normal to the interface & is divided from medium (1) to medium (2) by the boundary in free space (the media are not conductors (for  $\sigma$  is zero) & density  $\rho$  is same). eq (6) becomes

$$[H_1 t = H_2 t] \text{ or } \frac{B_1 t}{\mu_1} = \frac{B_2 t}{\mu_2} \quad \rightarrow (9)$$

Thus the tangential component of  $H$  is continuous while that of  $B$  is discontinuous at the boundary.

If the field make an angle  $\theta$  with the normal to the interface, eq<sup>2</sup> ④ results in

$$B_1 \cos \theta_1 = B_1 n_i = B_2 n = B_2 \cos \theta_2 \quad \text{--- (10)}$$

while eq<sup>2</sup> ⑥ produces

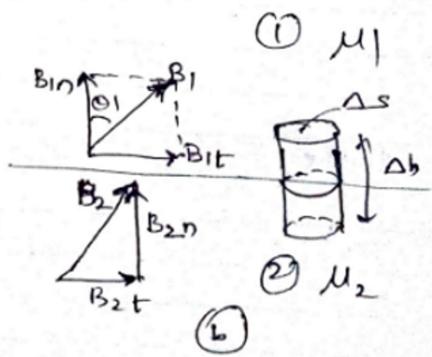
$$\frac{B_1}{\mu_1} \sin \theta_1 = H_{1t} = H_{2t} = \frac{B_2}{\mu_2} \sin \theta_2 \quad \text{--- (11)}$$

Dividing eq<sup>2</sup> ⑩ by eq<sup>2</sup> ⑩

$$\frac{\tan \theta_1}{\mu_1} = \frac{\tan \theta_2}{\mu_2}$$

$$\left[ \frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2} \right] \quad \text{--- (12)}$$

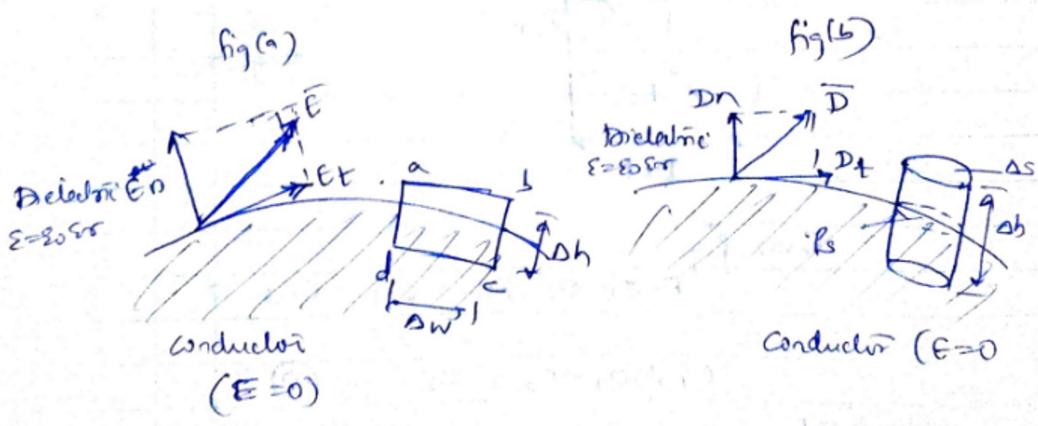
which is the law of refraction for magnetic flux density at a boundary with no surface current.



[B] Conductor-Dielectric boundary conditions  
consider perfect conductor ( $\sigma \rightarrow \infty, \epsilon_c \rightarrow 0$ )

The properties of good conductor are

- (i) within a conductor there is zero charge density & a surface charge density resides on the exterior surface.
- (ii) the electric field intensity within a conductor is zero



