

ORIGINAL
NATIONAL UNIVERSITY OF SINGAPORE

EXAMINATION FOR
(Semester II : 2017/2018)

EE5801 – ELECTROMAGNETIC COMPATIBILITY

April/May 2018 - Time Allowed: 2 Hours

INSTRUCTIONS TO CANDIDATES

1. This paper contains **FOUR (4)** questions and comprises **EIGHT (8)** printed pages including this cover page.
2. Candidates are required to answer all **FOUR (4)** questions.
3. All questions carry equal marks.
4. This is a **CLOSED BOOK** examination with authorized materials only. You are allowed to bring into the examination hall a single A4-size formula sheet filled on both sides with any handwritten material of your choice. You may refer to this sheet during the examination.
5. Take:
 $\mu_0 = 4\pi \times 10^{-7} \text{ H/m}$
 $\epsilon_0 = 8.852 \times 10^{-12} \text{ F/m}$
 c : velocity of light = $3 \times 10^8 \text{ m/s}$
 η_0 : free space intrinsic impedance = $120\pi \text{ } \Omega$
 k = Boltzmann's constant = $1.38 \times 10^{-23} \text{ J/K}$
6. Smith Charts are available on request.
7. All symbols not specifically defined in this examination paper carry their normally accepted meanings.

	Any Medium	Lossless Medium ($\sigma = 0$)	Low-loss Medium ($\epsilon''/\epsilon' \ll 1$)	Good Conductor ($\epsilon''/\epsilon' \gg 1$)	Units
$\alpha =$	$\omega \left[\frac{\mu\epsilon'}{2} \left[\sqrt{1 + \left(\frac{\epsilon''}{\epsilon'}\right)^2} - 1 \right] \right]^{1/2}$	0	$\frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$	$\sqrt{\pi f \mu \sigma}$	(Np/m)
$\beta =$	$\omega \left[\frac{\mu\epsilon'}{2} \left[\sqrt{1 + \left(\frac{\epsilon''}{\epsilon'}\right)^2} + 1 \right] \right]^{1/2}$	$\omega \sqrt{\mu\epsilon}$	$\omega \sqrt{\mu\epsilon}$	$\sqrt{\pi f \mu \sigma}$	(rad/m)
$\eta_c =$	$\sqrt{\frac{\mu}{\epsilon'}} \left(1 - j \frac{\epsilon''}{\epsilon'} \right)^{-1/2}$	$\sqrt{\frac{\mu}{\epsilon}}$	$\sqrt{\frac{\mu}{\epsilon}}$	$(1 + j) \frac{\alpha}{\sigma}$	(Ω)
$u_p =$	ω/β	$1/\sqrt{\mu\epsilon}$	$1/\sqrt{\mu\epsilon}$	$\sqrt{4\pi f/\mu\sigma}$	(m/s)
$\lambda =$	$2\pi/\beta = u_p/f$	u_p/f	u_p/f	u_p/f	(m)
Notes: $\epsilon' = \epsilon$; $\epsilon'' = \sigma/\omega$; in free space, $\epsilon = \epsilon_0$, $\mu = \mu_0$; in practice, a material is considered a low-loss medium if $\epsilon''/\epsilon' = \sigma/\omega\epsilon < 0.01$ and a good conducting medium if $\epsilon''/\epsilon' > 100$.					

- Q.1** (a) A TV transmitter is transmitting 1 kW of RF power at 200 MHz. The transmitting antenna gain is 15 dB. What would be the power output of a 20-dB gain receiving antenna at a distance of 10 km away from the transmitter?
(5 marks)
- (b) Two horn antennas, both operating in the same frequency band, have different aperture sizes. Discuss the differences in gains and radiation patterns of these two horn antennas.
(5 marks)
- (c) An airport Long Range Radar (LORAD) operating at 3 GHz carrier frequency is transmitting at 100 W via a 30 dB antenna. The transmitted square-wave modulated pulse has a pulse width of 1 μ s and Pulse Repetition Frequency (PRF) of 1 kHz. The antenna is revolving at a rate of 2 revolutions per second. What is the peak electric field due to this transmission at a distance of 1 km away?
(5 marks)

