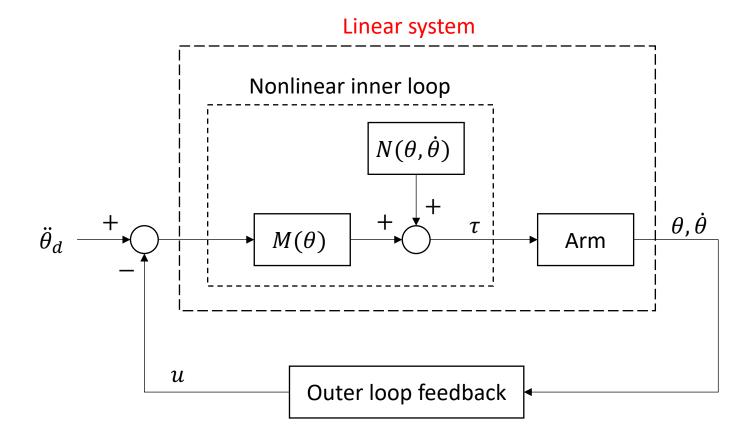
ME729 Advanced Robotics - Computed-Torque Control

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☐ Introduction

- A special application of feedback linearization of the nonlinear system.
- Feedforward loop: for eliminating nonlinear terms of the system.
- Feedback loop: for tracking a reference input.



- ☐ Derivation of inner feedforward loop
 - The robot dynamics:

$$M(\theta)\ddot{\theta} + V(\theta,\dot{\theta}) + G(\theta) = \tau$$

• For convenience, $V(\theta, \dot{\theta}) + G(\theta) = N(\theta, \dot{\theta})$:

$$M(\theta)\ddot{\theta} + N(\theta,\dot{\theta}) = \tau$$

Define tracking error:

$$e(t) = \theta_d(t) - \theta(t)$$

where, $\theta_d(t)$ is a desired trajectory.

• Differentiate the error twice:

$$\dot{e} = \dot{\theta}_d - \dot{\theta}$$
, and $\ddot{e} = \ddot{\theta}_d - \ddot{\theta}$

• To eliminate nonlinear term and track a desired trajectory, define the computed-torque control law:

$$\tau = M(\ddot{\theta}_d - u) + N$$

, where u is the outer loop feedback control input.

Substituting into the robot dynamics:

$$M\ddot{\theta} + N = M(\ddot{\theta}_d - u) + N$$

 $M(\ddot{\theta}_d - \ddot{\theta}) = Mu$
 $\therefore \ddot{e} = u$

• Therefore, if we select a control u that stabilizes $\ddot{e} = u$, then e goes to zero.

- ☐ PD controller for the outer loop
 - One way to select the outer loop feedback control input u is the PD feedback,

$$u = -k_d \dot{e} - k_p e$$

Then the control law becomes

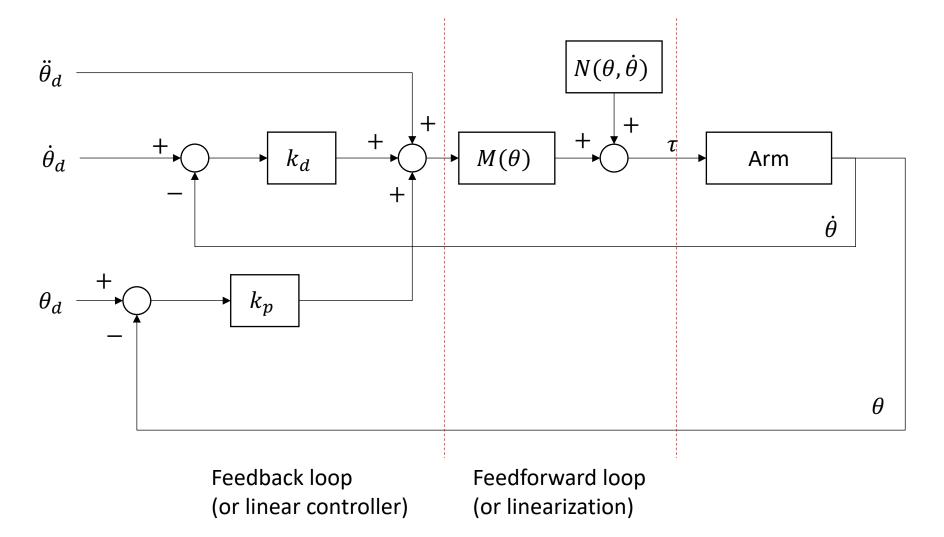
$$\tau = M(\ddot{\theta}_d + k_d \dot{e} + k_p e) + N$$

The closed-loop error dynamics are

$$\ddot{e} + k_d \dot{e} + k_p e = 0$$

• The error system is asymptotically stable as long as the k_d and k_p are all positive.