Consider conductor in an external field  $\vec{E}$ . Decompose  $\vec{E}$  into two components such as:-

$$\vec{E} = \vec{E}_t + \vec{E}_n$$

where  $E_t$  — tangential &  $E_n$  is normal component

Apply  $\oint \vec{E} \cdot d\vec{l} = 0$  to closed path abcd,

$$E_t \Delta W - \frac{1}{2} E_n \Delta h + \frac{1}{2} E_n \Delta h = 0$$

$$\therefore E_t = 0 \quad \textcircled{14}$$

$$\text{Since } \vec{D} = \epsilon \vec{E}$$

$$D_t = 0 \quad \textcircled{15}$$

As far as normal component is concern apply Gauss law to the pillbox shown in fig(b)

$$\oint \vec{D} \cdot d\vec{s} = Q$$

$$\Delta Q = D_n \Delta S - 0 \Delta S = P_s \Delta S$$

$$\therefore D_n = P_s \quad \textcircled{16}$$

$$\text{or} \quad \epsilon_0 E_n = P_s \quad \textcircled{17}$$

## Introduction to EM waves

11 February 2022 09:15

Waves are a means for transferring energy or information from one place to another

Electromagnetic waves as the name suggests, are a means for transferring electromagnetic energy

Plane wave :- If each field has same direction at every pt in any plane  $\perp$  to the direction of wave travel, it is called as plane wave

Uniform Plane Wave :- If the field has the same direction and magnitude at every point in any plane  $\perp$  to the direction of wave travel, it is called as Uniform plane wave

Electromagnetic (EM) waves.

All forms of EM energy share 3 fundamental characteristics

- (i) They all travel at high velocity
- (ii) In travelling, they assume the properties of waves.
- (iii) They radiate outward from a source.

\* EM wave propagation through various media

- (i) Free space ( $\sigma = \epsilon_0 ; \epsilon = \epsilon_0, \mu = \mu_0$ )
- (ii) Lossless dielectric ( $\sigma \ll \omega \epsilon, \epsilon = \epsilon_0 \epsilon_r, \mu = \mu_0 \mu_r$ )

(iii) Lossy dielectric ( $\sigma \neq 0, \epsilon = \epsilon_0 \epsilon_r, \mu = \mu_0 \mu_r$ )

(iv) Good conductor ( $\sigma = \infty, \epsilon = \epsilon_0, \mu = \mu_0 \mu_r; \sigma \gg \epsilon \omega$ )

Lossy dielectric is the most general case & will be discussed first.

## Extra Numericals

27 January 2022 10:29

- Q1) Consider 2 pt charges  $q_1 = 2 \text{ mC}$  at  $(-3, 7, 4)$  &  $q_2 = 5 \text{ mC}$  at  $(2, 4, -1)$ .  
Find force  $F_2$  on  $q_2$  ( $F_2$  &  $F_1$ )



(i) Force  $F_2$  on  $q_2$  is given by

$$F_2 = \frac{q_1 q_2}{4\pi\epsilon_0 r_{12}^2} \hat{a}_{12}$$

$$\begin{aligned} \vec{r}_{12} = \vec{r}_2 - \vec{r}_1 &= (2\hat{a}_x + 4\hat{a}_y - \hat{a}_z) - (-3\hat{a}_x + 7\hat{a}_y + 4\hat{a}_z) \\ &= 5\hat{a}_x - 3\hat{a}_y - 5\hat{a}_z \end{aligned}$$

$$\rightarrow \hat{a}_{12} = \frac{\vec{r}_2 - \vec{r}_1}{|\vec{r}_{12}|} = \frac{5\hat{a}_x - 3\hat{a}_y - 5\hat{a}_z}{\sqrt{25+9+25}} = \frac{5\hat{a}_x - 3\hat{a}_y - 5\hat{a}_z}{7.6811}$$

$$\therefore \hat{a}_{12} = 0.651 \hat{a}_x - 0.391 \hat{a}_y - 0.651 \hat{a}_z$$

$$\rightarrow \therefore \vec{F}_2 = \frac{2 \times 10^{-3} \times 5 \times 10^{-3}}{4\pi \times 8.85 \times 10^{-12} \times (7.6811)^2} (0.651 \hat{a}_x - 0.391 \hat{a}_y - 0.651 \hat{a}_z)$$

$$\vec{F}_2 = \frac{10 \times 10^{-6}}{6561.45 \times 10^{-12}} (0.651 \hat{a}_x - 0.391 \hat{a}_y - 0.651 \hat{a}_z)$$

$$= 1524.05 (0.651 \hat{a}_x - 0.391 \hat{a}_y - 0.651 \hat{a}_z)$$

$$\boxed{\vec{F}_2 = 992.158 \hat{a}_x - 595.91 \hat{a}_y - 990.63 \hat{a}_z \text{ N}}$$

