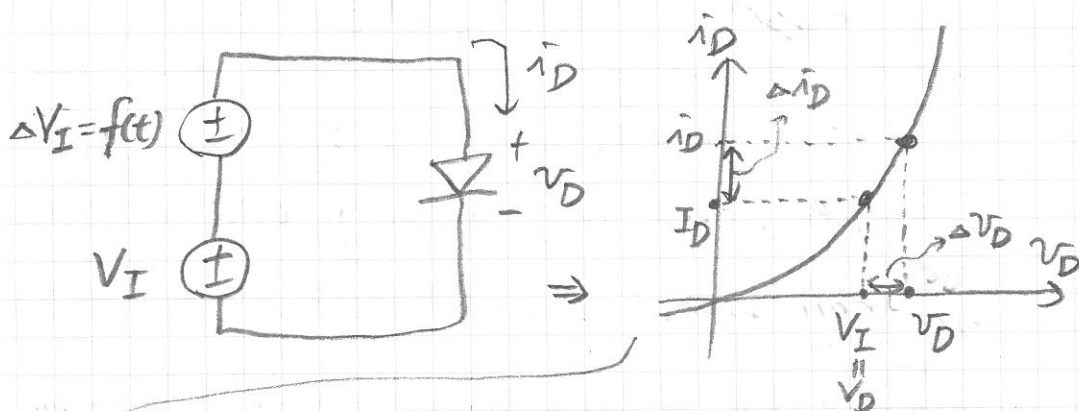


★ Small-Signal Analysis for Nonlinear Devices P43

- In many sensor applications and most audio amplifiers, the input voltage/current to a circuit often consists of two parts:

- ① a time-invariant source (large signal)
- ② a time-varying source (small signal)



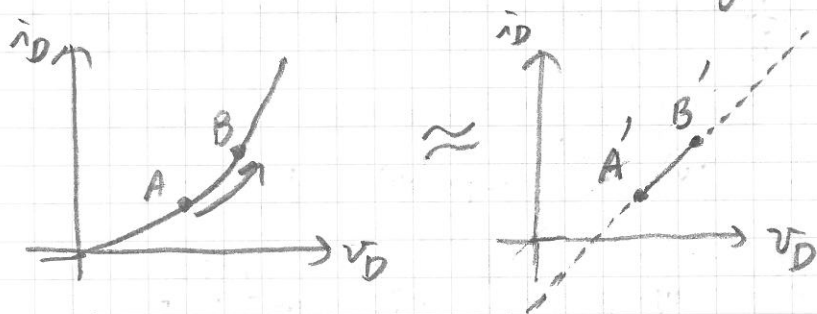
The large signal is used to determine the region of operation (i.e., which part of the \hat{i}_D - v_D curve), and the small signal is the "real" input (e.g., those induced by human voice, as in the case of a microphone).

that

$$v_D = \underset{\substack{\uparrow \\ \text{large}}}{V_I} + \underset{\substack{\uparrow \\ \text{small signal}}}{\Delta v_D}$$

$$\hat{i}_D = I_D + \Delta \hat{i}_D$$

P44 as we will see, moving along a small distance on "the $i_D - v_D$ curve" can be approximated as moving along a small distance on "a straight line"

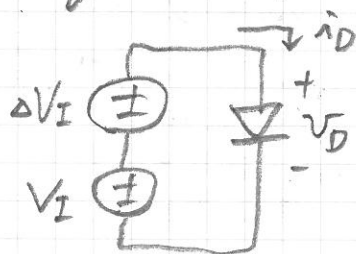


Therefore, we may simplify our analysis of small signal by considering the signal's response on a nonlinear device as if it is the response on a linear device (resistor).

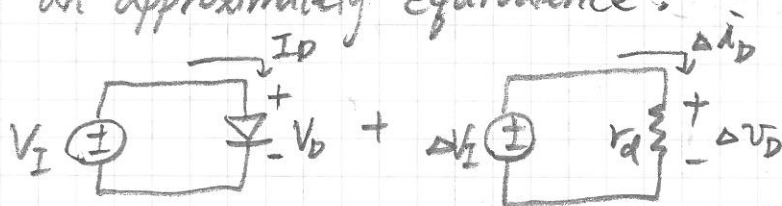
Review P13, where we've shown that the $i-v$ characteristic of a resistor on the $i-v$ plot is a straight line; further, the slope of the line is equal to the reciprocal of the resistance (R) of the resistor.

Now, a question is: how do we determine the resistance of that linear device?

Let r_d be the resistance of the linear device. Using small-signal analysis, we essentially transform the original circuit



into an approximately equivalence:

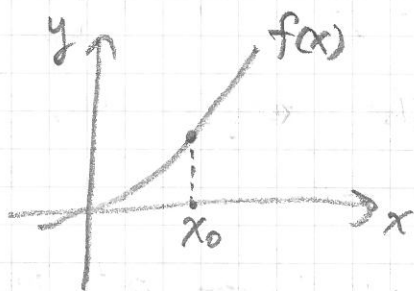


where $i_D = I_D + \Delta i_D$

$$\frac{V_{THE}}{I_D}$$

Now, let's see how to determine r_d !

