

#### **MA2011 MECHATRONICS SYSTEMS INTERFACING**

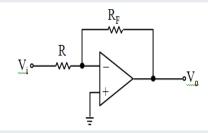
Tutorial 5

Prof. Cai Yiyu

College of Engineering
School of Mechanical and Aerospace Engineering

# Operational amplifier:

- Very large (infinite) impedance
- Very small (zero) current



Finite Loop Gain A of Inverting Amplifier

A). Show that the closed loop gain G is a function of A, R and R<sub>F</sub>

$$G = \frac{-AR_F}{AR + R + R_F}$$

(1)

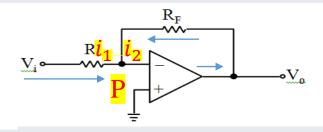
B). For large value A, G can be approximated by

$$G' = \frac{-R_F}{R}$$

(2)

#### A). Show that the closed loop gain

$$G = \frac{-AR_F}{AR + R + R_F} \quad (1)$$



#### SOLUTION: At point P

For an op-amp with infinite input resistance and zero output resistance,  $i_1 = i_2$ .

So, 
$$\frac{(V_i - V_P)}{R} = \frac{(V_P - V_o)}{R_F}$$

And 
$$R_F(V_i - V_p) = R(V_p - V_o)$$

$$V_P(R_F+R) = V_0R + V_iR_F$$

But 
$$V_P = -V_0/A$$
 Because Finite loop gain  $A = -V_0/V_P$ 

So 
$$\frac{-V_o(R+R_F)}{A} = V_o R + V_i R_F$$

$$-V_o(R + R_F + AR) = V_i A R_F$$

$$\frac{V_0}{V_i} = \frac{-AR_F}{AR + R + R_F}$$

Therefore, closed loop (op-amp) gain G

$$G = \frac{V_0}{V_i} = \frac{-AR_F}{AR + R + R_F}$$

Therefore, the closed loop gain

$$G = \frac{-AR_F}{AR + R + R_F} \tag{1}$$

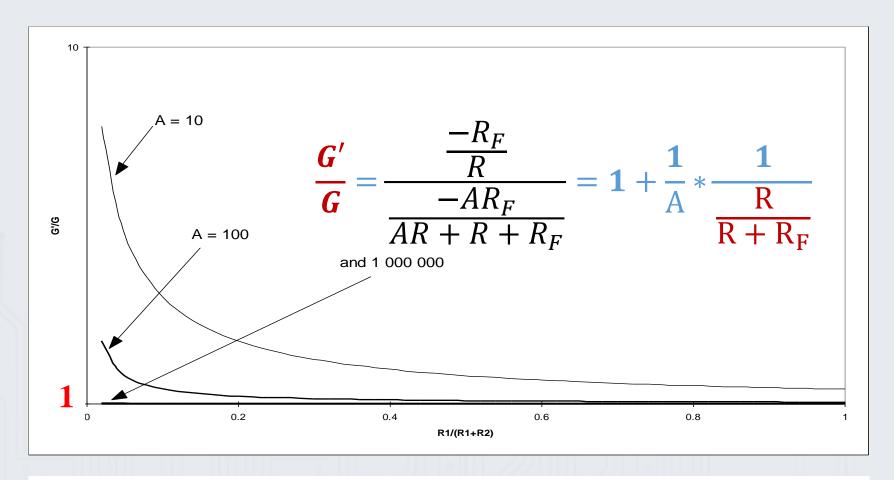
$$=\frac{-R_F}{R+\frac{R+R_F}{A}}$$

$$A \gg R + R_F$$
, or  $\frac{R + R_F}{A} \rightarrow 0$ 

$$G \to G' \equiv \frac{-R_F}{R}$$
