

EE5801 Tutorial 3 Solutions

Q1

check for spherical symmetry \rightarrow can apply Gauss's Law

$$\text{LHS} = \oint \vec{E} \cdot d\vec{A} = E_r \oint dA = E_r 4\pi r^2$$

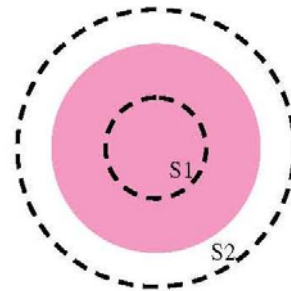
$$\text{RHS} = \frac{1}{\epsilon} \iiint \rho(r) dV = \frac{1}{\epsilon} \int_0^a \frac{\rho_0 r}{a} r^2 dr \int_0^\pi \sin\theta d\theta \int_0^{2\pi} d\phi = \frac{\pi \rho_0 r^4}{\epsilon a}$$

equate LHS and RHS expressions for S1 within sphere

$$\vec{E}(r < a) = \frac{\rho_0 r^2}{4\epsilon a} \hat{u}_r$$

change upper bound of RHS for S2 outside sphere to obtain $Q = 4\pi \int_0^a \frac{\rho_0 r}{a} r^2 dr = \pi \rho_0 a^3$

$$\vec{E}(r > a) = \frac{\rho_0 a^3}{4\epsilon_0 r^2} \hat{u}_r$$



add metallic spherical shell (to shield charged sphere)

$-Q$ induced on $r = b$ surface of spherical shell

(i) without earthing

$+Q$ residing on $r = c$ surface of spherical shell

no change in total charge for RHS expression

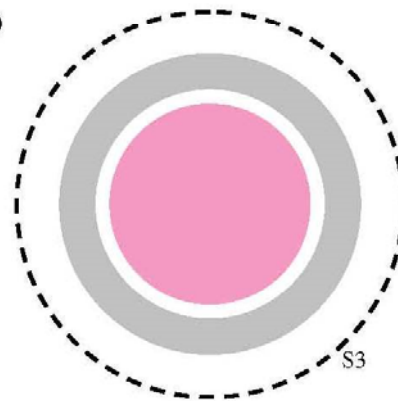
$$\vec{E}(r > c) = \frac{\rho_0 a^3}{4\epsilon_0 r^2} \hat{u}_r \text{ before earthing}$$

(ii) with earthing

zero charge on $r = c$ surface of spherical shell

need to include in RHS expression addition of charge $-Q$ from earth

$$\vec{E}(r > c) = 0 \quad \text{after earthing}$$



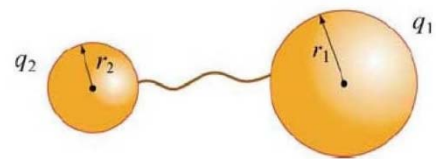
Q2

(a)

common potential because of wire connection

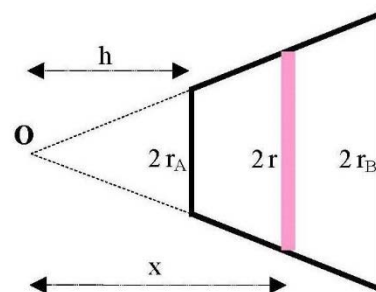
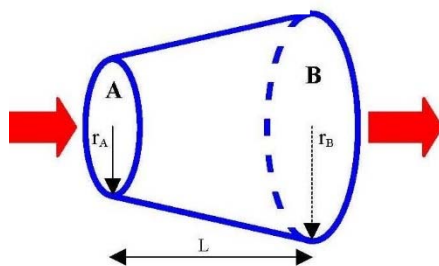
$$\frac{q_1}{4\pi\epsilon_0 r_1} = \frac{q_2}{4\pi\epsilon_0 r_2} \quad \frac{q_1}{q_2} = \frac{r_1}{r_2}$$

$$\therefore \frac{E_1}{E_2} = \frac{\frac{q_1}{4\pi\epsilon_0 r_1^2}}{\frac{q_2}{4\pi\epsilon_0 r_2^2}} = \frac{q_1}{q_2} \frac{r_2^2}{r_1^2} = \frac{r_2}{r_1}$$



implication: stronger electric field expected at sharper corners since $E \propto \frac{1}{r}$

