



ΠΑΝΕΠΙΣΤΗΜΙΟ
ΠΑΤΡΩΝ
UNIVERSITY OF PATRAS

Robotic Systems I

Lecture 1: Introduction, Rigid Body Motion, Jacobians,
Forward and Inverse Kinematics

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Template made by Panagiotis Papagiannopoulos





Laboratory of Automation & Robotics

■ Lectures:

- 10 + 1 Recitation Lecture
- ≥8 Lab Exercises

■ Examination:

- Lab code (**20% of total grade**)
- Intermediate exams (**30% of total grade**)
- For **50% of total grade** you select **one of the two**:
 - Team Project (max 2 per team) — only for the June exams
 - Final exam
- **IMPORTANT:** All exams are hybrid: multiple choice + code

■ Office Hours:

- **Tue-Wed (10:00-12:00)**
- 24/7 by email (costashatz@upatras.gr, subject: *ECE_RSI_AM*)

■ Material and Announcements



What is this course about?

- 3D Rigid Body Motions
- Dynamics and Control of Manipulators
- Mobile Robots, Simulators
- Orientation Representations
- Lie Algebra
- Splines
- Optimization
- Localization, SLAM
- Optimization-based Control of Complex Robots/Whole Body Controllers
- **We focus on implementation/robotics applications. You are required to write code!** Not a theory course!

- **3-hour lectures:**

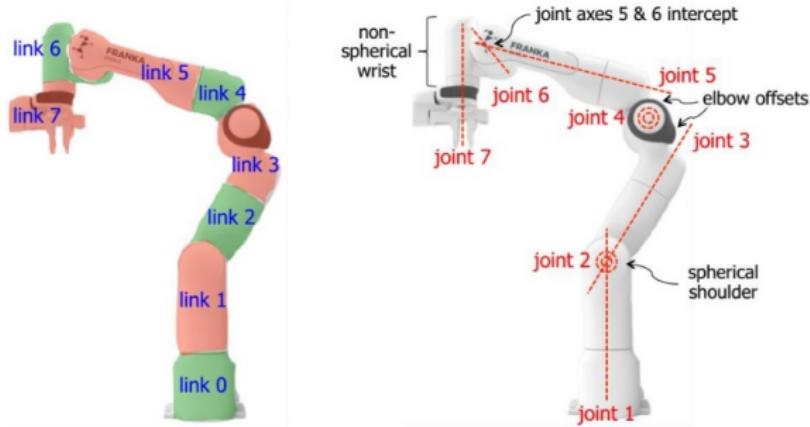
- A lot of theory! Hints for personal reading!
- Live code examples + analyses!
- Ask questions please!

- **2-hour lab exercises:**

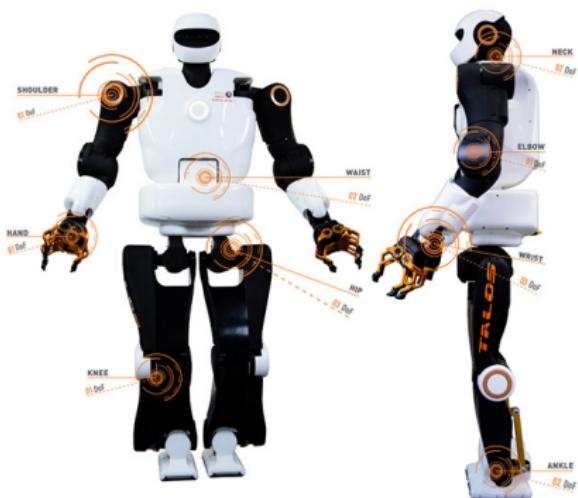
- **20% of total grade**
- Small code examples that you need to fill
- You need to deliver code
- Ask questions, experiment!

What is a robot?

A robot is a mechanical system that consists of bodies (**links**) which are connected with various types of **joints**. **Motors** or actuators exert **torque** or **force** to the bodies, and thus we get body movement. Usually one motor corresponds to one joint.



Robot Examples (1)

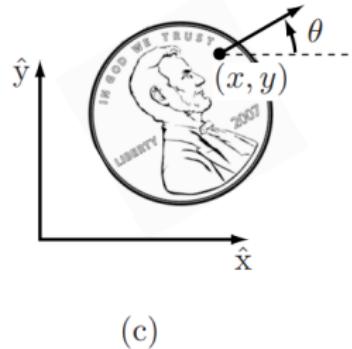
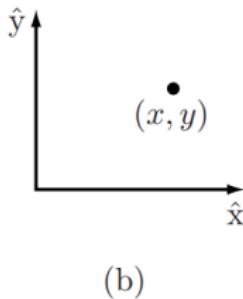
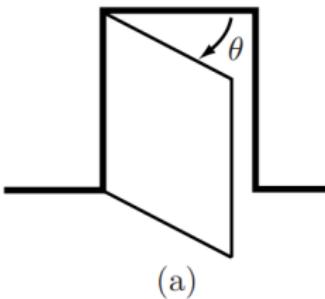


Robot Examples (2)



Robot Configuration

Configuration of a robot is a description that fully defines the positions (in 3D space) of all points of the robot.