Note:- As  $\hat{a}_{21} = -\hat{a}_{12}$   
 $\therefore \vec{F}_1 = -\vec{F}_2$

(ii) Force  $F_1$  on  $q_1$

$$\therefore \vec{F}_1 = -992.158 \hat{a}_x + 595.91 \hat{a}_y + 990.63 \hat{a}_z \text{ N}$$

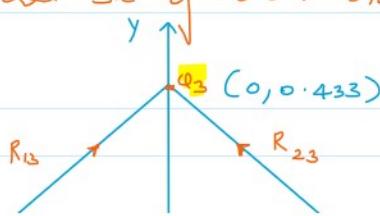
- Q2) Three pt charges  $q_1 = 10^{-6} \text{ C}$ ;  $q_2 = 10^{-6} \text{ C}$  &  $q_3 = 0.5 \times 10^{-6} \text{ C}$  are located at the corners of an equilateral triangle of 50 cm side. Determine force on charge  $q_3$ .



$$q_1 = 10^{-6} \text{ C at } (-0.25, 0)$$

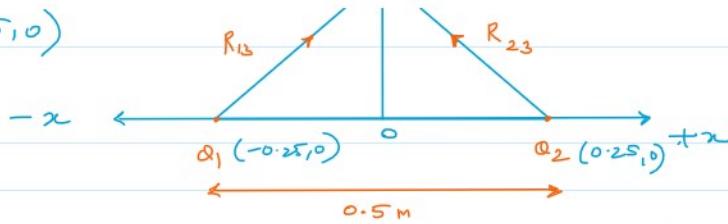
$$q_2 = 10^{-6} \text{ C at } (0.25, 0)$$

$$q_3 = 0.5 \times 10^{-6} \text{ C at }$$



$$q_2 = 10^{-6} C \text{ at } (0.25, 0)$$

$$q_3 = 0.5 \times 10^{-6} C \text{ at } (0, 0.433)$$



Force on charge  $q_3$  is given by

$$\overline{F}_3 = \overline{F}_{13} + \overline{F}_{23}$$

$$= =$$

Calculating unit vectors

$$\hat{a}_{13} = \frac{\tau_3 - \tau_1}{|\tau_{13}|} = \frac{\overline{R}_{13}}{|\overline{R}_{13}|}$$

$$\overline{R}_{13} = \tau_3 - \tau_1 = 0.433\hat{a}_y - (-0.25\hat{a}_x) = 0.25\hat{a}_x + 0.433\hat{a}_y$$

$$\therefore \hat{a}_{13} = \frac{0.25\hat{a}_x + 0.433\hat{a}_y}{\sqrt{(0.25)^2 + (0.433)^2}} = \frac{0.25\hat{a}_x + 0.433\hat{a}_y}{0.495}$$

$$\therefore \hat{a}_{13} = 0.5\hat{a}_x + 0.8677\hat{a}_y$$

Similarly  $\overline{R}_{23} = \tau_3 - \tau_2 = 0.433\hat{a}_y - 0.25\hat{a}_x$

$$\therefore \hat{a}_{23} = \frac{\overline{R}_{23}}{|\overline{R}_{23}|} = \frac{-0.25\hat{a}_x + 0.433\hat{a}_y}{\sqrt{(-0.25)^2 + (0.433)^2}}$$

$$\hat{a}_{23} = -0.5\hat{a}_x + 0.8677\hat{a}_y$$

$$F_{13} = \frac{q_1 q_3}{4\pi\epsilon_0 R_{13}^2} \hat{a}_{13} = \frac{10^{-6} \times 0.5 \times 10^{-6}}{4\pi \times 8.85 \times 10^{-12} \times (0.495)^2} \cdot (0.5\hat{a}_x + 0.8677\hat{a}_y)$$

$$= 0.0181 (0.5\hat{a}_x + 0.8677\hat{a}_y) = (9.05\hat{a}_x + 15.7\hat{a}_y) \text{ mN}$$

$$\therefore F_{13} = 9.05\hat{a}_x + 15.7\hat{a}_y \text{ mN}$$

$$F_{23} = \frac{q_2 q_3}{4\pi\epsilon_0 R_{23}^2} \hat{a}_{23} = \frac{10^{-6} \times 0.5 \times 10^{-6}}{4\pi \times 8.85 \times 10^{-12} \times (0.495)^2} \times (-0.5\hat{a}_x + 0.8677\hat{a}_y)$$

