



## MA3010 Tutorial Answers

Mechanical Engineering (Nanyang Technological University)



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1. A steam power plant receives heat from a furnace at a rate of 280 GJ/h. Heat losses to the surroundings as well as the steam as it passes through the pipes and other components are estimated to be about 8 GJ/h. If the waste heat is transferred to the cooling water at a rate of 145 GJ/h, determine:

- the net power output
- the thermal efficiency of this power plant

Assumptions: Steady-state

a) Energy balance

$$\begin{aligned}
 \dot{Q}_{in} - \dot{Q}_L - \dot{Q}_{loss} - \dot{W}_{out} &= 0 \\
 \dot{W}_{out} &= \dot{Q}_{in} - \dot{Q}_L - \dot{Q}_{loss} \\
 &= 280 - 145 - 8 = 127 \text{ GJ/h} \\
 &= 35.27 \text{ MW}
 \end{aligned}$$

b) Thermal efficiency

$$\eta = \frac{\dot{W}_{out}}{\dot{Q}_{in}} = \frac{127}{280} = 0.454$$

Handwritten notes on the screen:

- $Q_{in} = 280$ ,  $Q_{out} = 0$
- $Q_{in} - W = 0$
- Diagram of a Heat Engine (HE) cycle with  $T_H$  at the top,  $T_L$  at the bottom,  $Q_{in}$  entering from the top,  $Q_{out}$  leaving to the bottom, and  $W_{out}$  leaving to the right.

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- the thermal efficiency of this power plant

Assumptions: Steady-state

b) Thermal efficiency

$$\begin{aligned}
 \eta &= \frac{\text{Desired Output}}{\text{Required Input}} = \frac{\dot{W}_{out}}{\dot{Q}_{in}} \\
 &= \frac{127}{280} = 0.454
 \end{aligned}$$

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- $Q_{in} = 280$ ,  $Q_{out} = 0$
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- Diagram of a Heat Engine (HE) cycle with  $T_H$  at the top,  $T_L$  at the bottom,  $Q_{in}$  entering from the top,  $Q_{out}$  leaving to the bottom, and  $W_{out}$  leaving to the right.

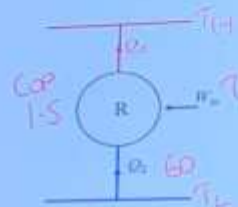
2. A household refrigerator with a COP of 1.5 removes heat from the refrigerated space at a rate of 60 kJ/min. Determine
- the electric power consumed by the refrigerator
  - the rate of heat transfer to the kitchen air

Assumptions: Steady-state

a) COP

$$\text{COP}_R = \frac{\text{Desired Output}}{\text{Required Input}} = \frac{Q_L}{W_{\text{in}}}$$

$$W_{\text{in}} = \frac{Q_L}{\text{COP}_R} = \frac{60}{1.5} = 40 \text{ kJ/min}$$



DISPLAY 5

2. A household refrigerator with a COP of 1.5 removes heat from the refrigerated space at a rate of 60 kJ/min. Determine
- the electric power consumed by the refrigerator
  - the rate of heat transfer to the kitchen air

Assumptions: Steady-state

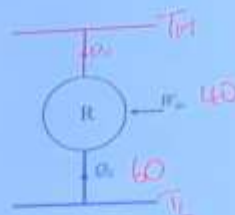
b) Energy balance

$$Q_H = W_{\text{in}} + Q_L$$

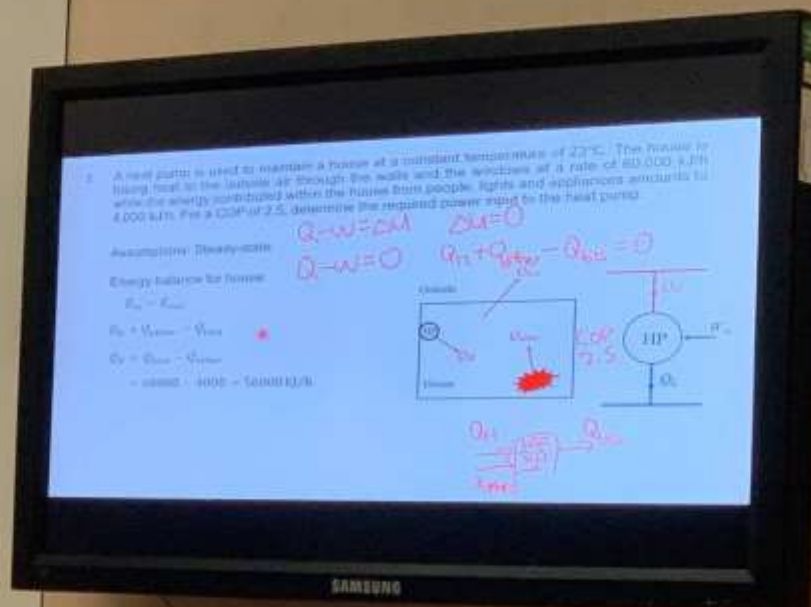
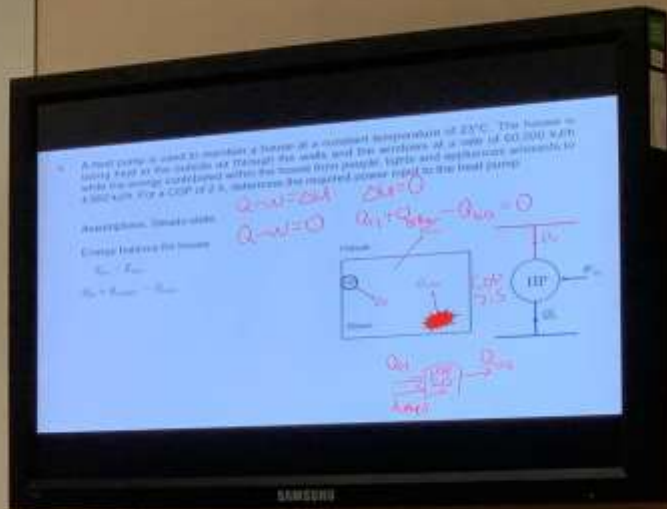
$$= 40 + 60 = 100 \text{ kJ/min}$$

kitchen 100 kJ/min

$$W = Q_H - Q_L$$



GROUP  
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DISPLAY 5



# 5 DISPLAY 5

A heat pump is used to maintain a house at a constant temperature of 23°C. The house is losing heat to the outside at through the walls and the windows at a rate of 80,000 kJ/h while the energy generated within the house from people, lights and appliances amounts to 4,000 kJ/h. For a COP of 2.5, determine the required power input to the heat pump.

Assumptions: Steady-state

$$COP_{HP} = \frac{\text{Desired Output}}{\text{Required Input}} = \frac{\dot{Q}_H}{\dot{W}_{in}}$$

$$\dot{Q}_{loss} = \frac{\dot{Q}_H}{COP_{HP}}$$

$$\dot{Q}_{loss} = \frac{80,000}{2.5} = 32,000 \text{ kJ/h}$$

A heat pump is used to maintain a house at a constant temperature of 23°C. The house is losing heat to the outside at through the walls and the windows at a rate of 80,000 kJ/h while the energy generated within the house from people, lights and appliances amounts to 4,000 kJ/h. For a COP of 2.5, determine the required power input to the heat pump.

Assumptions: Steady-state

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$$\dot{Q}_{loss} = \frac{\dot{Q}_H}{COP_{HP}}$$

$$\dot{Q}_{loss} = \frac{80,000}{2.5} = 32,000 \text{ kJ/h}$$

$$\dot{W}_{in} = \dot{Q}_{loss} - \dot{Q}_{gen} = 32,000 - 4,000 = 28,000 \text{ kJ/h}$$



4. An innovative way of power generation involves the utilization of geothermal energy: the energy of hot water that exists naturally underground – as the heat source. If a supply of hot water at  $140^{\circ}\text{C}$  is discovered at a location where the environmental temperature is  $20^{\circ}\text{C}$ , determine the maximum thermal efficiency a geothermal power plant built at that location can have. How does it compare with steam power plants using fossil fuels (steam temperature around  $500^{\circ}\text{C}$ )? Also, what would happen to the efficiency if the environmental temperature drops to  $0^{\circ}\text{C}$  or rises to  $40^{\circ}\text{C}$ ?

Assumptions: Steady-state

Maximum thermal efficiency = Carnot efficiency

Solution:  $\eta_{\text{th,max}} = \frac{\text{Desired Output}}{\text{Required Input}} = \frac{W_{\text{net}}}{Q_H}$

$$= \frac{Q_H - Q_L}{Q_H} = 1 - \frac{Q_L}{Q_H}$$

$$= 1 - \frac{T_L}{T_H}$$

$$= 1 - \frac{20 + 273}{140 + 273} = 0.291$$

$W_{\text{net}} = Q_H - Q_L = W_{\text{net}}$

$\left(\frac{Q_L}{Q_H}\right)_{\text{max}} = \frac{T_L}{T_H}$

4. An innovative way of power generation involves the utilization of geothermal energy: the energy of hot water that exists naturally underground – as the heat source. If a supply of hot water at  $140^{\circ}\text{C}$  is discovered at a location where the environmental temperature is  $20^{\circ}\text{C}$ , determine the maximum thermal efficiency a geothermal power plant built at that location can have. How does it compare with steam power plants using fossil fuels (steam temperature around  $500^{\circ}\text{C}$ )? Also, what would happen to the efficiency if the environmental temperature drops to  $0^{\circ}\text{C}$  or rises to  $40^{\circ}\text{C}$ ?

$\eta_{\text{th,max}} = 1 - \frac{T_L}{T_H}$

For steam power plants,  $T_H = 500^{\circ}\text{C}$

$$\eta_{\text{th,max}} = 1 - \frac{20 + 273}{500 + 273} = 0.621$$

When:  $T_L = 0^{\circ}\text{C}$

$$\eta_{\text{th,max}} = 1 - \frac{0 + 273}{140 + 273} = 0.339$$

When:  $T_L = 40^{\circ}\text{C}$

$$\eta_{\text{th,max}} = 1 - \frac{40 + 273}{140 + 273} = 0.242$$

5. A Carnot heat engine receives heat from a reservoir at  $927^{\circ}\text{C}$  at a rate of  $740 \text{ kJ/min}$  and rejects the waste heat to the ambient air at  $27^{\circ}\text{C}$ . The entire work output of the heat engine is used to drive a refrigerator that removes heat from the refrigerated space at  $-7^{\circ}\text{C}$  and transfers it to the same ambient at  $27^{\circ}\text{C}$ . Determine (a) the maximum rate of heat removal from the refrigerated space and (b) the total rate of heat rejection to the ambient air.

