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Example 8.1

Leakage Flow Past a Piston:-

Given:-

Gage Pressure = 20 MPa at 55°C

fluid is SAE 10W 0.6

Diameter = 25 mm

low Pressure = 1.0 MPa

mean radial clearance = 0.005 mm

To Find:-

Leakage flow rate:?

Solution:-

$$\text{Governing eq} = \frac{Q}{J} = \frac{a^3 \Delta P}{12 \mu L}$$

Assumption:-

- (1) Laminar flow
- (2) Steady flow
- (3) Incompressible flow
- (4) Fully developed flow

So Hole width is πD

eq. become

For SAE oil at 55° $\mu = 0.08 \text{ kg/m.s}$

$$Q = \frac{\pi}{12} \times 25 \text{ mm} \times (0.0005)^3 \text{ mm}^3 \times (20-1) \times 10^6 \frac{\text{N}}{\text{m}^2} \\ \times \frac{\text{m.s}}{0.018 \text{ kg}} \times \frac{1}{15 \text{ mm}} \times \frac{\text{kg.m}}{\text{N.s}^2}$$

$$Q = 57.6 \text{ mm}^3/\text{s}$$

Example 8.2

Torque and Power in a Journal Bearing:-

Given:-

SAE 30 oil at 210°F

diameter is = 3 in

diametral clearance is 0.0025 in.

Shaft rotates at 3600 rpm.

shaft length is 1.25 in.

Find:-

(a) Torque T .

(b) Power dissipated.

Solution:-

$$\text{Governing eq} = T_{\text{vis}} = \mu \frac{U}{a} + a \left(\frac{\partial p}{\partial x} \right) \left[\frac{y}{a} - \frac{1}{2} \right]$$

due to flow is symmetric

Assumption:

- ① Laminar flow
- ② steady flow
- ③ Incompressible flow
- ④ fully developed flow
- ⑤ infinite width ($b/a = 1.25/0.00125 = 1000$)
- ⑥ $\partial p/\partial x = 0$ (flow is symmetric).

So

$$\tau_{yx} = \mu \frac{u}{a} = \mu \frac{\omega R}{a} = \frac{\mu \omega D}{2a}$$

For SAE 30 at 210°F $\mu = 9.6 \times 10^{-3} \text{ N}\cdot\text{s}/\text{m}^2$

$$\tau_{yx} = 2.01 \times 10^{-4} \frac{\text{lb}\cdot\text{s}}{\text{ft}^2} \times 3600 \frac{\text{rev}}{\text{min}} \times \frac{2\pi \text{ rad}}{\text{rev}} \times \frac{\text{min}}{60\text{s}} \times 3 \text{ in} \times \frac{1}{2} \times \frac{1}{0.00125 \text{ in}}$$

$$\tau_{yx} = 90.9 \text{ lb}/\text{ft}^2$$

$$T = FR$$

$$= \tau_{yx} \pi D L R = \frac{\pi}{2} \tau_{yx} D^2 L$$

$$= \frac{\pi}{2} \times 90.9 \frac{\text{lb}}{\text{ft}^2} \times (3)^2 \text{ in}^2 \times \frac{\text{ft}}{144 \text{ in}^2} \times 125 \text{ in}$$

$$T = 11.2 \text{ in}\cdot\text{lb}\cdot\text{ft}$$

Power dissipated

$$W = F U = F R \omega = T \omega$$

$$= 11.2 \text{ in}\cdot\text{lb}\cdot\text{ft} \times 3600 \frac{\text{rev}}{\text{min}} \times \frac{\text{min}}{60\text{s}} \times \frac{2\pi \text{ rad}}{\text{rev}}$$
$$\times \frac{\text{ft}}{12 \text{ in}} \times \frac{\text{hp}\cdot\text{s}}{550 \text{ ft}\cdot\text{lb}}$$

$$W = 0.666 \text{ hp}$$

Example 8.3

Laminar Film on a vertical wall

Given:

Fully developed Laminar Incompressible flow. Newtonian fluid down a vertical wall, thickness and film is constant.