Source: Modern Robotics: Mechanics, Planning, and Control, *Kevin M. Lynch and Frank C. Park*, 2017, Cambridge University Press.

Degrees of freedom (dofs) of a robot is the minimum number of parameters that we need to represent its configuration.

For example:

- The door has 1 dof
- A 2D point has 2 dofs
- A coin moving on a 2D plane, has 3 dofs
- ...

In this course, we will handle only rigid bodies and robots that consist of rigid bodies only.

A rigid body:

- Moving on a 2D plane, has 3 dofs: (x, y, θ)
- Moving in 3D space, has 6 dofs:
$$(x, y, z, \theta_x, \theta_y, \theta_z)$$
- This holds only when there are no constraints in the movement! If we have constraints, then we can find the dofs as follows:

$$\text{DoFs} = (\text{sum of all dofs of all bodies}) - (\text{number of independent constraints})$$

- A robot consists of multiple bodies that are connected via joints
- Every joint **imposes one or more constraints**
- We can also say that each joint **allows for one or more degrees of freedom**
- We assume that **each joint connects exactly two bodies**

Typical Joints (1)

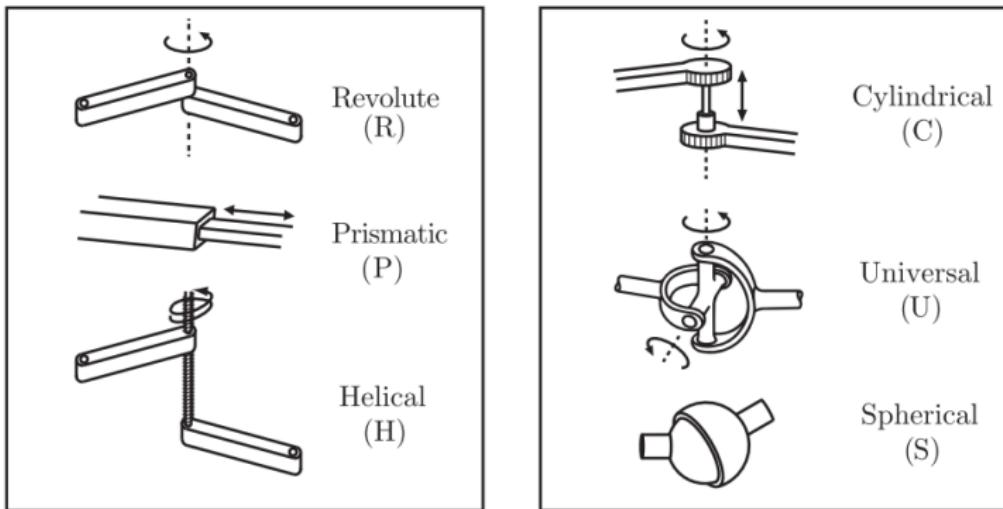


Figure: Typical joint types

Source: Modern Robotics: Mechanics, Planning, and Control, *Kevin M. Lynch and Frank C. Park*, 2017, Cambridge University Press.

■ Joints of 1 dof:

- **Revolute/Hinge**: allows rotational movement around an axis
- **Prismatic**: allows translational movement along an axis
- **Helical/Screw**: allows both rotational and translational movement around a helical axis (like a screw)

■ Joints of multiple dofs:

- **Cylindrical**: allows for independent rotational and translational movement around an axis (2 dofs)
- **Universal**: basically 2 revolute joints with perpendicular axes (2 dofs)
- **Spherical/Ball-and-Socket**: it has 3 dofs and behaves like our shoulder joint

Transformations

- A rigid body in 3D space needs at least six values to completely determine its pose¹
- But where is the body's pose? With respect to what?

¹We need at least 3 for bodies in 2D space.

- A rigid body in 3D space needs at least six values to completely determine its pose¹
- But where is the body's pose? With respect to what? We need a *reference frame*
- We always assume a static reference frame that does not change or move at all: we usually refer to it as “*world frame*”
- Each body has its own local static reference frame (It can have more than one!): we usually refer to it as “*body frame*”

¹We need at least 3 for bodies in 2D space.

What is orientation?

The transformation that transforms a vector/point, v_b , expressed in “body frame” to the same vector/point, but expressed in the “fixed/world frame” orientation, v_w .

$$v_w = R_{wb} v_b$$

where $R_{wb} \in \mathcal{SO}(3)$ is a **rotation matrix** that rotates the “fixed/world frame” such that it matches the “body frame”. We use this rotation (transformation) matrix to rotate a vector from “body frame” to the “world frame”.