Assumptions: Steady-state

- a) Max rate of heat removal possible only with max COP refrigerator

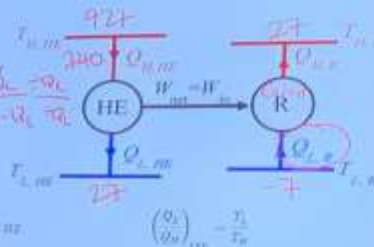
Max COP refrigerator = Carnot refrigerator

$$\text{COP}_{\text{R,max}} = \frac{\text{Desired Output}}{\text{Required Input}} = \frac{Q_{L,R}}{W_{\text{net}}} = \frac{Q_{L,R}}{Q_{H,HE} - Q_{L,HE}}$$

$$= \frac{1}{\frac{Q_{H,HE}}{Q_{L,R}} - 1}$$

$$= \frac{1}{\frac{T_{H,HE}}{T_{L,R}} - 1}$$

$$= \frac{1}{\frac{(27 + 273)(1.7 + 273) - 1}{1}} = 3.02$$



5. A Carnot heat engine receives heat from a reservoir at  $927^{\circ}\text{C}$  at a rate of  $740 \text{ kJ/min}$  and rejects the waste heat to the ambient air at  $27^{\circ}\text{C}$ . The entire work output of the heat engine is used to drive a refrigerator that removes heat from the refrigerated space at  $-7^{\circ}\text{C}$  and transfers it to the same ambient at  $27^{\circ}\text{C}$ . Determine (a) the maximum rate of heat removal from the refrigerated space and (b) the total rate of heat rejection to the ambient air.

Assumptions: Steady-state

a)  $\text{COP}_{\text{R,max}} = \frac{Q_{L,R}}{W_{\text{net}}}$

$$= Q_{L,R} = \text{COP}_{\text{R,max}} \times W_{\text{net}}$$

Need to find  $W_{\text{net}}$  ( $W_{\text{net}}$  from heat engine)

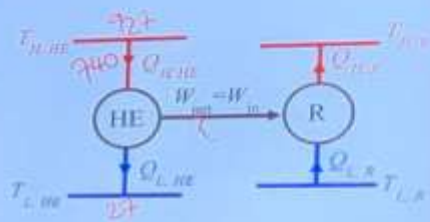
For heat engine (Carnot)

$$\eta_{\text{Carnot}} = 1 - \frac{T_L}{T_H} = \frac{W_{\text{net}}}{Q_{H,HE}}$$

$$= 1 - \frac{27 + 273}{927 + 273} = 0.75$$

$$W_{\text{net}} = \eta_{\text{Carnot}} \times Q_{H,HE}$$

$$= 0.75 \times 740 = 555 \text{ kJ/min}$$



5. A Carnot heat engine receives heat from a reservoir at  $927^{\circ}\text{C}$  at a rate of  $740 \text{ kJ/min}$  and rejects the waste heat to the ambient air at  $27^{\circ}\text{C}$ . The entire work output of the heat engine is used to drive a refrigerator that removes heat from the refrigerated space at  $-7^{\circ}\text{C}$  and transfers it to the same ambient at  $27^{\circ}\text{C}$ . Determine (a) the maximum rate of heat removal from the refrigerated space and (b) the total rate of heat rejection to the ambient air.

Assumptions: Steady-state

a)  $\text{COP}_{\text{Refr}} = \frac{Q_{L,R}}{W_{\text{in}}}$

$\rightarrow Q_{L,R} = \text{COP}_{\text{Refr}} \times W_{\text{in}}$

Need to find  $W_{\text{in}}$  ( $W_{\text{out}}$  from heat engine)

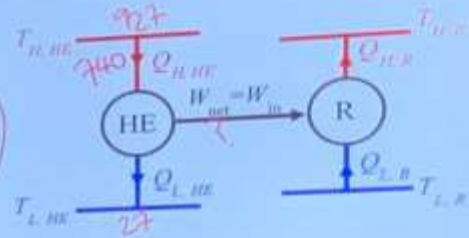
For heat engine (Carnot):

$\eta_{\text{Carnot}} = 1 - \frac{T_L}{T_H} = \frac{W_{\text{out}}}{Q_{H,HE}}$

$\rightarrow 1 - \frac{27 + 273}{927 + 273} = 0.75$

$W_{\text{out}} = \eta_{\text{Carnot}} \times Q_{H,HE}$

$\rightarrow 0.75 \times 740 = 555 \text{ kJ/min}$



$\therefore Q_{L,R} = 7.82 \times 555 = 4340 \text{ kJ/min}$



GROUP  
5  
DISPLAY 5.

1. Two 5 kg identical iron blocks, one at 100°C and the other at 0°C are brought into thermal contact. Assuming no heat loss to the surroundings, calculate the total entropy change for both blocks after reaching thermal equilibrium. Assume a constant specific heat of 0.45 kJ/kg K for the iron blocks.

Equilibrium temperature: 50°C  $\rightarrow T_2$

For the hot block, it cools from 100°C to 50°C.

$$\Delta S_{\text{hot}} = mc \ln \left( \frac{T_2}{T_1} \right)_{\text{hot}}$$

$$= 5 \times 0.45 \ln \left( \frac{50 + 273}{100 + 273} \right) = -0.3238 \text{ kJ/K}$$

For the cold block, it heats up from 0°C to 50°C.

$$\Delta S_{\text{cold}} = mc \ln \left( \frac{T_2}{T_1} \right)_{\text{cold}}$$

$$= 5 \times 0.45 \ln \left( \frac{50 + 273}{0 + 273} \right) = 0.3784 \text{ kJ/K}$$

$$\Delta S = m(S_2 - S_1) = m \left( c \ln \frac{T_2}{T_1} + R \ln \frac{P_2}{P_1} \right)$$

$$= m \left( c \ln \frac{T_2}{T_1} + R \ln \frac{P_2}{P_1} \right)$$

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## DISPLAY 5.

1. Two 5 kg identical iron blocks, one at 100°C and the other at 0°C are brought into thermal contact. Assuming no heat loss to the surroundings, calculate the total entropy change for both blocks after reaching thermal equilibrium. Assume a constant specific heat of 0.45 kJ/kg K for the iron blocks.

Total entropy change:

$$\begin{aligned}\Delta S_{\text{tot}} &= \Delta S_{\text{hot}} + \Delta S_{\text{cold}} \\ &= 0.0546 \text{ kJ/K}\end{aligned}$$

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GROUP  
5  
DISPLAY 5

2. A 12-kg iron block initially at 350°C is quenched in an insulated tank that contains 100 kg of water at 22°C. Assuming the water that vaporizes during the process condenses back in the tank, determine the total entropy change during the process.

Assumptions: Constant specific heats for both iron and water  
Tank is an isolated system:  $\Delta E_{total} = 0$

$c_{iron} = 0.45 \text{ kJ/kg} \cdot \text{K}$ ,  $c_{water} = 4.18 \text{ kJ/kg} \cdot \text{K}$  (Table A-3)

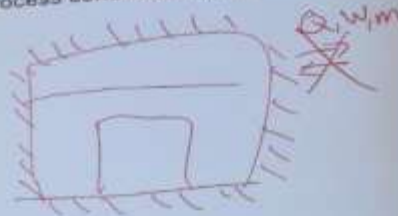
Equilibrium temperature must be determined:

$$\Delta E_{iron} + \Delta E_{water} = 0$$

$$m_{iron} c_{iron} (T_2 - T_1)_{iron} + m_{water} c_{water} (T_2 - T_1)_{water} = 0$$

$$12 \times 0.45 (T_2 - 350) + 100 \times 4.18 (T_2 - 22) = 0$$

$$\rightarrow T_2 = \frac{1890 + 9196}{5.4 + 418} = 26.18^\circ\text{C}$$



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GROUP  
5

DISPLAY 5.

2. A 12-kg iron block initially at 350°C is quenched in an insulated tank that contains 100 kg of water at 22°C. Assuming the water that vaporizes during the process condenses back in the tank, determine the total entropy change during the process.

Entropy change of iron block:

$$\Delta S_{\text{iron}} = \left( mc \ln \frac{T_2}{T_1} \right)_{\text{iron}} \\ = 12 \times 0.45 \ln \left( \frac{26.18 + 273}{350 + 273} \right) = -3.9609 \text{ kJ/K}$$

Entropy change of water:

$$\Delta S_{\text{water}} = \left( mc \ln \frac{T_2}{T_1} \right)_{\text{water}} \\ = 100 \times 4.18 \ln \left( \frac{26.18 + 273}{22 + 273} \right) = 5.8813 \text{ kJ/K}$$

Total entropy change:

$$\Delta S_{\text{tot}} = \Delta S_{\text{iron}} + \Delta S_{\text{water}} \\ = -3.9609 + 5.8813 = 1.92 \text{ kJ/K}$$

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GROUP  
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DISPLAY 5

2. Water vapour enters a turbine at 6 MPa and 400°C and leaves the turbine at 100 kPa with the same specific entropy as that at the inlet. Calculate the difference between enthalpy of the water at the turbine inlet and exit.

Assumptions: Steady state operation

Inlet properties @ 6 MPa, 400°C (Table A-6):

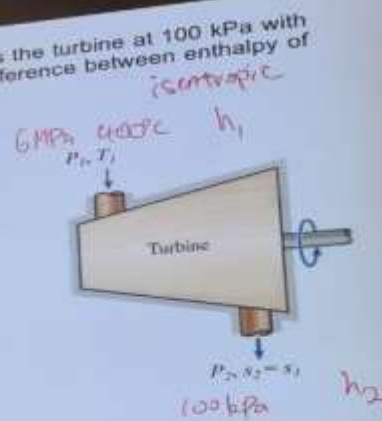
$$s_1 = 6.5432 \text{ kJ/kg} \cdot \text{K}$$

$$h_1 = 3179.3 \text{ kJ/kg}$$

Outlet properties:

$$P_2 = 100 \text{ kPa}$$

$$s_2 = s_1 = 6.5432 \text{ kJ/kg} \cdot \text{K}$$



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GROUP  
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DISPLAY 5

3. Water vapour enters a turbine at 6 MPa and 400°C and leaves the turbine at 100 kPa with the same specific entropy as that at the inlet. Calculate the difference between enthalpy of the water at the turbine inlet and exit.
- Outlet properties,  $P_2 = 100 \text{ kPa}$ ,  $s_2 = s_1 = 6.5432 \text{ kJ/kg} \cdot \text{K}$

Mass fraction,  $s_2 = s_f + x \cdot s_{fg} \rightarrow x = \frac{s_2 - s_f}{s_{fg}}$

$$x = \frac{6.5432 - 1.3028}{6.0562} = 0.865$$

Enthalpy at outlet:

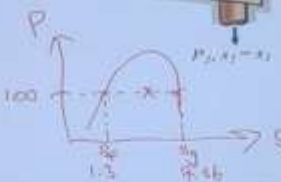
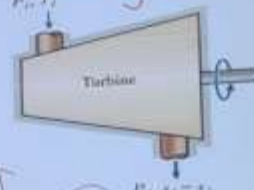
$$h_2 = h_f + x \cdot h_{fg} = 417.51 + 0.865 \times 2257.5 = 2370.2 \text{ kJ/kg}$$

