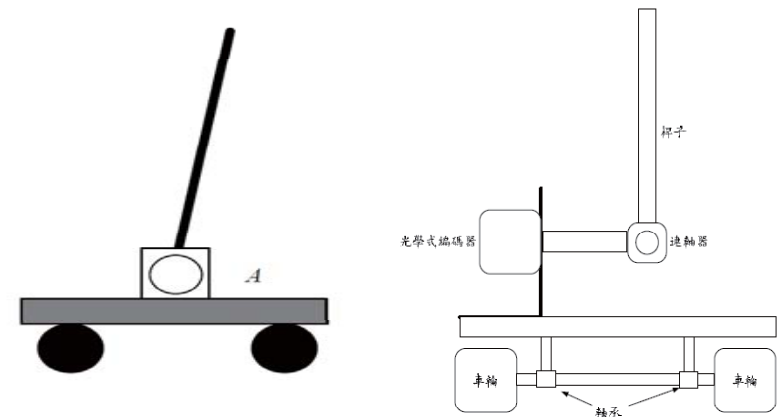


Inverted Pendulum Car

電機工程學系 鄭智湧

正面側面示意圖

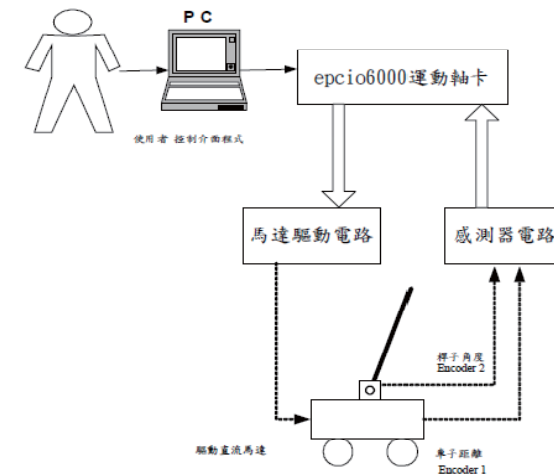


車與桿倒單擺系統機構

系統的機械結構由直流馬達、齒輪、車輪、編碼器組成車子的部分；角度編碼器、桿子組合成倒單擺部份

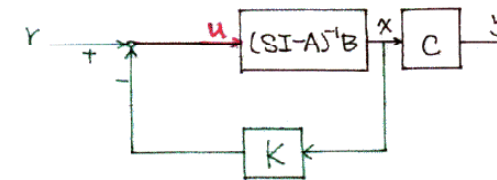
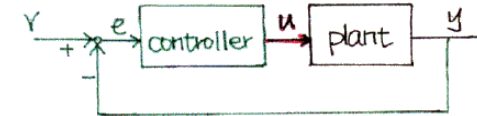


系統結構圖



State Feedback Controller Design

State Feedback Design



$$\dot{x} = Ax + Bu$$

$$y = Cx$$

$$u = -Kx + r \quad \text{state feedback control law}$$

Eigenvalue (pole) Placement

Thm:

consider the system $\dot{x} = Ax + bu$ with the state feedback $u = -Kx$

If the system is **controllable**

then eigenvalues of $A - bK$ can be

arbitrarily moved around the complex plane

(with complex conjugate pairs)

```
interrupt void eva_timer1_isr(void)
{
    QEP1 = EvaRegs.T2CNT;           // counting value of pendulum encoder
    QEP2 = EvbRegs.T3CNT;           // counting value of car encoder

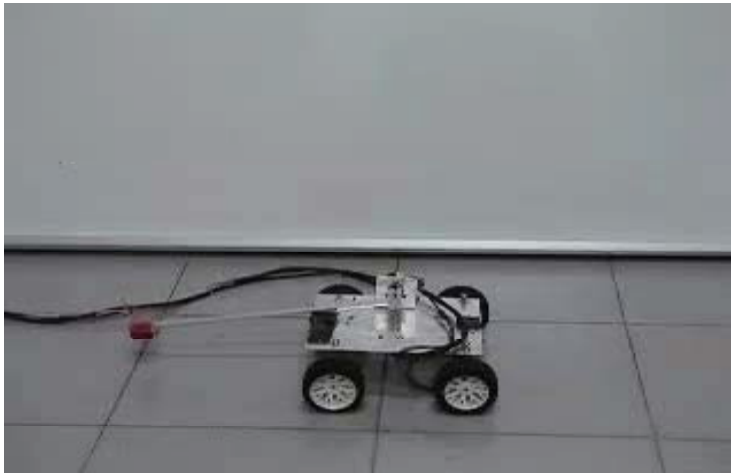
    arm = QEP1*0.0031416;           // theta=QEP2*(2*pi/2000) rad
    arm_dot = ((arm-arm_old)/0.001); // sampling time=0.001s
    arm_old = arm;

    pend = QEP2*0.0031416;           // thetb=QEP3*(2*pi/2000) rad
    pend_dot = ((pend-pend_old)/0.001); // sampling time=0.001s
    pend_old = pend;

    U = balance_LQR();

    // state feedback control law for balancing control
    float balance_LQR(void)
    {
        float law;
        law = -((k1*arm)+(k2*pend)+(k3*arm_dot)+(k4*pend_dot));
        return law;
    }
}
```

