



Universität Stuttgart

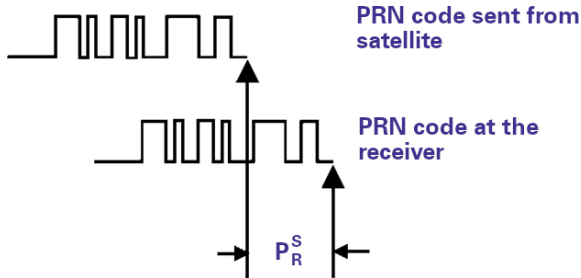
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Satellite Navigation

Observables and error budget

Observables and error budget



- A GNSS receiver measures the time offset it needs to apply to its replica of the code to reach maximum correlation with received signal
- Thus, it is measuring the time difference between when a signal was transmitted (based on satellite clock) and when it was received (based on receiver clock).
- If the satellite and receiver clocks were synchronized, this would be a measure of range
- since they are not synchronized, it is called "pseudorange" P_R^S

Observables and error budget

Pseudorange Pseudorange P_k^p is defined as

$$P_k^p = (\tilde{t}_k - \tilde{t}^p) \cdot c \quad (6.1)$$

where subscript k denotes the receiver and superscript p the satellite. \tilde{t}_k is the reception in receiver clock time, \tilde{t}^p is the transmission epoch and c is the speed of light.

However, the true range (expressed in units of time) between the satellite and the receiver is not equal to P_k^p since the receiver and satellite clocks are offset by small time differences due to clock offsets.

$$\begin{aligned} \tilde{t}_k &= t_k + \tau_k \\ \tilde{t}^p &= t^p + \tau^p \end{aligned} \quad (6.2)$$

t_k and t^p are true times; τ_k and τ^p are the clock offsets.

Substituting (6.2) into (6.1) yields

$$P_k^p = [(t_k - t^p) + (\tau_k - \tau^p)] \cdot c \quad (6.3)$$

Observables and error budget

Since signals propagate slower than the speed of light in the ionosphere and troposphere, Eq. (6.3) can be written as

$$P_k^p = \rho_k^p + (\tau_k - \tau^p) \cdot c + \underbrace{I_k^p}_{\text{ionosphere delay}} + \underbrace{A_k^p}_{\text{troposphere delay}} \quad (6.4)$$

where ρ_k^p is the true (geometrical) range between receiver k and satellite p . This range is equal to the Euclidian distance computed from the position of the satellite at transmission time t_p and the position of the receiver at the time t the signal was captured.

Dropping now the index k , i.e. focusing on a single receiver, we obtain

$$\rho^p(t, t^p) = \sqrt{[X^p(t^p) - x(t)]^2 + [Y^p(t^p) - y(t)]^2 + [Z^p(t^p) - z(t)]^2} \quad (6.5)$$

which implies that we have four unknowns (three position components + the receiver clock)

Observables and error budget

Ignoring tropospheric and ionospheric delays, we can set up a non-linear equation system for N pseudorange observations collected at epoch t

$$\begin{aligned} P^1 &= \sqrt{(X^1 - x)^2 + (Y^1 - y)^2 + (Z^1 - z)^2} + c\tau - c\tau^1 + \epsilon_1 \\ P^2 &= \sqrt{(X^2 - x)^2 + (Y^2 - y)^2 + (Z^2 - z)^2} + c\tau - c\tau^2 + \epsilon_2 \\ &\vdots \\ P^N &= \sqrt{(X^N - x)^2 + (Y^N - y)^2 + (Z^N - z)^2} + c\tau - c\tau^N + \epsilon_N \end{aligned} \quad (6.6)$$

which implies that we have four unknowns (three position components + the receiver clock).