Enthalpy difference:

$$\Delta h = h_2 - h_1 = 2370.2 - 3178.3 = -808.1 \text{ kJ/kg}$$

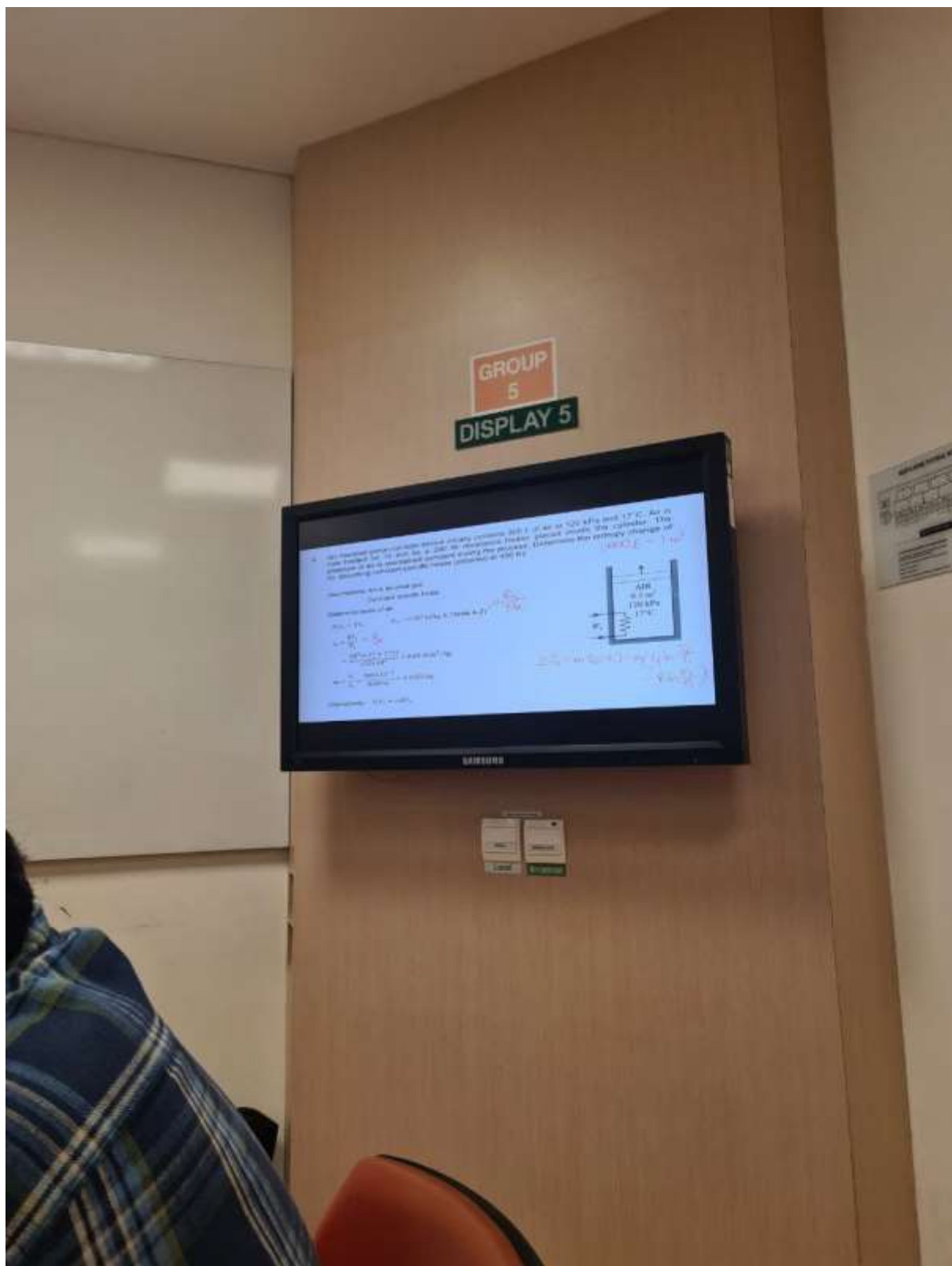
$$h = h_f + x h_{fg}$$

$$s = s_f + x s_{fg}$$



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GROUP  
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DISPLAY 5

4. An insulated piston-cylinder device initially contains 300 L of air at 120 kPa and 17°C. Air is now heated for 15 min by a 200 W resistance heater placed inside the cylinder. The pressure of air is maintained constant during the process. Determine the entropy change of air, assuming constant specific heats (obtained at 450 K)

Determine final temperature:

$$Q - W = \Delta U$$

There is boundary work ( $W_b$ ) to maintain constant pressure:

$$Q + W_e = W_b = \Delta U$$

$$W_e - P_0(V_2 - V_1) = \Delta U = u_2 - u_1 = m(u_2 - u_1)$$

$$W_e - mP_0(v_2 - v_1) = m(u_2 - u_1)$$

$$W_e = m(u_2 - u_1) + mP_0(v_2 - v_1)$$

$$= m[(u_2 + P_0v_2) - (u_1 + P_0v_1)] = m(h_2 - h_1)$$

$$= mc_p(T_2 - T_1)$$

$$\rightarrow T_2 = \frac{W_e}{mc_p} + T_1 = \frac{15 \times 60 \times 200}{0.4325 \times 1.02 \times 10^3} + 17 = 425^\circ\text{C}$$

$$W_b = \int_1^2 P_0 dV = P_0(V_2 - V_1)$$

$$= P_0(mv_2 - mv_1)$$

$$= P_0m(v_2 - v_1)$$



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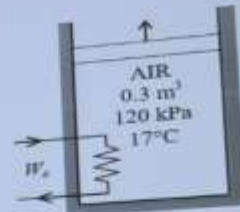
GROUP  
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DISPLAY 5.

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Entropy change of air:  $c_p = 1.02 \text{ kJ/kg} \cdot \text{K}$ ,  $c_v = 0.753 \text{ kJ/kg} \cdot \text{K}$  (Table A-2)

$$\Delta S_{\text{air}} = m \left( c_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right)$$

$$= 0.4325 \left[ 1.02 \ln \left( \frac{425 + 273}{17 + 273} \right) \right] = 0.3875 \text{ kJ/K}$$



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GROUP  
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DISPLAY 5.

5. An insulated rigid tank is divided into two equal parts by a partition. One part of the tank contains 1.5 kg of air at 250 kPa and 40°C while the other part is evacuated. The partition is now removed, and the air expands to fill the entire tank. Determine the total entropy change during this process.

Assumptions: Air is an ideal gas  
Constant specific heats

Tank is an isolated system:  $\Delta E_{total} = 0$

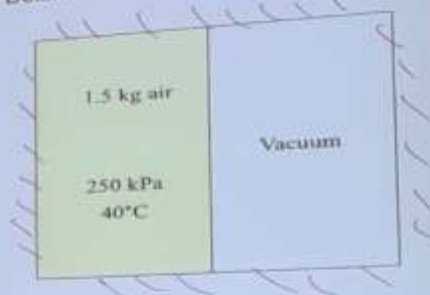
$$m c_v \Delta T = 0$$

$$T_2 = T_1$$

Specific volume ratio:

$$V_2 = 2V_1$$

$$m P_2 = 2m P_1 \rightarrow \frac{P_2}{P_1} = 2$$



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GROUP  
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DISPLAY 5.

8. An insulated rigid tank is divided into two equal parts by a partition. One part of the tank contains 1.5 kg of air at 250 kPa and 40°C while the other part is evacuated. The partition is now removed, and the air expands to fill the entire tank. Determine the total entropy change during this process.

Entropy change:

$$\Delta S_{\text{air}} = m \left( c_p \ln \frac{T_2}{T_1} + R \ln \frac{P_2}{P_1} \right)$$

$$= 1.5 (0.287 \ln 2) = 0.2484 \text{ kJ/K}$$

$$m \left( c_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right) = -mR \ln \frac{1}{2}$$



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1. A completely reversible heat pump produces heat at a rate of 300 kW to warm a house maintained at 24 °C. The exterior air which is at 7 °C serves as a source. Calculate the rate of entropy change of the two reservoirs and determine if this heat pump satisfies the second law according to the increase of entropy principle.

Assumptions: Steady state operation  
Completely reversible heat pump = Carnot heat pump.

$$\left(\frac{Q_H}{Q_L}\right)_{\text{rev}} = \frac{T_H}{T_L} \rightarrow Q_L = Q_H \cdot \frac{T_L}{T_H}$$

$$Q_L = 300 \times \frac{7 + 273}{24 + 273} = 282.83 \text{ kW}$$

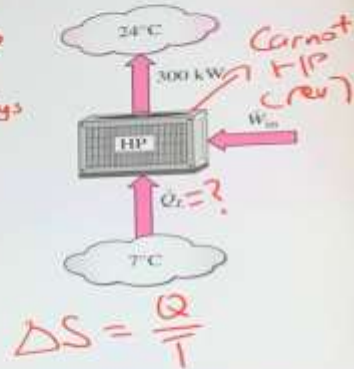
Entropy change for heat sink ( $T_H$ )

$$\dot{S}_H = \frac{\dot{Q}_H}{T_H}$$

$$= \frac{300}{24 + 273} = 1.01 \text{ kW/K}$$

$$S_{\text{gen}} = \Delta S_{\text{iso}}$$

$$= \sum \Delta S_{\text{sys}}$$



1. A completely reversible heat pump produces heat at a rate of 300 kW to warm a house maintained at 24 °C. The exterior air which is at 7 °C serves as a source. Calculate the rate of entropy change of the two reservoirs and determine if this heat pump satisfies the second law according to the increase of entropy principle.

Entropy change for heat source ( $T_L$ )

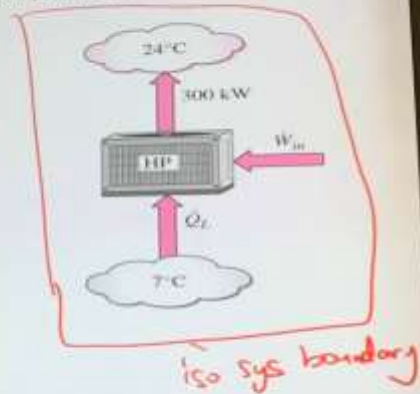
$$\dot{S}_L = \frac{\dot{Q}_L}{T_L}$$

$$= \frac{-282.83}{7 + 273} = -1.01 \text{ kW/K}$$

Total entropy change is the same as entropy change for an isolated system:

$$\dot{S}_{\text{iso}} = \dot{S}_L + \dot{S}_H + \dot{S}_{\text{HP}}$$

$$= \dot{S}_{\text{gen}} = 0 \text{ kW/K} \geq 0$$



# DISPLAY 6

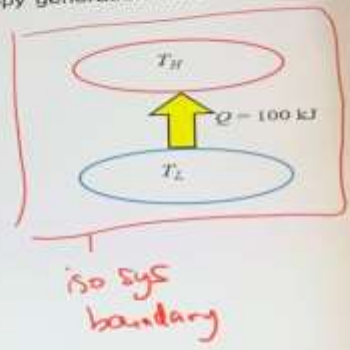
2. Assuming that 100 kJ heat is transferred from a cold reservoir of 600K to a hot reservoir of 1200K in violation of the Clausius statement. Calculate the entropy generation for such a case.