Explain why this peak electric field could not be measured using a field strength meter (Fig. 1.1).
(5 marks)



Fig. 1.1 Field strength meter

Explain why is this measurement also could not be easily accomplished with a spectrum analyzer (Fig. 1.2).
(5 marks)

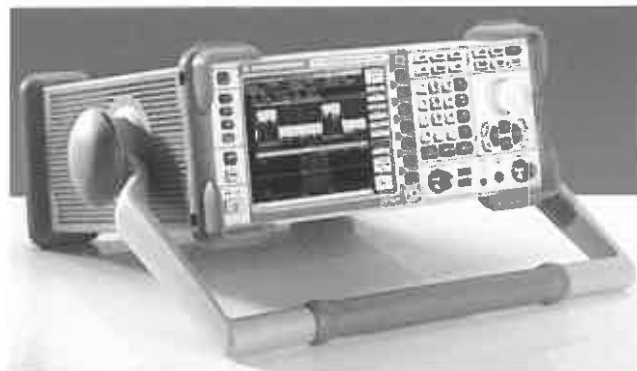


Fig. 1.2 Spectrum analyzer

Q.2

Fig. 2.1 shows a simple PCB trace. At DC, the current flows uniformly across the copper strip (conductivity $\sigma = 5.8 \times 10^7$) as well as the ground plane. However, as frequencies increases, the current tends to concentrate in the shaded area due to *skin effect*, where skin depth $\delta = 1/\sqrt{\pi f \mu \sigma}$. Given that $H = 3$ mm, $w = 2$ mm, and the thickness of the trace $s = 100$ μm :

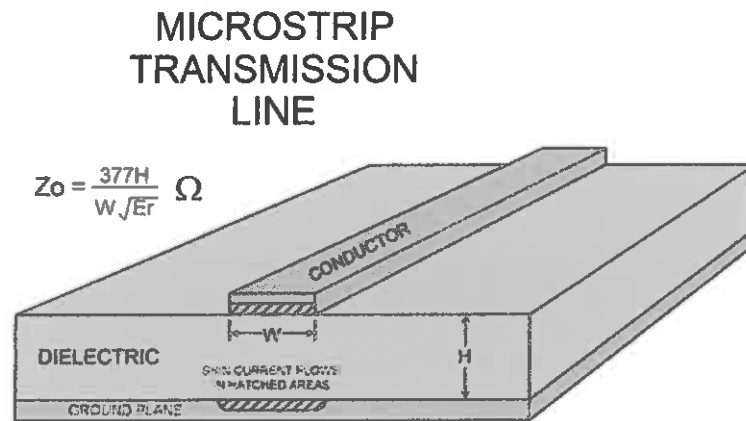


Fig. 2.1

Compute the resistance per unit length of the PCB trace at DC. (2 marks)

Compute the resistance per unit length at 1 GHz. (4 marks)

Comment on the difference and the implication to designer. (2 marks)

Fig. 2.2 shows a pair of PCB traces constructed on the same substrate as in Fig. 2.1, separated by a distance d . It is clear that coupling between traces is common for high-speed digital transmission as illustrated. Estimate the peak induced current on the victim trace due to a 5 volts, 1 GHz digital pulse train (rise time 10 picosecond) propagating on the culprit trace using the simple mutual capacitance model as suggested in Fig. 2.2. The parameters are: $H = 3$ mm, $L = 2$ cm, $d = 4$ mm, $s = 100$ μm , $w = 2$ mm, $\epsilon_r = 2.54$.

(4 marks)

What would the peak induced current be if the mutual capacitance model is modified to replace the trace thickness s by the skin depth δ ?

(2 marks)

Why is the modified model more accurate?

(2 marks)

Comment on the results.