Eq. (6.6) is non-linear in position coordinates (x, y, z) and the terms ϵ_k denote the (random) noise contribution to a pseudorange observation. Linearization of (6.5) of the pseudorange equations yields,

$$\begin{aligned} P^k(x, y, z, \tau) = & \underbrace{P^k(x_0, y_0, z_0, \tau_0)}_{P^k_{\text{computed}}} + \underbrace{(x - x_0)}_{\Delta x} \frac{\partial P^k}{\partial x} + \underbrace{(y - y_0)}_{\Delta y} \frac{\partial P^k}{\partial y} + \\ & + \underbrace{(z - z_0)}_{\Delta z} \frac{\partial P^k}{\partial z} + \underbrace{(\tau - \tau_0)}_{\Delta \tau} \frac{\partial P^k}{\partial \tau} \end{aligned} \quad (6.7)$$

Observables and error budget

$$\begin{aligned}\Delta P^k &= P_{\text{observed}}^k - P_{\text{computed}}^k \\ &= \frac{\partial P^k}{\partial x} \Delta x + \frac{\partial P^k}{\partial y} \Delta y + \frac{\partial P^k}{\partial z} \Delta z + \frac{\partial P^k}{\partial \tau} \Delta \tau + \epsilon\end{aligned}\quad (6.8)$$

In matrix notation

$$\Delta P^k = \begin{pmatrix} \frac{\partial P^k}{\partial x} & \frac{\partial P^k}{\partial y} & \frac{\partial P^k}{\partial z} & \frac{\partial P^k}{\partial \tau} \end{pmatrix} \cdot \begin{pmatrix} \Delta x \\ \Delta y \\ \Delta z \\ \Delta \tau \end{pmatrix} + \epsilon \quad (6.9)$$

Thus, the equation array (6.6) can be written as

$$\Delta P = \underbrace{\begin{pmatrix} \frac{x_0 - X^1}{\rho^1} & \frac{y_0 - Y^1}{\rho^1} & \frac{z_0 - Z^1}{\rho^1} & c \\ \frac{x_0 - X^2}{\rho^2} & \frac{y_0 - Y^2}{\rho^2} & \frac{z_0 - Z^2}{\rho^2} & c \\ \vdots & \vdots & \vdots & \vdots \\ \frac{x_0 - X^N}{\rho^N} & \frac{y_0 - Y^N}{\rho^N} & \frac{z_0 - Z^N}{\rho^N} & c \end{pmatrix}}_A \cdot \underbrace{\begin{pmatrix} \Delta x \\ \Delta y \\ \Delta z \\ \Delta \tau \end{pmatrix}}_{\Delta \mathbf{x}} + \underbrace{\begin{pmatrix} \epsilon_1 \\ \epsilon_2 \\ \vdots \\ \epsilon_N \end{pmatrix}}_{\epsilon} \quad (6.10)$$

Observables and error budget

In case of $N > 4$ Eq. (6.10) poses an over-determined problem and Δx can be solved by a least-squares adjustment

$$\Delta x = \underbrace{(A^T A)^{-1}}_{Q_{xx}} A^T \Delta P \quad (6.11)$$

where Q_{xx} is the cofactor matrix of the corrections Δx which relates to the covariance matrix Σ_{xx} by

$$\Sigma_{xx} = \sigma_r^2 Q_{xx} = \sigma_r^2 \begin{bmatrix} q_{xx} & q_{xy} & q_{xz} & q_{x\tau} \\ q_{yx} & q_{yy} & q_{yz} & q_{y\tau} \\ q_{zx} & q_{zy} & q_{zz} & q_{z\tau} \\ q_{\tau x} & q_{\tau y} & q_{\tau z} & q_{\tau\tau} \end{bmatrix} \quad (6.12)$$

where σ_r is the measurement accuracy of a single pseudorange observation.

In GNSS applications (especially in real-time applications in which positions are determined "instantaneously"), precision is represented by **Dilution of Precision (DOP)** values.

Observables and error budget

- PDOP: Overall 3D position precision

$$\sigma_P = \sigma_r \underbrace{\sqrt{q_{xx} + q_{yy} + q_{zz}}}_{\text{PDOP}}$$

- HDOP: 2D position precision (NB: you need to transform the covariance in the local coordinate system!)

$$\sigma_H = \sigma_r \underbrace{\sqrt{q_{nn} + q_{ee}}}_{\text{HDOP}}$$

- VDOP: vertical position precision (NB: you need to transform the covariance in the local coordinate system!)

