

# Direct Numerical Simulations of Flow Over Smooth and Rough Wavy Walls at $Re_\lambda = 4,780$

Vedant Puri<sup>123</sup>, Ramesh Balakrishnan<sup>1</sup>,  
Aleksandr Obabko<sup>1</sup>, Paul Fischer<sup>12</sup>

<sup>1</sup>Argonne National Laboratory

<sup>2</sup>University of Illinois Urbana-Champaign

<sup>3</sup>Julia Computing

November 23, 2021



# Introduction

## Problem:

- To model the dynamics of the atmospheric boundary layer over complex terrains with application to windfarm simulations
- LES calculations often do not resolve near-surface regions, thereby requiring additional subgrid modelling

## Objectives:

- Understand physics of turbulent flows over periodic, wavy boundaries
- Study the effects of small boundary irregularities on on LES calculation

## Method:

- Perform DNS of flow over a wavy wall (Smooth Wavy Wall, SWW), and a wavy wall with added roughness (Rough Wavy Wall, RWW) that an LES would not capture
- Compare Reynolds stress budgets statistics of SWW, RWW

# NEK5000 Spectral Element Code

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \frac{1}{Re} \nabla^2 \mathbf{u} + \rho \mathbf{f}$$

$$\nabla \cdot \mathbf{u} = 0, \quad Re = \frac{\rho U L}{\mu}$$

## NEK5000

- Flexible like finite elements, accurate like spectral methods
- 7<sup>th</sup> order GLL polynomial within each element
- 3<sup>rd</sup> order BDF/Ext formula for time-integration (explicit handling of nonlinear term)
- Excellent scalability (32768 cores on Argonne resources)
- Linear Stokes problem (pressure-viscous decoupling) for solving Navier-Stokes

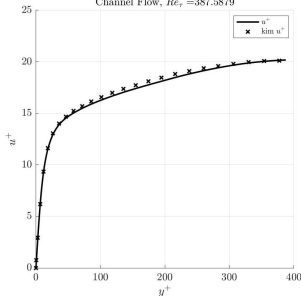
# Validation Turbulence Budgets Subroutines in NEK5000

Validation on Reynolds Stress budgets subroutines in NEK5000 against channel flow dataset of Kim et al. 1998 at  $Re_\tau = 394$

$$\partial_t k + \underbrace{\langle u_i \rangle k_{,i}}_{\text{convection}} = - \underbrace{\langle u'_j u'_i \rangle \langle u_{j,i} \rangle}_{\text{production}} - \underbrace{\langle u'_i k \rangle_{,i}}_{\text{turbdiff}} - \underbrace{\langle p'_{,j} u'_j \rangle}_{\text{presdiff}} + \underbrace{\frac{k_{,ii}}{Re}}_{\text{visc.diff}} - \underbrace{\frac{\langle u'_{j,i} u'_{j,i} \rangle}{Re}}_{\text{dissipation}}$$

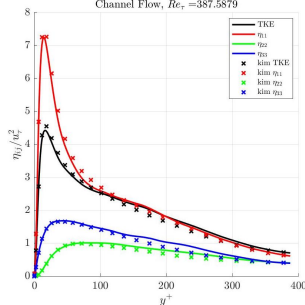
$$\langle u \rangle$$

Channel Flow,  $Re_\tau = 387.5879$



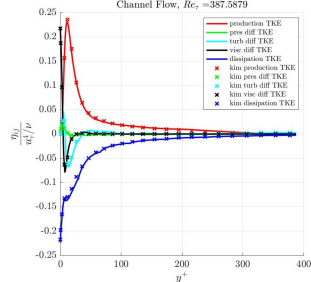
$$\eta_{ij} = \langle u'_i u'_j \rangle$$

Channel Flow,  $Re_\tau = 387.5879$

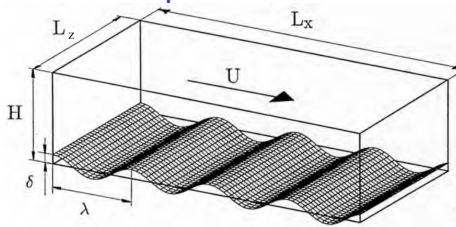


$$\dot{\eta}_{ij}$$

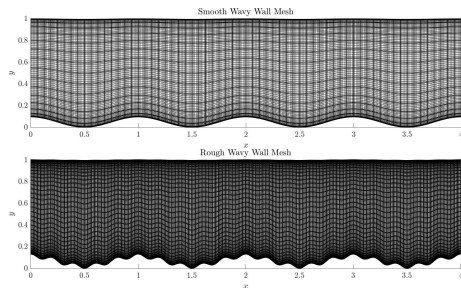
Channel Flow,  $Re_\tau = 387.5879$



# Case Setup



(SWW schematic, Maass and Schumann, 1994)

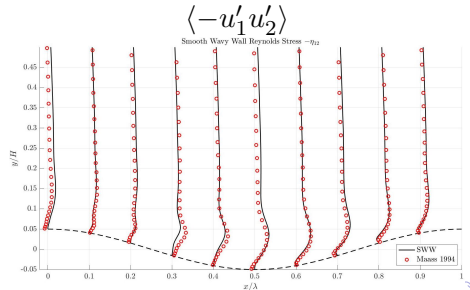
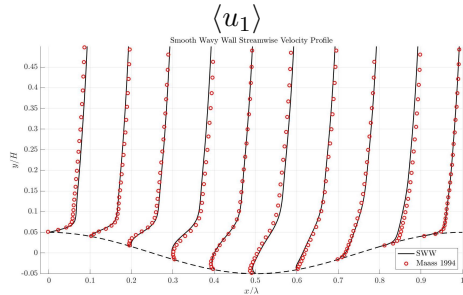
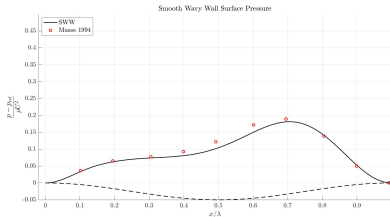


