## CHAPTER 14 - MEASUREMENTS IN PRESSURE CONDUITS

## 13. Trajectory Methods

Basically, trajectory methods consist of measuring the horizontal and vertical coordinates of a point in the jet issuing from the end of a pipe (Stock, 1955). The pipe may be oriented either vertically or horizontally. The principal difficulty with this method is in measuring the coordinates of the flowing stream accurately.

## (a) Vertical Pipes

Lawrence and Braunworth (1906) noted that two kinds of flow occur from the end of vertical pipes. With a small rise of water (up to 0.37d) above the end of the pipe, the flow acts like a circular weir. When the water rises more than 1.4d, jet flow occurs. When the rise is between these values, the mode of flow is in transition. Lawrence and Braunworth (1906) determined that when the height of the jet exceeded 1.4 d, as determined by sighting over the jet to obtain the maximum rise, the discharge is given by:

$$Q = 5.01d^{1.99}h^{0.53}$$

where:

Q = rate of flow, gal/min

d =inside diameter of the pipe, in

h = height of jet, in

When the rise of water above the end of the pipe is less than 0.37d, discharge is given by:

$$Q = 6.17 d^{1.25} h^{1.35}$$

For jet heights between 0.37d and 1.4d, the flow is considerably less than that given by either of these equations. Figure 14-12, prepared using data from Stock (1955) gives flow rates in gallons per minute for standard pipes 2 to 12 in in diameter and jet heights from 12 to 60 in. Bos (1989) assigns to this method an accuracy of +/-10 percent for the jet flow range to +/-15 percent for the weir flow range.

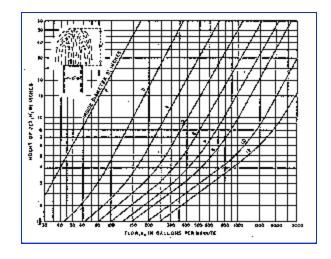


Figure 14-12 -- Discharge curves for measurement of flow from vertical standard pipes. The curves are based on data from experiments of Lawrence and Braunworth, American Society of Civil Engineers, Transactions, Vol. 57, 1906 (courtesy of Utah State University)..

For irrigation convenience, the Natural Resources Conservation Service produced a table from curves for vertical pipes in Stock (1955) for the NRCS *National Engineering Handbook* (1962a). This table is reproduced here as table 14-1. The table gives discharges

Table 14-1 -- Flow from vertical pipes<sup>1</sup>

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<sup>&</sup>lt;sup>1</sup> Table prepared from discharge curves in Utah Engineering Experimental Station, Bulletin 5, "Measurement of Irrigation Water," June 1955.

for different heads up to 40 in for standard nominal pipe diameters from 2 to 12 in and for outside diameters of well casings from 4 to 12 in. As mentioned before, accuracies better than 15 and 10 per-cent should not be expected, depending on whether the flow is acting as a weir or jet-type flow.

## (b) Horizontal Pipes

When brink depths are greater than 0.5D, the more general Purdue pipe method developed by Greve (1928) should be used, rather than the California pipe method. The Purdue method applies equally well to both partially and completely filled pipes. The Purdue method consists of measuring coordinates of the upper surface of the jet as shown on figure 14-13. If the water in the pipe is flowing at a depth of less than 0.8D at the outlet, the vertical distance, Y, can be measured at the end of the pipe where X = 0. For higher rates of flow, Y may be measured at horizontal distances, X, from the pipe exit of 6, 12, or 18 in. Flow values in gallons per minute for 2- to 6-in-diameter standard pipes are shown in graphs on figure 14-14 (Stock, 1955).

<sup>&</sup>lt;sup>2</sup> Standard pipe.

<sup>&</sup>lt;sup>3</sup> Outside diameter of well casing.

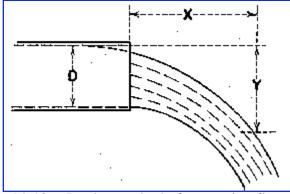


Figure 14-13 -- Purdue method of measuring flow from a horizontal pipe (courtesy of Utah State University)..