Frames and Rotation Matrices

A frame is basically a set of 3 unit-norm vectors, that are orthogonal to each other:

$$\mathbf{w}_x \cdot \mathbf{w}_y = 0$$

$$\mathbf{w}_x \cdot \mathbf{w}_z = 0$$

$$\mathbf{w}_y \cdot \mathbf{w}_z = 0$$

where $\mathcal{W} = (\mathbf{w}_x, \mathbf{w}_y, \mathbf{w}_z)$ is the world frame. If we also define a body frame as \mathcal{B} , then we have:

$$\mathbf{R}_{wb} = \begin{bmatrix} (\mathbf{w}_x \cdot \mathbf{b}_x) & (\mathbf{w}_x \cdot \mathbf{b}_y) & (\mathbf{w}_x \cdot \mathbf{b}_z) \\ (\mathbf{w}_y \cdot \mathbf{b}_x) & (\mathbf{w}_y \cdot \mathbf{b}_y) & (\mathbf{w}_y \cdot \mathbf{b}_z) \\ (\mathbf{w}_z \cdot \mathbf{b}_x) & (\mathbf{w}_z \cdot \mathbf{b}_y) & (\mathbf{w}_z \cdot \mathbf{b}_z) \end{bmatrix}$$

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We refer to this version of derivation of the rotation matrix as the **Direction Cosine Method/Matrix (DCM)**.

Rotation Matrices

- If $\mathbf{R}_1, \mathbf{R}_2$ are rotation matrices, then $\mathbf{R}_1\mathbf{R}_2$ is also a rotation matrix
- $(\mathbf{R}_1\mathbf{R}_2)\mathbf{R}_3 = \mathbf{R}_1(\mathbf{R}_2\mathbf{R}_3)$
- $\mathbf{R}\mathbf{I} = \mathbf{I}\mathbf{R} = \mathbf{R}$ (\mathbf{I} is the identity matrix)
- $\mathbf{R}^{-1}\mathbf{R} = \mathbf{I}$
- $\mathbf{R}^{-1} = \mathbf{R}^T$, aka $\mathbf{R}_{wb}^T = \mathbf{R}_{bw}$
- $\det(\mathbf{R}) = 1$
- $\mathbf{R}_{az} = \mathbf{R}_{ab}\mathbf{R}_{bc}\mathbf{R}_{cd}\dots\mathbf{R}_{yz}$

Rotations around Principal Axes

Rotation around x-axis:

$$\mathbf{R}_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

Rotation around y-axis:

$$\mathbf{R}_y(\theta) = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix}$$

Rotation around z-axis:

$$\mathbf{R}_z(\theta) = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Full Pose Transformations

We have:

$$\blacksquare \quad \boldsymbol{p}_s = \begin{bmatrix} p_x^s \\ p_y^s \\ p_z^s \end{bmatrix} \in \mathbb{R}^3$$

$$\blacksquare \quad \boldsymbol{R}_{sb} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \in \mathbb{R}^{3 \times 3}$$

- ($\boldsymbol{p}_s, \boldsymbol{R}_{sb}$) represent the transformation from the *b frame* to the *s frame*
- We can get the coordinates of a point $\boldsymbol{a}_b = [a_x^b, a_y^b, a_z^b]^T$ from the *b frame* to the *s frame*, using the following:
$$\boldsymbol{a}_s = \boldsymbol{p}_s + \boldsymbol{R}_{sb}\boldsymbol{a}_b$$

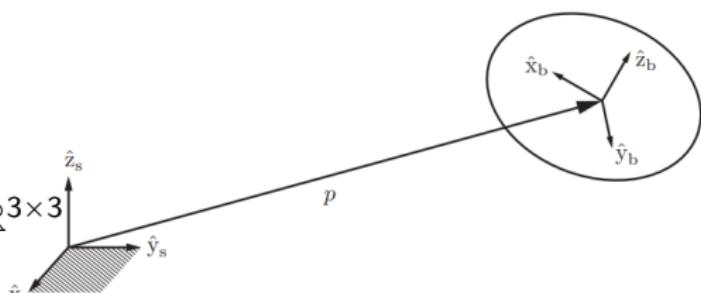


Figure Source: Modern Robotics: Mechanics, Planning, and Control, Kevin M. Lynch and Frank C. Park, 2017, Cambridge University Press.