, or  $\frac{G'}{G} \to 1$ 

B). For large value A, G can be approximated by

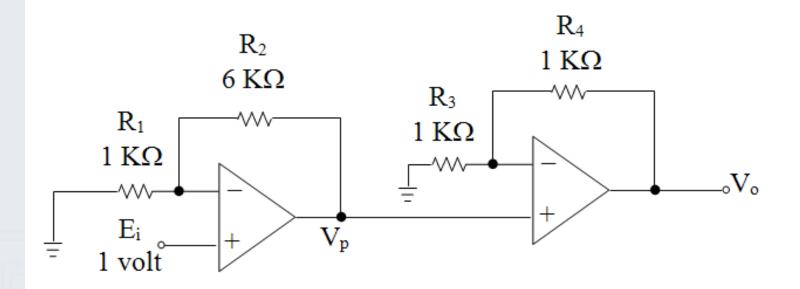
$$G' = \frac{-R_F}{R} \tag{2}$$



For high open-loop gain A (10<sup>5</sup> ~ 10<sup>6</sup>), and the values of R and R<sub>F</sub>(k $\Omega$ ~M $\Omega$ ), G can be approximated by G' =  $\frac{-R_F}{R}$ 

Find V<sub>o</sub> for the following op-amp circuits:

a) Two non-inverting amplifiers in series.



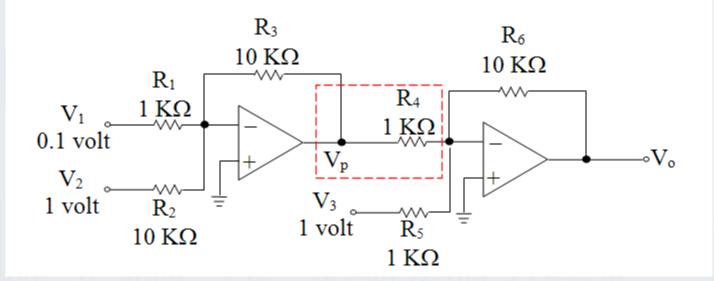
#### SOLUTION:

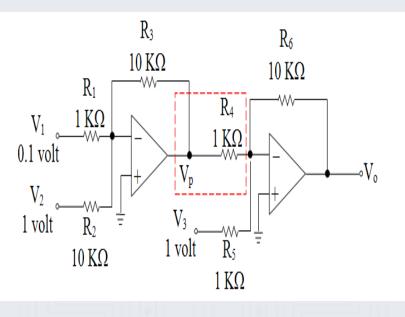
$$G = \frac{R + R_F}{R} = 1 + \frac{R_F}{R}$$
 (General equation)

$$\mathbf{V_p} = \left(1 + \frac{\mathbf{R_2}}{\mathbf{R_1}}\right) \mathbf{V_i} = \left(1 + \frac{6}{1}\right) \times 1 = 7 \mathbf{V}$$

$$\mathbf{V}_{o} = \left(1 + \frac{\mathbf{R}_{4}}{\mathbf{R}_{3}}\right) \mathbf{V}_{p} = \left(1 + \frac{1}{1}\right) \times 7 = 14 \text{ V}$$

b) Two summing amplifiers in series.





#### SOLUTION:

General equation: 
$$V_o = -\left(\frac{V_1}{R_1} + \frac{V_2}{R_2} + \cdots\right) R_F$$

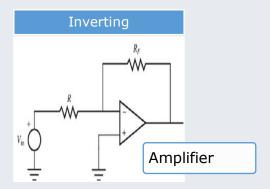
$$V_p = -\frac{R_3 V_1}{R_1} - \frac{R_3 V_2}{R_2} = -10 \times 0.1 - 1 \times 1$$

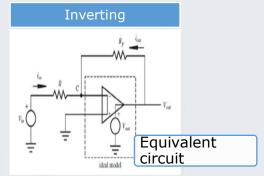
$$= -2 V$$

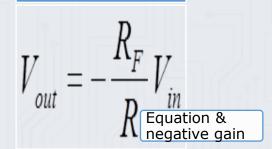
$$V_o = -\frac{R_6 V_p}{R_4} - \frac{R_6 V_3}{R_5} = -\{10 \times (-2)\} - (10 \times 1)$$

$$= 10 V$$

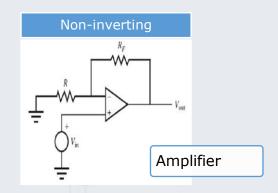
#### COMPARISON OF INVERTING AND NONINVERTING AMPLIFIER