Entropy change for heat sink ( $T_H$ )

$$\Delta S_H = \frac{Q_H}{T_H} = \frac{100}{1200} = 0.0833 \text{ kJ/K}$$

Entropy change for heat source ( $T_L$ )

$$\Delta S_L = \frac{-Q_L}{T_L} = \frac{-100}{600} = -0.1667 \text{ kJ/K}$$



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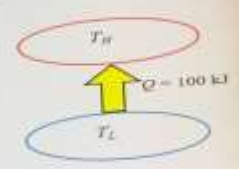
2. Assuming that 100 kJ heat is transferred from a cold reservoir of 600K to a hot reservoir of 1200K in violation of the Clausius statement. Calculate the entropy generation for such a case.

Total entropy change is the same as entropy change for an isolated system:

$$\Delta S_{iso} = \Delta S_L + \Delta S_H = S_{gen}$$

$$S_{gen} = -0.1667 + 0.0833 = -0.0834 \text{ kJ/K} < 0$$

Impossible process



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3. An adiabatic pump is to be used to compress saturated liquid water at 10 kPa to a pressure of 15 MPa in a reversible manner. Determine the work input using :

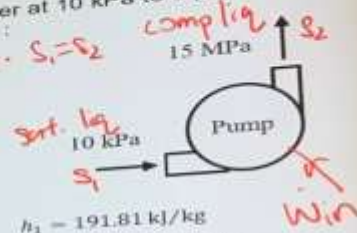
- Enthalpy data from the compressed liquid table,
- Inlet specific volume and pressure values, and
- Average specific volume and pressure values.

Determine the errors in parts (b) and (c).  
Assumptions: Steady-state

**TABLE A-7**  
Compressed liquid water

T, °C	$\rho$ , kg/m <sup>3</sup>	$h$ , kJ/kg	$u$ , kJ/kg	$s$ , kJ/kg·K	$v$ , m <sup>3</sup> /kg	$h$ , kJ/kg	$u$ , kJ/kg	$s$ , kJ/kg·K	$v$ , m <sup>3</sup> /kg
0	999.8	0.01	0.01	0.0000	0.001000	0.01	0.01	0.0000	0.001000
10	999.7	0.04	0.04	0.0000	0.001000	0.04	0.04	0.0000	0.001000
20	999.6	0.08	0.08	0.0000	0.001000	0.08	0.08	0.0000	0.001000
30	999.4	0.12	0.12	0.0000	0.001000	0.12	0.12	0.0000	0.001000
40	999.1	0.16	0.16	0.0000	0.001000	0.16	0.16	0.0000	0.001000
50	998.7	0.20	0.20	0.0000	0.001000	0.20	0.20	0.0000	0.001000
60	998.2	0.24	0.24	0.0000	0.001000	0.24	0.24	0.0000	0.001000
70	997.6	0.28	0.28	0.0000	0.001000	0.28	0.28	0.0000	0.001000
80	996.9	0.32	0.32	0.0000	0.001000	0.32	0.32	0.0000	0.001000
90	996.1	0.36	0.36	0.0000	0.001000	0.36	0.36	0.0000	0.001000
100	995.2	0.40	0.40	0.0000	0.001000	0.40	0.40	0.0000	0.001000
110	994.2	0.44	0.44	0.0000	0.001000	0.44	0.44	0.0000	0.001000
120	993.1	0.48	0.48	0.0000	0.001000	0.48	0.48	0.0000	0.001000
130	991.9	0.52	0.52	0.0000	0.001000	0.52	0.52	0.0000	0.001000
140	990.6	0.56	0.56	0.0000	0.001000	0.56	0.56	0.0000	0.001000
150	989.2	0.60	0.60	0.0000	0.001000	0.60	0.60	0.0000	0.001000
160	987.7	0.64	0.64	0.0000	0.001000	0.64	0.64	0.0000	0.001000
170	986.1	0.68	0.68	0.0000	0.001000	0.68	0.68	0.0000	0.001000
180	984.4	0.72	0.72	0.0000	0.001000	0.72	0.72	0.0000	0.001000
190	982.6	0.76	0.76	0.0000	0.001000	0.76	0.76	0.0000	0.001000
200	980.7	0.80	0.80	0.0000	0.001000	0.80	0.80	0.0000	0.001000
210	978.7	0.84	0.84	0.0000	0.001000	0.84	0.84	0.0000	0.001000
220	976.6	0.88	0.88	0.0000	0.001000	0.88	0.88	0.0000	0.001000
230	974.4	0.92	0.92	0.0000	0.001000	0.92	0.92	0.0000	0.001000
240	972.1	0.96	0.96	0.0000	0.001000	0.96	0.96	0.0000	0.001000
250	969.7	1.00	1.00	0.0000	0.001000	1.00	1.00	0.0000	0.001000
260	967.2	1.04	1.04	0.0000	0.001000	1.04	1.04	0.0000	0.001000
270	964.6	1.08	1.08	0.0000	0.001000	1.08	1.08	0.0000	0.001000
280	961.9	1.12	1.12	0.0000	0.001000	1.12	1.12	0.0000	0.001000
290	959.1	1.16	1.16	0.0000	0.001000	1.16	1.16	0.0000	0.001000
300	956.2	1.20	1.20	0.0000	0.001000	1.20	1.20	0.0000	0.001000

$$s_{1s} = s_1 = s_2$$



$$h_1 = 191.81 \text{ kJ/kg}$$

$$s_1 = 0.6492 \text{ kJ/kg} \cdot \text{K}$$

$$v_1 = 0.001010 \text{ m}^3/\text{kg}$$

Reversible & adiabatic:

$$s_2 = s_1$$

$$P_2 = 15 \text{ MPa}$$

$$h_2 = 207.46 \text{ kJ/kg}$$

$$v_2 = 0.001004 \text{ m}^3/\text{kg}$$

3. An adiabatic pump is to be used to compress saturated liquid water at 10 kPa to a pressure of 15 MPa in a reversible manner. Determine the work input using :

- Enthalpy data from the compressed liquid table,
- Inlet specific volume and pressure values, and
- Average specific volume and pressure values.

Determine the errors in parts (b) and (c).  
Assumptions: Steady-state

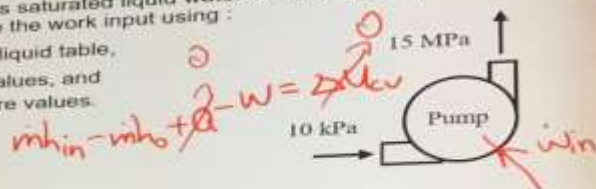
a) Power consumption using enthalpy values:

$$E_{in} = E_{out}$$

$$W_{in} + h_1 = h_2$$

$$W_{in} = h_2 - h_1$$

$$= 207.46 - 191.81 = 15.65 \text{ kJ/kg}$$



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# DISPLAY 6

3. An adiabatic pump is to be used to compress saturated liquid water at 10 kPa to a pressure of 15 MPa in a reversible manner. Determine the work input using :
- Enthalpy data from the compressed liquid table,
  - Inlet specific volume and pressure values, and
  - Average specific volume and pressure values.
- Determine the errors in parts (b) and (c).

Assumptions: Steady-state

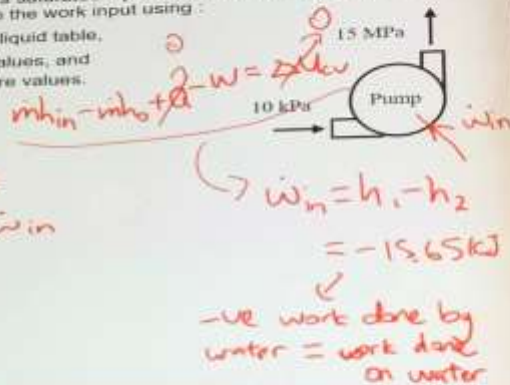
a) Power consumption using enthalpy values:

$$E_{in} = E_{out}$$

$$W_{in} + h_1 = h_2$$

$$W_{in} = h_2 - h_1$$

$$= 207.46 - 191.81 = 15.65 \text{ kJ/kg}$$



4. Air is compressed by a 15-kW compressor from  $P_1$  to  $P_2$ . The air temperature is maintained constant at  $25^\circ\text{C}$  during this process as a result of heat transfer to the surrounding medium at  $20^\circ\text{C}$ . Determine the rate of entropy change of the air. State the assumptions made in solving this problem.

Assumptions: Steady-state

Air as an ideal gas

\* Internally reversible

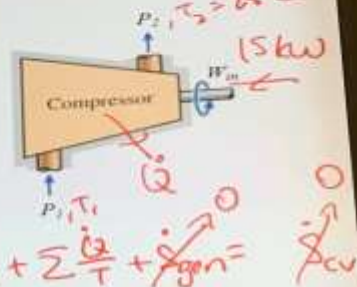
$$E_{in} = E_{out}$$

$$\dot{Q}_{in} + \dot{W}_{in} = \dot{Q}_{out} + \dot{Q}_{out}$$

Since process is isothermal, and enthalpy for ideal gas is a function of temperature only

$$T_{in} = T_{out} \rightarrow h_{in} = h_{out}$$

$$\therefore \dot{W}_{in} = \dot{Q}_{out}$$



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# DISPLAY 6

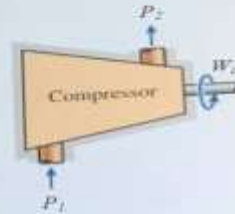
4. Air is compressed by a 15-kW compressor from  $P_1$  to  $P_2$ . The air temperature is maintained constant at  $25^\circ\text{C}$  during this process as a result of heat transfer to the surrounding medium at  $20^\circ\text{C}$ . Determine the rate of entropy change of the air. State the assumptions made in solving this problem.

Assumptions: Steady-state  
Air as an ideal gas  
Internally reversible

$$W_{in} = \dot{Q}_{out}$$

Entropy change of air:

$$\dot{S}_{out} = \frac{-\dot{Q}_{out}}{T_s} = \frac{-15}{25 + 273} = -0.0503 \text{ kW/K}$$



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# GROUP 6

# DISPLAY 6

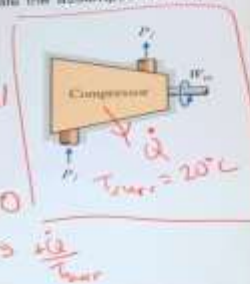
4. Air is compressed by a 15-kW compressor from  $P_1$  to  $P_2$ . The air temperature is maintained constant at  $25^\circ\text{C}$  during this process as a result of heat transfer to the surrounding medium at  $20^\circ\text{C}$ . Determine the rate of entropy change of the air. State the assumptions made in solving this problem.