$$\sigma_V = \sigma_r \underbrace{\sqrt{q_{uu}}}_{\text{VDOP}}$$

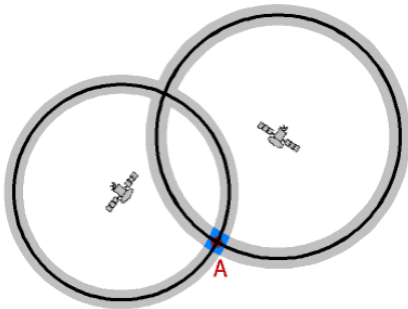
- TDOP: time precision

$$\sigma_T = \sigma_r \underbrace{\sqrt{q_{\tau\tau}}}_{\text{TDOP}}$$

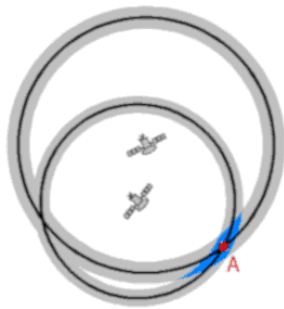
How is DOP related to the geometry? What is a "good" or "bad" geometry?

Observables and error budget

Geometric considerations



"good" geometry

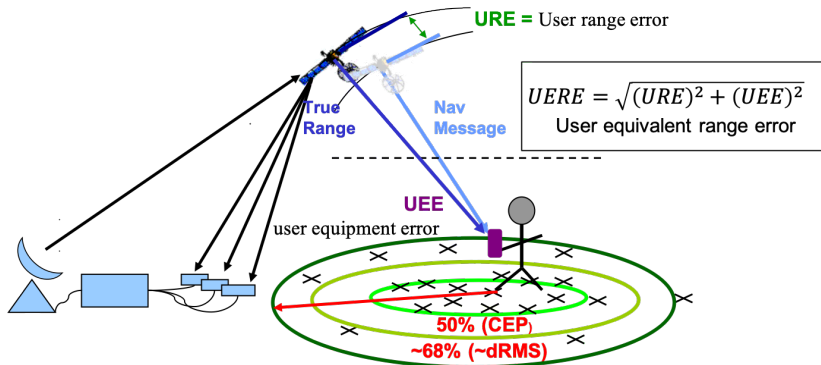


"bad" geometry

The DOP factors can be computed from the geometry.
E.g. see this planning tool <https://www.gnssplanning.com/>

Observables and error budget

Accuracy



Observables and error budget

Typical Pre-2000 GPS Error Budget σ_r (with Selective Availability)

Error Source	One-sigma Error (meters)		
	Bias	Random	Total
Ephemeris	1.0	0.0	1.0
Satellite clock	20.0	0.7	20.0
Ionosphere	4.0	0.5	4.0
Troposphere	0.5	0.0	0.5
Multipath	0.2	0.2	0.3
Receiver noise	0.0	0.1	0.1
<hr/>			
User equivalent range error, RME	20.5	0.9	20.5
Filtered UERE, RMS	20.5	0.4	20.5
<hr/>			
Vertical one-sigma errors - VDOP = 1.7			34.8
Horizontal one-sigma errors - HDOP = 1.0			20.5

Observables and error budget

Typical Single-Frequency Error Budget σ_T (no Selective Availability)

Error Source	One-sigma Error (meters)		
	Bias	Random	Total
Ephemeris	0.8	0.0	0.8
Satellite clock	1.0	0.0	1.0
Ionosphere*	7.0	0.0	7.0
Troposphere	0.2	0.0	0.2
Multipath	0.2	0.2	0.3
Receiver noise	0.0	0.1	0.1
<hr/>			
User equivalent range error, RME	7.1	0.2	7.1
Filtered UERE, RMS	7.1	0.1	7.1
<hr/>			
Vertical one-sigma errors - VDOP = 1.7			12.1
Horizontal one-sigma errors - HDOP = 1.0			7.1

* Note that residual ionospheric delay errors tend to be highly correlated among satellites, and thus observed position-domain errors tend to be less than predicted by DOP UERE.