(b)



elemental resistance of dx strip at x from O:

$$dR = \frac{dx}{\pi\sigma r^2}$$

need to integrate from $x = h$ to $x = h+L$:

$$R = \frac{1}{\pi\sigma} \int_h^{h+L} \frac{dx}{r^2} = \frac{L}{\pi\sigma r_A r_B}$$

based on geometrical relationships $\frac{r}{x} = \frac{r_A}{h} = \frac{r_B}{h+L}$

(c)

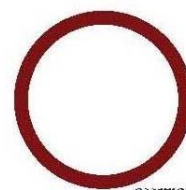
$$I = \int_{\text{circle}} J_0 \exp\left(\frac{r^2 a^2}{\delta^2}\right) r dr d\phi$$

$$= J_0 \int_0^a \exp\left(\frac{r^2 a^2}{\delta^2}\right) r dr \int_0^{2\pi} d\phi$$

$$= J_0 \pi \delta^2 \left\{ 1 - \exp\left(-\frac{a^2}{\delta^2}\right) \right\}$$

(using substitution $u = \frac{r^2 a^2}{\delta^2}$ as integration aid)

$$\rightarrow J_0 \pi \delta^2 \quad \text{when } \delta \ll a$$



current flowing within thin layer

Q3

choose to place (fictitious) current I on straight wire

can thus apply Ampere's Law

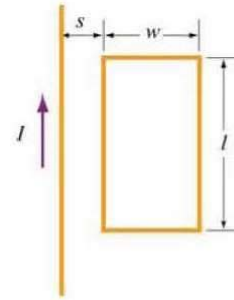
$$B_\phi = \frac{\mu_0 I}{2\pi r} \quad (\text{valid only if wire is sufficiently long})$$

gives rise to flux linkage with loop

$$d\Phi = B_\phi dA = \frac{\mu_0 I}{2\pi r} (l dr) = \frac{\mu_0 I l}{2\pi} \frac{dr}{r}$$

obtain mutual inductance by dividing total flux to current

$$M = \frac{\Phi}{I} = \frac{\mu_0 l}{2\pi} \int_s^{s+w} \frac{dr}{r} = \frac{\mu_0 l}{2\pi} \ln\left(1 + \frac{w}{s}\right)$$



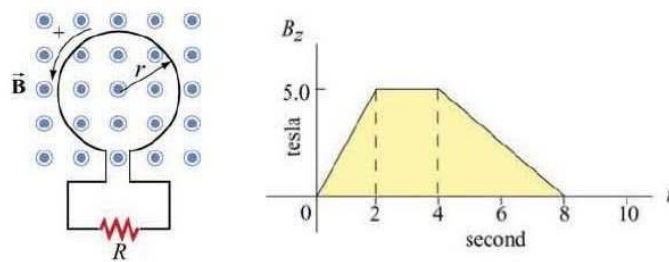
alternate approach: place (fictitious) current on wire loop

will obtain same numerical answer for M

prefer not to pursue this option:

- more cumbersome to derive B of loop
- also need to consider question of area enclosed by straight wire.

Q4



current in R due to EMF given by Faraday's Law

$$I = \frac{V_{\text{EMF}}}{R} = -\frac{1}{R} \frac{d}{dt} \iint \vec{B} \cdot d\vec{A} = -\frac{\pi r^2}{R} \frac{dB_z}{dt}$$

Lenz's Law: negative sign \rightarrow current in clockwise sense if $\frac{dB_z}{dt} > 0$

for $0 < t < 2$, EMF due to (linear) increase in B

$$\therefore I = -\frac{\pi 0.5^2}{100} \frac{5}{2} = -19.6 \text{ mA (i.e. clockwise)}$$

for $2 < t < 4$, no EMF due to constant B

$$\therefore I = -\frac{\pi 0.5^2}{100} \frac{0}{2} = 0$$

for $4 < t < 8$, EMF due to (linear) decrease in B

$$\therefore I = -\frac{\pi 0.5^2}{100} \left(-\frac{5}{4}\right) = +9.8 \text{ mA (i.e. anti-clockwise)}$$

for $t > 8$, no EMF due to constant B and hence back to zero current