$$= 0.0181 (-0.5\hat{a}_x + 0.8677\hat{a}_y)$$

$$= -9.05\hat{a}_x + 15.7\hat{a}_y$$

$$\therefore F_{23} = -9.05\hat{a}_m + 15.7\hat{a}_y \text{ N}$$

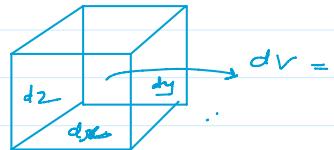
∴ Using the principle of superposition

$$\begin{aligned} F_3 &= \cancel{F_{13}} + \cancel{F_{23}} \\ &= \cancel{9.05\hat{a}_m} + 15.7\hat{a}_y - \cancel{9.05\hat{a}_m} + 15.7\hat{a}_y \end{aligned}$$

$$F_3 = 31.4\hat{a}_y \text{ N} \quad \leftarrow$$

- (Q3) For  $x, y \& z$  +ve ; Let  $\rho_V = 40xyz \text{ C/m}^3$  . Find the total charge within the region bounded by  $0 \leq x, y, z \leq 2$

$$\Rightarrow Q = \iiint_{z \leq y \leq x} \rho_V dV$$



$$= \int_0^2 \int_0^2 \int_0^2 40xyz \cdot dz \cdot dy \cdot dx$$

$$= 40 \left[ \frac{x^2}{2} \right]_0^2 \left[ \frac{y^2}{2} \right]_0^2 \left[ \frac{z^2}{2} \right]_0^2$$

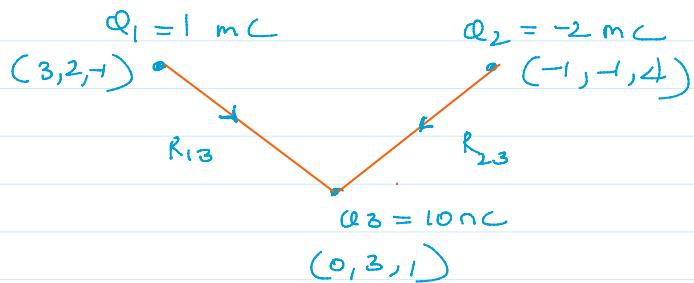
$$= \frac{40}{8} (64) = 320 \text{ C}$$

$$\therefore Q = 320 \text{ C}$$

- (Q4) Two point charges  $1\text{mC}$  &  $-2\text{mC}$  are located at  $(3, 2, -1)$  &  $(-1, -1, 4)$  respectively . Calculate the electric force on a  $10\text{nC}$  charge located at  $(0, 3, 1)$  & the electric field at that point -



$$\text{Let } Q_3 = 10\text{nC}$$



- (i) Find force  $F_3$
- (ii) Find  $\bar{E}$

iii

(ii) Find E

$$Q_3 = 10 \text{ nC}$$

$$(0, 3, 1)$$

(i)

$$\bar{F}_3 = \bar{F}_3 + \bar{F}_{23}$$

$$F_{13} = \frac{Q_1 Q_3}{4\pi\epsilon_0 R_{13}^2} \cdot \hat{a}_{13} = \frac{Q_1 Q_3}{4\pi\epsilon_0 |R_{13}|^3} (\vec{r}_3 - \vec{r}_1)$$

$$\begin{aligned} \vec{r}_3 - \vec{r}_1 &= 3\hat{a}_y + \hat{a}_z - (3\hat{a}_x + 2\hat{a}_y - \hat{a}_z) \\ &= -3\hat{a}_x + \hat{a}_y + 2\hat{a}_z \quad ; \quad R_{13} = \sqrt{9+1+4} = (\sqrt{14}) \end{aligned}$$

$$F_{13} = \frac{1 \times 10^{-3} \times 10 \times 10^{-9}}{4\pi \times 8.85 \times 10^{-12} \times (\sqrt{14})^3} (-3\hat{a}_x + \hat{a}_y + 2\hat{a}_z)$$

$$F_{13} = 1.7165 \times 10^{-3} (-3\hat{a}_x + \hat{a}_y + 2\hat{a}_z) \text{ N}$$