(2 marks)

One common way to reduce the capacitive coupling as shown is to introduce a ground trace in between the two traces as shown in Fig. 3.2. However, a student argues that now the culprit trace is coupled to the victim trace via two series capacitances, C_1 from the culprit to ground trace and C_2 from the ground trace to victim. He further argues that as C_1 and C_2 are much higher than the original capacitance C due to the closer separations between traces, the new coupling capacitance C_{new} would be higher

than C, even after taking into account the reduction factor caused by the series connection ($1/C_{\text{new}} = 1/C_1 + 1/C_2$). Thus, the arrangement not only does not help, rather, it aggravate the situation. Comment on the student's arguments and point out his mistake/omission, if any.

(5 marks)

Does the ground trace help in reducing the inductive coupling? Explain with justifications.

(2 marks)

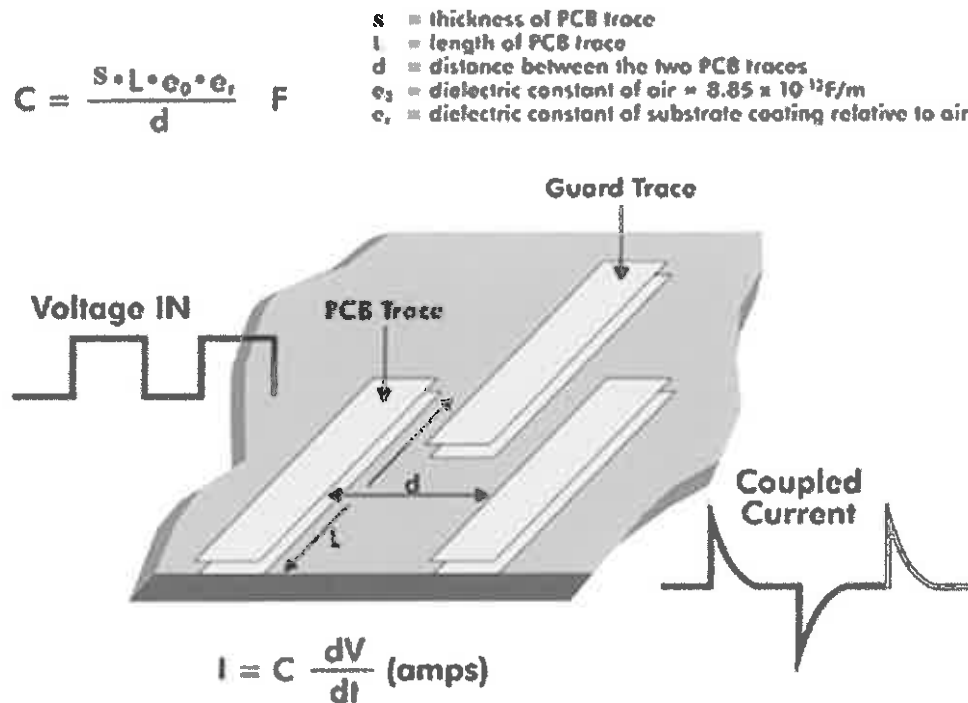


Fig. 2.2

Q.3 Fig. 3.1 shows a portable mobile EMI shielded room made with conductive clothing material X of the following specifications:

Thickness = 2 mm

Relative permeability $\epsilon_r = 3$

Relative permeability $\mu_r = 1$

The frequency-dependence conductivity is given in Fig. 3.2.

Assuming plane wave incident, estimate the followings at 3 GHz. You may assume that the material is a good conductor and that the skin depth is given by $\delta = 1/\sqrt{(\pi f \mu \sigma)}$.