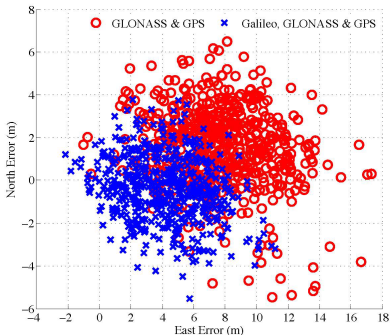
Observables and error budget

- The equation for the pseudorange uses the true range and corrections applied for propagation delays because the propagation velocity is not the in-vacuum value, c , 299 792 458 m/s
- To convert times to distance c is used and then corrections applied for the actual velocity not equaling c .
- The true range is related to the positions of the ground receiver and satellite.
- Also need to account for noise in measurements
- Pseudorange noise (random and not so random errors in measurements) contributions:
 - Correlation function width: The width of the correlation is inversely proportional to the bandwidth of the signal. Therefore the 1 MHz bandwidth of C/A code produces a peak $1\ \mu\text{s}$ wide (300m) compared to the P(Y) code 10 MHz bandwidth which produces $0.1\ \mu\text{s}$ peak (30 m) Rough rule is that peak of correlation function can be determined to 1% of width (with care). Therefore 3 m for C/A code and 0.3 m for P(Y) code.
 - Thermal noise: Effects of other random radio noise in the GPS bands Since C/A code has narrower bandwidth, tracking it in theory has less thermal noise power than the P(Y) code. Thermal noise is general smallest effect
 - Multipath: see previous lecture

Observables and error budget

Summary: Code phase/pseudorange observations

- The main noise sources are related to reflected signals and tracking approximations.
- High quality receiver: noise about 10 cm
- Low cost receiver: noise is a few meters (depends on surroundings and antenna)
- In general: C/A code pseudoranges are of similar quality to P(Y) code ranges. C/A can use narrowband tracking which reduces amount of thermal noise



Observables and error budget

Carrier phase measurements

- Carrier phase measurements are similar to pseudorange in that they are the difference in phase between the transmitting and receiving oscillators. Integration of the oscillator frequency gives the clock time.
- Basic notion in carrier phase (in cycles):

$$\varphi = f\Delta t \quad (6.13)$$

where ϕ is phase and f is frequency

- The "Big problem" is how to know the number of cycles in the phase measurements

$$\Phi_k^p + N_k^p = \varphi_k - \varphi^p \quad (6.14)$$

where φ corresponds to the true phase state of the receiver k and satellite p and N represents the (unknown) number of integer cycles.

Dropping the index for the receiver and re-arranging Eq. (6.14) we obtain

$$\Phi^p(\tilde{t}) = \varphi(\tilde{t}) - \varphi^p(\tilde{t}^p) - N^p \quad (6.15)$$

whereas N is constant over time as long as the receiver does not loose phase lock.

Observables and error budget

Carrier phase measurements In general both, the receiver and the satellite phases are expressed as the sum of a time varying part and a constant phase offset, i.e.

$$\varphi(\tilde{t}) = f_0 \cdot \tilde{t} + \varphi_0 \qquad \varphi^p(\tilde{t}^p) = f_0 \cdot \tilde{t}^p + \varphi_0^p$$

Thus, the observed carrier phase can be denoted as

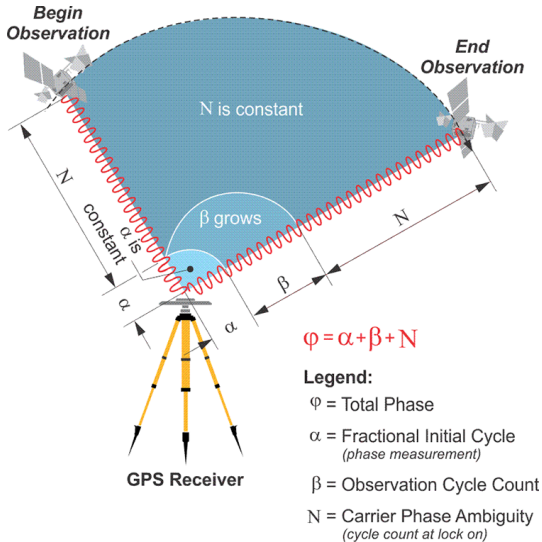
$$\begin{aligned} \Phi^p(\tilde{t}) &= f_0 \cdot \tilde{t} + \varphi_0 - f_0 \cdot \tilde{t}^p - \varphi_0^p - N^p \\ &= f_0(\tilde{t} - \tilde{t}^p) + \varphi_0 - \varphi_0^p - N^p \end{aligned} \tag{6.16}$$

Multiplication of (6.16) with the corresponding wavelength λ_0 yields the carrier phase observation in units of distance, i.e.