- ☐ PD controller for the outer loop
 - Block diagram for PD computed-torque controller.



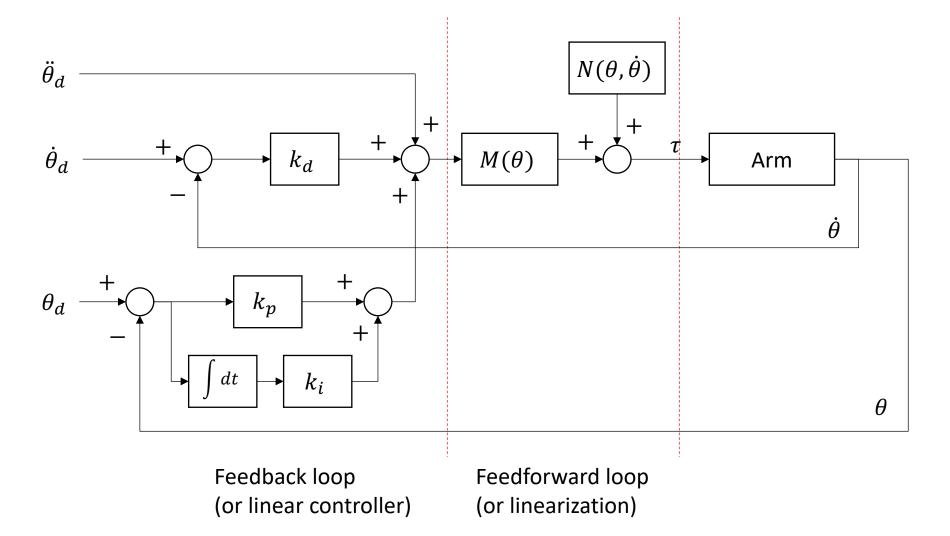
- ☐ PID controller for the outer loop
 - PD computed-torque control is very effective if all the arm parameters are known and there is no disturbance.
 - → it gives a nonzero steady-state error.
 - Consequently, we add an integral controller in the feedback loop.

$$u = -k_d \dot{e} - k_p e - k_i \int e^{-k_p t} e^{-k_p t} dt$$

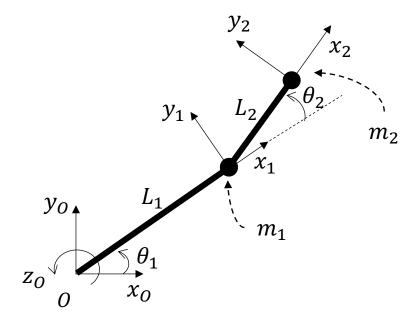
Then the control law becomes

$$\tau = M\left(\ddot{\theta}_d + k_d\dot{e} + k_pe - k_i\int e\right) + N$$

- ☐ PID controller for the outer loop
 - Block diagram for PID computed-torque controller.



- ☐ For example
 - The two-link planar manipulator.
 - Take the link masses as 1 kg and their lengths as 1 m.



The manipulator's equations of motion

$$\tau = M(\theta)\ddot{\theta} + V(\theta, \dot{\theta})$$

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} 3 + 2c_2 & 1 + c_2 \\ 1 + c_2 & 1 \end{bmatrix} \begin{bmatrix} \ddot{\theta_1} \\ \ddot{\theta_2} \end{bmatrix} + \begin{bmatrix} -\left(2\dot{\theta_1}\dot{\theta_2} + \dot{\theta_2^2}\right)s_2 \\ \dot{\theta_1^2}s_2 \end{bmatrix}$$