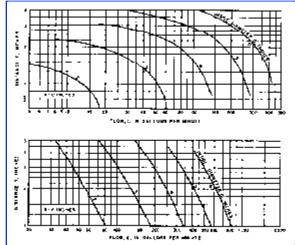


Figure 14-14 -- Flow from horizontal standard pipes by Purdue coordinate method (courtesy of Utah State University) (sheet 1 of 2)..

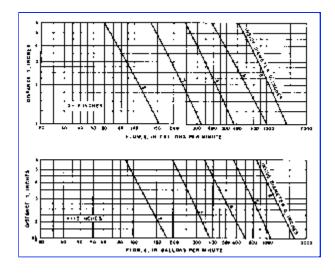


Figure 14-14 -- Flow from horizontal standard pipes by Purdue coordinate method (courtesy of Utah State University) (sheet 2 of 2)..

The most accurate results will be obtained when the pipe is truly horizontal. If it slopes upward, the indicated discharge will be too high. If it slopes downward, the indicated discharge will be too low.

Difficulty occurs in making the vertical measurement, *Y*, because the top of the jet will usually not be smooth and well defined.

The NRCS produced table 14-2 for horizontal pipe discharge for *X* of 0, 6, 12 and 18 in and *Y* up to about 8 in for pipe diameters from 2 to 6 in. As mentioned previously, accuracies better than 10 percent should not be expected.

Table 14-2 Flow from horizontal pipes <sup>1</sup>

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0 95 4 27 4 67 4 887 7 (Jaches) 7 (Jaches) 86 1 05 1 05 1 05 1 05 1 05 1 05 1 05 1 05	2 esh 2 esh 137 146 156 156 166 52 166 55 75 76 45 45 45	Sure of po- 2 minutes 274 274 277 289 716 200 100 100 100 100 100 100 100 100 100	4 proc   4 proc   543   563   44p   563   44p   577   586   587   588   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589   589	5   Sect	6 mch 9 mch 9 mch 1
0.95 4.27 4.67 4.68  See trainele at 9  (Inches-  1.24 26 48 86 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05	2 mch 2 m.T. 137 146 145 140 52 15 60 61 45 45 45 27 27 27	Sure of po- 2 minutes 274 minutes 274 minutes 275 minu	4 # #00*  4 # #00*  502  4.67  503  4.58  4.58  4.58  537  557  557  557  557  559  259  170  159  171  159	5 / Correction	6 mm 5 mm 6 mm 6 mm 6 mm 6 mm 6 mm 6 mm
9 95 425 425 465 465 465 465 465 465 465 465 465 46	2 exh 24ch 137 146 146 146 146 146 146 146 146	Sure of 20 3 years 200 ft 274 277 279 216 200 100 100 100 100 100 100 100	4 #100 4 #100 92.201 503 603 604 605 607 605 607 605 607 605 607 605 607 607 607 607 607 607 607 607	5 males 5 year 542 % 950 957 772 906 906 906 907 906 907 906 907 907 907 907 907 907 907 907	6 mm 5 mm 6 mm 6 mm 6 mm 6 mm 6 mm 6 mm
0 95   4 27   4 26   4 27   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4 26   4	2 mch 2 m.T. 137 146 145 140 52 15 60 61 45 45 45 27 27 27	Sure of po- 2 mem  270  274  277  270  718  200  100  100  100  100  100  100  1	4 # #00**  4 # #00**  503  503  655  656  657  657  658  657  658  657  658  657  658  657  658  657  658  657  658  658	5 males 5 year 542 % 950 957 772 906 906 906 907 906 907 906 907 907 907 907 907 907 907 907	6 mm 5 mm 6 mm 6 mm 6 mm 6 mm 6 mm 6 mm

Table 14-2 Flow from horizontal pipes (continued)