$$\begin{aligned} L^p(\tilde{t}) &= \lambda_0 \Phi^p(\tilde{t}) \\ &= \lambda_0 f_0(\tilde{t} - \tilde{t}^p) + \lambda_0(\varphi_0 - \varphi_0^p - N^p) \\ &= c(\tilde{t} - \tilde{t}^p) + \underbrace{\lambda_0(\varphi_0 - \varphi_0^p - N^p)}_{B^p} \\ &= \rho^p(t, t^p) + c\tau - c\tau^p + A^p - I^p + B^p \end{aligned} \tag{6.17}$$

Observables and error budget

The carrier phase observations



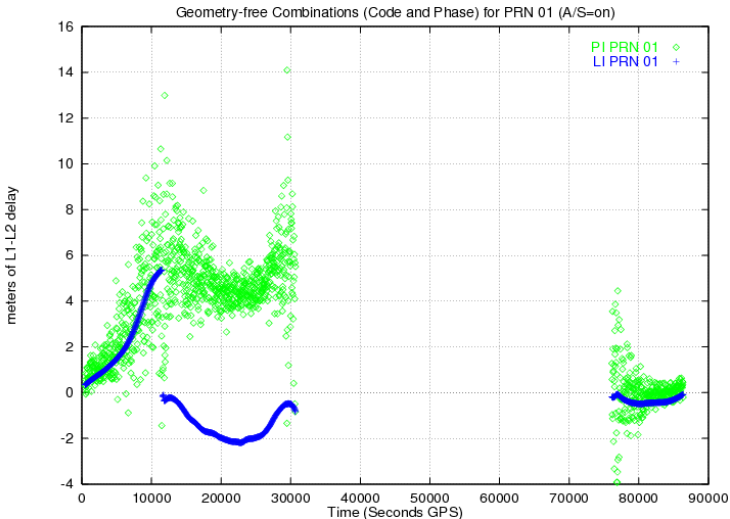
Observables and error budget

The carrier phase observations

- When carrier phase is used it is converted to distance using the standard L1 and L2 frequencies and vacuum speed of light.
- Clock terms are introduced to account for difference between true frequencies and nominal frequencies. As with range ionospheric and atmospheric delays account for propagation velocity
- Nominally carrier phase can be measured to 1% of wavelength (2mm L1 and 2.4 mm L2)
- Also effected by multipath, ionospheric delays (30m), atmospheric delays (3-30m).
- Since carrier phase is more precise than range, more effects need to be carefully accounted for with phase.
- Precise and consistent definition of time of events is one the most critical areas
- In general, carrier phase can be treated like pseudorange (code phase) measurements with an unknown offset due to cycles and offsets of oscillator phases.

Observables and error budget

Code vs. carrier phase observations (NB: Shown here are the L1-L2 / P1-P2 differences!)



Observables and error budget

GNSS data formats

- National Marine Electronics Association (NMEA) Format
 - NMEA is used to output measurement data from a sensor in a pre-defined ASCII format
 - in the case of GNSS, it outputs position, velocity, time and satellite related data
 - NMEA sentences (output) begins with a "Talker ID" and "Message Description"
 - Example:
\$GPGGA,123519,4807.038,N,01131.000,E,1,08,0.9,545.4,M,46.9,M,,*47

which decodes to:

Global Positioning System Fix Data Fix (1) taken at 12:35:19 UTC Latitude 48 deg 07.038' N Longitude 11 deg 31.000' E,

other fields:

08 ... Number of satellites being tracked

0.9 ... Horizontal dilution of position

545.4,M ... Altitude, Meters, above mean sea level

46.9,M ... Height of geoid (mean sea level) above WGS84 ellipsoid

Observables and error budget

GNSS observation formats

- The **Receiver Independent Exchange (RINEX)** format allows to exchange raw satellite data among different types of receivers
- RINEX only provides Raw Data. It does not provide position output.
- Raw data consists of pseudorange, carrier phase, Doppler, SNR
- RINEX basically consists of two data types
 - *.N files for satellite ephemeris and related data. Also called Navigation Data.
 - *.O files for observational data like pseudorange, carrier Phase, doppler, SNR. Also called Observation Data
- Two format versions in use currently
- RINEX 2.11, still used for many applications, does not support all modern GNSS signals
Format description: <ftp://igs.org/pub/data/format/rinex211.txt>
- RINEX 3.XX, very flexible, support all GNSS signal types
Format description: <ftp://igs.org/pub/data/format/rinex303.pdf>