Find: $\frac{\partial P}{\partial x} = 0$

Expression for the velocity distribution

Solution:-

$$F_{Sx} + F_{Bx} = \frac{\partial}{\partial t} \int_V u \rho dV + \int_A u \rho \vec{v} \cdot d\vec{A}$$

For steady flow $\frac{\partial}{\partial t} \int_V u \rho dV = 0$

For fully developed flow $= \Rightarrow \int_A u \rho \vec{v} \cdot d\vec{A} = 0$

Thus the momentum eq can be reduce to

$$F_{Sx} + F_{Bx} = 0$$

$$F_{Bx} = \rho g dV = \rho g dx dy dz$$

$$\text{shear stress on L.H.S} = T_{yxL} = \left(T_{yx} - \frac{dT_{yx}}{dy} \frac{dy}{2} \right)$$

$$\text{shear stress on R.H.S} = T_{yxR} = \left(T_{yx} + \frac{dT_{yx}}{dy} \frac{dy}{2} \right)$$

$$-T_{yxL} dx dz + T_{yxR} dx dz + \rho g dx dy dz = 0$$

$$-\left(\tau_{yx} - \frac{d\tau_{yx}}{dy} \frac{dy}{2}\right) dx dz + \left(\tau_{yx} + \frac{d\tau_{yx}}{dy} \frac{dy}{2}\right) dx dz + \rho g dx dy dz = 0$$

$$\frac{d\tau_{yx}}{dy} dx dy dz = -\rho g dx dy dz$$

$$\frac{d\tau_{yx}}{dy} = -\rho g$$

Since

$$\tau_{yx} = \mu \frac{du}{dy}$$

Put in above result

$$\frac{d}{dy} \left(\mu \frac{du}{dy} \right) = -\rho g$$

$$\mu \frac{d^2 u}{dy^2} = -\rho g \Rightarrow \frac{d^2 u}{dy^2} = \frac{-\rho g}{\mu}$$

Integrating w.r. to y .

$$\frac{du}{dy} = \frac{-\rho g}{\mu} y + C_1$$

again Integrating w.r. to y .

$$u = \frac{-\rho g}{\mu} \frac{y^2}{2} + C_1 y + C_2$$

applying boundary conditions.

$$y = 0, u = 0$$

$$y = 0, \frac{du}{dy} = 0$$

$$C_2 = 0$$

$$0 = \frac{-\rho g}{\mu} \frac{y^2}{2} + C_1 y$$

So

$$u = - \frac{\rho g}{\mu} \frac{y^2}{2} + \frac{\rho g}{\mu} \delta y$$

$$u = \frac{\rho g}{\mu} \delta \left[\left(\frac{y}{\delta} \right) - \frac{1}{2} \left(\frac{y}{\delta} \right)^2 \right]$$

Example 8.4

Capillary viscometer:-

Given:-

Flow in capillary viscometer.
The flow rate is $Q = 8.80 \text{ mm}^3/\text{s}$

Find:-

The fluid viscosity.

solution:-

Governing eq

$$Q = \frac{\pi D P \Delta^4}{128 \mu L}$$

Assumptions:-

- (1) Laminar flow
- (2) Steady flow
- (3) Incompressible flow
- (4) Fully developed flow
- (5) Horizontal tube.

Then

$$\mu = \frac{\pi \Delta p D^4}{128 L}$$

$$= \frac{\pi}{128} \times 1.0 \times 10^6 \frac{\text{N}}{\text{m}^2} \times (0.50)^4 \text{ mm}^4 \times \frac{5}{880 \text{ mm}} \times \frac{1}{4} \times 10^{-3} \frac{\text{m}}{\text{mm}}$$

$$= 1.74 \times 10^{-3} \text{ N}\cdot\text{s}/\text{m}^2$$