	7-inch	1-mat	+urch	5- mar	Kereti		
	Spm	Gρπ	Ģpm.	G p.구. 한번	Gpm		
.#0	177	310	770				
1/05	148	305	788	H74	1212		
1 22	185	272	730	A25	1257		
180	104	247	164	767	lera.		
3.42	52	216	799	656	525		
2000	ė <sup>7</sup>	123	259	623	541 277		
2,60	19	:26	230	920 #89	712		
4.42	79	151	236				
4.62	- EB	145	257 270	458	673 683		
tAD tada	e9 	140	259 258	428 404	592		
nuc nac	60 57	126 14b	250	368	574		
7.42 7.42	<u> </u>	1,5	250	368	546		
7.6	50	116	254	355	520		
solnerse e:	end of bable						
	WHEN X 15 MOHES						
٠.							
rdes)		Serie	ol presidental	d s mater)			
rahen)	2 metr	2 045	a jegh	3 601			
	Spm	2 m.m Gp m	a jech Gazera	Jiner Gen	54:::4		
150	Spm list	2 nun Gp m 341	a jegh Gagari, gas	3 fg1 Gg.11 1014	\$25.00 1400		
150	3 p.m. 167 184	2 out 0 o m .wi .wr	4 (126 GG/m, 584 557	3 601 GB.11 1014 907	\$2:::: 1401 1261		
267	30 m 67 144 125	2 nun Gern 341 375 274	4 (15h) Gagari, 554 557 500	2 601 GB.11 1014 907 106	\$26.00 1400 1261 1150		
150 540 370 370	30 m 67 184 125 117	2 005 00 m 341 375 274 201	# (10h) GGW, 584 587 500 486	9 601 Guin 1914 987 195 754	\$28.03 1909 1261 1150 1000		
150 540 360 360 450 450	3 p.m. 167 184 125 117 103	2 out Go m 341 377 274 271 277	# (10h) GGW, 584 587 500 485 411	7 (6) 1 G (5, 1) 1014 907 105 154 100	52:05 (40) (20) (10) (00) (52)		
150 540 300 300 450 450	30 m 67 184 125 117	2 005 00 m 341 375 274 201	# (10h) GGW, 584 587 500 486	9 601 Guin 1914 987 195 754	\$28.03 1909 1261 1150 1000		
150 540 370 370 450 450 540	30 m 167 144 125 117 105 101	2 mm Gp m 341 345 274 271 277 280	4 (10h)  Gayr, 534 537 500 450 411 404	0.40° Ge. 11 1014 907 1076 1594 100 865	52:05 (40) (20) (10) (10) (60) (60)		
150	3.0 m 167 144 125 117 105 101 55	2 645 Gp m 341 345 274 271 277 283 284	4 (10h)  Gam, 554 557 550 450 450 451 450 450	7 401* GB.11 1014 907 106 154 106 155 155 155 155	52:00 1401 1261 1150 1090 552 504 204		
150 540 370 370 380 480 540 600	30 m 167 184 125 117 165 161 55 88	2 (6.8) Gp m 341 375 274 271 275 285 287 183	4 (10h)  Gayr, 534 557 500 450 411 400 110 110	7 1011 G : 11 1014 907 1076 154 103 855 8 : 5 570	526.05 1400 1201 1100 1000 552 504 204 204		
150 540 360 360 451 451 561 661	30 m 167 144 125 103 103 101 55 69	2 005 GB W 341 375 274 271 277 280 287 183	4 (10h)  Gam, 154 1557 1500 1450 171 170 170 170 146	7 90 1 Quint 1014 907 1025 154 100 855 8 5 579 548	1409 1261 1160 1069 592 504 718 758 758		

<sup>&</sup>lt;sup>1</sup> Table for standard steel pipe prepared from data resulting from actual experiments conducted at Purdue University Experimental Station, Bulletin 32, "Measurement of Pipe Flow by the Coordinate Method," August 1928.

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