$$F_{13} = 5.15 \hat{a}_x + 1.7165 \hat{a}_y + 3.433 \hat{a}_z \text{ MN}$$

Similarly

$$F_{23} = \frac{Q_2 Q_3}{4\pi\epsilon_0 |R_{23}|^3} \times (\vec{r}_3 - \vec{r}_2)$$

$$\vec{r}_3 - \vec{r}_2 = 3\hat{a}_y + \hat{a}_z - (-\hat{a}_x - \hat{a}_y + 4\hat{a}_z)$$

$$\vec{r}_3 - \vec{r}_2 = \hat{a}_x + 4\hat{a}_y - 3\hat{a}_z \quad \text{Also} \quad |R_{23}| = \sqrt{1+16+9} = \sqrt{26}$$

$$F_{23} = \frac{-2 \times 10^{-3} \times 10 \times 10^{-9}}{4\pi \times 8.85 \times 10^{-12} \times (\sqrt{26})^3} (\hat{a}_x + 4\hat{a}_y - 3\hat{a}_z)$$

$$F_{23} = -1.356 \times 10^{-3} (\hat{a}_x + 4\hat{a}_y - 3\hat{a}_z)$$

$$F_{23} = -1.356 \hat{a}_x - 5.424 \hat{a}_y + 4.068 \hat{a}_z \text{ MN}$$

$$\therefore F_3 = F_{13} + F_{23}$$

$$= (5.15 \hat{a}_x + 1.7165 \hat{a}_y + 3.433 \hat{a}_z) + (-1.356 \hat{a}_x - 5.424 \hat{a}_y + 4.068 \hat{a}_z)$$

$$\boxed{\bar{F}_3 = 3.794 \hat{a}_x - 3.707 \hat{a}_y + 7.501 \hat{a}_z \text{ MN}}$$

iii Electric field is given by

$$S = -\omega t \mathbf{a}_x - \omega r \mathbf{a}_y + r \omega \mathbf{a}_z \dots$$

(ii) Electric field is given by

$$\bar{E} = \frac{\bar{F}_3}{q_3} = \frac{(3.794 \hat{a}_x - 3.707 \hat{a}_y + 7.501 \hat{a}_z)}{10 \times 10^{-9}} \text{ mN}$$

$$\bar{E} = (0.3794 \hat{a}_x - 0.3707 \hat{a}_y + 0.7501 \hat{a}_z) \times 10^6$$

$$\bar{E} = 379.4 \hat{a}_x - 370.7 \hat{a}_y + 750.1 \hat{a}_z \frac{kV}{m}$$

Q5) Find  $\bar{E}$  at the origin if the following charge distributions are present in free space

(i) Point charge of  $12 \text{ nC}$  at  $(2, 0, 6)$

(ii) Uniform line charge density of  $3 \text{ nC/m}$  at  $x = -2, y = 3$

(iii) Uniform surface charge density of  $0.2 \text{ nC/m}^2$  at  $x = 2$

$\Rightarrow$

$$(i) \bar{E}_q = \frac{q}{4\pi\epsilon_0 |R_1|^3} (\mathbf{r}_0 - \mathbf{r}_1) = \frac{12 \times 10^{-9}}{4\pi \times 8.85 \times 10^{-12} \times (\sqrt{40})^3} (-2\hat{a}_x - 6\hat{a}_z)$$

$$\bar{E}_q = 0.4265 (-2\hat{a}_x - 6\hat{a}_z) = -0.853 \hat{a}_x - 2.559 \hat{a}_z \text{ V/m}$$

$$\therefore \bar{E}_q = -0.853 \hat{a}_x - 2.559 \hat{a}_z \text{ V/m}$$

$$(ii) \bar{E}_L = \frac{\rho_L}{2\pi\epsilon_0 |R_1|^3} (\mathbf{r}_0 - \mathbf{r}_2) = \frac{3 \times 10^{-9}}{2\pi \times 8.85 \times 10^{-12} \times (\sqrt{13})^3} (2\hat{a}_x - 3\hat{a}_y)$$

$$\bar{E}_L = 2.302 \hat{a}_x - 3.451 \hat{a}_y \text{ V/m}$$

$$(iii) \bar{E}_s = \frac{\rho_s}{2\epsilon_0} \hat{a}_n = \frac{0.2 \times 10^{-9}}{2 \times 8.85 \times 10^{-12}} (-2\hat{a}_x)$$