Assumptions: Steady-state  
Air as an ideal gas  
Internally reversible

$$W_{in} = \dot{Q}_{out}$$

Entropy change of air:

$$\dot{S}_{out} = \frac{-\dot{Q}_{out}}{T_s} = \frac{-15}{25 + 273} = -0.0503 \text{ kW/K}$$



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DISPLAY 6

5. Refrigerant 134a enters the coils of the evaporator of a refrigeration system as a saturated liquid-vapour mixture at a pressure of 140 kPa. The refrigerant absorbs 180 kJ of heat from the cooled space, which is maintained at  $-10^{\circ}\text{C}$ , and leaves as saturated vapour at the same pressure. Determine (a) the entropy change of the refrigerant, (b) the entropy change of the cooled space, and (c) the total entropy change for this process. Assume no internal irreversibilities. *= int rev.*

Assumptions: Internally reversible  
isothermal process (phase-change)

a) Entropy change of refrigerant:

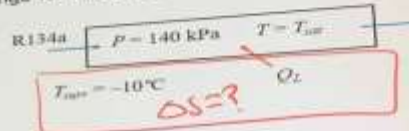
$$\Delta S_R = \frac{Q_L}{T_{sat}} \quad T_{sat} = -18.77^{\circ}\text{C} \quad (\text{Table A-12})$$

$$= \frac{180}{-18.77 + 273} = 0.7076 \text{ kJ/K}$$

b) Entropy change of refrigerated space (thermal energy reservoir):

$$\Delta S_{RST} = \frac{-Q_L}{T_{RST}}$$

$$= \frac{-180}{-10 + 273} = -0.6844 \text{ kJ/K}$$



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DISPLAY 6

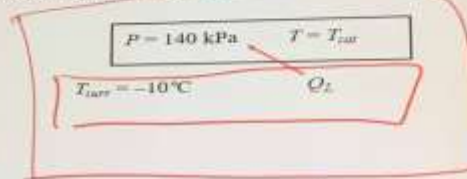
5. Refrigerant 134a enters the coils of the evaporator of a refrigeration system as a saturated liquid-vapour mixture at a pressure of 140 kPa. The refrigerant absorbs 180 kJ of heat from the cooled space, which is maintained at  $-10^{\circ}\text{C}$ , and leaves as saturated vapour at the same pressure. Determine (a) the entropy change of the refrigerant, (b) the entropy change of the cooled space, and (c) the total entropy change for this process. Assume no internal irreversibilities.

Assumptions: Internally reversible  
isothermal process (phase-change)

c) Total entropy change:

$$\Delta S_T = \Delta S_R + \Delta S_{RST} = \Delta S_{tot} = S_{gen}$$

$$= 0.7076 + (-0.6844) = 0.0232 \text{ kJ/K} > 0$$



iso sys  
boundary

SAMSUNG

GROUP  
5

DISPLAY 5

1. Nitrogen gas is compressed from 80 kPa and 27°C to 480 kPa by a 10-kW compressor. Determine the mass flow rate of nitrogen through the compressor, assuming the compression process to be (a) isentropic, (b) polytropic with  $n = 1.3$ , (c) isothermal, and (d) ideal two-stage polytropic with  $n = 1.3$

Assumptions: Nitrogen is an ideal gas with constant specific heats  
Reversible steady flow  
Negligible K.E. and P.E. changes  
 $T_{avg} = 400$  K (estimated)

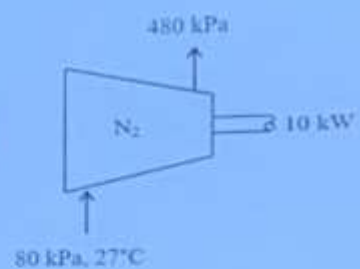
Properties:  $R = 0.297$  kJ/kg K,  $k = 1.397$

Check  $T_{avg}$ :

$$T_2 = T_1 \left( \frac{P_2}{P_1} \right)^{(k-1)/k}$$

$$= (27 + 273) \left( \frac{480}{80} \right)^{(1.397-1)/1.397} = 499.2 \text{ K}$$

$T_{avg} = 400$  K (verified)



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GROUP  
5

DISPLAY 5

1 Nitrogen gas is compressed from 80 kPa and 27°C to 480 kPa by a 10-kW compressor. Determine the mass flow rate of nitrogen through the compressor, assuming the compression process to be (a) isentropic, (b) polytropic with  $n = 1.3$ , (c) isothermal, and (d) ideal two-stage polytropic with  $n = 1.3$ .

a) isentropic compression ( $n = \gamma$ )

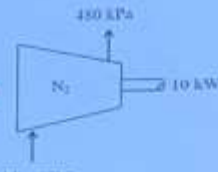
$$h_{\text{isent}} = \frac{nRT_1}{n-1} \left[ \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right]$$

work done by fluid per unit mass

$$h_{\text{isent}} = \frac{nRT_1}{n-1} \left[ \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right]$$

$$\dot{Q} = \dot{m} \left[ \frac{1.397 \times 0.297 \times (27 + 273)}{1.397 - 1} \left[ \left( \frac{480}{80} \right)^{\frac{1.397-1}{1.397}} - 1 \right] \right]$$

$$\dot{m} = 0.0400 \text{ kg/s}$$



work done on fluid = - work done by fluid

$$= - \left[ - \frac{nRT_1}{n-1} \left( \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right) \right]$$



GROUP  
5  
DISPLAY 5.

1. Nitrogen gas is compressed from 80 kPa and 27°C to 480 kPa by a 10-kW compressor. Determine the mass flow rate of nitrogen through the compressor, assuming the compression process to be (a) isentropic, (b) polytropic with  $n = 1.3$ , (c) isothermal, and (d) ideal two-stage polytropic with  $n = 1.3$ .

b) Polytropic compression ( $n = 1.3$ )

$n < k$

$$W_{\text{comp}} = m \frac{nRT_1}{n-1} \left[ \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right]$$

$$10 = (m) \frac{1.3 \times 0.297 \times (27 + 273)}{1.3 - 1} \left[ \left( \frac{480}{80} \right)^{\frac{(1.3-1)}{1.3}} - 1 \right]$$

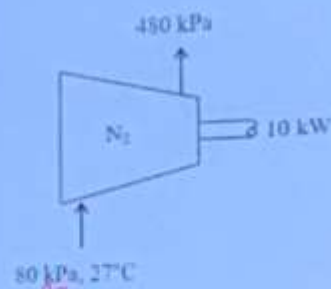
$$m = 0.0506 \text{ kg/s}$$

c) Isothermal compression ( $n = 1$ )

$\rightarrow \int v dP$  sub.  $v = \frac{RT}{P}$

$$W_{\text{comp}} = -mRT \ln \frac{P_2}{P_1} \quad 10 = m \times 0.297 \times (27 + 273) \ln \left( \frac{480}{80} \right)$$

$$W_{\text{comp}} = -mRT \ln \frac{P_2}{P_1} \quad m = 0.0626 \text{ kg/s}$$



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GROUP  
5

DISPLAY 5

1. Nitrogen gas is compressed from 80 kPa and 27°C to 480 kPa by a 10-kW compressor. Determine the mass flow rate of nitrogen through the compressor, assuming the compression process to be (a) isentropic, (b) polytropic with  $n = 1.3$ , (c) isothermal, and (d) ideal two-stage polytropic with  $n = 1.3$

$$\frac{P_2}{P_1} = \frac{P_2}{P_2}$$

- d) Ideal 2-stage compression ( $n = 1.3$ )

Pressure ratio across each stage is the same:

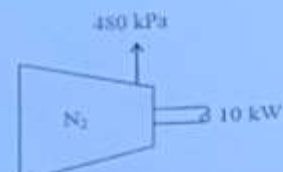
$$P_2 = \sqrt{P_1 P_3} = 195.96 \text{ kPa}$$

Since the pressure ratio across each stage is the same, the work for each stage is also the same:

$$W_{\text{comp}} = 2W_{\text{stage}} = 2m \frac{nRT_1}{n-1} \left[ \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right]$$

$$10 = 2(m) \frac{1.3 \times 0.297 \times 300}{0.3} \left[ \left( \frac{195.96}{80} \right)^{\frac{0.3}{1.3}} - 1 \right]$$

$$m = 0.0564 \text{ kg/s}$$



$$2m \frac{nRT_1}{n-1} \left[ \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} - 1 \right]$$

GROUP  
5

DISPLAY 5

2. Steam enters an adiabatic turbine at 8 MPa and 500°C with a mass flow rate of 3 kg/s and leaves at 30 kPa. The isentropic efficiency of the turbine is 0.90. Neglecting the kinetic energy change of the steam, determine (a) the temperature at the turbine exit and (b) the power output of the turbine.

Assumptions: Steady state, steady flow

Adiabatic turbine

Negligible K.E. & P.E.

Inlet properties (State 1):  $h_1 = 3399.5 \text{ kJ/kg}$

$s_1 = 6.7266 \text{ kJ/kg} \cdot \text{K}$

State 2s (Isentropic, saturated liquid-vapour mixture)

$$x_{2s} = \frac{h_{2s} - h_f}{h_{fg}} = \frac{6.7266 - 0.9441}{6.5234} = 0.8425$$

$$h_{2s} = h_f + x_{2s} h_{fg} = 299.27 + 0.8425 \times 2335.3 = 2266.23 \text{ kJ/kg}$$

$$\frac{h_1 - h_{2s}}{h_1 - h_2} = \eta_t$$



$P_1 = 8 \text{ MPa}$   
 $T_1 = 500^\circ\text{C}$



$P_2 = 30 \text{ kPa}$   
 $T_{2s} = ?$

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GROUP  
5  
DISPLAY 5

2. Steam enters an adiabatic turbine at 6 MPa and 500°C with a mass flow rate of 3 kg/s and leaves at 30 kPa. The isentropic efficiency of the turbine is 0.90. Neglecting the kinetic energy change of the steam, determine (a) the temperature at the turbine exit and (b) the power output of the turbine.

a) Isentropic efficiency:

$$\eta_T = \frac{h_1 - h_{2s}}{h_1 - h_{2a}}$$

$$h_{2a} = h_1 - \eta_T(h_1 - h_{2s})$$

$$= 3399.5 - 0.9(3399.5 - 2268.3) = 2381.4 \text{ kJ/kg} < h_g$$

From property table, actual turbine exit temperature is also 69.09°C

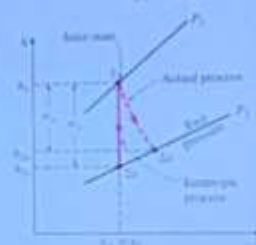
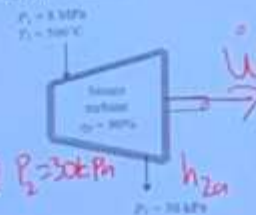
b) Energy balance to obtain power output:

$$\dot{E}_{in} = \dot{E}_{out}$$

$$m\dot{h}_1 = \dot{W}_{out} + m\dot{h}_2$$

$$\dot{W}_{out} = m(\dot{h}_1 - \dot{h}_2)$$

$$= 3(3399.5 - 2381.4) = 3054 \text{ kW}$$





GROUP  
5  
DISPLAY 5

1. Air is compressed by an adiabatic compressor from 95 kPa and 27°C to 600 kPa and 277°C. Assuming constant specific heats and neglecting the changes in kinetic and potential energies, determine (a) the isentropic efficiency of the compressor and (b) the exit temperature of air if the process were reversible.