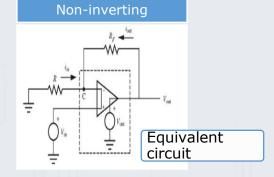


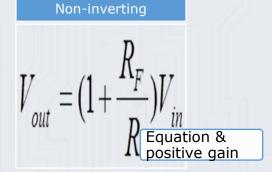




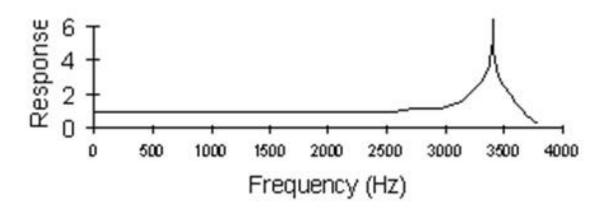
Inverting







3. An accelerometer that is used to measure the vibration of a machine has a frequency response as shown in the figure below:



The vibration signal is filtered to ensure that the vibration signal beyond 2.5 kHz does not affect the recording of the measurements.

Select an appropriate filter consisting of a resistor, with resistance R, and a capacitor, with capacitance C, that will remove the error due to the frequency response of the accelerometer. Suggest appropriate values of R and C. Sketch the frequency response of the filter, indicating all relevant parameters on the sketch.

KNOWN: To filter off signal of 2.5 kHz or more.

FIND: (i) Filter type, values of R and C, and frequency response of filter

#### SOLUTION:

As frequencies below 2.5 kHz are required and those above have to be removed, a low pass filter is required.

Cut-off frequency must be at least 2.5 kHz (required) and less than about 3 kHz, (where the accelerometer response becomes > 1).

Impedance-based relationship between frequency, resistance and capacity.

If the cut-off frequency is 2.5 kHz, 
$$f_c = \frac{1}{2\pi RC}$$

Or RC = 
$$\frac{1}{2\pi f_c}$$

So, RC = 
$$\frac{1}{2\pi \times 2500}$$
 = 6.37 x 10<sup>-5</sup> s

Choose any value of R and C such that the combination results in  $6.37 \times 10^{-5}$  s.

For example,  $R = 63.7 \text{ k}\Omega$ ,  $C = 1000 \text{ pF} (1 \text{ pF} = 10^{-12} \text{ F})$ .

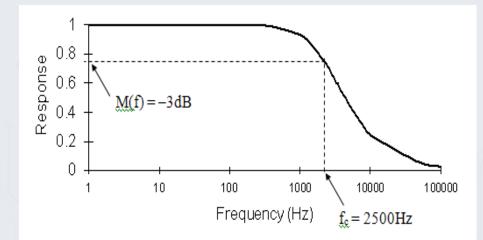
The frequency response of the filter, with the relevant parameters is:

$$\mathbf{M(f)} = \frac{1}{\sqrt{1 + (f/2500)^2}}$$

$$M(3400)_{\text{filter}} = \frac{1}{\sqrt{1 + \left(\frac{3400}{2500}\right)^2}} = 0.592.$$

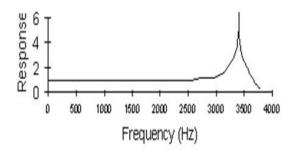
Magnitude ratio M(
$$\omega$$
)=  $\frac{1}{\sqrt{1+(\omega\tau)^2}}$   
Since  $\omega$ = 2 $\pi$ f, and  $\tau$ = 1/(2 $\pi$ f<sub>c</sub>), M(f)=  $\frac{1}{\sqrt{1+(f/fc)^2}}$ 

For 
$$f_c$$
=2500, M(2500)= $\frac{1}{\sqrt{1+(1)^2}}$ =0.707



The frequency response of the accelerometer-filter combination is:

An accelerometer that is used to measure the vibration of a machine has a frequency response as shown in the figure below:



The vibration signal is filtered to ensure that the vibration signal beyond 2.5 kHz does not affect the recording of the measurements.