We use Taylor's Theorem, which provides a way to approximate a curve near a certain point $x = x_0$:



$$y = f(x) = f(x)|_{x=x_0} + f'(x)|_{x=x_0} (x-x_0) + \frac{1}{2!} f''(x)|_{x=x_0} (x-x_0)^2 + \frac{1}{3!} f'''(x)|_{x=x_0} (x-x_0)^3 + \dots$$

P46 in our case of a nonlinear diode,
recall that

$$i_D = I_s (e^{v_D/v_{THER}} - 1) = f(v_D)$$

↑
we define it

$$\Rightarrow i_D \underset{v_D \text{ near } V_D}{=} f(v_D) \Big|_{v_D=V_D} + f'(v_D) \Big|_{v_D=V_D} (v_D - V_D) \\ + \frac{1}{2!} f''(v_D) \Big|_{v_D=V_D} (v_D - V_D)^2 \\ + \frac{1}{3!} f'''(v_D) \Big|_{v_D=V_D} (v_D - V_D)^3 + \dots$$

$$= f(v_D) \Big|_{v_D=V_D} + (v_D - V_D) \left(f'(v_D) \Big|_{v_D=V_D} \right. \\ \left. + \frac{1}{2!} f''(v_D) \Big|_{v_D=V_D} (v_D - V_D) \right. \\ \left. + \frac{1}{3!} f'''(v_D) \Big|_{v_D=V_D} (v_D - V_D)^2 \right. \\ \left. + \dots \right)$$

we choose to ignore these terms

using the chain rule, we get $f'(v_D) = \frac{I_s}{v_{THER}} e^{v_D/v_{THER}}$

$$\Rightarrow i_D \underset{v_D \text{ near } V_D}{=} \underbrace{f(v_D) \Big|_{v_D=V_D}} + \underbrace{(v_D - V_D) \cdot \frac{I_s}{v_{THER}} e^{v_D/v_{THER}} \Big|_{v_D=V_D}} \\ = \underbrace{I_s (e^{V_D/v_{THER}} - 1)} + \underline{\underline{\Delta v_D \cdot \frac{I_s}{v_{THER}} \cdot e^{V_D/v_{THER}}}}$$

since we know that

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$$e^{V_D/V_{THER}} \gg 1$$

so we can think of $e^{V_D/V_{THER}} \approx e^{V_D/V_{THER}} - 1$

With that, we may rewrite the equation as

$$\hat{I}_D = I_s (e^{V_D/V_{THER}} - 1) + \Delta V_D \frac{I_s}{V_{THER}} (e^{V_D/V_{THER}} - 1)$$

$v_D \text{ near } V_D$

Now, by observation we see $I_s (e^{V_D/V_{THER}} - 1) = I_D$

$$\text{Thus, } \hat{I}_D = I_D + \frac{\Delta V_D}{V_{THER}} I_D$$

$v_D \text{ near } V_D$

Compare to $\hat{I}_D = I_D + \Delta \hat{I}_D$, we have $\Delta \hat{I}_D = \frac{\Delta V_D}{V_{THER}} I_D$

Think in terms of relation of $\Delta \hat{I}_D$ and ΔV_D
and we may choose to define

$$r_d = \frac{V_{THER}}{I_D} \quad **$$

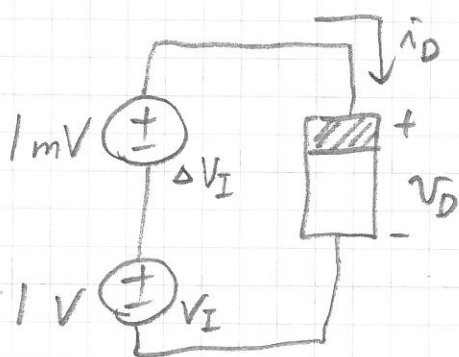
In the hindsight, we may generalize our result by saying that for an arbitrary nonlinear element, we have


$$r_d = \frac{1}{f'(V_D)|_{V_D=V_D}} = \frac{1}{\frac{df(V_D)}{dV_D} |_{V_D=V_D}} \quad ** \text{ (finally!)} \quad = V_D$$

P48

Example :

find $\hat{i}_D = ?$



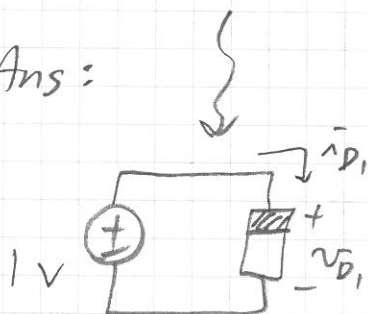
recall that for  (P35)

$$\hat{i}_D = K \cdot v_D^2 \text{ for } v_D > 0$$

and here we suppose

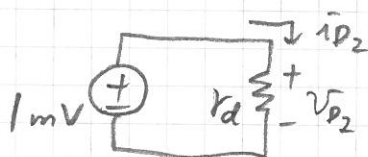
$$K = 1 \text{ mA}/\text{V}^2$$

Ans :



$$v_{D1} = 1 \text{ (KVL)}$$

$$\Rightarrow \hat{i}_{D1} = K \cdot v_{D1}^2 = 1 \text{ mA}$$



$$v_{D2} = 1 \text{ mV (KVL)}$$

$$r_d = \frac{1}{f'(v_D)|_{v_D=v_D}} = \frac{1}{2 \cdot K \cdot v_D}|_{v_D=1 \text{ V}}$$

$$= 500 \Omega$$

$$\Rightarrow \hat{i}_{D2} = \frac{v_{D2}}{r_d} = 2 \mu\text{A}$$

$$\Rightarrow \hat{i}_D = \hat{i}_{D1} + \hat{i}_{D2} = 1.002 \text{ mA}^*$$