Video Demo 1



Video Demo 2



Simulation Study

IP Modeling

For pendulum,

$$J\ddot{\theta} = F_y l \sin \theta - F_x l \cos \theta$$

where

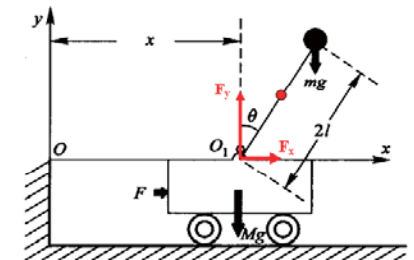
$$F_x = m \frac{d^2}{dt^2} (x + l \sin \theta)$$

and

$$F_y - mg = m \frac{d^2}{dt^2} (l \cos \theta)$$

For cart,

$$F - F_x = M \frac{d^2 x}{dt^2}$$



$$(J + ml^2)\ddot{\theta} + ml \cos \theta \cdot \ddot{x} = mlg \sin \theta$$

$$(M + m)\ddot{x} + ml(\cos \theta \cdot \ddot{\theta} - \sin \theta \cdot \dot{\theta}^2) = F$$

Note: Lagrange dynamics is another approach for modeling.

$$\ddot{\theta} = \frac{ml \cos \theta \cdot F + m^2 l^2 \sin \theta \cos \theta \cdot \dot{\theta}^2 - (M + m)mlg \sin \theta}{m^2 l^2 \cos^2 \theta - (J + ml^2)(M + m)}$$

$$\ddot{x} = \frac{(J + ml^2)F + lm(J + ml^2) \sin \theta \cdot \dot{\theta}^2 - m^2 l^2 g \sin \theta \cos \theta}{(J + ml^2)(M + m) - m^2 l^2 \cos^2 \theta}$$

Linearization $\implies \dot{\theta}^2 \approx 0, \sin \theta \approx \theta, \cos \theta \approx 1$

$$\ddot{\theta} = \frac{(M + m)mlg\theta - mlF}{J(M + m) + mml^2}$$

$$\ddot{x} = \frac{(J + ml^2)F - m^2 l^2 g\theta}{J(M + m) + mml^2}$$

Assume $M = 1, m = 1, 2l = 0.6, g = 10, J = \frac{ml^2}{3} = 0.03$

$$\ddot{\theta} = \frac{0.3 \cos \theta \cdot F + 0.09 \sin \theta \cdot \cos \theta \cdot \dot{\theta}^2 - 6 \sin \theta}{0.09 \cos^2 \theta - 0.24}$$

Model (NL)

$$\ddot{x} = \frac{0.12F + 0.036 \sin \theta \cdot \dot{\theta}^2 - 0.9 \sin \theta \cdot \cos \theta}{0.24 - 0.09 \cos^2 \theta}$$

$$\ddot{\theta} = 40\theta - 2F$$

Model (L)

$$\ddot{x} = -6\theta + 0.8F$$

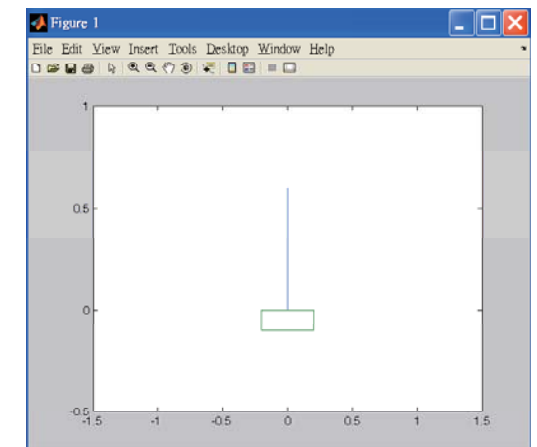
State space model

$$x_1 = \theta, x_2 = \dot{\theta}, x_3 = x, x_4 = \dot{x}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 40 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ -6 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ -2 \\ 0 \\ 0.8 \end{bmatrix} F$$

