# 1 Turbulent transport of momentum and heat

Turbulent velocity fluctuations can generate large momentum fluxes between different parts of a flow. A momentum flux can be thought of as a stress, turbulent momentum fluxes are commonly called Reynolds stresses.

# 1.1 The Reynolds equations

The equations of motion of an incompressible fluid are

$$\frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = \frac{1}{\rho} \frac{\partial}{\partial x_j} \tilde{\sigma}_{ij}$$
$$\frac{\partial \tilde{u}_i}{\partial x_i} = 0$$

 $\tilde{\sigma}_{ij}$ : the sress tensor.

Repeated indices: summation over all three values of the index.

Tilde ( $\tilde{}$ ): instantaneous value at  $(x_i, t)$  of a variable without Reynolds decomposition.

For Newtonian fluid,

$$\tilde{\sigma}_{ij} = -\tilde{p}\delta_{ij} + 2\mu\tilde{s}_{ij}$$

 $\tilde{p}$ : hydrodynamic pressure.

 $\mu$ : dynamic viscosity (constant).

 $\tilde{s}_{ij}$ : rate of strain,

$$\tilde{s}_{ij} = \frac{1}{2} \left( \frac{\partial \tilde{u}_i}{\partial x_j} + \frac{\partial \tilde{u}_j}{\partial x_i} \right)$$

Sub into former N-S equation,

$$\frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial \tilde{p}}{\partial x_i} + \nu \frac{\partial^2 \tilde{u}_i}{\partial x_j \partial x_j}$$

#### The Reynolds decomposition

For a steady flow,

$$\frac{\partial U_i}{\partial t} = 0$$

We can have a time average of the flow. We decompose velocity into a mean flow  $U_i$  and velocity fluctuations  $u_i$ ,

$$\tilde{u}_i = U_i + u_i$$

 $U_i$  should be a time average, thus

$$U_i = \lim_{T \to \infty} \frac{1}{T} \int_{t_0}^{t_0 + T} \tilde{u}_i dt$$

and then the average of fluctuation term

$$\bar{u}_i = \lim_{T \to \infty} \frac{1}{T} \int_{t_0}^{t_0 + T} (tildeu_i - U_i) dt \equiv 0$$

The mean value of a spatial derivative of a variable is equal to the corresponding spatial derivative of the mean value of that variable, in other words, we are able to change the order of averaging and taking derivatives.

$$\frac{\partial^{\bar{-}}_{i}_{i}}{\partial x_{j}} = \frac{\partial U_{i}}{\partial x_{j}}$$
$$\frac{\partial \bar{u}_{i}}{\partial x_{j}} = \frac{\partial}{\partial x_{j}} \bar{u}_{i} = 0$$

For the pressure  $\tilde{p}$  and the stress  $\tilde{\sigma}_{ij}$ , we can also decompose them in a similar way.

$$\begin{split} \tilde{p} &= P + p \\ \bar{p} &\equiv 0 \\ \tilde{\sigma}_{ij} &= \Sigma_{ij} + \sigma_{ij} \\ \bar{\sigma}_{ij} &\equiv 0 \end{split}$$

Mean stress tensor  $\Sigma_{ij}$  is given by

$$\Sigma_{ij} = -P\delta_{ij} + 2\mu S_{ij}$$

And stress fluctuations  $\sigma_{ij}$  is given by

$$\sigma_{ij} = -p\delta_{ij} + 2\mu s_{ij}$$

Whre  $S_{ij}$  and  $s_{ij}$  are the mean strain rate and strain-rate fluctuations,

$$S_{ij} = \frac{1}{2} \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)$$
$$s_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

#### Correlated variables

An example (the proof is simple):

$$\tilde{u}_i \overline{\tilde{u}}_j = (U_i + u_i) (U_j + u_j)$$
  
=  $U_i U_J + u_i u_j$ 

If  $u_i\bar{u}_j\neq 0$ , then they are said to be correlated; if  $u_i\bar{u}_j=0$ , then they are uncorrelated.