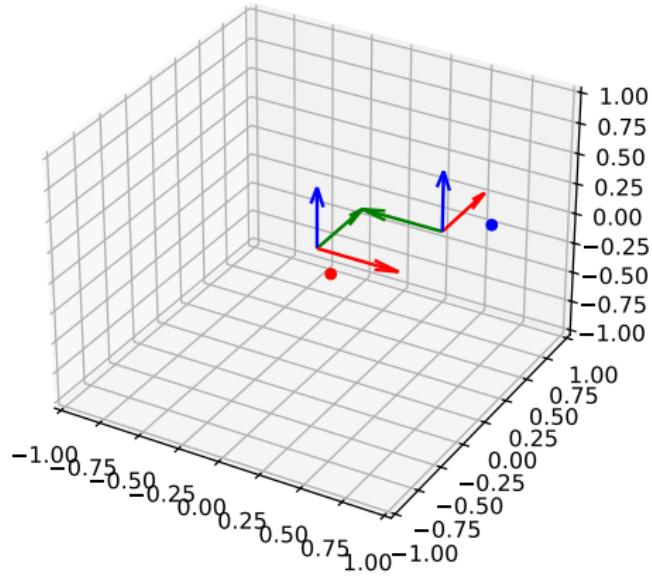
Homogeneous Transformations

- We assume that every point in 3D space can be defined as:
 $\mathbf{p} = [x, y, z, 1]$
- Whereas every vector as: $\mathbf{v} = [x, y, z, 0]$
- We define the Homogeneous Transformation Matrix
 $\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{t} \\ 0 & 1 \end{bmatrix}$, where \mathbf{R} is a rotation matrix and \mathbf{t} a translation vector
- \mathbf{T} transforms point \mathbf{p} as follows: $\mathbf{p}' = \mathbf{T}\mathbf{p} = \mathbf{R}\mathbf{p} + \mathbf{t}$
- $\mathbf{v}' = \mathbf{T}\mathbf{v} = \mathbf{R}\mathbf{v}$: vectors can only be rotated!

Homogeneous Transformation Matrices

- If $\mathbf{T}_1, \mathbf{T}_2$ are transformation matrices, then $\mathbf{T}_1 \mathbf{T}_2$ is also a transformation matrix
- $(\mathbf{T}_1 \mathbf{T}_2) \mathbf{T}_3 = \mathbf{T}_1 (\mathbf{T}_2 \mathbf{T}_3)$
- $\mathbf{T}\mathbf{I} = \mathbf{I}\mathbf{T} = \mathbf{T}$ (there exist the identity matrix)
- $\mathbf{T}^{-1}\mathbf{T} = \mathbf{I}$
- $\mathbf{T}^{-1} = \begin{bmatrix} \mathbf{R} & \mathbf{t} \\ 0 & 1 \end{bmatrix}^{-1} = \begin{bmatrix} \mathbf{R}^T & -\mathbf{R}^T \mathbf{t} \\ 0 & 1 \end{bmatrix}$

Transformations Code Example



Skew Symmetric Matrices

The **skew symmetric matrix** representation of a 3-D vector $\mathbf{v} = [v_1 \ v_2 \ v_3]^T$ is:

$$\mathbf{v}^\wedge = [\mathbf{v}] = \mathbf{v}_\times = \begin{bmatrix} 0 & -v_3 & v_2 \\ v_3 & 0 & -v_1 \\ -v_2 & v_1 & 0 \end{bmatrix} \in \mathbb{R}^{3 \times 3}$$

Many names in the literature:

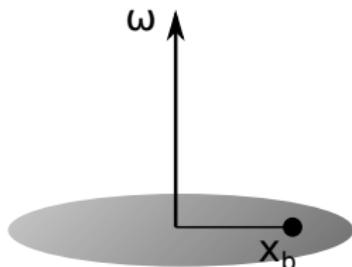
- hat map or matrix, \mathbf{v}^\wedge or $\hat{\mathbf{v}}$
- skew symmetric matrix, $[\mathbf{v}]$
- cross product matrix, \mathbf{v}_\times or $[\mathbf{v}]_\times$

We define $[\mathbf{v}]^\vee = [v_1 \ v_2 \ v_3]^T$ as the inverse operator.

Rotation Kinematics (aka velocities)

$$\mathbf{x}_w = \mathbf{R}_{wb}\mathbf{x}_b$$

\mathbf{x}_b is static. **How can we compute $\dot{\mathbf{x}}_w$?**

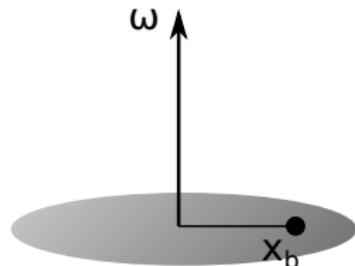


Rotation Kinematics (aka velocities)

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$$\begin{aligned}\dot{\mathbf{x}}_w &= \boldsymbol{\omega}_w \times \mathbf{x}_w \\ &= \mathbf{R}_{wb}(\boldsymbol{\omega}_b \times \mathbf{x}_b)\end{aligned}$$



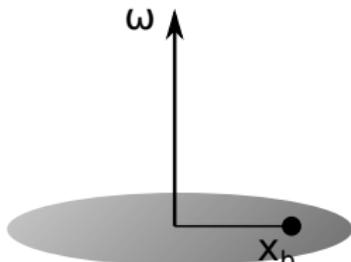
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How else?

$$\mathbf{x}_w = \mathbf{R}_{wb}\mathbf{x}_b \Rightarrow$$

$$\dot{\mathbf{x}}_w = \dot{\mathbf{R}}_{wb}\mathbf{x}_b + \mathbf{R}_{wb}\dot{\mathbf{x}}_b$$

$$\dot{\mathbf{x}}_w = \dot{\mathbf{R}}_{wb}\mathbf{x}_b, \text{ since } \dot{\mathbf{x}}_b = 0$$

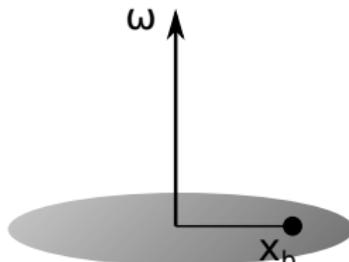
So, what we do have?