Assumptions: Steady state, steady flow  
Air as an ideal gas with constant specific heats  
Adiabatic compressor  
Negligible K.E. & P.E.

Air properties:  $T_{ref} = 425 \text{ K}$ ,  $c_p = 1.0165 \text{ kJ/kg} \cdot \text{K}$ ,  $k = 1.393$

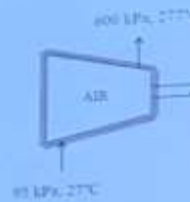
to Adiabatic & reversible process = isentropic process

$$\left( \frac{T_2}{T_1} \right)_{\text{isent}} = \left( \frac{P_2}{P_1} \right)^{\frac{k-1}{k}}$$

$$T_{2s} = T_1 \left( \frac{P_2}{P_1} \right)^{\frac{k-1}{k}}$$

$$= (27 + 273) \left( \frac{600}{95} \right)^{\frac{1.393-1}{1.393}} = 504.8 \text{ K}$$

$$T_{2s} = 400 \text{ K}, c_p = 1.013 \text{ kJ/kg} \cdot \text{K}, k = 1.397$$

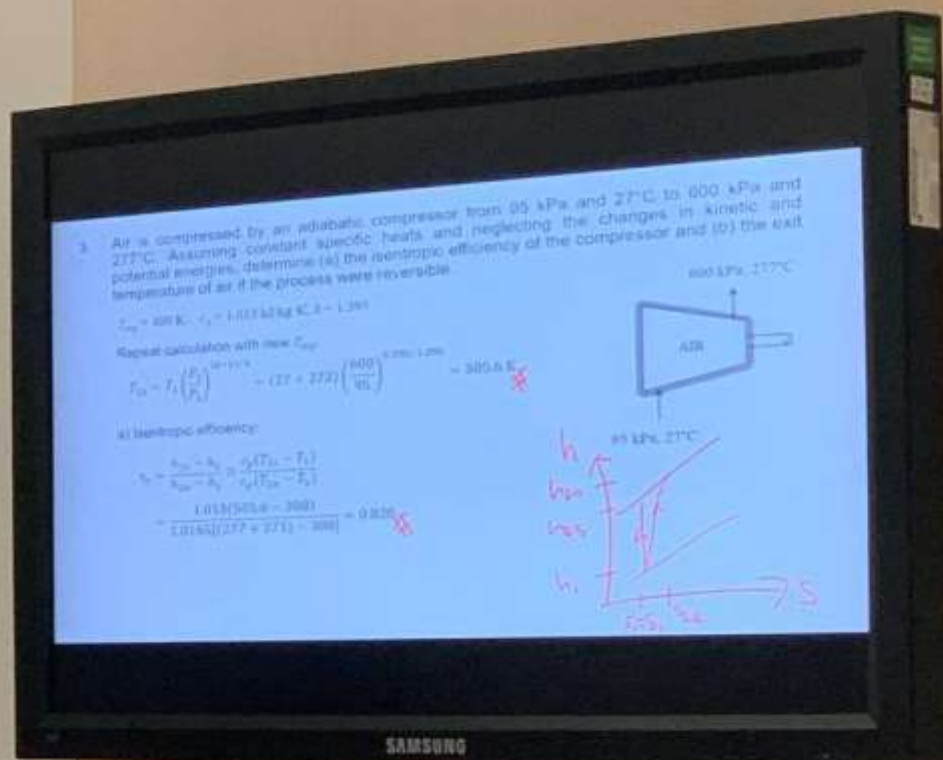


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GROUP  
5  
DISPLAY 5

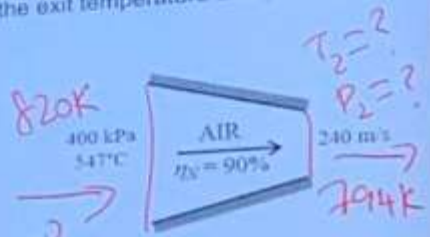


GROUP  
5

DISPLAY 5.

4. Air enters an adiabatic nozzle at 400 kPa and 547 °C with low velocity and exits at 240 m/s. If the isentropic efficiency of the nozzle is 90%, determine the exit temperature and pressure of the air.

Assumptions: Steady state; steady flow  
Air as an ideal gas with constant specific heats  
Adiabatic nozzle  
Negligible P.E.  
 $T_{\text{ref}} = 800 \text{ K}$



Energy balance for actual nozzle:  $E_{\text{in}} = E_{\text{out}}$

$$\dot{m} \left( h_1 + \frac{v_1^2}{2} \right) = \dot{m} \left( h_{2a} + \frac{v_{2a}^2}{2} \right) \rightarrow 2(h_1 - h_{2a}) = v_{2a}^2 - v_1^2$$

$$2(h_1 - h_{2a}) = v_{2a}^2$$

$$2c_p(T_1 - T_{2a}) = v_{2a}^2$$

$$T_{2a} = T_1 - \frac{v_{2a}^2}{2c_p} = (547 + 273) - \frac{240^2}{2 \times 1.049 \times 10^3} = 791.8 \text{ K}$$

$$v_{2a} \gg v_1$$

$$v_{2a}^2 \gg v_1^2$$

$$v_{2a}^2 - v_1^2 \approx v_{2a}^2$$

GROUP  
5

DISPLAY 5

4. Air enters an adiabatic nozzle at 400 kPa and 547 °C with low velocity and exits at 240 m/s. If the isentropic efficiency of the nozzle is 90%, determine the exit temperature and pressure of the air.

Exit pressure for actual nozzle is the same as isentropic nozzle

$$\left(\frac{T_2}{T_1}\right)_{\text{isent}} = \left(\frac{P_2}{P_1}\right)^{\frac{\gamma-1}{\gamma}} \quad \left(\frac{P_2}{P_1}\right) = \left(\frac{T_2}{T_1}\right)^{\frac{\gamma}{\gamma-1}}$$

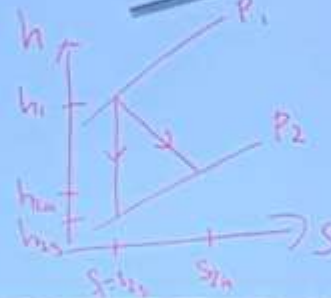
Use isentropic efficiency to calculate isentropic exit temperature

$$\eta_N = \frac{h_1 - h_{2s}}{h_1 - h_{2a}} = \frac{c_p(T_1 - T_{2s})}{c_p(T_1 - T_{2a})}$$

$$T_{2s} = T_1 - \frac{T_1 - T_{2a}}{\eta_N}$$

$$= 820 - \frac{820 - 793.8}{0.9} = 798.9 \text{ K}$$

$$P_2 = P_1 \left(\frac{T_{2s}}{T_1}\right)^{\frac{\gamma}{\gamma-1}} = 400 \left(\frac{798.9}{820}\right)^{\frac{1.4}{1.4-1}} = 348.4 \text{ kPa}$$



SAMSUNG

GROUP  
5

DISPLAY 5

3. Long cylindrical steel rods ( $\rho = 7833 \text{ kg/m}^3$ ) and  $c_p = 0.465 \text{ kJ/kg} \cdot \text{K}$ ) of 10 cm diameter are heat treated by drawing them at a speed of 3 m/min through a 7 m long oven maintained at  $600^\circ\text{C}$ . If the rods enter the oven at  $30^\circ\text{C}$  and leave at  $700^\circ\text{C}$ , determine (a) the rate of heat transfer to the rods in the oven and (b) the rate of entropy generation with the heat transfer process.

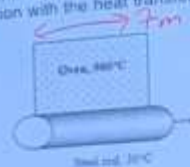
Assumptions: Steady state  
Constant specific heat  
Negligible K.E. & P.E.

Rods are moving continuously through the oven at 3 m/min.  
Analyze the rod using a period of 1 min interval.

Mass of rod treated per min:

$$\dot{m} = \rho V = \rho \times \frac{\pi D^2}{4} \times L$$

$$= 7833 \times \pi \times \frac{0.1^2}{4} \times 3 = 184.54 \text{ kg/min}$$



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GROUP  
5

DISPLAY 5

5. Long cylindrical steel rods ( $\rho = 7833 \text{ kg/m}^3$ ) and  $c_p = 0.465 \text{ kJ/kg} \cdot \text{K}$ ) of 10 cm diameter are heat treated by drawing them at a speed of 3 m/min through a 7 m long oven maintained at  $900^\circ\text{C}$ . If the rods enter the oven at  $30^\circ\text{C}$  and leave at  $700^\circ\text{C}$ , determine (a) the rate of heat transfer to the rods in the oven and (b) the rate of entropy generation with the heat transfer process.

a) Energy balance:

$$\begin{aligned} Q &= \dot{m} \Delta T = \dot{m} c_p (T_2 - T_1) \\ &= 184.36 \times 0.465 \times (700 - 30) = 57500 \text{ kJ/min} \\ &= 958.3 \text{ kW} \end{aligned}$$

*Handwritten notes:  $\dot{m} = 184.36 \text{ kg/min}$  (circled),  $\Delta T = 670^\circ\text{C}$  (circled), and  $Q = \dot{m} \Delta T = \dot{m} c_p \Delta T$  (circled).*



SAMSUNG



GROUP  
5

DISPLAY 5

5. Long cylindrical steel rods ( $\rho = 7833 \text{ kg/m}^3$  and  $c_p = 0.465 \text{ kJ/kg} \cdot \text{K}$ ) of 10 cm diameter are heat treated by drawing them at a speed of 3 m/min through a 7 m long oven maintained at  $900^\circ\text{C}$ . If the rods enter the oven at  $30^\circ\text{C}$  and leave at  $700^\circ\text{C}$ , determine (a) the rate of heat transfer to the rods in the oven and (b) the rate of entropy generation with the heat transfer process.