Correlation coefficient:

$$c_{ij} = \frac{u_i \bar{u}_j}{\sqrt{\bar{u}_i^2 \bar{u}_j^2}}$$

Standard deviation or root-mean-square (rms) amplitude (denoted by '):

$$u_i' = \sqrt{\bar{u_i^2}}$$

#### Equations for the mean flow

Decompose the equation of continuity  $\frac{\partial \tilde{u_i}}{\partial x_i} = 0$ , we have

$$\frac{\partial U_i}{\partial x_i} + \frac{\partial u_i}{\partial x_i} = 0$$

Take average of all terms,  $\partial u_i/\partial x_i$  vanishes, thus  $\partial U_i/\partial x_i=0$ . Sub back into the former equation, then  $\partial u_i/\partial x_i=0$ .

The mean flow is incompressible, and the turbulent fluctuations are also incompressible.

Go back to the equations of motion, we take average

$$U_{j}\frac{\partial U_{i}}{\partial x_{i}} + u_{j}\frac{\bar{\partial}u_{i}}{\partial x_{j}} = \frac{1}{\rho}\frac{\partial}{\partial x_{j}}\Sigma_{ij}$$

Where

$$u_j \frac{\partial u_i}{\partial x_j} = \overline{\frac{\partial}{\partial x_j}} u_i \overline{u}_j$$

represents the mean transport of fluctuating momentum.

Rearrange, we have the Reynolds momentum equation:

$$U_{j}\frac{\partial U_{i}}{\partial x_{j}} = \frac{1}{\rho} \frac{\partial}{\partial x_{j}} \left( \Sigma_{ij} - \rho \bar{u_{i}} u_{j} \right)$$

Thus, we have the total mean stress  $T_{ij}$  defined as

$$T_{ij} = \Sigma_{ij} - \rho \bar{u_i} u_j = -P \delta_{ij} + 2\mu S_{ij} - \rho \bar{u_i} u_j$$

#### The Reynolds stress

The Reynolds stress tensor, representing the contribution of the turbulent motion to the mean stress tensor,

$$\tau_{ij} = -\rho u_i u_j$$

The diagonal components are normal stresses, they contribute little to the transport of mean momentum; the off-diagonal components are shear stresses,  $\tau_{ij} = \tau_{ji}$ .

## Turbulent transport of heat

We start from the diffusion equation for heat:

$$\frac{\partial \tilde{\theta}}{\partial t} + \tilde{u_j} \frac{\partial \tilde{\theta}}{\partial x_j} = \gamma \frac{\partial^2 \tilde{\theta}}{\partial x_j \partial x_j}$$

In the same way, we decompose the temperature  $\tilde{\theta}$ :

$$\tilde{\theta} = \Theta + \theta, \bar{\theta} = 0, \partial \Theta / \partial t = 0$$

Then we have

$$\begin{split} U_{j} \frac{\partial \Theta}{\partial x_{j}} &= \frac{\partial}{\partial x_{j}} \left( -\theta \bar{u}_{j} + \gamma \frac{\partial \Theta}{\partial x_{j}} \right) \\ Q_{j} &= c_{p} \rho \left( \theta u_{j} - \bar{\gamma \partial \Theta} / \partial x_{j} \right) \end{split}$$

The transport of heat and momentum are analogical, thus we believe that in turbulence, they are transported in the same way.

# 1.2 Elements of the kinetic theory of gases

#### Pure shear flow

A steady pure shear flow, where  $U_2 = U_3 = 0$ ,  $U_1 = U_1(x_2)$ . The viscous shear stress

$$\sigma_{12} = \sigma_{21} = \mu \partial U_1 / \partial x_2$$

It must result from molecular transport of momentum in the  $x_2$  direction. Here,  $v_1$ ,  $v_2$  are the velocity of a molecule relative to the mean flow.

$$\sigma_{12} = -\rho \bar{v_1} v_2$$

## Molecular collisions

Mean free path:  $\xi$ .