- i) The reflection loss of the material. (10 marks)
- ii) The absorption loss of the material. (5 marks)
- iii) The shielding effectiveness of the material. (5 marks)

Observing the small difference between the conductivity at 50 Hz (650 S/m) and at 3 GHz (1450 S/m), a student deduced the followings at 50 Hz:

Wave impedance = $7.8 \times 10^{-4} e^{j\pi/4} \Omega$

Reflection loss = -107 dB

Absorption loss = 0 dB

Total shielding effectiveness = -107 dB

and concluded that material X is equally good and the shielded room can be used at frequency as low as 50 Hz. Comment on the student's postulation with justifications. (Note: You may assume the student's calculations at 50 Hz are correct and there is no need to re-calculate them.)

(5 marks)



Fig. 3.1

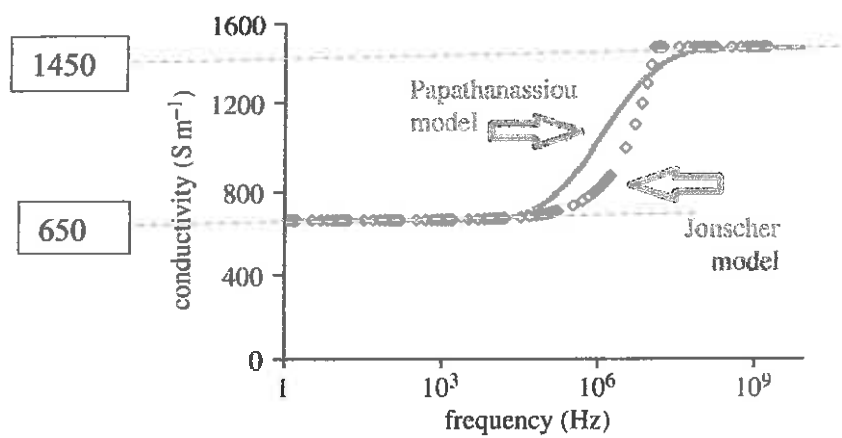


Fig. 3.2

Q.4

Fig. 4 shows a metallic shielded box made of copper plates with conductivity = 5.8×10^7 , relative permittivity = 1, relative permeability = 1 and thickness = 1 mm. The glass display panel has dimensions of 90 mm x 30 mm x 1 mm, and conductivity = 0, relative permittivity = 2, and relative permeability = 1.

The goal of the shielded box is to provide a 30 dB shielding in the frequency band of 10 MHz to 10 GHz. Is the goal achievable? Explain with justifications.

(5 marks)

What is the upper usable frequency (f_u) for this box?

(2 marks)

What is the shielding efficiency at $0.9 f_u$? Can it achieve the goal of 30 dB? If not, suggest a method in achieving the 30 dB shielding at $0.9 f_u$. You may make use of the following formula, or otherwise:

$$\alpha = \omega_c \sqrt{\mu \epsilon} \sqrt{1 - \left(\frac{f}{f_c}\right)^2} \quad \text{for } f < f_c$$

where α is the attenuation constant, $\omega_c = 2\pi f_c$, and f_c is the cutoff frequency of a waveguide.

(10 marks)

Suggest a more practical method in extending the usable frequency and achieving the shielding objective. Only a descriptive answer is needed. Detailed design is not needed.

(5 marks)

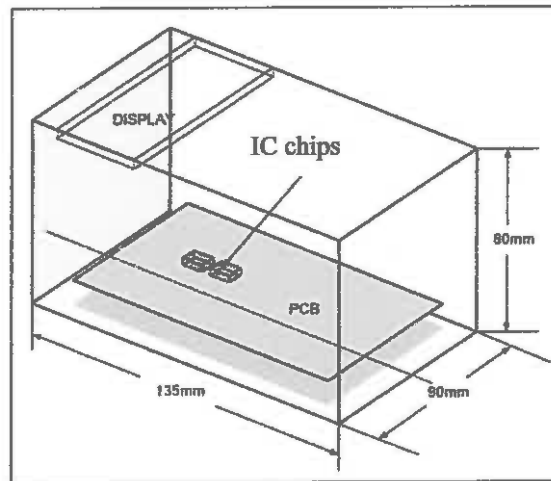


Fig. 4

END OF PAPER