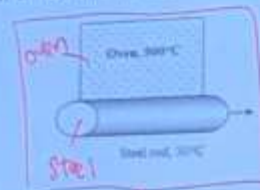
a) Energy balance:

$$\dot{Q} - \dot{W} = \dot{m}(h_2 - h_1) \quad \text{kg/min}$$

$$\dot{Q} = \dot{m}(T_2 - T_1) \quad \text{kg/min}$$

$$= 184.56 \times 0.465 \times (700 - 30) = 57100 \text{ kJ/min}$$

$$= 955.3 \text{ kW}$$



b) For a 1 min interval

Rate of entropy change for steel rod:

$$\dot{S}_{\text{rod}} = \dot{m} \ln \frac{T_2}{T_1} \quad \text{kJ/min}$$

$$= 184.56 \times 0.465 \ln \frac{700 + 273}{30 + 273} = 100.122 \text{ kJ/K} \cdot \text{min}$$

isolated  
sys.  
boundary

SAMSUNG



GROUP  
5

DISPLAY 5

5. Long cylindrical steel rods ( $\rho = 7833 \text{ kg/m}^3$ ) and  $c_p = 0.465 \text{ kJ/kg K}$ ) of 10 cm diameter are heat treated by drawing them at a speed of 3 m/min through a 7 m long oven maintained at  $900^\circ\text{C}$ . If the rods enter the oven at  $30^\circ\text{C}$  and leave at  $700^\circ\text{C}$ , determine (a) the rate of heat transfer to the rods in the oven and (b) the rate of entropy generation with the heat transfer process.

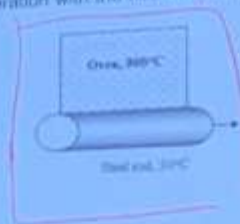
Interior of the oven is a thermal energy reservoir

Rate of entropy change in oven interior:

$$\begin{aligned} \dot{S}_{\text{oven}} &= \frac{\dot{Q}}{T_{\text{oven}}} \\ &= \frac{-0.7586}{900 + 273} = -49.02 \text{ kJ/K} \cdot \text{min} \end{aligned}$$

Rate of entropy generation:

$$\begin{aligned} \dot{S}_{\text{gen}} &= \dot{S}_{\text{rod}} - \dot{S}_{\text{oven}} = \dot{S}_{\text{rod}} \\ &= 100.122 - 49.02 = 51.1 \text{ kJ/K} \cdot \text{min} \\ &= 0.852 \text{ kW/K} \end{aligned}$$



GROUP  
5

DISPLAY 5

The volumetric analysis of mixture of gases is 30% oxygen, 40% nitrogen, 10% carbon dioxide, and 20% methane. This mixture is heated from 20°C to 200°C while flowing through a tube in which the pressure is maintained at 150 kPa. Determine the heat transfer to the mixture per unit mass of the mixture. Use specific heat values at  $T = 300\text{K}$ .

Assumptions: Ideal gas mixture with constant specific heats  
Steady-state flow

Molar properties:  $O_2 = 31.999\text{ kg/kmol}$ ,  $N_2 = 28.013\text{ kg/kmol}$ ,  
 $CO_2 = 44.01\text{ kg/kmol}$ ,  $CH_4 = 16.043\text{ kg/kmol}$

For ideal gases, volume fraction = mole fraction

Considering 100 kmol of mixture

Mass of each component  $\rightarrow n = 100\text{ kmol of mixture}$

$$m_{O_2} = N_{O_2} M_{O_2} = 30\text{ kmol} \cdot 31.999\text{ kg/kmol} = 959.97\text{ kg}$$

$$m_{N_2} = N_{N_2} M_{N_2} = 40\text{ kmol} \cdot 28.013\text{ kg/kmol} = 1120.52\text{ kg}$$

$$m_{CO_2} = N_{CO_2} M_{CO_2} = 10\text{ kmol} \cdot 44.01\text{ kg/kmol} = 440.1\text{ kg}$$

$$m_{CH_4} = N_{CH_4} M_{CH_4} = 20\text{ kmol} \cdot 16.043\text{ kg/kmol} = 320.86\text{ kg}$$

$$\frac{V_i}{V_m} = y_i = \frac{P_i}{P_m}$$



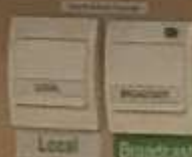
$$E_{in} = E_{out}$$

$$m h_i + Q = m h_o$$

$$h_i + \frac{Q}{m} = h_o$$

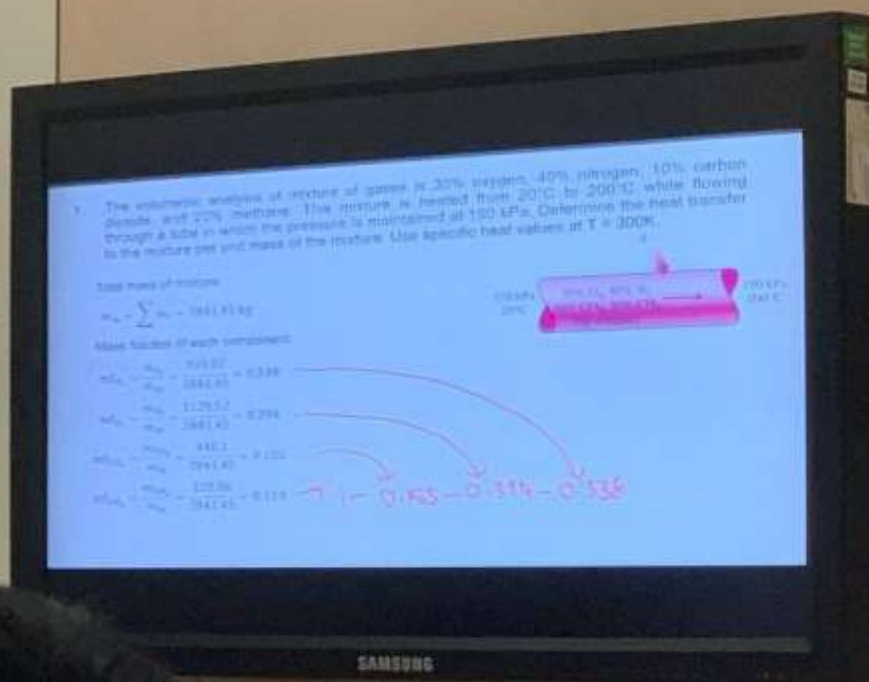
$$q = h_o - h_i = q_{in} + q_{out}$$

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GROUP  
5

DISPLAY 5



GROUP  
5  
DISPLAY 5

The volumetric analysis of mixture of gases is 30% oxygen, 40% nitrogen, 10% carbon dioxide, and 20% methane. This mixture is heated from 20°C to 200°C while flowing through a tube in which the pressure is maintained at 150 kPa. Determine the heat transfer to the mixture per unit mass of the mixture. Use specific heat values at  $T = 300\text{K}$ .

Specific heats for each gas are obtained from Table A-2a with  $T = 300\text{K}$

Specific heat for the gas mixture

$$c_{p,m} = \sum m_i c_{p,i}$$

$$= m_{O_2} c_{p,O_2} + m_{N_2} c_{p,N_2} + m_{CO_2} c_{p,CO_2} + m_{CH_4} c_{p,CH_4}$$

$$= 0.3(0.918) + 0.4(1.039) + 0.1(1.684) + 0.2(1.716)$$

$$= 1.105 \text{ kJ/kg} \cdot \text{K}$$

Energy balance

$$\dot{E}_{in} = \dot{E}_{out}$$

$$\dot{Q} + \dot{m} c_{p,m} T_{in} = \dot{m} c_{p,m} T_{out}$$

$$\dot{Q} = \dot{m} c_{p,m} (T_{out} - T_{in})$$

$$= 1.105(200 - 20) = 199 \text{ kJ/kg}$$

Diagram of a tube with gas flowing from left to right. Inlet conditions: 150 kPa, 20°C. Outlet conditions: 150 kPa, 200°C.

Handwritten equations:

$$Q = \dot{m} \Delta h_m$$

$$= \sum \dot{m}_i \Delta h_i$$




GROUP  
5  
DISPLAY 5

1. The volumetric analysis of mixture of gases is 30% oxygen, 40% nitrogen, 10% carbon dioxide, and 20% methane. This mixture is heated from 20°C to 200°C while flowing through a tube in which the pressure is maintained at 150 kPa. Determine the heat transfer to the mixture per unit mass of the mixture. Use specific heat values at  $T = 300\text{K}$ .

Specific heats for each gas are obtained from Table A-2a with  $T = 300\text{K}$ .

Specific heat for the gas mixture

$$c_{p,m} = \sum m_i c_{p,i}$$

$$= m_{O_2} c_{p,O_2} + m_{N_2} c_{p,N_2} + m_{CO_2} c_{p,CO_2} + m_{CH_4} c_{p,CH_4}$$

$$= 0.3(0.918) + 0.4(1.039) + 0.1(1.55) + 0.2(1.337)$$

$$= 1.105 \text{ kJ/kg} \cdot \text{K}$$


Energy balance

$$E_{in} = E_{out}$$

$$\dot{Q} + c_{p,m} \dot{m} T_{in} = c_{p,m} \dot{m} T_{out}$$

$$\dot{Q} = c_{p,m} \dot{m} (T_{out} - T_{in})$$

$$= 1.105(200 - 20) = 199.0 \text{ kJ/kg}$$



$Q = m \Delta u_m = \sum m_i \Delta u_i$

$Q = m \Delta h_m \text{ (cv)}$

$= \sum m_i \Delta h_i$

GROUP  
5

DISPLAY 5

2. An insulated tank that contains 1 kg of  $O_2$  at  $15^\circ\text{C}$  and 300 kPa is connected to a  $2\text{-m}^3$  uninsulated tank that contains  $N_2$  at  $50^\circ\text{C}$  and 500 kPa. The valve connecting the two tanks is opened, and the two gases form a homogeneous mixture at  $25^\circ\text{C}$ . Determine (a) the final pressure in the tank, (b) the heat transfer to the surroundings, and (c) the entropy generated during this process. Assume the surrounding temperature to be  $T_s = 25^\circ\text{C}$ .

Assumptions: All gases are ideal gases with constant specific heats

Gas constants:  $R_{O_2} = 0.2598 \text{ kJ/kg} \cdot \text{K}$   
 $R_{N_2} = 0.2968 \text{ kJ/kg} \cdot \text{K}$

Volume of  $O_2$  tank

$$V_{O_2} = \left( \frac{m R_{O_2} T_1}{P_1} \right) \rightarrow \text{K}$$

$$1 \times 0.2598 \times (273 + 15) = 0.249 \text{ m}^3$$

Mass of  $N_2$

$$m_{N_2} = \left( \frac{P_2 V_2}{R_{N_2} T_2} \right) \rightarrow \text{K}$$

$$\frac{500 \times 2}{0.2968 \times (273 + 50)} = 10.43 \text{ kg}$$



Negligible  $\Delta KE$  &  $\Delta PE$

$$P_m V_m = m R_m T_m$$

$$PV = mRT \text{ for } O_2 \text{ \& } N_2$$

GROUP  
5

DISPLAY 5

2. An insulated tank that contains 1 kg of  $O_2$  at  $15^\circ\text{C}$  and 300 kPa is connected to a  $2\text{-m}^3$  uninsulated tank that contains  $N_2$  at  $50^\circ\text{C}$  and 500 kPa. The valve connecting the two tanks is opened, and the two gases form a homogeneous mixture at  $25^\circ\text{C}$ . Determine (a) the final pressure in the tank, (b) the heat transfer to the surroundings, and (c) the entropy generated during this process. Assume the surrounding temperature to be  $T_o = 25^\circ\text{C}$ .