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$$\dot{\mathbf{x}}_w = \dot{\mathbf{R}}_{wb}\mathbf{x}_b, \text{ since } \dot{\mathbf{x}}_b = 0$$

So, what we do have?

$$\dot{\mathbf{R}}_{wb}\mathbf{x}_b = \mathbf{R}_{wb}(\boldsymbol{\omega}_b \times \mathbf{x}_b) = \mathbf{R}_{wb}\boldsymbol{\omega}_b^\wedge \mathbf{x}_b \Rightarrow$$

$$\dot{\mathbf{R}}_{wb} = \mathbf{R}_{wb}\boldsymbol{\omega}_b^\wedge$$

Rotation Kinematics (2)

Let's appreciate the previous result:

$$\dot{\boldsymbol{R}}_{wb} = \boldsymbol{R}_{wb} \boldsymbol{\omega}_b^{\wedge}$$

What does this mean? What can I do with it?

Let's appreciate the previous result:

$$\dot{\boldsymbol{R}}_{wb} = \boldsymbol{R}_{wb} \boldsymbol{\omega}_b^{\wedge}$$

What does this mean? What can I do with it?

It means that if I have a measurement of the angular velocity $\boldsymbol{\omega}_b$, I can use it to integrate the full rotation matrix!

In other words:

- I can do forward simulation
- I can use it in combination with gyros/IMUs for state estimation/odometry

With some math manipulation, we can also have (“world space angular velocity”):

$$\dot{\boldsymbol{R}}_{wb} = \boldsymbol{\omega}_w^{\wedge} \boldsymbol{R}_{wb}$$

Let's summarize:

$$\omega_w^{\wedge} = \dot{R}_{wb} R_{wb}^T$$

$$\omega_b^{\wedge} = R_{wb}^T \dot{R}_{wb}$$

- $\omega_w \in \mathbb{R}^3$ is the angular velocity of the body with respect to (wrt) the world frame
- $\omega_b \in \mathbb{R}^3$ is the angular velocity of the body wrt the body frame
- ω_b **IS NOT** the angular velocity relative to the moving body frame, but relative to the fixed world frame
- ω_w **DOES NOT** depend on the choice of the body frame
- ω_b **DOES NOT** depend on the choice of the world frame
- $\dot{R}_{wb} R_{wb}^T$ is independent from the body frame
- $R_{wb}^T \dot{R}_{wb}$ is independent from the world frame
- Let's assume an angular velocity expressed in frame $\{d\}$, ω_d , we can express it in the frame $\{c\}$: $\omega_c = R_{cd}\omega_d$

Spatial Velocity (1)

Let's try to do the same for homogeneous transformation matrices:

Spatial Velocity (1)

Let's try to do the same for homogeneous transformation matrices:

$$\begin{aligned}\mathbf{T}_{wb}^{-1} \dot{\mathbf{T}}_{wb} &= \begin{bmatrix} \mathbf{R}_{wb}^T & -\mathbf{R}_{wb}^T \dot{\mathbf{p}}_w \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\mathbf{R}}_{wb} & \dot{\mathbf{p}}_w \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} \mathbf{R}_{wb}^T \dot{\mathbf{R}}_{wb} & \mathbf{R}_{wb}^T \dot{\mathbf{p}}_w \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} \boldsymbol{\omega}_b^\wedge & \mathbf{v}_b \\ 0 & 0 \end{bmatrix}\end{aligned}$$

$\dot{\mathbf{p}}_w$ is the linear velocity of the body expressed in the world frame, and thus $\mathbf{R}_{wb}^T \dot{\mathbf{p}}_w$ is the linear velocity of the body expressed in body frame: \mathbf{v}_b .

Spatial Velocity (2)

Let's put ω_b and \mathbf{v}_b in one vector and call it **Body Spatial Velocity** (or **body twist**): $\mathcal{V}_b = \begin{bmatrix} \omega_b \\ \mathbf{v}_b \end{bmatrix} \in \mathbb{R}^6$. We can now write:

$$\mathbf{T}_{wb}^{-1} \dot{\mathbf{T}}_{wb} = [\mathcal{V}_b] = \begin{bmatrix} \hat{\omega}_b & \mathbf{v}_b \\ 0 & 0 \end{bmatrix}$$

We also have the **World Spatial Velocity** (or **spatial twist**):

$$\mathcal{V}_w = \begin{bmatrix} \omega_w \\ \mathbf{v}_w \end{bmatrix} \in \mathbb{R}^6. \text{ We write as well:}$$

$$\dot{\mathbf{T}}_{wb} \mathbf{T}_{wb}^{-1} = [\mathcal{V}_w] = \begin{bmatrix} \dot{\mathbf{R}}_{wb} \mathbf{R}_{wb}^T & \dot{\mathbf{p}}_w - \dot{\mathbf{R}}_{wb} \mathbf{R}_{wb}^T \mathbf{p}_w \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} \hat{\omega}_w & \mathbf{v}_w \\ 0 & 0 \end{bmatrix}$$