Observables and error budget

RINEX 2.11 navigation file example

```
2.11          N: GPS NAV DATA          RINEX VERSION / TYPE
XXRINEXN V2.10      AIUB          3-SEP-99 15:22      PGM / RUN BY / DATE
EXAMPLE OF VERSION 2.11 FORMAT      COMMENT
.1676D-07 .2235D-07 -.1192D-06 -.1192D-06      ION ALPHA
.1208D+06 .1310D+06 -.1310D+06 -.1966D+06      ION BETA
.133179128170D-06 .107469588780D-12 552960 1025 DELTA-UTC: A0,A1,T,W
13      LEAP SECONDS
      END OF HEADER
6 99 9 2 17 51 44.0 -.839701388031D-03 -.165982783074D-10 .000000000000D+00
.910000000000D+02 .934062500000D+02 .116040547840D-08 .162092304801D+00
.484101474285D-05 .626740418375D-02 .652112066746D-05 .515365489006D+04
.409904000000D+06 -.242143869400D-07 .329237003460D+00 -.596046447754D-07
.111541663136D+01 .326593750000D+03 .206958726335D+01 -.638312302555D-08
.307155651409D-09 .000000000000D+00 .102500000000D+04 .000000000000D+00
.000000000000D+00 .000000000000D+00 .000000000000D+00 .910000000000D+02
.406800000000D+06 .000000000000D+00
13 99 9 2 19 0 0.0 .490025617182D-03 .204636307899D-11 .000000000000D+00
.133000000000D+03 -.963125000000D+02 .146970407622D-08 .292961152146D+01
-.498816370964D-05 .200239347760D-02 .928156077862D-05 .515328476143D+04
.414000000000D+06 -.279396772385D-07 .243031939942D+01 -.558793544769D-07
.110192796930D+01 .271187500000D+03 -.232757915425D+01 -.619632953057D-08
-.785747015231D-11 .000000000000D+00 .102500000000D+04 .000000000000D+00
.000000000000D+00 .000000000000D+00 .000000000000D+00 .389000000000D+03
.410400000000D+06 .000000000000D+00
```

Observables and error budget

RINEX 2.11 observation data - header

2.11	OBSERVATION DATA	G (GPS)	RINEX VERSION / TYPE
teqc 20110ct11		20111023 09:34:07UTC	PGM / RUN BY / DATE
Linux 2.4.20-8 Pentium IV gcc -static Linux 486/DX+			COMMENT
BIT 2 OF LLI FLAGS DATA COLLECTED UNDER A/S CONDITION			COMMENT
INSA (COGO code)			COMMENT
INSA			MARKER NAME
INSA			MARKER NUMBER
-Unknown-	-Unknown-		OBSERVER / AGENCY
4925K35627	TRIMBLE NETR8	4.14	REC # / TYPE / VERS
n	TRM55971.00	NONE	ANT # / TYPE
4157188.6232	671202.3189	4774769.4135	APPROX POSITION XYZ
0.0000	0.0000	0.0000	ANTENNA: DELTA H/E/N
1	1		WAVELENGTH FACT L1/2
4	C1	L1	# / TYPES OF OBSERV
15			LEAP SECONDS
SNR is mapped to RINEX snr flag value [0-9]			COMMENT
L1 & L2: min(max(int(snr_dBHz/6), 0), 9)			COMMENT
2011	10	21	TIME OF FIRST OBS
21	0	0.0000000	END OF HEADER
		GPS	