- $Re_\lambda = 4780$ ; wave amplitude  $\delta/\lambda = 0.05$
- Periodic BC in streamwise and spanwise directions
- Flow averaged over 60 convective time units ( $\bar{U}/4\lambda$ )

Case	Element Mesh	Order	$L_x \times H \times L_z$	$\lambda$	$\delta$	$\lambda'$	$\delta'$
SWW	$64 \times 16 \times 32$	7	$4 \times 1 \times 2$	1	0.05		
RWW	$128 \times 24 \times 32$	7	$4 \times 1 \times 2$	1	0.05	0.2	0.02

# Validation of Smooth Wavy Wall DNS

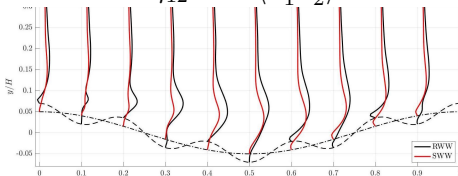
- Mesh refinement near wall
  - $\approx 2$  points within  $y^+ \leq 1$ ,  
2 elements within  $y^+ \leq 10$
  - $\Delta x^+ = \Delta z^+ \approx 5$
- Flow separation at crest of wave, reattachment at  $x/\lambda = 0.69$
- Residual of TKE budgets is 2 orders of magnitude than TKE



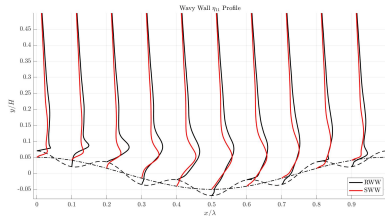
# Mean Flow

- Flow separates at crest of wave ( $x/\lambda = 0$ ) and reattaches at  $x/\lambda = 0.69$
- Outer region ( $y/H > 0.3$ ) where flow is not effected by wavy wall; inner region is  $y/H < 0.1$ ; and buffer region in between
- Flow is largely undisturbed in the outer region - Townsend's hypothesis holds!

$$-\eta_{12} = -\langle u'_1 u'_2 \rangle$$

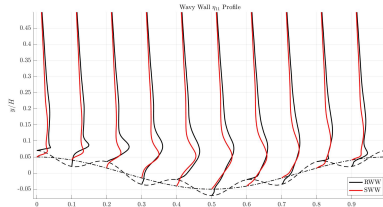
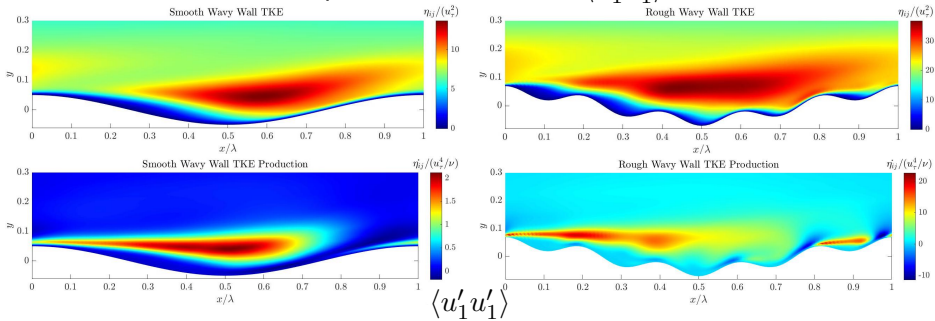


$$\eta_{11} = \langle u'_1 u'_1 \rangle$$



# Turbulent Kinetic Energy Budgets

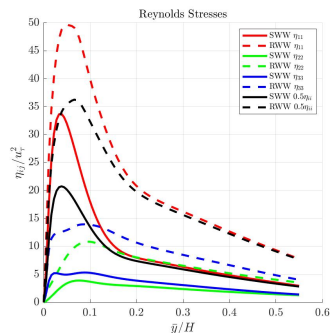
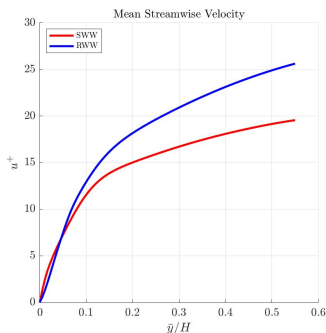
- Roughness disrupts inner flow and causes larger TKE and budgets
- Correlation between production term and  $\langle u'_1 u'_1 \rangle$





# Homogenized Statistics

- Spatially average statistics over lateral directions (including sinusoidal waves) to obtain a single profile
- $Re_\tau = 142, 104$  for SWW, RWW respectively



# Conclusion

- Extensive computations on flow over smooth and rough wavy walls have been done
- Results of Maass and Schumann have been reproduced with a high-order code
- Reynolds Stress budgets are computed for both Smooth Wavy Wall, and Rough Wavy Wall cases
- The effects of roughness have been observed to remain in the inner flow
- Work is underway to model the effects of roughness in subgrid models for Large Eddy Simulations of high Reynolds number wall-bounded flows

# Acknowledgements

- This research used resources of the Argonne Leadership Computing Facility, which is a DOE Office of Science User Facility supported under Contract DE-AC02-06CH11357.
- We gratefully acknowledge the computing resources provided on Bebop, a high-performance computing cluster operated by the Laboratory Computing Resource Center at Argonne National Laboratory.