Spatial Velocity (3)

A few remarks:

- $\boldsymbol{v}_w = \dot{\boldsymbol{p}}_w - \dot{\boldsymbol{R}}_{wb} \boldsymbol{R}_{wb}^T \boldsymbol{p}_w$ — **IS NOT** the linear velocity of the body expressed in the world frame

Spatial Velocity (3)

A few remarks:

- $\boldsymbol{v}_w = \dot{\boldsymbol{p}}_w - \dot{\boldsymbol{R}}_{wb} \boldsymbol{R}_{wb}^T \boldsymbol{p}_w$ — **IS NOT** the linear velocity of the body expressed in the world frame (this would just be $\dot{\boldsymbol{p}}_w$)
- $\boldsymbol{v}_w = \dot{\boldsymbol{p}}_w + \boldsymbol{\omega}_w \times (-\boldsymbol{p}_w)$ — now \boldsymbol{v}_w is the velocity of the center of the world frame expressed in the world frame if the body was big enough to include this point
- $\boldsymbol{\omega}_b$ is the angular velocity of the body expressed in the body frame and $\boldsymbol{\omega}_w$ is the angular velocity of the body expressed in the world frame
- \boldsymbol{v}_b is the linear velocity of the center of the body frame
- \boldsymbol{v}_w is the linear velocity of the center of the world frame

Spatial Velocity (4)

We can go from \mathcal{V}_b to \mathcal{V}_w :

$$[\mathcal{V}_b] = \mathbf{T}_{wb}^{-1} \dot{\mathbf{T}}_{wb} = \mathbf{T}_{wb}^{-1} [\mathcal{V}_w] \mathbf{T}_{wb}$$

And backwards:

$$[\mathcal{V}_w] = \dot{\mathbf{T}}_{wb} \mathbf{T}_{wb}^{-1} = \mathbf{T}_{wb} [\mathcal{V}_b] \mathbf{T}_{wb}^{-1}$$

Let's do some calculations:

$$[\mathcal{V}_w] = \begin{bmatrix} \mathbf{R}_{wb} \omega_b^\wedge \mathbf{R}_{wb}^T & -\mathbf{R}_{wb} \omega_b^\wedge \mathbf{R}_{wb}^T \mathbf{p}_w + \mathbf{R}_{wb} \mathbf{v}_b \\ 0 & 0 \end{bmatrix}$$

$$\begin{bmatrix} \omega_w \\ \mathbf{v}_w \end{bmatrix} = \begin{bmatrix} \mathbf{R}_{wb} & 0 \\ \mathbf{p}_{wb}^\wedge \mathbf{R}_{wb} & \mathbf{R}_{wb} \end{bmatrix} \begin{bmatrix} \omega_b \\ \mathbf{v}_b \end{bmatrix}$$

Adjoint Representation

Let's assume a transformation $\mathbf{T} = (\mathbf{R}, \mathbf{p})$. We say that its adjoint form, $[Ad_{\mathbf{T}}] \in \mathbb{R}^{6 \times 6}$, is:

$$[Ad_{\mathbf{T}}] = \begin{bmatrix} \mathbf{R} & 0 \\ \mathbf{p}^\wedge \mathbf{R} & \mathbf{R} \end{bmatrix}$$

In other words:

- $\mathcal{V}_w = [Ad_{\mathbf{T}_{wb}}]\mathcal{V}_b$
- $\mathcal{V}_b = [Ad_{\mathbf{T}_{bw}}]\mathcal{V}_w$

A few properties:

- $[Ad_{\mathbf{T}}]^{-1} = [Ad_{\mathbf{T}^{-1}}]$
- $[Ad_{\mathbf{T}_1}][Ad_{\mathbf{T}_2}]\mathcal{V} = [Ad_{\mathbf{T}_1 \mathbf{T}_2}]\mathcal{V}$

Velocities Code Example

```
omega_w = T1[:3, :3] @ omega_b # rotate local omega to world frame
Vw = np.vstack([omega_w, np.zeros((3, 1))])
T1d = spatial_velocity_to_deriv_homogeneous(Vw, T1)
T2d = spatial_velocity_local_to_deriv_homogeneous(Vb, T2)

T1 = T1 + T1d * dt # Euler integration!
T2 = T2 + T2d * dt # Euler integration!

# These two should be very similar
print(T1)
print("====")
print(T2)
print("====")
print(np.linalg.norm(T1-T2))

[[ 1.        0.        0.        0.      ]
 [ 0.        -0.49001 -0.9005   0.      ]
 [ 0.        0.9005  -0.49001  0.      ]
 [ 0.        0.        0.        1.      ]]
=====
[[ 1.        0.        0.        0.      ]
 [ 0.        -0.49001 -0.9005   0.      ]
 [ 0.        0.9005  -0.49001  0.      ]
 [ 0.        0.        0.        1.      ]]
=====
0.0
```