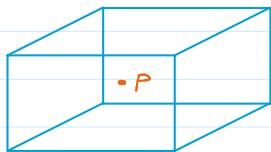
$$\bar{E}_s = -22.598 \hat{a}_n V/m$$

$$\therefore \bar{E} = \bar{E}_q + \bar{E}_L + \bar{E}_s$$

$$\bar{E} = -21.598 \hat{a}_n - 3.451 \hat{a}_y - 2.559 \hat{a}_z V/m$$

Q6) Find the total charge enclosed in a cube defined by a volume of  $10^{-10} m^3$  located at  $(2, 3, 4)$ . How much flux leaves this volume.

$\rightarrow$



$$\varrho = \int_{V} e_r dv = \int_{V} (\nabla \cdot \bar{D}) dv$$

$$\nabla \cdot \bar{D} = \frac{\partial}{\partial x} D_x + \frac{\partial}{\partial y} D_y + \frac{\partial}{\partial z} D_z \Rightarrow \left\{ \begin{array}{l} \left( \frac{\partial \hat{a}_x}{\partial x} + \frac{\partial \hat{a}_y}{\partial y} + \frac{\partial \hat{a}_z}{\partial z} \right) \\ (D_x \hat{a}_x + D_y \hat{a}_y + D_z \hat{a}_z) \end{array} \right.$$

- Experimental law deals with force between two point charges
- The law states that the force F between two point charges  $Q_1$  and  $Q_2$  is-
  - directly proportional to the products ( $Q_1 \times Q_2$ ) of the charges
  - Inversely proportional to square of distance (R) between them
  - along the line joining them.
  - depends upon medium
  - depends upon the nature of charges (+ or - ).



- The force is expressed as –
- $F = \frac{Q_1 Q_2}{4\pi\epsilon R^2}$
- where  $\epsilon$  is permittivity of the medium. For free space  $\epsilon = \epsilon_0\epsilon_r = \epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$  i.e.  $\epsilon_r = 1$

# Vector Form:

- The force  $\bar{F}_2$  on  $Q_2$  due to  $Q_1$  is given by-

$$\therefore \bar{F}_2 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \bar{a}_{12}$$

Where  $\bar{a}_{12}$  is unit vector in the direction of  $\bar{R}_{12}$

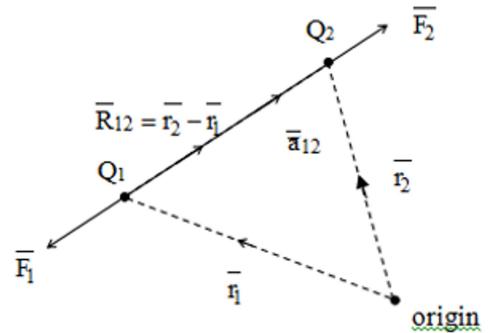
$$\bar{a}_{12} = \frac{\bar{R}_{12}}{|\bar{R}_{12}|} = \frac{\bar{r}_2 - \bar{r}_1}{|\bar{r}_2 - \bar{r}_1|}$$

Similarly, force  $\bar{F}_1$  on  $Q_1$  due  $Q_2$  is given by

$$\bar{F}_1 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{21}^2} \bar{a}_{21}$$

$$= \frac{-Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \bar{a}_{12}$$

$$\bar{F}_1 = -\bar{F}_2$$



# Principle of Superposition:

- Consider system of  $n$  point charges. The total force is given as-

$$\bar{F} = \bar{F}_1 + \bar{F}_2 + \bar{F}_3 + \dots + \bar{F}_n$$

$$\begin{aligned} &= \frac{QQ_1(\bar{r} - \bar{r}_1)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_1\|)^3} + \frac{QQ_2(\bar{r} - \bar{r}_2)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_2\|)^3} + \dots + \frac{QQ_n(\bar{r} - \bar{r}_n)}{4\pi\epsilon_0(\|\bar{r} - \bar{r}_n\|)^3} \\ &= \frac{Q}{4\pi\epsilon_0} \sum_{k=1}^n \frac{Q_k(\bar{r} - \bar{r}_k)}{\|\bar{r} - \bar{r}_k\|^3} \end{aligned}$$