☐ For example

Rewrite the manipulator's equations of motion

$$\ddot{\theta} = M(\theta)^{-1} \{ \tau - V(\theta, \dot{\theta}) \}$$

The PD computed-torque control law is given as

$$\tau = M(\theta)(\ddot{\theta}_d + k_d \dot{e} + k_p e) + V(\theta, \dot{\theta})$$

$$e = \theta_d - \theta$$

• Let the desired trajectory $heta_d$

$$\theta_{1d} = 0.1 \sin \pi t$$
$$\theta_{2d} = 0.1 \cos \pi t$$

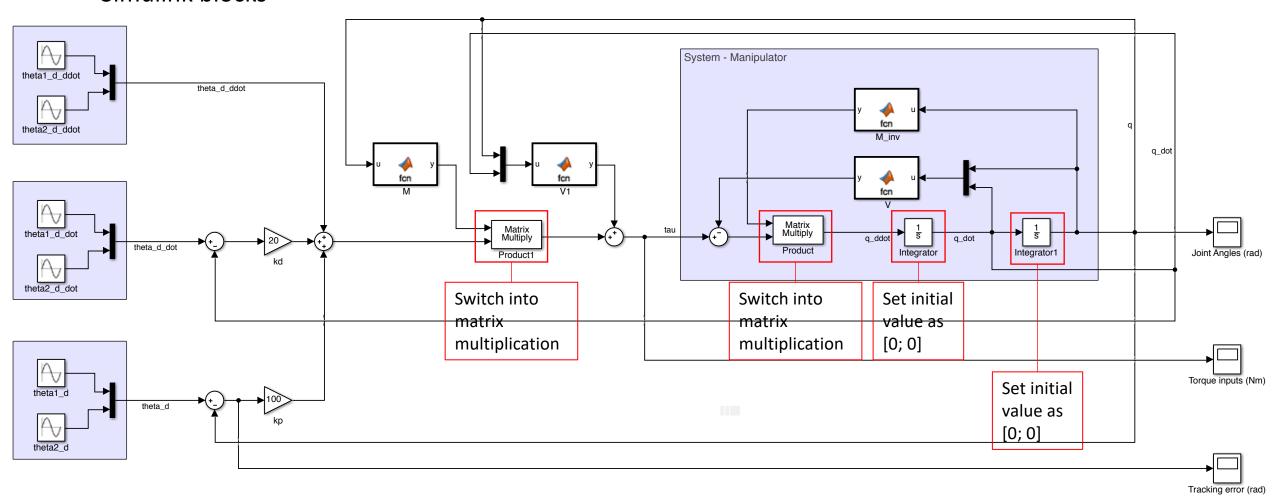
Differentiate the desired trajectory

$$\begin{split} \dot{\theta}_{1d} &= 0.1\pi\cos\pi t\\ \dot{\theta}_{2d} &= -0.1\pi\sin\pi t\\ \ddot{\theta}_{1d} &= -0.1\pi^2\sin\pi t\\ \ddot{\theta}_{2d} &= -0.1\pi^2\cos\pi t \end{split}$$

Set the gains as

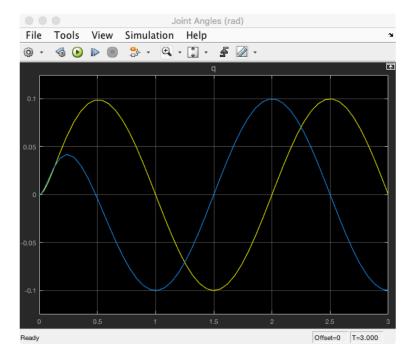
$$k_p = 100, k_v = 20$$

- ☐ For example
 - Simulink blocks

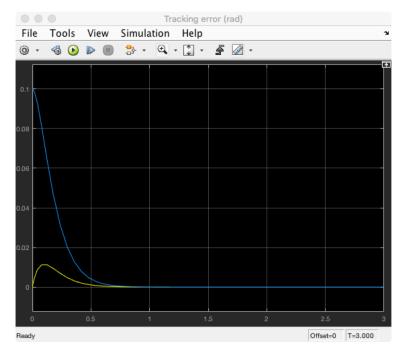


☐ For example

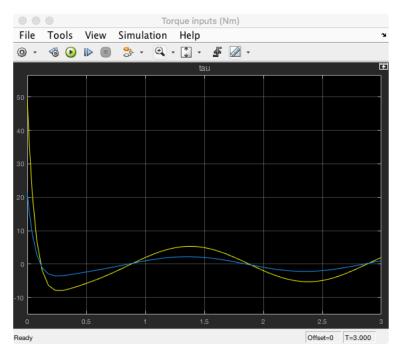
- Simulation results
- Yellow line is regarding to θ_1 .
- Blue line is regarding to θ_2 .



[Joint angles (rad)]



[Tracking error (rad)]



[Computed torque input (Nm)]