Spatial Forces

Analogously to the velocities we can study the forces, \mathbf{f} , and moments, \mathbf{m} , that are exerted on a rigid body:

$$\mathcal{F} = \begin{bmatrix} \mathbf{m} \\ \mathbf{f} \end{bmatrix} \in \mathbb{R}^6$$

We call \mathcal{F} **spatial force** (or **wrench**). If we have a *spatial force* \mathcal{F}_b expressed in a frame $\{b\}$, we can express it in frame $\{w\}$:

$$\mathcal{F}_w = [Ad_{T_{bw}}]^T \mathcal{F}_b$$

and backwards:

$$\mathcal{F}_b = [Ad_{T_{wb}}]^T \mathcal{F}_w$$

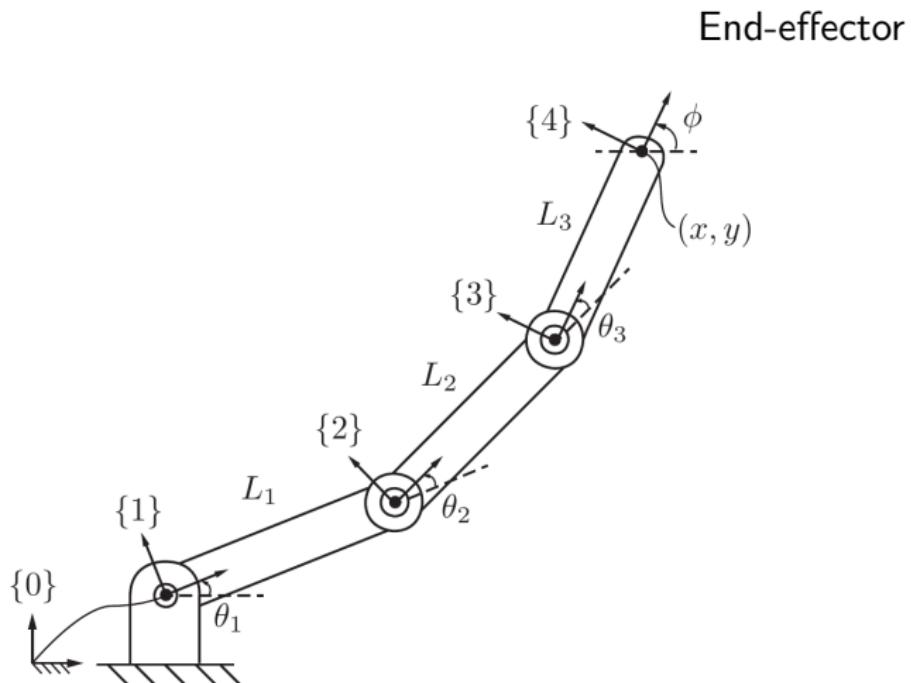
End-effectors



End-effectors (2)

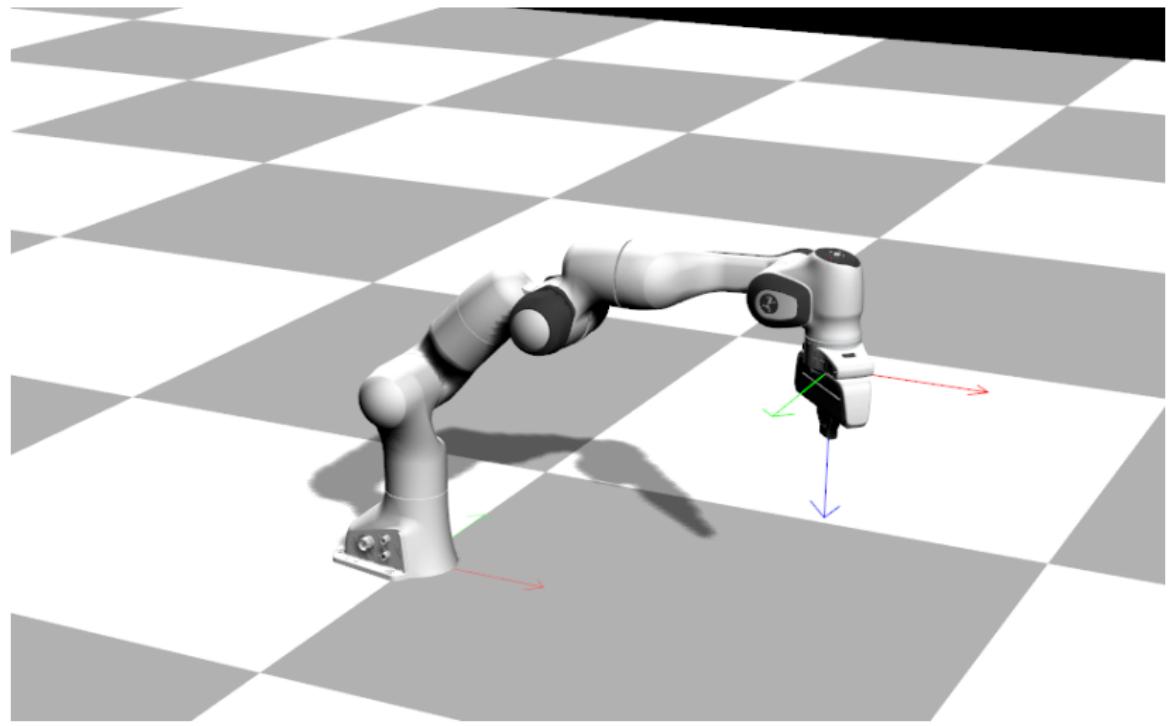


Forward Kinematics (1)



Source: Modern Robotics: Mechanics, Planning, and Control, Kevin M. Lynch and Frank C. Park, 2017,
Cambridge University Press.