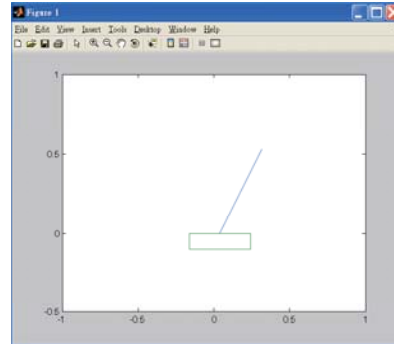
Check controllability (under-actuated or non-holonomic)

IP graphics test



test_IP_gra.m

- length=0.6; len=0.2; width=0.1;
- x_pos=0; angle=pi/3;
- N=100;
- for i=1:N
- x_pos=x_pos+1/N;
- angle=angle+1/N;
- stick_x=[x_pos, x_pos+length*cos(angle)];
- stick_y=[0 , length*sin(angle)];
- car_x=[x_pos-len x_pos+len x_pos+len x_pos-len x_pos-len];
- car_y=[0 0 -width -width 0];
- plot(stick_x,stick_y,car_x,car_y); axis([-1 1 -0.5 1]);
- MA(:,i)=getframe;
- end



ODE simulation

$$\dot{x} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 40 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ -6 & 0 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ -2 \\ 0 \\ 0.8 \end{bmatrix} u$$

function dx=IP(t,x)

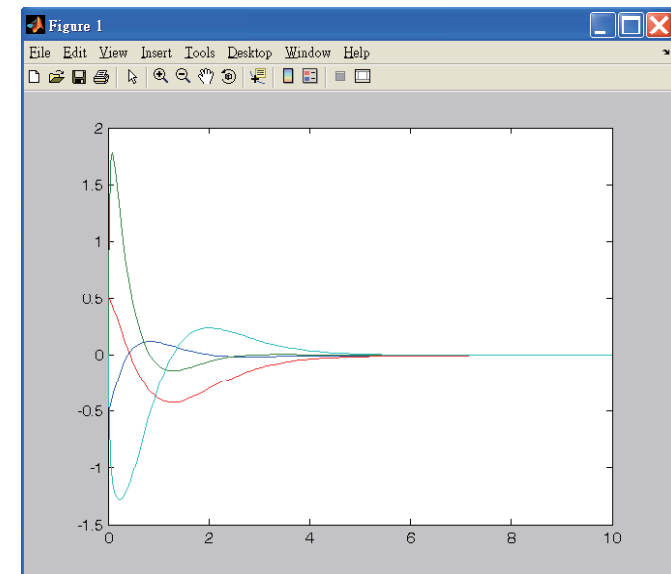
% state feedback design

u = [-95.4861 -22.3475 -7.0711 -12.5201]*x;

dx = [0 1 0 0
40 0 0 0
0 0 0 1
-6 0 0 0]*x + [0 -2 0 0.8]*u;

IPcar.m

- length=0.6; len=0.2; width=0.1;
- [t,x]=ode23(@IP,[0 10],[-0.5 0 0.5 0]);
- N=max(size(x));
- for i=1:N
- angle=pi/2-x(i,1);
- x_pos=x(i,3);
- stick_x=[x_pos, x_pos+length*cos(angle)];
- stick_y=[0 , length*sin(angle)];
- car_x=[x_pos-len x_pos+len x_pos+len x_pos-len x_pos-len];
- car_y=[0 0 -width -width 0];
- plot(stick_x,stick_y,car_x,car_y); axis([-1.5 1.5 -0.5 1]);
- MA(:,i)=getframe;
- end



Acker in Matlab

% Use the example discussed in class.

% The desired eigenvalues are at -2, -1, -1

```
A=[1 0 0; -1 0 2; 0 -1 1]; B=[1;0;0];
```

```
J=[-2 -1 -1];
```