Observables and error budget

RINEX 2.11 observation data - observations

```
:
END OF HEADER
11 10 21 21 0 0.0000000 0 11G13G32G17G20G04G07G23G31G10G30G02
20155765.0784 105919197.42048 817.1844 49.6004
24807272.2424 130363271.39747 -2984.4964 42.7004
24583721.500 129188341.904 6 -3155.723 41.100
22156274.0784 116432358.94747 -2734.5274 47.8004
20893261.2584 109794764.97748 562.8324 50.5004
24006470.539 126154961.773 7 3728.004 42.000
20438748.2114 107406456.87448 -978.6214 51.4004
25302810.977 132967108.753 6 -3258.719 40.000
21910621.5554 115141275.85048 2638.1604 48.8004
24859456.7274 130637340.19546 -315.5234 37.8004
23734534.2194 124725786.40647 3218.8484 44.8004
11 10 21 21 0 1.0000000 0 11G13G32G17G20G04G07G23G31G10G30G02
20155610.1094 105918380.42148 816.9064 49.1004
24807840.1954 130366255.89247 -2984.3124 42.6004
24584321.805 129191497.666 6 -3155.578 40.800
22156794.0004 116435093.43448 -2734.3914 48.0004
:
```

Observables and error budget

RINEX 3.03 observation data

Header hold table that lists observation type for each GNSS

E	8	C1X	C5X	D1X	D5X	L1X	L5X	S1X	S5X							SYS	/	#	/	OBS	TYPES
G	20	C1C	C1W	C2W	C2X	C5X	D1C	D1W	D2W	D2X	D5X	L1C	L1W	L2W		SYS	/	#	/	OBS	TYPES
		L2X	L5X	S1C	S1W	S2W	S2X	S5X								SYS	/	#	/	OBS	TYPES
J	17	C1C	C1Z	C2X	C5X	D1C	D1X	D1Z	D2X	D5X	L1C	L1Z	L2X	L5X		SYS	/	#	/	OBS	TYPES
		S1C	S1Z	S2X	S5X											SYS	/	#	/	OBS	TYPES
R	16	C1C	C1P	C2C	C2P	D1C	D1P	D2C	D2P	L1C	L1P	L2C	L2P	S1C		SYS	/	#	/	OBS	TYPES
		S1P	S2C	S2P												SYS	/	#	/	OBS	TYPES

Data section with one line for each satellite

```
> 2018 01 01 00 00 00.0000000 0 30
E02 24174379.051 0 24174382.216 0 783.933 0 585.401 0 127037224.150 8 94865462.237 9 49.750 0 ...
E07 26585495.945 0 26585500.951 0 -1630.526 0 -1217.585 0 139707745.275 7 104327210.887 7 43.250 0 ...
:
G02 24133922.029 0 24133920.426 0 24133916.354 0 -2482.863 0 -2482.863 0 ...
G04 20880431.607 0 20880431.627 0 20880429.176 0 -666.495 0 -666.495 0 ...
:
J01 42043537.415 0 42043534.463 0 42043535.474 0 42043539.625 0 617.664 0 617.658 0 617.527 0 ...
R03 22141543.842 0 22141544.405 0 22141548.497 0 22141551.286 0 -2894.487 0 -2894.487 0 -2251.255 0 ...
:
```

Observables and error budget

Single point positioning (SPP) - summary

- Signal, tagged with time from satellite clock, transmitted.
- About 66 msec (20,000 km) later the signal arrives at GNSS receiver. Satellite has moved about 66 m during the time it takes signal to propagate to receiver.
- Time the signal is received is given by clock in receiver. Difference between transmit time and receive time is pseudorange.
- During the propagation, signal passes through the ionosphere (10-100 m of delay, phase advance), and neutral atmosphere (2.3-30 m depending on elevation angle).
- To determine an accurate position from range data, we need to account for all these propagation effects (see following lectures) and time offsets.
- Basic clock treatment in GPS
 - True time of reception of signal needed
 - True time of transmission needed (af_0 , af_1 from broadcast ephemeris initially is good enough for SPP)
 - Position of satellite when signal transmitted

Observables and error budget

Single point positioning (SPP) - considerations

- Satellites move at about 1 km/s, therefore an error of 1 ms in time results in 1 m satellite position (and therefore in range estimate and receiver position).
- For pseudo-range positioning (SPP), 1 ms errors OK. For phase positioning (1 mm), time is needed to $1\mu\text{s}$.
- For low precision positioning (tens of meters) the satellite clocks are assumed known and given by the broadcast ephemeris.
 - Receiver clock can be estimated along with 3-D positions if 4 or more satellites are visible.

In the following lectures we will study the main error sources due to signal propagation and then discuss techniques that provide us more precise positions solutions from GNSS