Total volume of mixture = total volume of both tanks

$$V_m = V_{\text{tank}, O_2} + V_{\text{tank}, N_2} = 2.249 \text{ m}^3$$

Mol count for each component:

$$N_{O_2} = \frac{m_{O_2}}{M_{O_2}} = \frac{1}{31.998} = 0.0312 \text{ kmol}$$

$$N_{N_2} = \frac{m_{N_2}}{M_{N_2}} = \frac{10.43}{28.013} = 0.372 \text{ kmol}$$

Total number of mol in mixture:

$$N_m = N_{O_2} + N_{N_2} = 0.4032 \text{ kmol}$$

a) Final mixture pressure:

$$P_m = \frac{N_m R_u T_m}{V_m} = \frac{0.4032 \times 8.314 \times (25 + 273)}{2.249} = 444.3 \text{ kPa}$$



$$P_m V_m = N_m R_u T_m$$

$$P_m V_m = m_m R_m T_m$$

$$R = \frac{R_u}{M} \rightarrow R_m = \frac{R_u}{M_m}$$

$$M = \frac{m}{N} \quad M_m = \frac{m_m}{N_m}$$

GROUP  
5  
DISPLAY 5

2. An insulated tank that contains 1 kg of  $O_2$  at 15°C and 300 kPa is connected to a 2-m<sup>3</sup> uninsulated tank that contains  $N_2$  at 50°C and 500 kPa. The valve connecting the two tanks is opened, and the two gases form a homogeneous mixture at 25°C. Determine (a) the final pressure in the tank, (b) the heat transfer to the surroundings, and (c) the entropy generated during this process. Assume the surrounding temperature to be  $T_0 = 25^\circ\text{C}$ .

b) Energy balance (closed system)

$$Q - W = \Delta U + \Delta KE + \Delta PE$$

$$Q = (m_{O_2} \Delta T)_{O_2} + (m_{N_2} \Delta T)_{N_2}$$

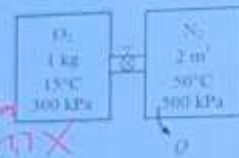
$$= m_{O_2} c_{v,O_2} (T_0 - T_{i,O_2}) + m_{N_2} c_{v,N_2} (T_0 - T_{i,N_2})$$

$$= 0.658(25 - 15) + 10.41 \times 0.743(25 - 50) = -187.2 \text{ kJ}$$

system

↑ -187.2 kJ  
of heat gained by system

$\Delta U = m_m \Delta u_m$   
 $= m_m (u_2 - u_1)_m$   
 $(m c_v (T_2 - T_1))_{O_2} \text{ or } (m c_v (T_2 - T_1))_{N_2}$



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GROUP  
5

DISPLAY 5

2. An insulated tank that contains 1 kg of  $O_2$  at 15°C and 300 kPa is connected to a 2-m<sup>3</sup> uninsulated tank that contains  $N_2$  at 50°C and 500 kPa. The valve connecting the two tanks is opened, and the two gases form a homogeneous mixture at 25°C. Determine (a) the final pressure in the tank, (b) the heat transfer to the surroundings, and (c) the entropy generated during this process. Assume the surrounding temperature to be  $T_s = 25^\circ\text{C}$ .

b) Energy balance (closed system)

$$Q - W = \Delta E_{\text{tot}} = \Delta U + \Delta KE + \Delta PE$$

$\Delta U = m_m \Delta u_m$   
 $\Delta U = m_m (u_2 - u_1)_m$   
 $\Delta U = m_m c_v (T_2 - T_1)_m$

$$Q = (m_{O_2} AT)_{O_2} + (m_{N_2} AT)_{N_2}$$

$$= m_{O_2} c_{v,O_2} (T_m - T_{1,O_2}) + m_{N_2} c_{v,N_2} (T_m - T_{1,N_2})$$

$$= 0.658(25 - 15) + 10.43 \times 0.743(25 - 50) = -187.2 \text{ kJ}$$

c) Entropy generation = Entropy change of gas mixture + Entropy change of surroundings

Mole fraction for each gas

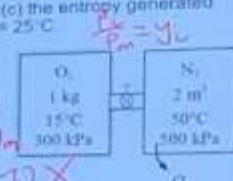
$$x_{O_2} = \frac{N_{O_2}}{N_m} = \frac{0.0312}{0.4033} = 0.0776$$

$$x_{N_2} = \frac{N_{N_2}}{N_m} = \frac{0.372}{0.4033} = 0.9224$$

$$[m c_v (T_2 - T_1)]_{O_2} + [m c_v (T_2 - T_1)]_{N_2}$$

$$\Delta S_{\text{gen}} = S_{\text{gen}}$$

$$= \Delta S_m + \Delta S_{\text{sur}}$$



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GROUP  
5  
DISPLAY 5

2. An insulated tank that contains 1 kg of  $O_2$  at 15°C and 300 kPa is connected to a 2-m<sup>3</sup> uninsulated tank that contains  $N_2$  at 50°C and 500 kPa. The valve connecting the two tanks is opened, and the two gases form a homogeneous mixture at 25°C. Determine (a) the final pressure in the tank, (b) the heat transfer to the surroundings, and (c) the entropy generated during this process. Assume the surrounding temperature to be  $T_0 = 25^\circ\text{C}$ .

Partial pressure of each gas in the mixture:

$$P_{O_2} = y_{O_2} P_m = 0.0776 \times 444.3 = 34.48 \text{ kPa}$$

$$P_{N_2} = y_{N_2} P_m = 0.9224 \times 444.3 = 409.82 \text{ kPa}$$

Entropy change of gas mixture:

$$\Delta S_m = \Delta S_{O_2} + \Delta S_{N_2}$$

$$= m_{O_2} \left( c_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right) + m_{N_2} \left( c_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right)$$

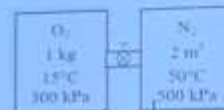
$$= 0.018 \ln \left( \frac{25 + 273}{15 + 273} \right) - 0.2598 \ln \left( \frac{34.48}{300} \right) + 10.43 \left( \ln \frac{25 + 273}{50 + 273} \right) - 0.2968 \ln \left( \frac{409.82}{500} \right)$$

$$= 0.593 + 0.2373 = 0.8303 \text{ kJ/K}$$

Entropy change of surroundings:

$$\Delta S_{surr} = \frac{Q}{T_{surr}} = \frac{183.2}{25 + 273} = 0.6324 \text{ kJ/K}$$

$$S_{gen} = \Delta S_m + \Delta S_{surr} = 0.964 \text{ kJ/K}$$



15070

# DISPLAY 5

3. A tank contains 15 kg of dry air and 0.17 kg of water vapour at 30°C and 100 kPa total pressure. Determine (a) the specific humidity, (b) the relative humidity, and (c) the volume of the tank.

Assumptions: Air and water vapour are ideal gases

a) Specific humidity:

$$\omega = \frac{m_v}{m_a} = \frac{0.17}{15} = 0.0113 \text{ kg/kg}$$

$$\phi = \frac{m_v}{m_g} = \frac{P_v}{P_g} \rightarrow P_{\text{sat}@T}$$

b) Sat. vapour properties:  $P_g = P_{\text{sat}@30^\circ\text{C}} = 4.2469 \text{ kPa}$

$$\phi = \frac{(0.622 + \omega)P_g}{0.0113 \times 100} = \frac{0.0113 \times 100}{(0.622 + 0.0113) \times 4.2469} = 0.420$$

SAMSUNG



GROUP  
5  
DISPLAY 5

3. A tank contains 15 kg of dry air and 0.17 kg of water vapour at 50°C and 100 kPa total pressure. Determine (a) the specific humidity, (b) the relative humidity, and (c) the volume of the tank.

(a) Partial pressure of dry air:

$$P_a = P - P_v = P - P_g$$

$$= 100 - 0.17 \times 0.2469 = 99.25 \text{ kPa}$$

$$P = \frac{m_a R_a T}{V}$$

$$V = \frac{m_a R_a T}{P} = \frac{15 \times 0.287 \times (50 + 273)}{99.25} = 18.29 \text{ m}^3$$

(b)  $P = \frac{P_a}{P_g} \rightarrow P_v = P_g$

$$P_a V_m = m_a R_a T_m$$

$$\text{try: } P_v V_m = m_v R_v T_m$$

$$P = P_a + P_v$$

↑  
100kPa

GROUP  
5  
DISPLAY 5

4. After a long walk in the 12°C outdoor, a person wearing glasses enters a room at 25°C and 55% relative humidity. Determine whether the glasses will become fogged.

$$T_{\text{glasses}} = 12^\circ\text{C}$$

$$\text{Sat. vapour properties: } P_g = P_{\text{sat}@25^\circ\text{C}} = 3.1698 \text{ kPa}$$

Vapour pressure of water vapour:

$$P_v = \phi P_g \\ = 0.55 \times 3.1698 = 1.743 \text{ kPa}$$

Dew point temperature of the air in the room:

$$T_{\text{dp}} = T_{\text{sat}@P_v} \\ = 15.2^\circ\text{C} > T_{\text{glasses}}$$

Yes.

$$T_{\text{dp}} > T_{\text{glasses}}$$

$$\textcircled{1} \text{ Find } P_g = P_{\text{sat}} @ T$$

$$\textcircled{2} \text{ Find } P_v = \phi P_g$$

$$\textcircled{3} \text{ Find } T_{\text{sat}} @ P_v$$

$$\downarrow \\ \text{Yes}$$



GROUP  
5

DISPLAY 5

5. Atmospheric air at a pressure of 1 atm and dry-bulb temperature of 28°C has a wet-bulb temperature of 20°C. ~~Using the psychrometric chart~~, determine (a) the relative humidity, (b) the humidity ratio, (c) the enthalpy, (d) the dew-point temperature, (e) the water vapour pressure.

a)  $\phi$   $\rightarrow$  find  $P_g$   
 (b)  $w$   $\rightarrow$  use adiab. sat. Formula  $T_1$  &  $T_2$   
 $\downarrow$   $\downarrow$   
 $T_{db}$   $T_{wb}$   
 d) Find  $P_v = \phi P_g$   
 Find  $T_{dp} = T_{sat}@P_v$   
 c)  $h = c_p T + w h_g = h_g @ T_{wb}$