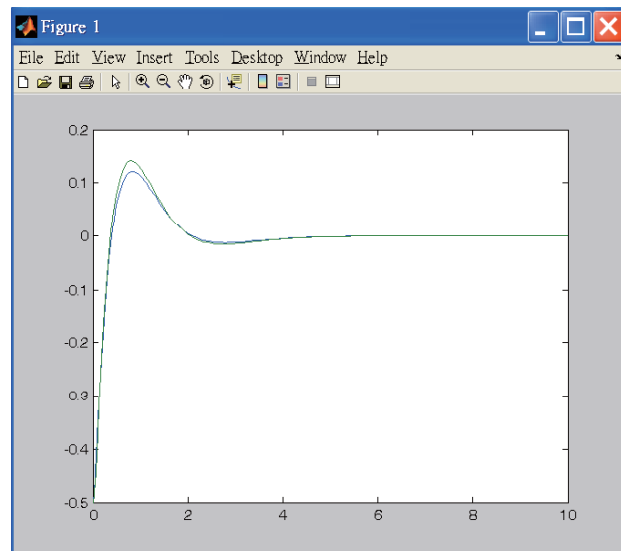
```
K=acker(A,B,J)
```

% The result is $K = \begin{bmatrix} 6 & -8 & 0 \end{bmatrix}$

IPcar_NL and IP_NL

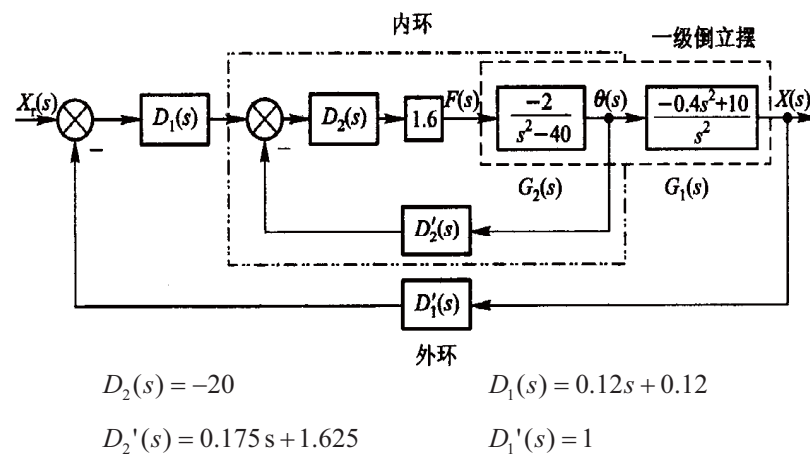
- `function dx=IP_NL(t,x)`
- % LQR design
- `u=[-95.4861 -22.3475 -7.0711 -12.5201]*x;`
- `dx=zeros(4,1);`
- `dx(1)=x(2);`
- `dx(2)=(0.3*cos(x(1))*u+0.09*sin(x(1))*cos(x(1))*x(1)^2-6*sin(x(1)))/(0.09*cos(x(1))^2-0.24);`
- `dx(3)=x(4);`
- `dx(4)=(0.12*u+0.036*sin(x(1))*x(1)^2-0.9*sin(x(1))*cos(x(1)))/(0.24-0.09*cos(x(1))^2);`

Comparison (NL could diverge)



PID control design
(linear simulation)

PID control of angle and position



IPpid.m

- $G2 = \text{tf}([-2], [1 \ 0 \ -40]);$
- $D2 = \text{tf}([-32], [1]);$
- $D2p = \text{tf}([0.175 \ 1.625], [1]);$
- $\text{sys_inner} = \text{feedback}(\text{series}(D2, G2), D2p);$
- $G1 = \text{tf}([-0.4 \ 0 \ 10], [1 \ 0 \ 0]);$
- $D1 = \text{tf}([0.12 \ 0.12], [1]);$
- $D1p = \text{tf}([1], [1]);$
- $\text{sys_outer} = \text{feedback}(\text{series}(\text{series}(D1, \text{sys_inner}), G1), D1p);$
- $\text{sys_angle} = \text{feedback}(\text{series}(D1, \text{sys_inner}), \text{series}(G1, D1p));$

- $t = 0:0.1:10;$
- $\text{pos} = 0.1 * \text{impulse}(\text{sys_outer}, t);$
- $\text{the} = 0.1 * \text{impulse}(\text{sys_angle}, t);$
- $\% \text{ plot}(t, \text{the}, t, \text{pos})$
- $\text{length} = 0.6; \text{len} = 0.2; \text{width} = 0.1;$
- $N = \text{max}(\text{size}(\text{the}));$
- for $i = 1:N$
- $\text{angle} = \text{pi}/2 - \text{the}(i);$
- $\text{x_pos} = \text{pos}(i);$
- $\text{stick_x} = [\text{x_pos}, \text{x_pos} + \text{length} * \cos(\text{angle})];$
- $\text{stick_y} = [0, \text{length} * \sin(\text{angle})];$
- $\text{car_x} = [\text{x_pos} - \text{len}, \text{x_pos}, \text{x_pos} + \text{len}, \text{x_pos} - \text{len}, \text{x_pos} - \text{len}];$
- $\text{car_y} = [0, 0, -\text{width}, -\text{width}, 0];$
- $\text{plot}(\text{stick_x}, \text{stick_y}, \text{car_x}, \text{car_y}); \text{axis}([-1.5 \ 1.5 \ -0.5 \ 1]);$
- $\text{MA}(:, i) = \text{getframe};$
- end

Pendulum angle and cart position