Forward Kinematics (2)



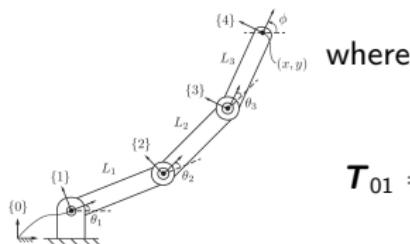
Forward Kinematics (3)

We can use our transformation matrices:

End-effector

$$(x, y, \phi) \equiv \mathbf{T}_{04} = \mathbf{T}_{01} \mathbf{T}_{12} \mathbf{T}_{23} \mathbf{T}_{34}$$

where



Source: Modern Robotics:
Mechanics, Planning, and
Control, Kevin M. Lynch and
Frank C. Park, 2017, Cambridge
University Press.

$$\mathbf{T}_{01} = \begin{bmatrix} \cos\theta_1 & -\sin\theta_1 & 0 & 0 \\ \sin\theta_1 & \cos\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{T}_{12} = \begin{bmatrix} \cos\theta_2 & -\sin\theta_2 & 0 & L_1 \\ \sin\theta_2 & \cos\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{T}_{23} = \begin{bmatrix} \cos\theta_3 & -\sin\theta_3 & 0 & L_2 \\ \sin\theta_3 & \cos\theta_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{T}_{34} = \begin{bmatrix} 1 & 0 & 0 & L_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Jacobians (1)

Let's assume that the *end-effector* of our robot is moving with velocity $\dot{\mathbf{x}}^1$. Let's also write the forward kinematics problem as a function of time:

$$\mathbf{x}(t) = f_{fk}(\mathbf{q}(t))$$

where f_{fk} is the function that gives us the forward kinematics, $\mathbf{x} \in \mathbb{R}^m$ the pose of the end-effector, and $\mathbf{q} \in \mathbb{R}^n$ the joint values of the robot. If we take the derivative over time:

$$\begin{aligned}\dot{\mathbf{x}} &= \frac{\partial f_{fk}(\mathbf{q})}{\partial \mathbf{q}} \frac{\partial \mathbf{q}(t)}{\partial t} \\ &= \mathbf{J}(\mathbf{q})\dot{\mathbf{q}}\end{aligned}$$

where $\mathbf{J}(\mathbf{q}) \in \mathbb{R}^{m \times n}$ is the Jacobian matrix.

¹This is an abstract velocity here.

Jacobians (2)

- Twist \mathcal{V}_w of the end-effector expressed in world frame
- We have: $\mathcal{V}_w = \mathbf{J}_w(\mathbf{q})\dot{\mathbf{q}}$, where $\mathbf{J}_w(\mathbf{q}) \in \mathbb{R}^{6 \times n}$
- We have: $\mathcal{V}_b = \mathbf{J}_b(\mathbf{q})\dot{\mathbf{q}}$, where $\mathbf{J}_b(\mathbf{q}) \in \mathbb{R}^{6 \times n}$ is the Jacobian expressed in body frame
- We also have: $\mathbf{J}_b = [Ad_{T_{bw}}]\mathbf{J}_w$ and $\mathbf{J}_w = [Ad_{T_{wb}}]\mathbf{J}_b$

From the principle of energy conservation, we can also derive an equation for the *wrenches*:

$$\begin{aligned}\boldsymbol{\tau} &= \mathbf{J}_w(\mathbf{q})^T \mathcal{F}_w \\ \boldsymbol{\tau} &= \mathbf{J}_b(\mathbf{q})^T \mathcal{F}_b\end{aligned}$$

where $\boldsymbol{\tau} \in \mathbb{R}^n$ are the joint torques/forces.

Inverse Kinematics

- This is the “opposite” problem of forward kinematics
- We can find closed-form solutions for many systems
- We can develop iterative algorithms based on the Jacobians
- We can view the problem as an optimization problem
 - We can still use the Jacobians
 - Or we can go black-box!
 - We can take advantage of numerical optimization methods
(more on this later in the course!)

Bibliography

Chapters 1-4, 6 from **Modern Robotics: Mechanics, Planning, and Control**, *Kevin M. Lynch and Frank C. Park*, 2017, Cambridge University Press. [ebook](#)

Thank you

- Any Questions?

- Office Hours:

- Tue-Wed (10:00-12:00)

- 24/7 by email (costashatz@upatras.gr, subject: *ECE_RSI_AM*)

- Material and Announcements



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